European Linear Collider Workshop
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FAST KICKERS R&D @ LNF-INFN

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*for the LNF fast kickers study group**

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PRESENTATION OUTLINE

1) General considerations on kickers with circular and elliptical cross section of the stripline.

2) Correction of the deflecting field flatness by tapering the stripline; Other advantages of tapers.

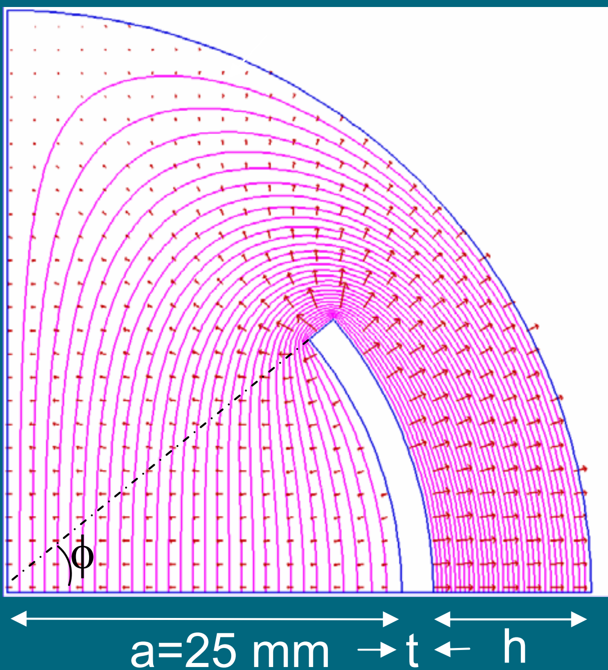
3) Design of the stripline kicker for the DAΦNE injection upgrade.

4) R&D and HV tests on kicker prototypes, feedthroughs and pulser (supplied by FID GmbH) @ LNF.

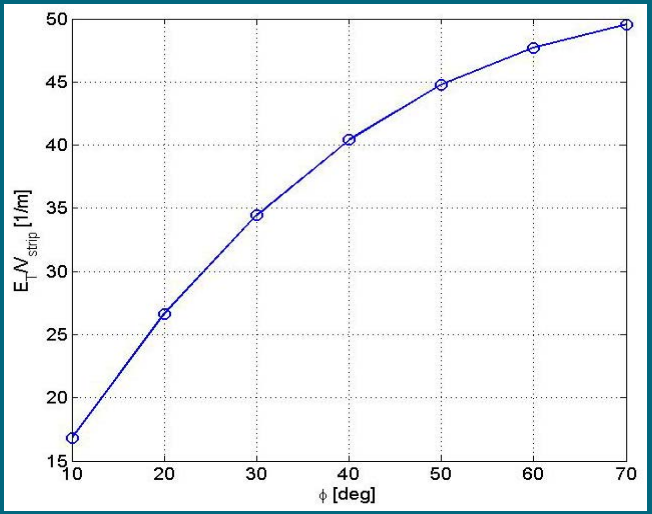
5) Future R&D plans.

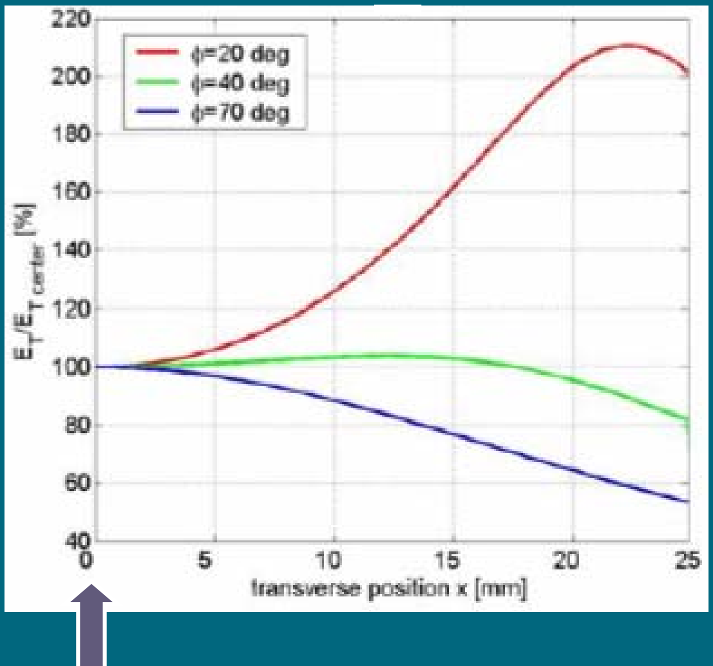
1) General considerations: transverse field profile properties (1/2)

CIRCULAR CROSS SECTION (50 Ω)



Horizontal component of the electric field (E_T) on the kicker axis as a function of the electrode coverage angle.



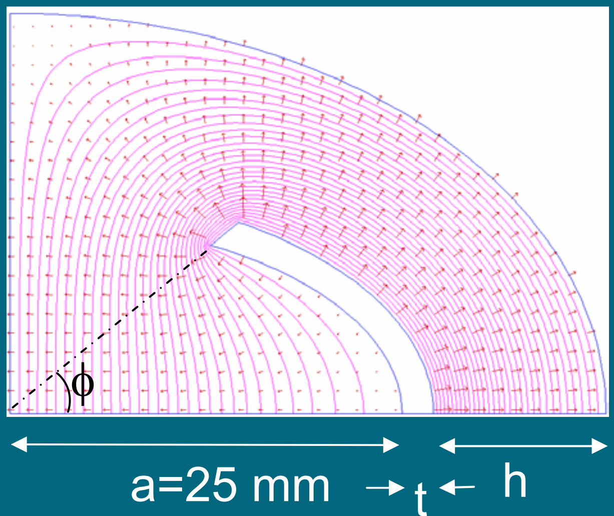


kicker axis

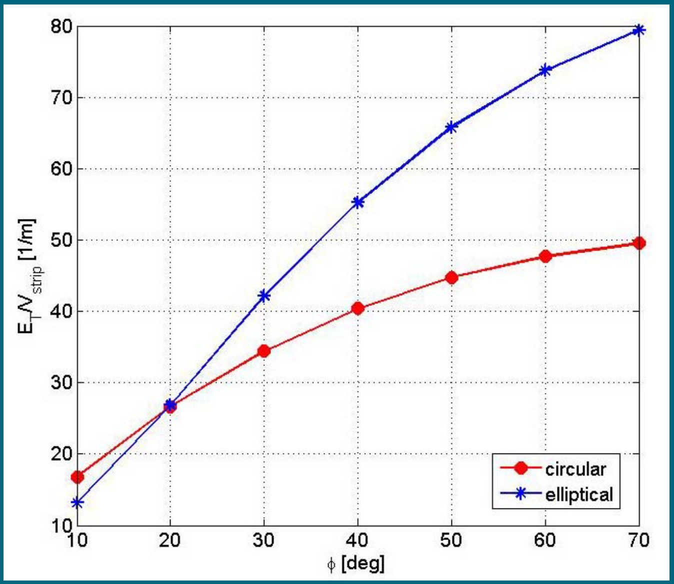
Horizontal component of the electric field (E_T) along the horizontal axis of the kicker cross section. The value is normalized to the value assumed by E_T on the center of the structure. Two different covarage angles for the electrode (20, 40 and 70 deg) are considered.

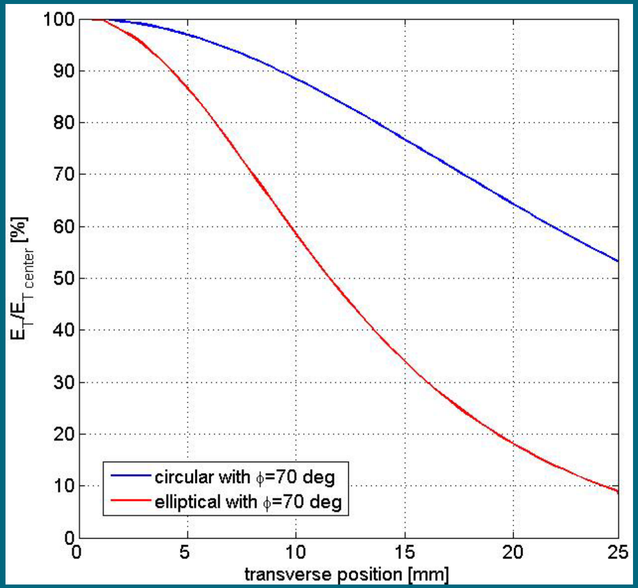
1) General considerations: transverse field profile properties (2/2)

ELLIPTICAL CROSS SECTIONS (50 Ω)



Horizontal component of the electric field (E_T) on the kicker axis as a function of the electrode coverage angle (Blue: elliptictal section; red: circular section). The efficiency of elliptical geometries is higher.

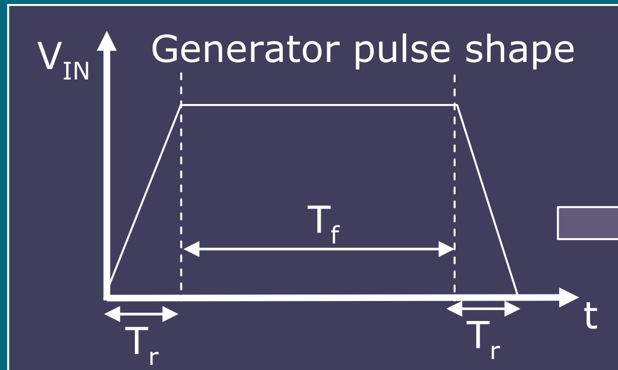


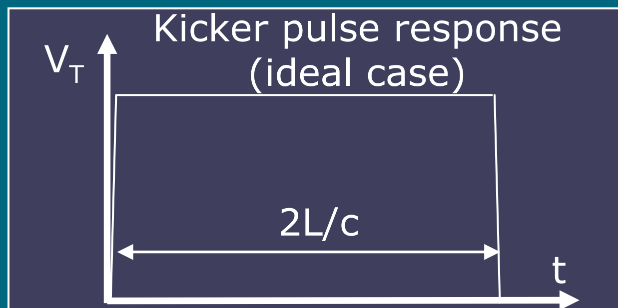


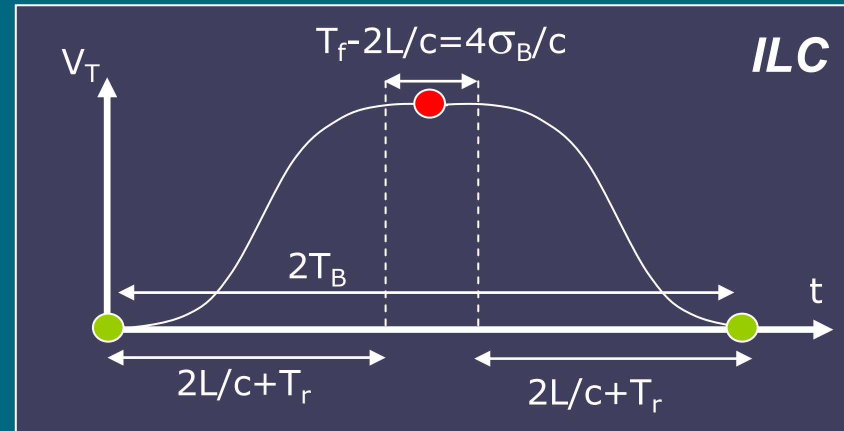
Normalized value of the horizontal component of the electric field (E_T) along the horizontal axis of the kicker cross section. The considered coverage angle is 70 deg both for the elliptical cross section (red) and for the circular section (blue).

1) General considerations: kicker length and pulse length

- L=kicker length
- T_r=rise time length
- T_f=flat top length
- σ_B=bunch length
- T_B=bunch spacing

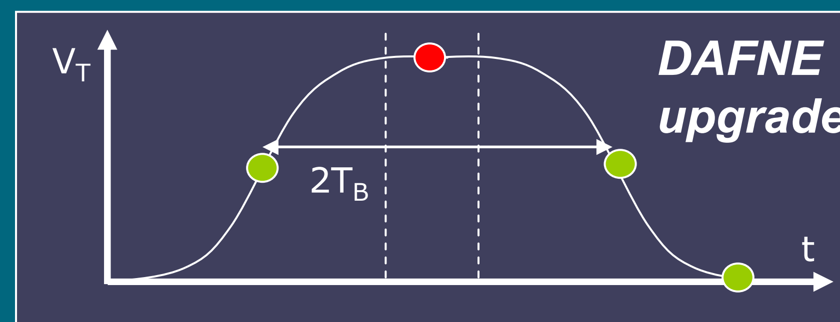






Injected bunch

Stored bunches

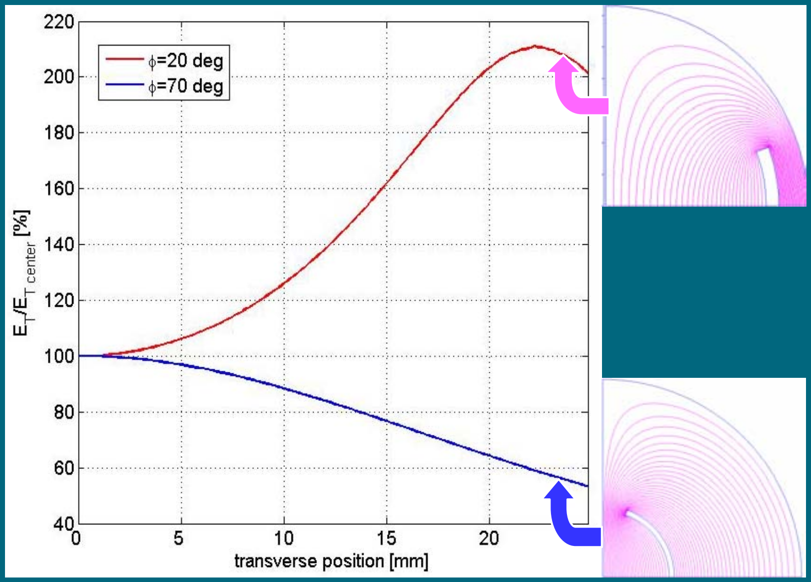


assuming T_r=300ps	DAFNE
E [GeV]	0.51
T_B [ns]	2.7
σ_B [mm]	35
Defl. [mrad]	5
L [cm]	73
T_f [ns]	5.3
σ_x [mm] @ septum and kicker	2
σ_y [mm] @ septum and kicker	1

2) Correction of the deflecting field flatness using tapers (1/2)

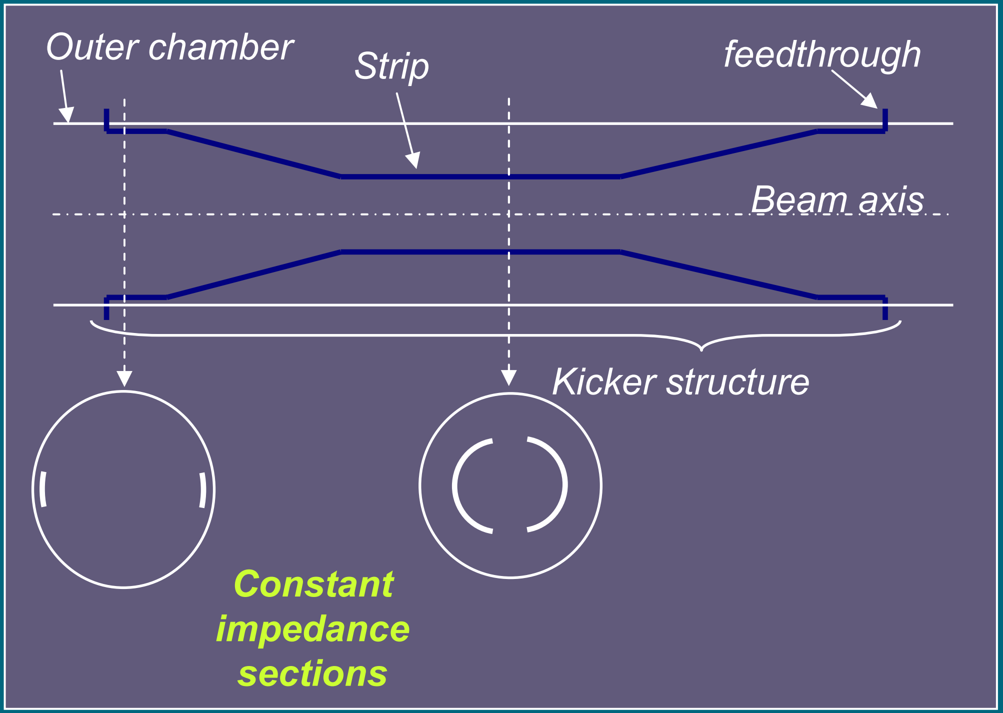
a) **Tapers** are usually used to avoid abrupt steps in the section of the vacuum chamber in order to **reduce the intensity of wakefields** and HOM (impedance of the machine).

b) The **uniformity of the deflection** depends on the coverage angle.



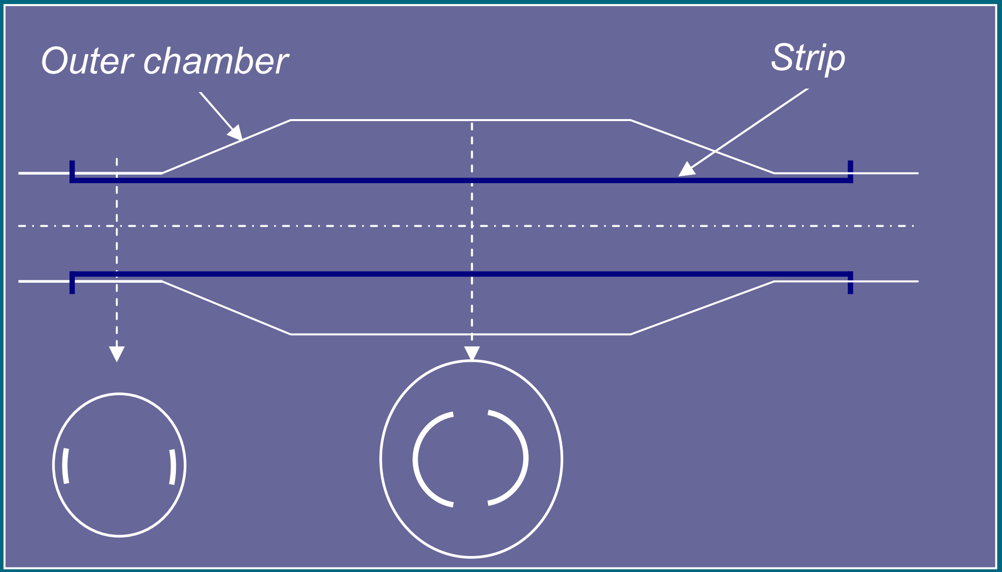
Tapering the transition between the kicker structure and the adjacent beam pipe it is possible to minimize:

- **The non uniformity of transverse deflection as a function of the transverse position;**
- **The contribution of the kicker to the impedance of the machine.**



2) Correction of the deflecting field flatness using tapers (2/2)

A different possible scheme

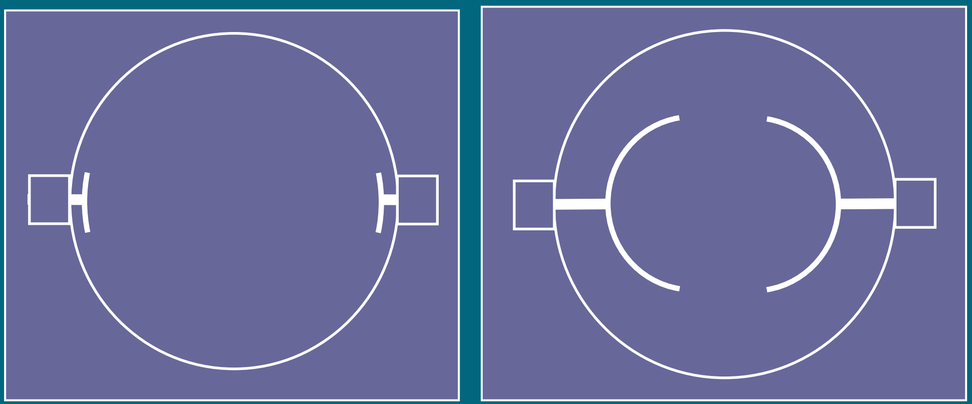


Furthermore:

smoother transition between feedthrough coax line and strip line

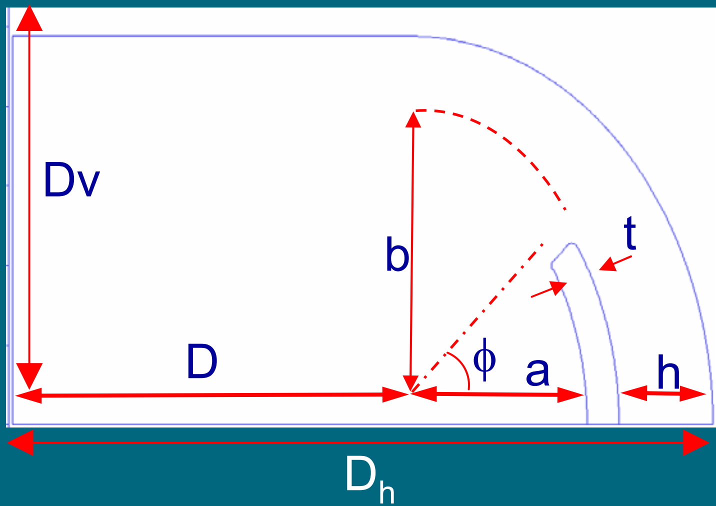
↓

smaller reflection coefficient at high frequency (short pulses)



Tapering is applicable to both cylindrical and elliptical geometries

3) Design of the DAΦNE kicker: transverse and longitudinal geometry



a) The elliptical geometry has been chosen to minimize the variation of the vertical dimension of the beam pipe between the injection region and the adjacent dipole region;

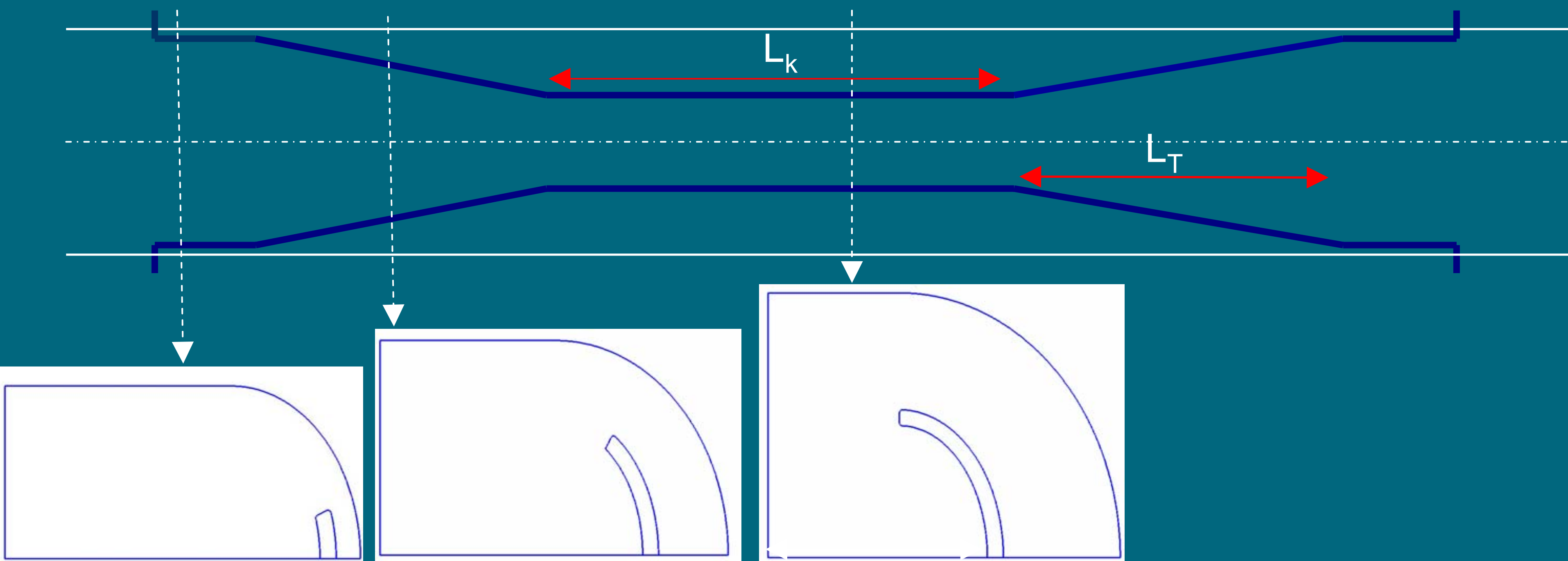
b) In each section along the structure Dh is a constant and Dv changes;

c) In each section ϕ has been chosen to have constant characteristic impedance of the line (50 Ω);

d) The value of a and b are the same for each sections and have been optimized together with the length L_k and L_T in order to contemporary achieve:

   1) optimum deflecting field uniformity over the horizontal coordinate;

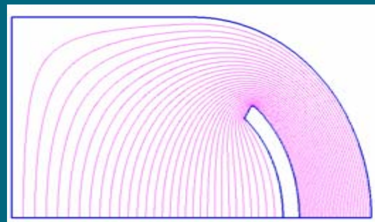
   2) total "effective length" of the kicker compatible with the bunch spacing.



3) DAΦNE stripline kickers design: optimization procedure (1/2)

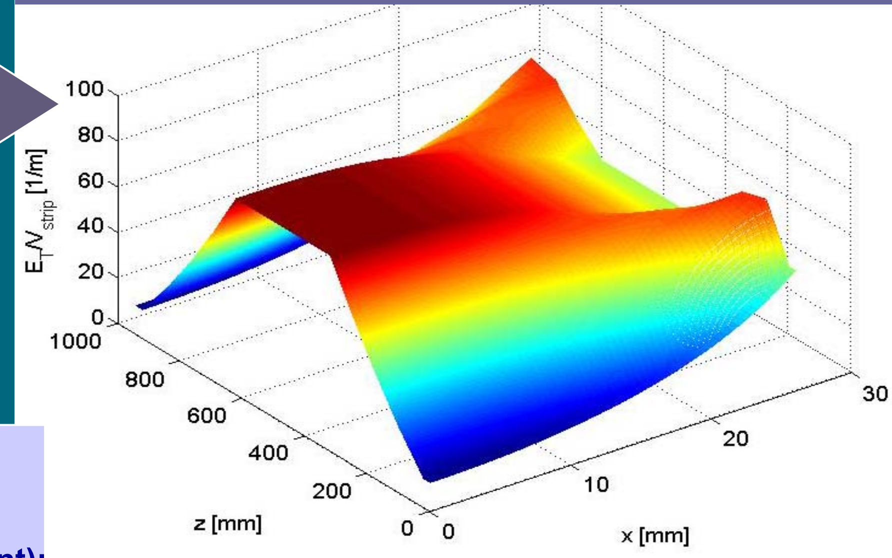
Choice of the optimum L_T/L_k for field flatness

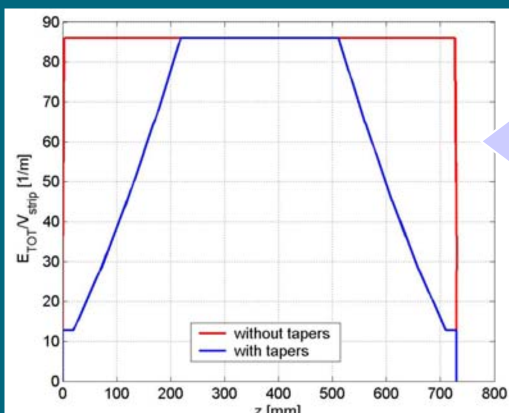
2D simulations of different sections along the kicker longitudinal axis



by interpolation

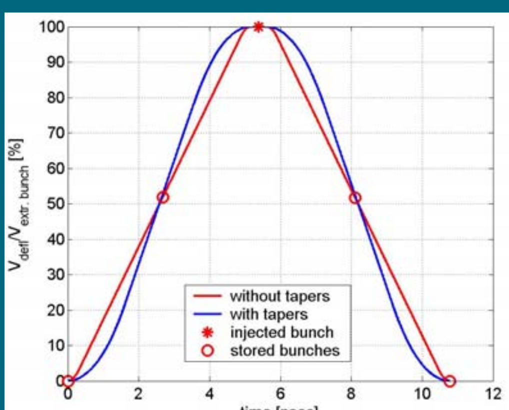
Construction of 3D map of the deflecting field



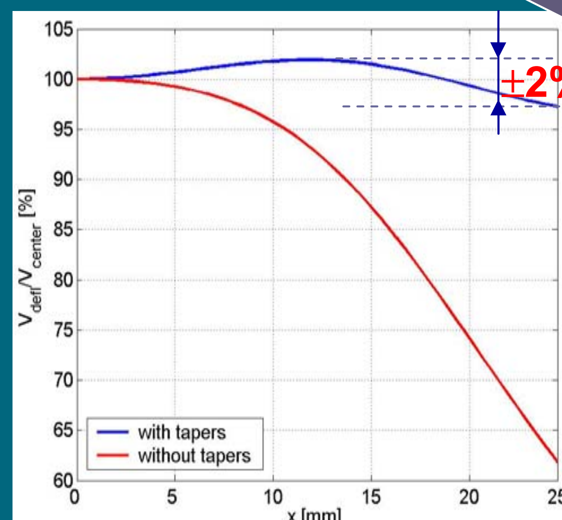


Straight, no tapers:
L_{TOT}=73 cm ⇒V=40 kV;

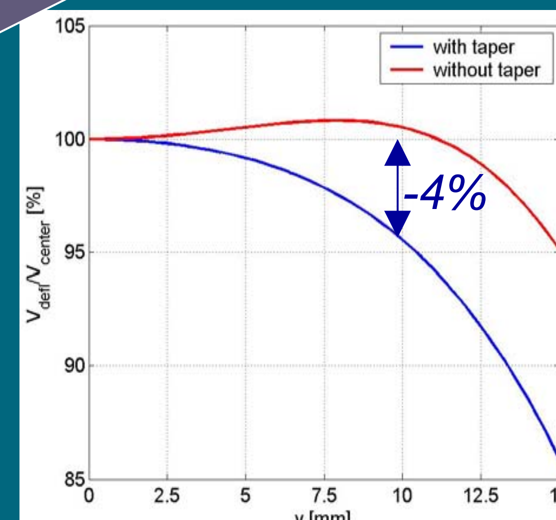
With tapers (less efficient):
L_{TOT}=73 cm, L_K=29 cm,
L_T=22 cm ⇒ V=58 kV



Field flatness by integration



horizontal axis



vertical axis

3) DAΦNE kicker design: optimization procedure (2/2)

L_T, L_k length tuning

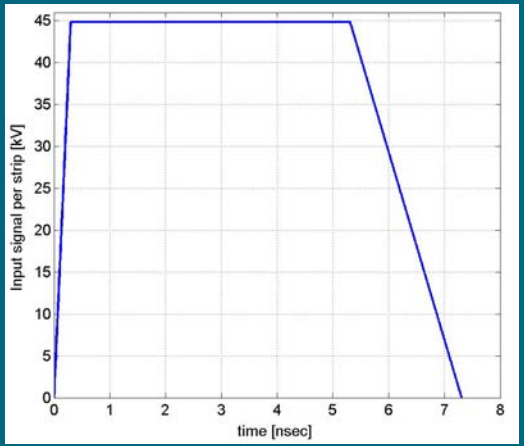
Increasing the total length of tapered striplines to reduce the required voltage:

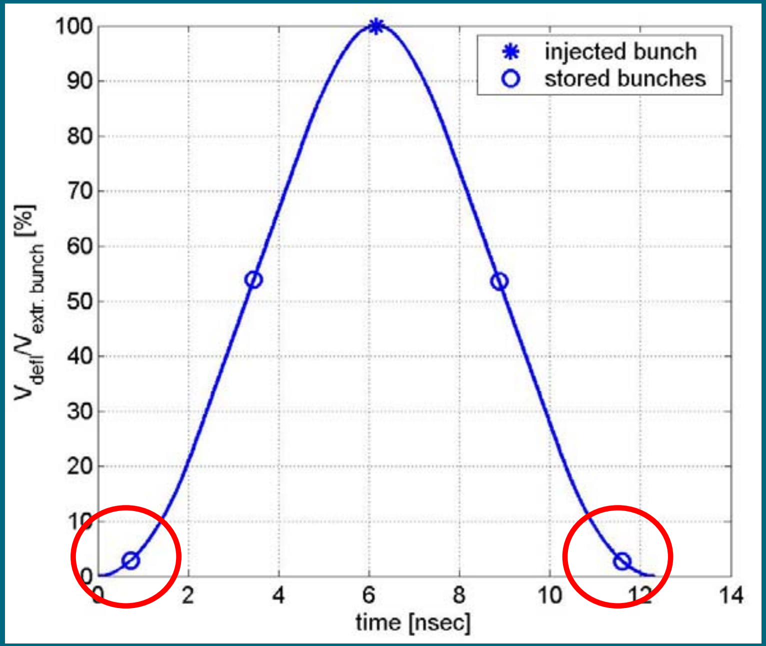
L_{TOT}=73 cm → **L_{TOT}=94 cm**

V=58 kV → **V=44 kV**

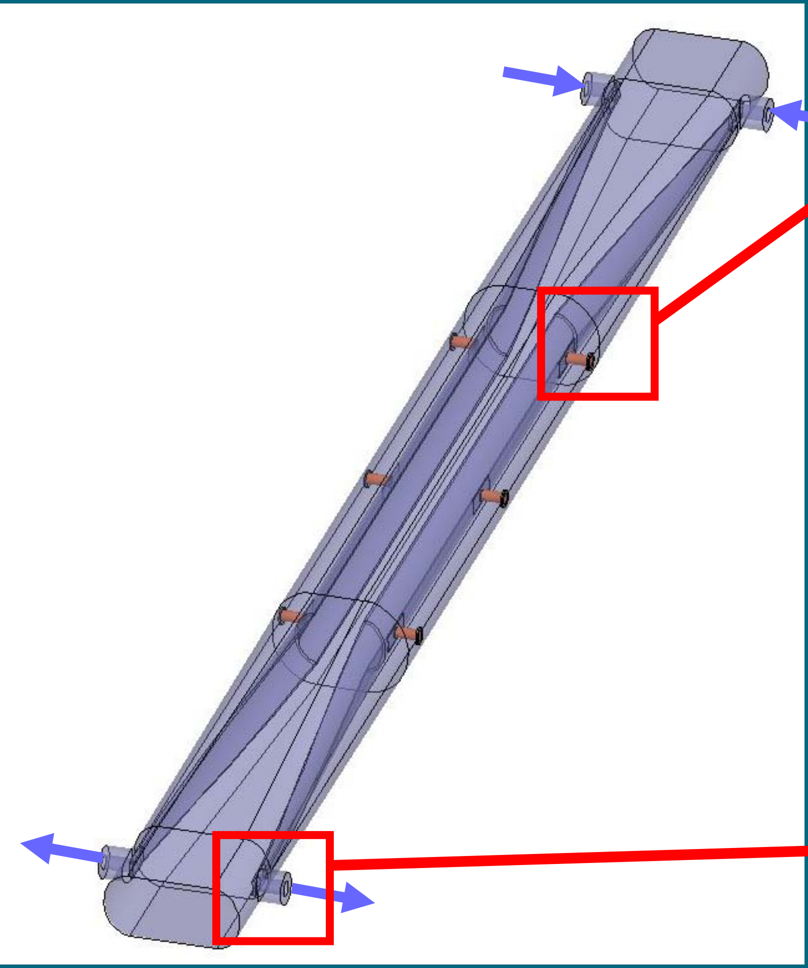
As a consequence the kicker impulse response becomes a bit longer.
The deflecting voltage as a function of time, which results from the convolution of a simplified model of the real input pulse with the kicker impulse response, spreads a bit over the two bunches that are two bucket away from the injected one.

Model of the real input pulse

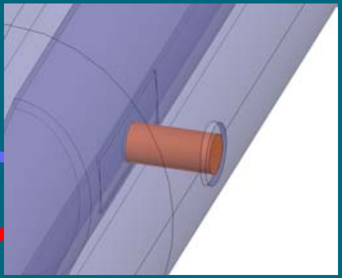




3) DAΦNE kicker design: 3D electromagnetic model (1/4)



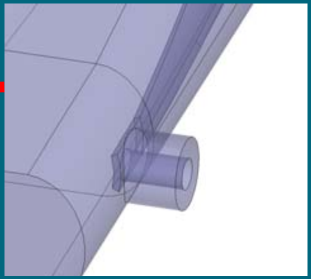
a) Effect of ceramic stand-off



b) HOM studies

c) Real deflecting field calculation and frequency response

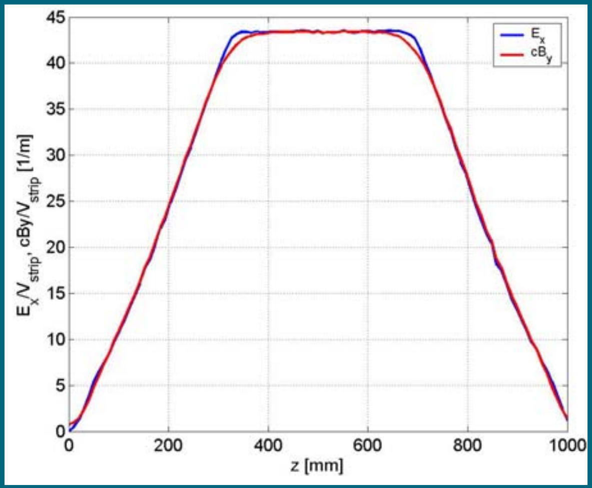
d) Coaxial-strip transition optimization and beam transfer impedance



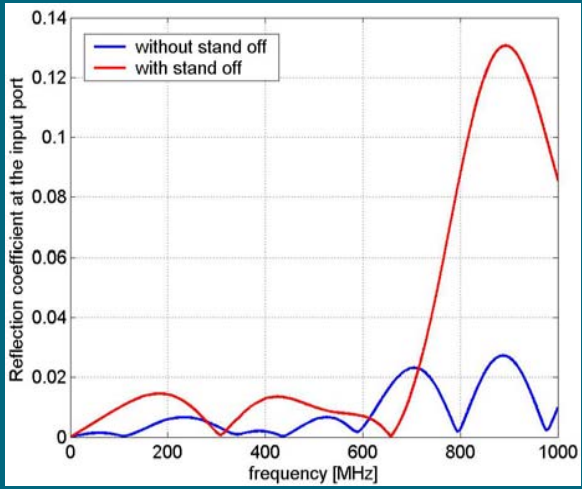
Optimization of the whole structure

3) DAΦNE kicker design: 3D electromagnetic model (2/4)

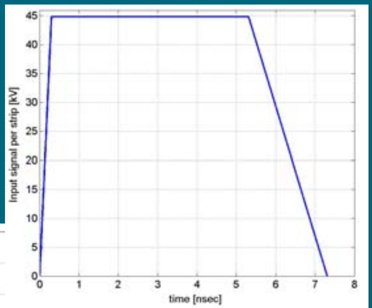
Deflecting field



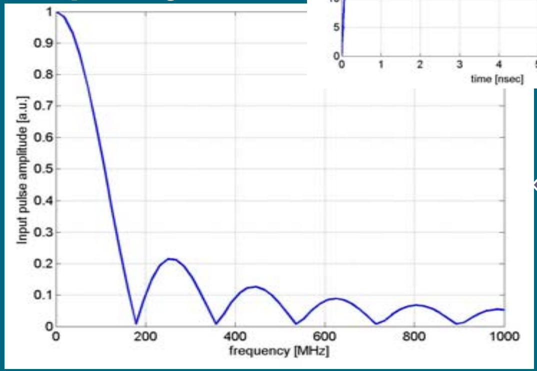
Reflection at the input coax port



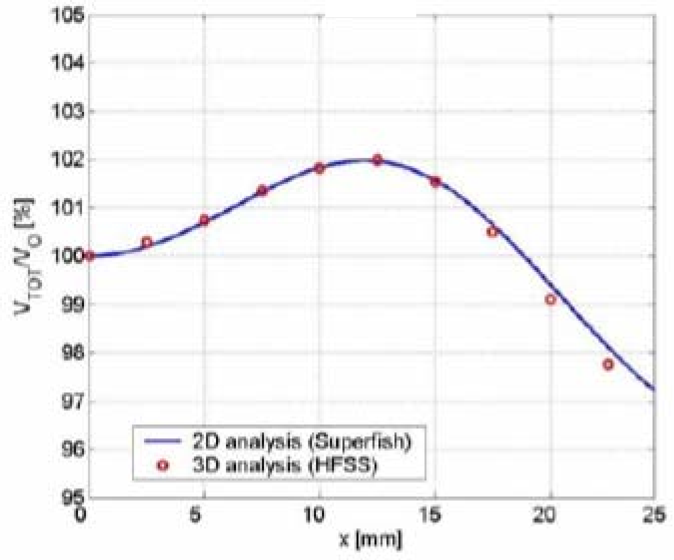
Pulse model vs. time

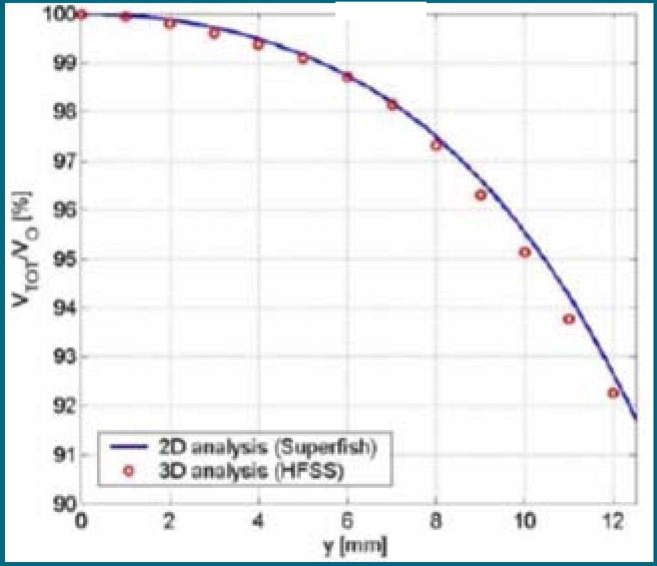


Pulse model vs. frequency

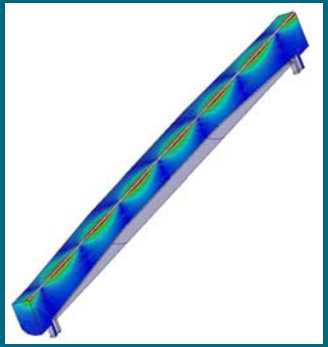


Deflecting field uniformity in the transverse plane (3D compared with 2D results)



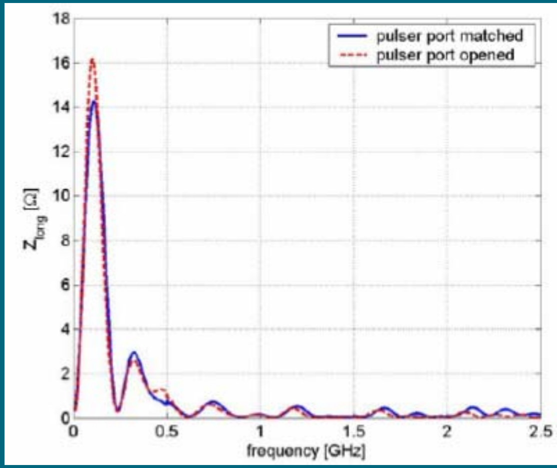


3) DAFNE kicker design: 3D electromagnetic model (3/4)

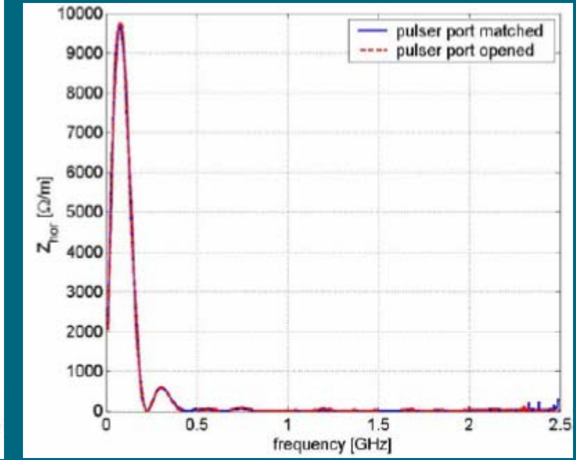


Evaluation of beam coupling impedance and transfer impedance using the wire method tecnique.

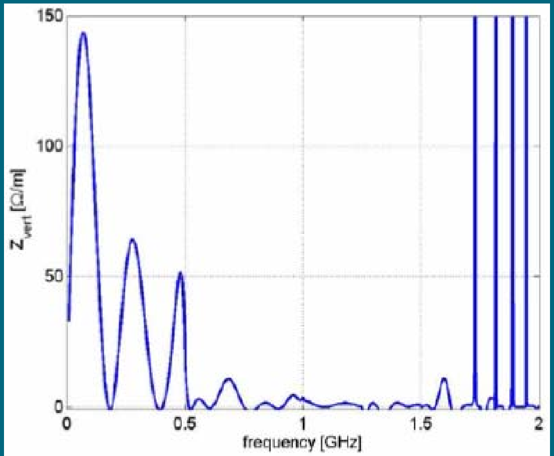
BEAM COUPLING IMPEDANCE



Longitudinal impedance



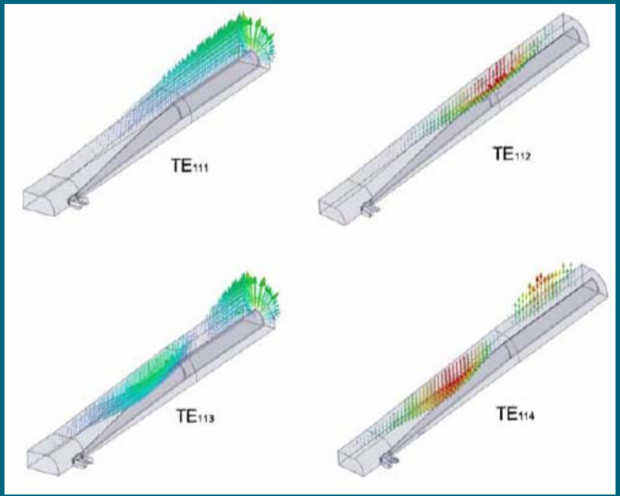
horizontal impedance



vertical impedance

4 vertical impedance HOMs found.
They belong to the TE_{11n} family.

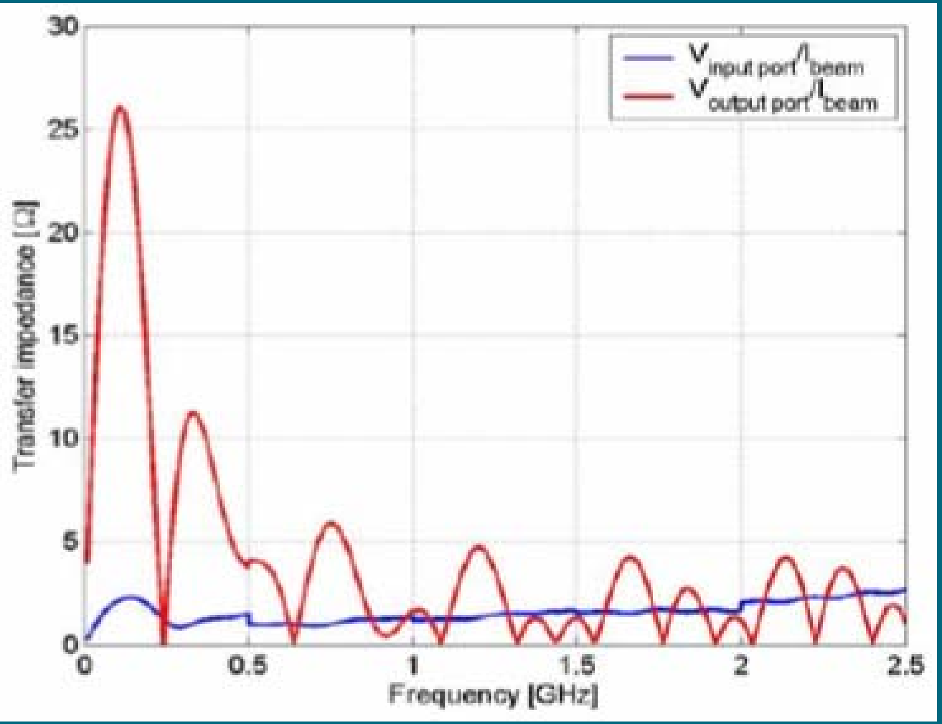
low transverse impedance
not a problem for the vertical feedback system



f_1=1.60 GHz
f_2=1.66 GHz
f_3=1.74 GHz
f_4=1.83 GHz

3) DAFNE kicker design: 3D electromagnetic model (4/4)

BEAM TRANSFER IMPEDANCE



Bunch Charge [nC]	Peak voltage into the downstream port [V]	Peak voltag into the upsteram port [V]
1	8	16
3	25	50
6	50	100

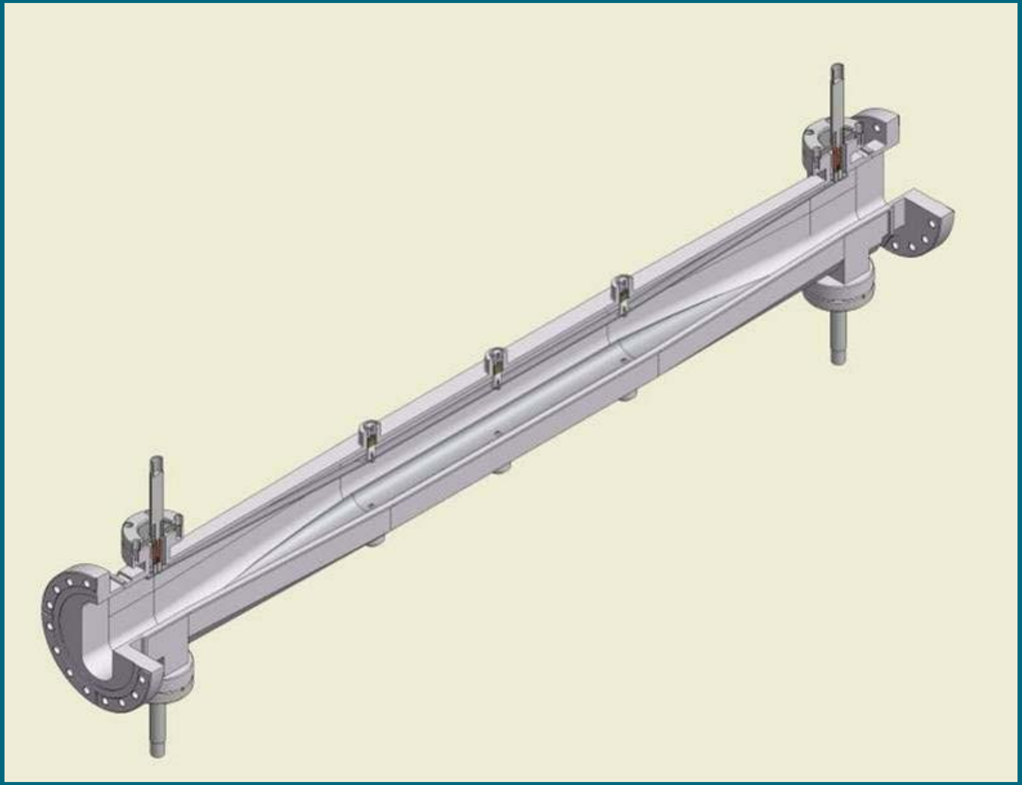
Beam induced peak voltage into the kicker coax ports

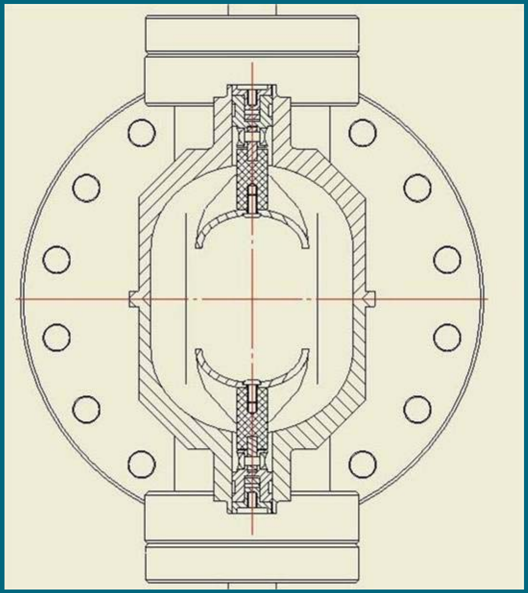
Beam current [A]	Average power into the downstream port [W]	Average power into the upsteram port [W]
1	1	5
2	4	20

Beam induced average power into the kicker coax ports

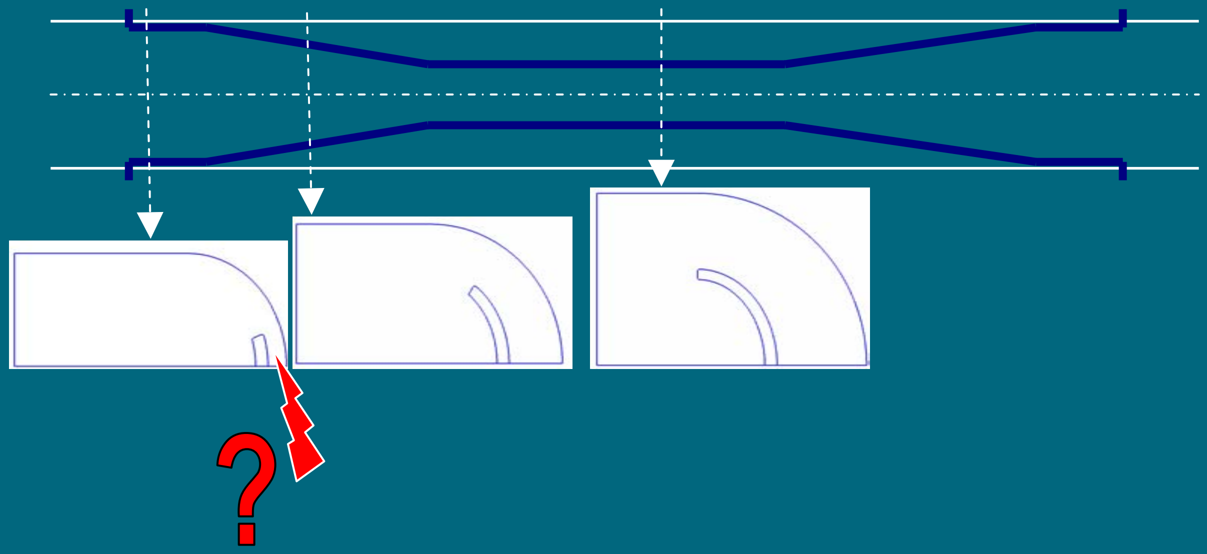
3) DAFNE kicker design: mechanical drawings

The kicker for the injection upgrade of DAFNE has been almost completely designed. The mechanical drawings are ready as well, except for some last details not yet completely defined (the feedthrough housing).
To get the required deflection, very high voltage (about 45 kV) has to be applied to each electrode.
HV tests on the most critical parts and components of the kicker are necessary for defining the final version of the drawings.

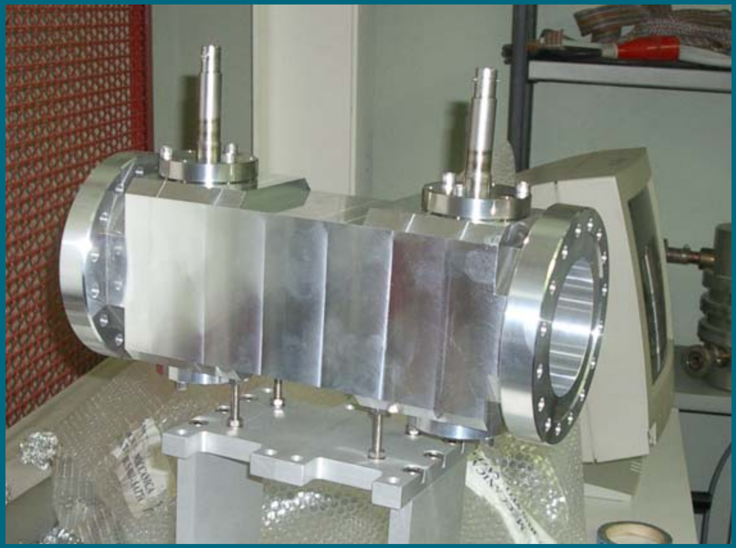




4) R&D and HV tests: the test stripline



When HV is applied the possibility of discharges is higher in the end-section of the kicker electrodes, where the electrode itself is closer to the vacuum tube.



A stripline with the same dimension and the same distance from the chamber of the kicker stripline in the end section has been built. Coax ceramic feedthrough can be mounted on this test device to apply the HV to the stripline.

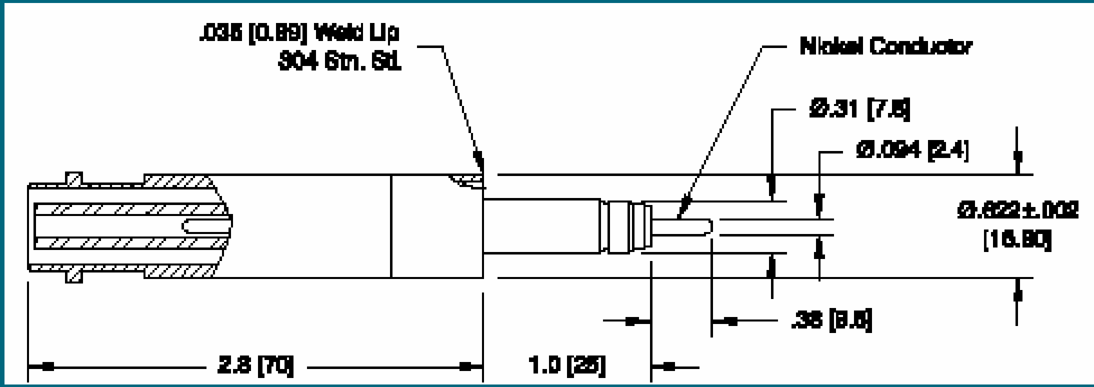
4) R&D and HV tests: the feedthrough

The ideal feedthrough for our purpose has to:

• be able to tolerate the applied voltage (45-50 kV)

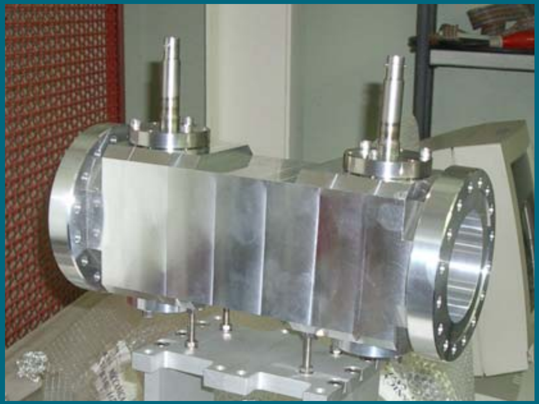
• have a constant 50 Ω characteristic impedance.

Second statement is important to keep low the beam impedance of the kicker even well beyond the frequencies contained in the spectrum of the pulse.
It is not obvious to find a feedthrough fulfilling at the same time this 2 specifications.
The design of a dedicated feedthrough is in progress at LNF.



First tests have been done with a commercial feedthrough (SHV20 standard).
It is specified for 20kV DC (but our pulse lenght is 5ns).
The value of the characteristic impedance is not specified, but it is not constant.

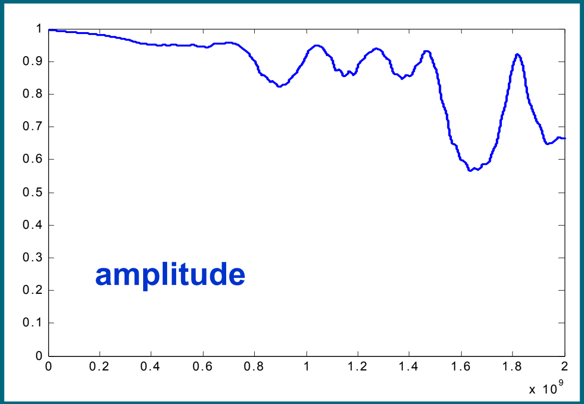
4) R&D and HV tests:
the feedthrough frequency response

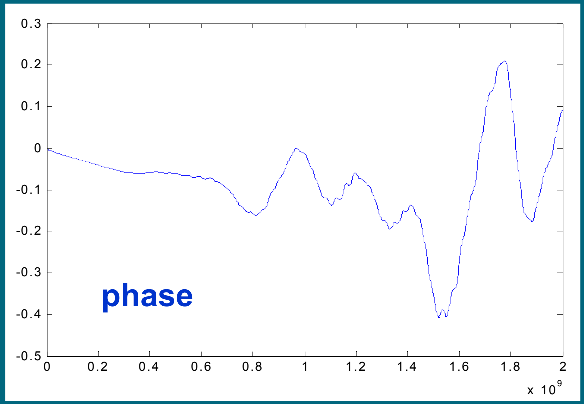


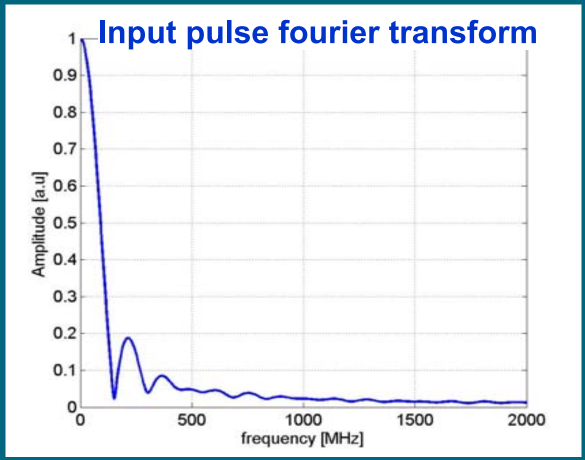
The test stripline has 2 flanges for housing 2 of such feedthroughs.

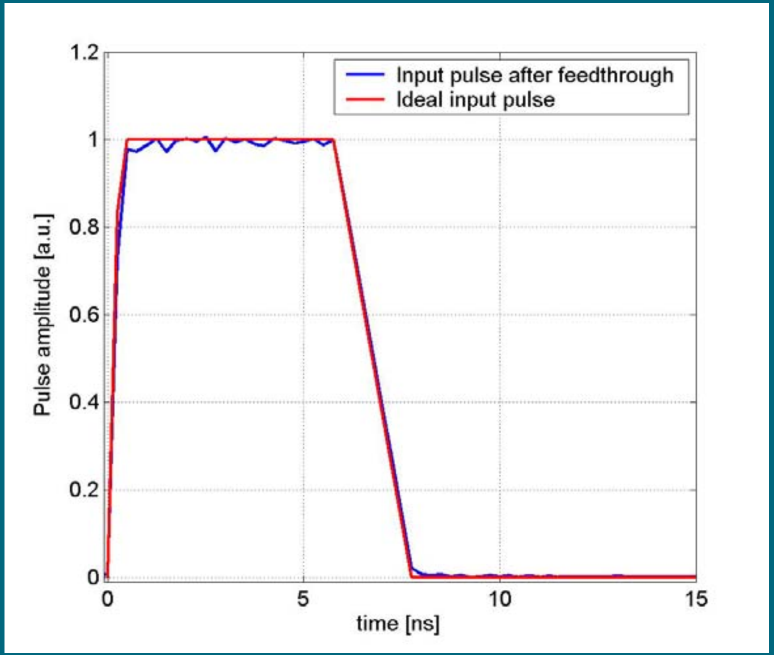
The frequency response of the feedthrough and the transition between foaxial and strip line can be measured with a N/A.

Measured transmission response







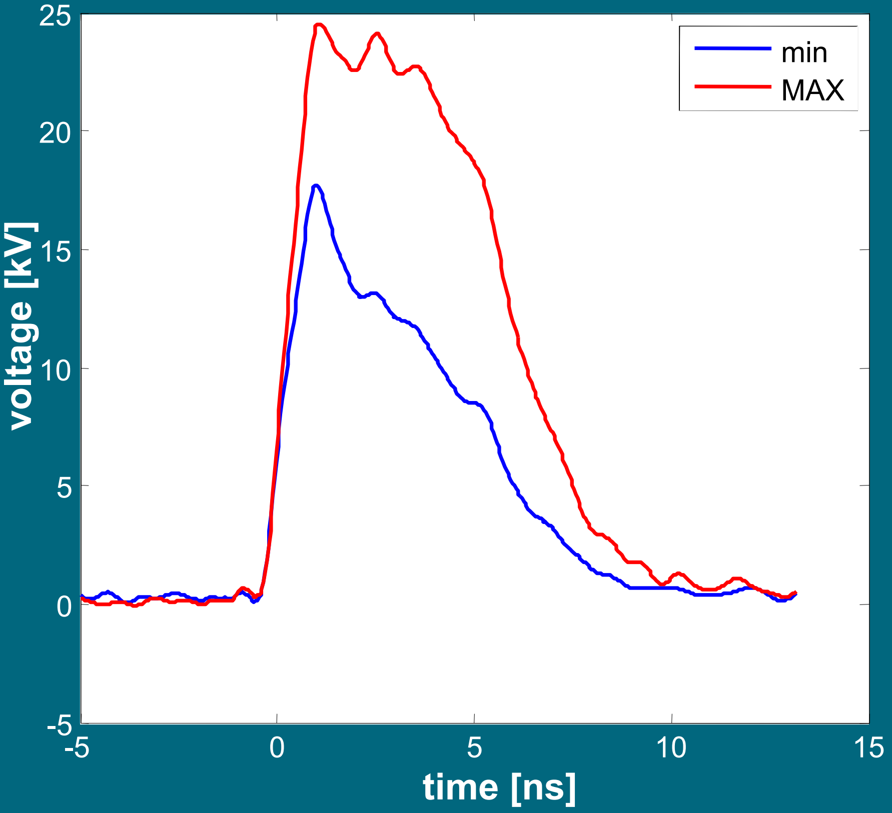


pulse shape distortion due to the real feedthrough

4) R&D and HV tests: the FID F10K10N207 pulser - V_{OUT} 16÷24kV.

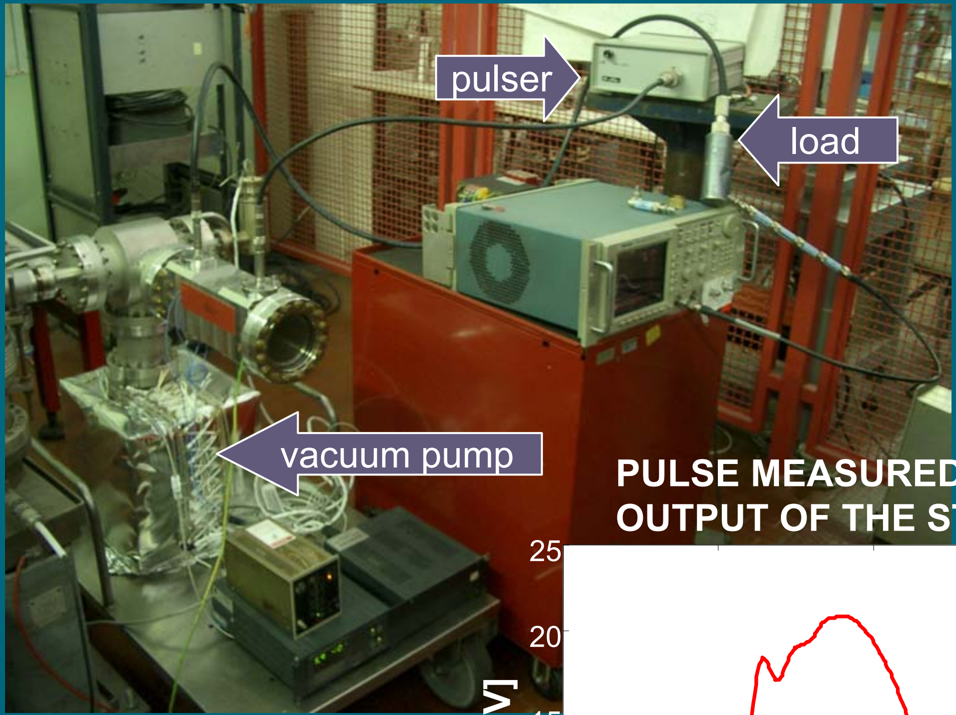
First HV tests have been performed using a pulser borrowed from FID GmbH in the meanwhile that the 50kV final pulser (FPG 50-01SP) was fabricated.
This test pulser has pulse length and rise time similar to the FPG 50-01SP, while the pulse amplitude is only 20kV.

PULSE MEASURED AT THE GENERATOR OUTPUT CONNECTOR

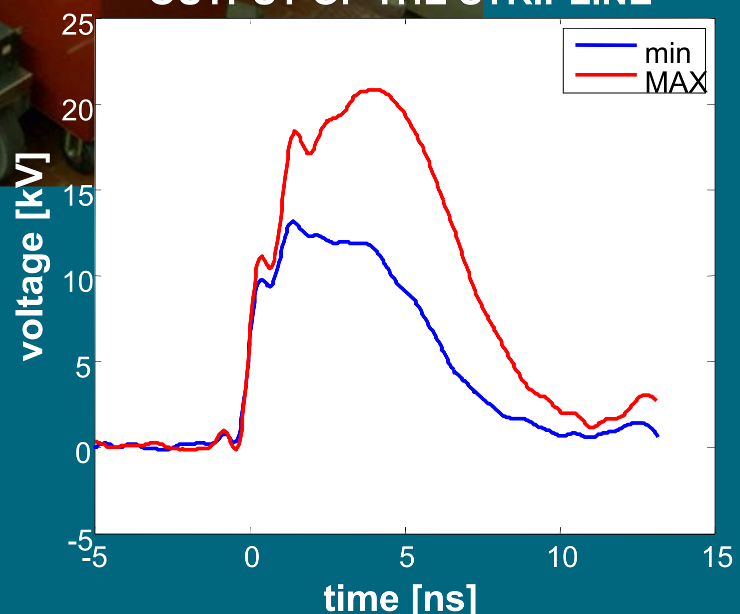


4) R&D and HV tests: results with F10K10N207

Using the pulser we have been able to test both the feedthroug and the stripline at HV operation.

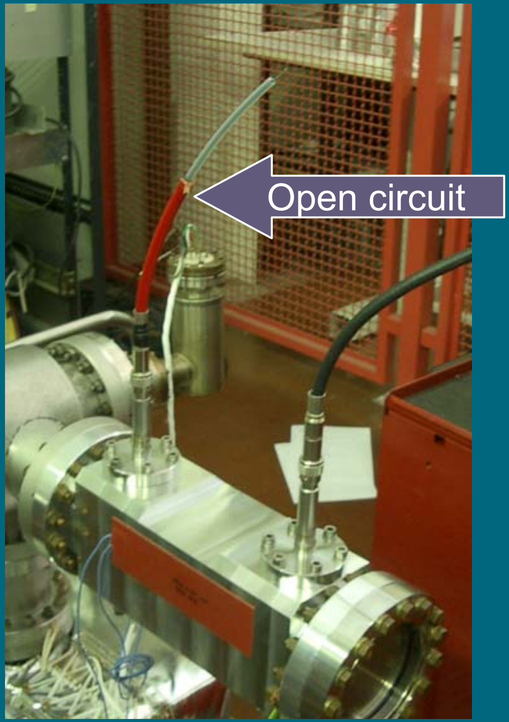


PULSE MEASURED AT THE OUTPUT OF THE STRIPLINE



To make the test **more probatory**:

- the load is disconnected from the stripline output which remain an **open circuit**
- **reflected pulse adds to the forward pulse**



Results:

- **no monitors** of the pulse waveform available
- just vacuum read out and inspection through the glass window
- **no phenomena attributable to electric discharges have been observed**

4) R&D and HV tests:
the FPG 50-01SP pulser

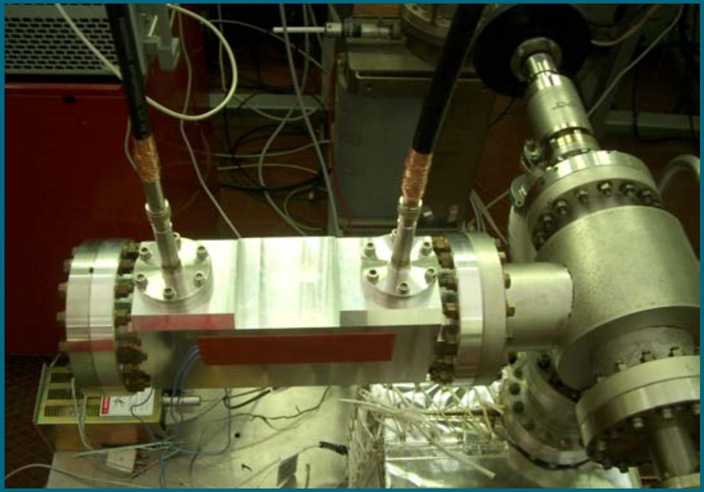
Test results:

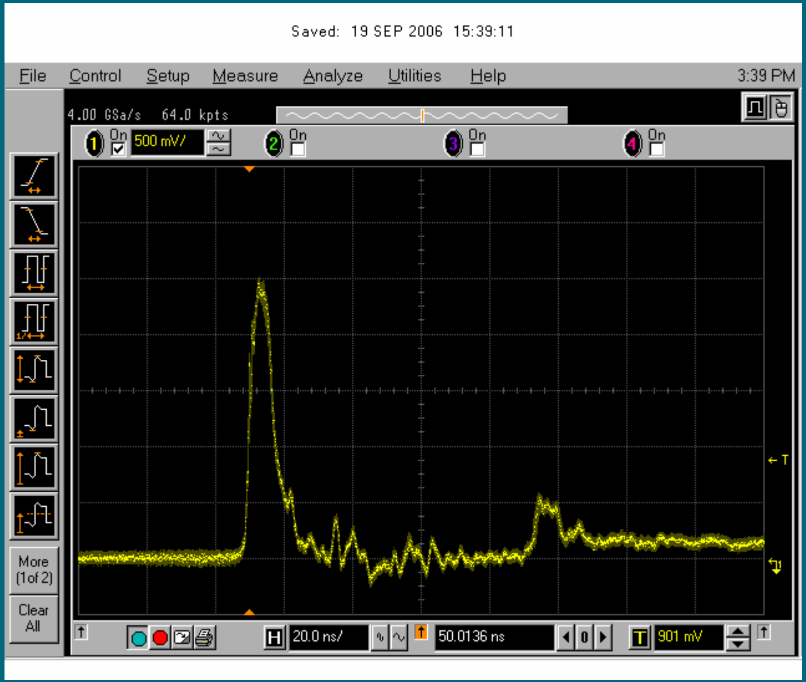
• even at maximum output voltage (50 kV) there are no discharges along the stripline.

• after few pulses (some hundreds) there has been a breakdown of the ceramic of one feedthrough which lost its vacuum tight.

• a modification in the feedthrough housing was done; but, after some thousands of pulses with the voltage set at 48 kV, discharges occured in the air side of the feedthrough. It has been irreversibly damaged.

HV tests have been repeated with the same set up when the 50kV pulser has been delivered at LNF.





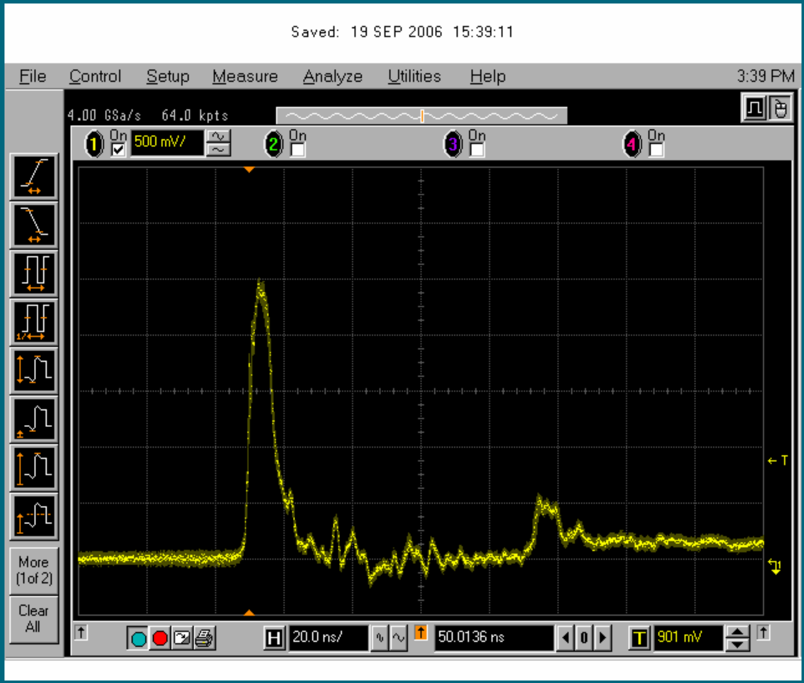
Grabbed waveform of the pulse (V_{OUT}=48kV) before the feedthrough damaging

5) R&D and HV tests:
the FPG 50-01SP pulser

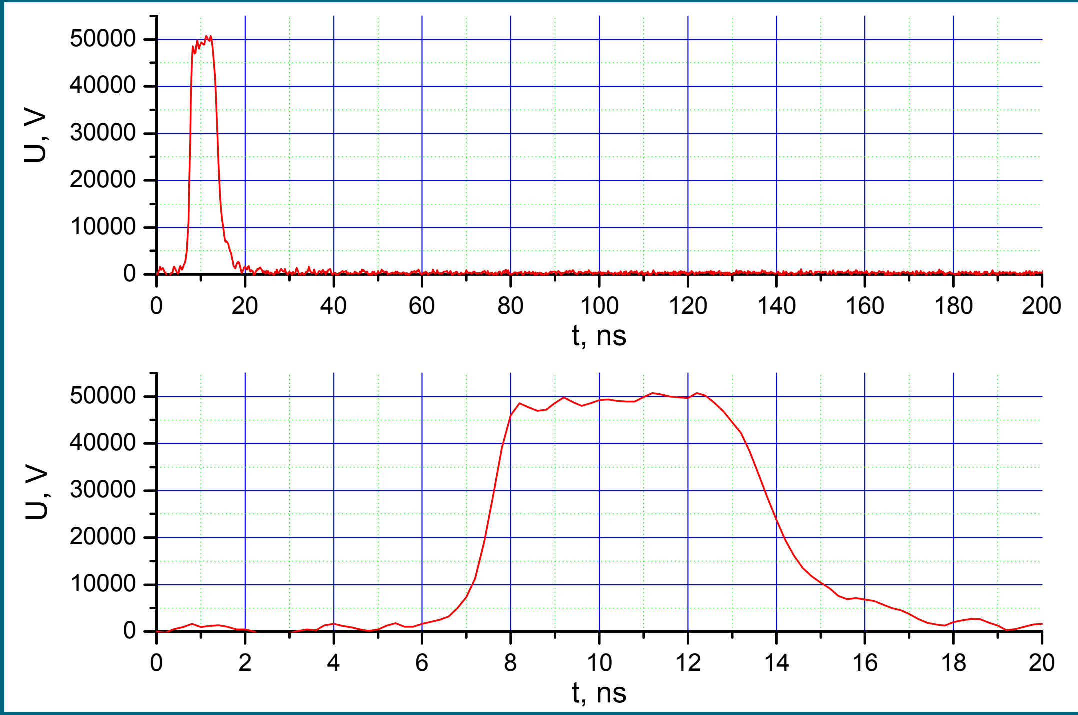
A second version of the 50kV pulser has been developed by FID to improve the pulse shape:

- Fall time shortened
- No secondary pulses
- Improved flatness of the pulse.

We are waiting for the delivering of this improved version of the pulser.



Waveform of the first version of the 50kV pulser measured at LNF



Waveform of the improved 50 kV pulser measured by FID

5) Future R&D plans.

Owing to the failure of HV tests on the SHV20 feedthrough we have decided to speed up the work on the special LNF feedthrough. We encounter problems with a first version of the feedthrough during the metallization of the ceramic surfaces. At present we are revising the design changing the ceramic material.

We hope to have at least a couple of feedtrough prototype ready to be RF measured and tested with the 50kV pulser in a couple of months.

Afterwards, if the upshot of it all will be positive, the mechanical drawing of the kicker can be finished with the details concerning the new feedthrough housing and the fabrication of the first kicker can start.

An improved version of the 50kV pulser should be delivered at LNF very soon.

Fundings have been already assigned for construction and installation of the 2 DAFNE kickers (with π phase advance distance), the 4 FID pulsers and in general for the whole injection system upgrade.

Concerning the kicker for ILC, a shorter stripline kicker is necessary, due to the reduced bunch spacing. The design of this kicker is in progress and is based on the same criteria (tapered stripline) developed in the case of the DAFNE kicker, finalized to minimize the coupling and transfer impedance of the device.

CONCLUSIONS

1) Varying the coverage angle of the stripline it is possible to control the amplitude and the distribution of deflecting field over the kicker transverse plane.

2) The tapered stripline design allows:
   - Correction of the deflecting field flatness.
   - Substantial reduction of the beam impedance (coupling and transfer).
   - Improved matching of the transition between stripline and coaxial input and output lines.

3) The results of the HV tests performed till now have been:
   - Successful for the stripline geometry.
   - Negative for the used commercial feedthrough.

4) The design of a dedicated feedthrough is in progress.