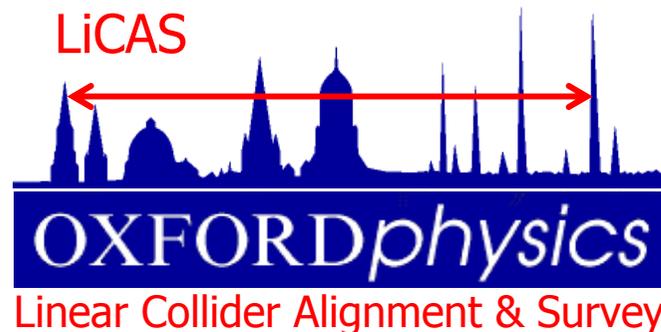


The LiCAS-RTRS

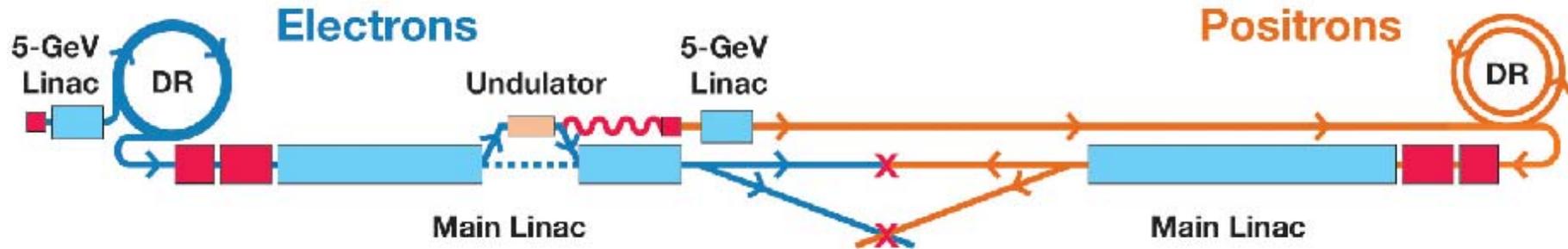
A Rapid and Cost Efficient Survey System for the ILC

Armin Reichold, JAI Oxford



Warsaw University

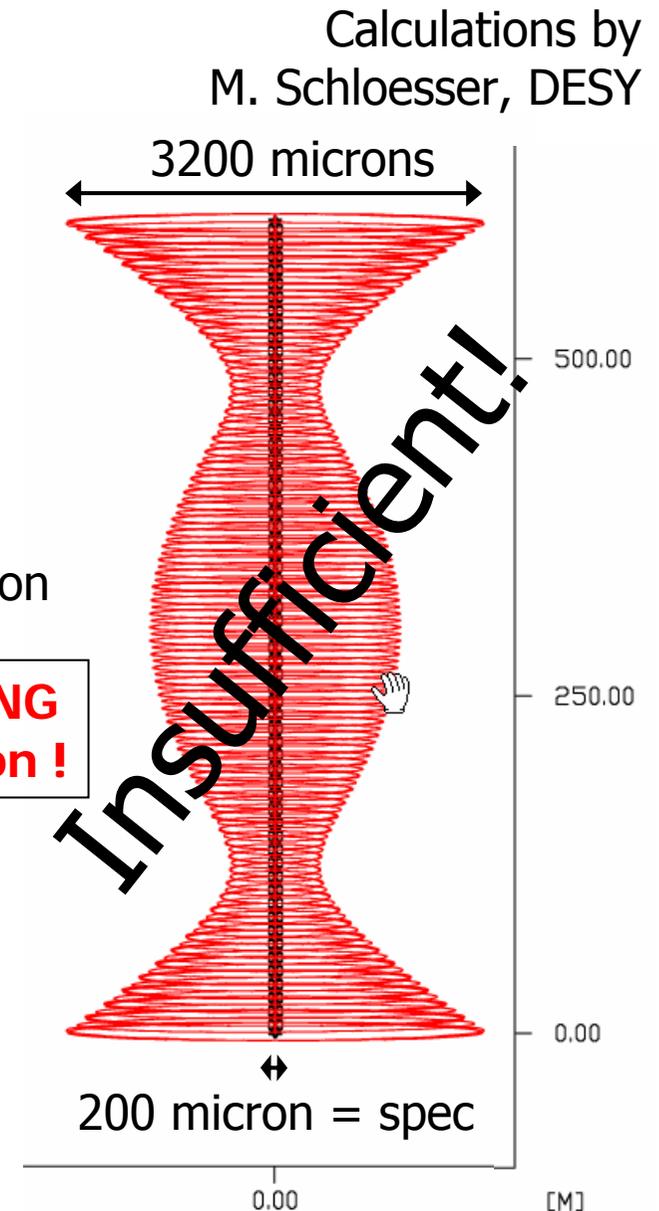
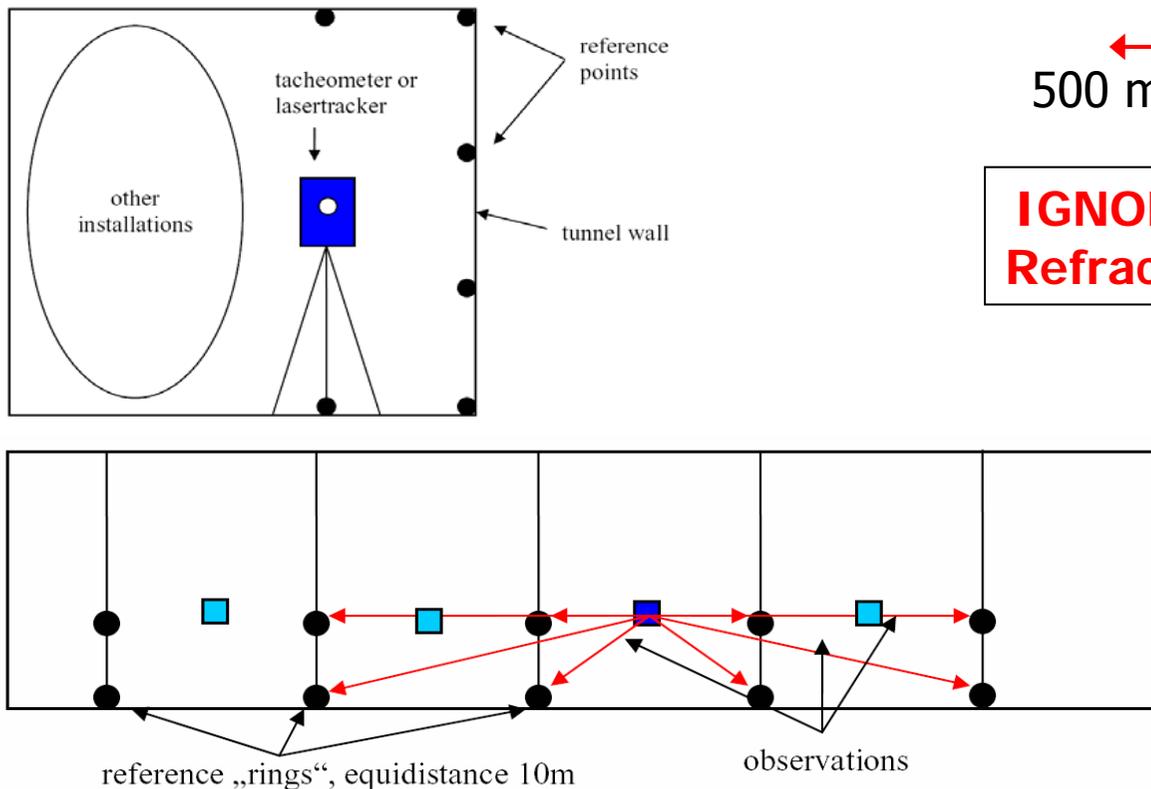
- Introduction
 - The ILC
 - LiCAS project mission
 - Comparison to traditional techniques
 - The RTRS concept
 - Cost modelling of the RTRS reference survey
- Project Status (news only)
 - Expected performance
 - Sub-systems
 - FSI (skipped)
 - LSM
 - electronics
 - mechanics
 - Installation



- Total length end to end ~ 30 km
- Total beam lines > 100 km
- E_{cm} adjustable from 200 – 500 GeV (>5*LEP)
- Design peak luminosity $2 \times 10^{34} \text{ cm}^{-2} \text{ s}^{-1}$ (~10,000*SLC)
- Energy stability and precision below 0.1%
- Energy upgradeable to 1 TeV
- Beam height at collision point ~ 5nm

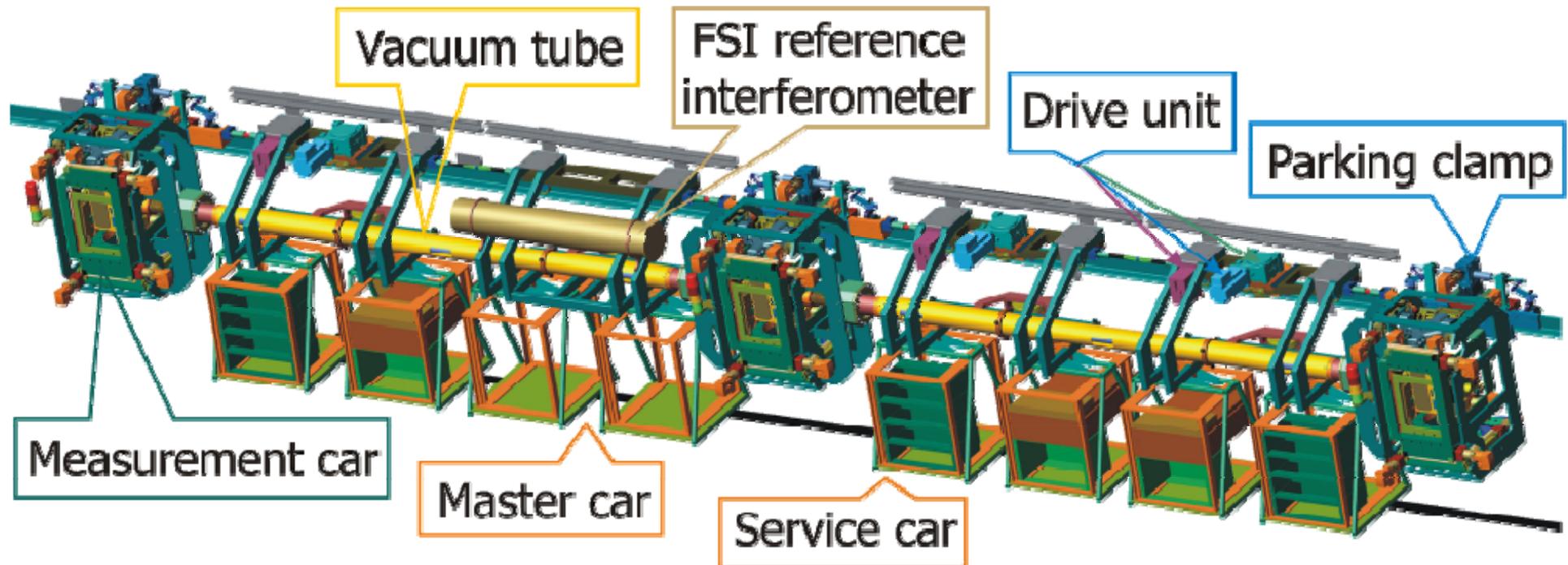
- All ILC elements need to be accurately aligned to produce full luminosity
- Survey = multi step process with single tolerance budget driven by **accelerator physics**:
 - component construction
 - component fiducialisation
 - **Survey ← LiCAS**
- Reference Network **S**urvey (Linac specs):
 - 200 μ m vertical = our slice of tolerance budget
 - over 600m = O(betatron) wavelength
- **Open air survey too inaccurate** (see next slide) due to instrument resolution and refraction and ...
- ... "somewhat" **slow** and ...
- ... "a touch" **expensive** (see later in this talk)
- Need new technique & instruments
 - ➔ **demonstrate Rapid Tunnel Reference Surveyor (RTRS)**

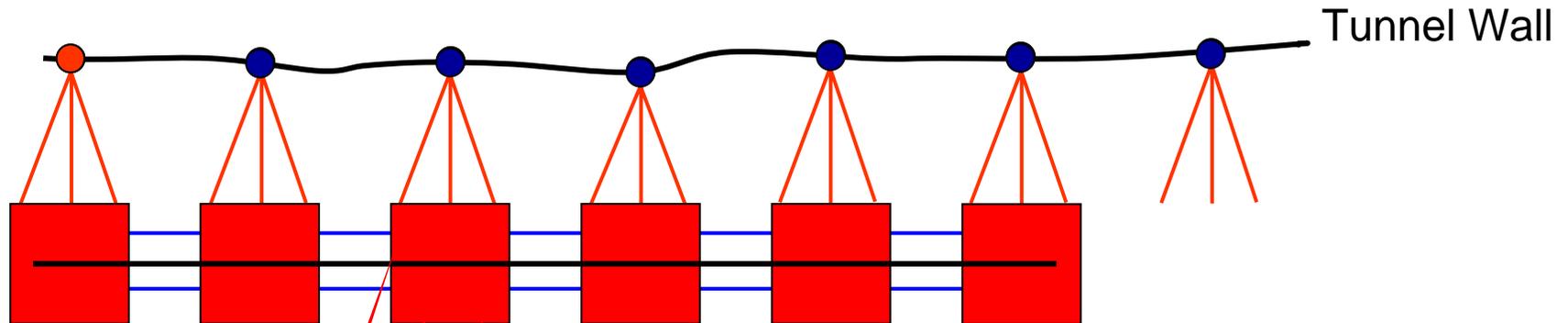
- Traditional in this context means:
 - Optical survey in open tunnel air using laser trackers
 - $\sigma_{\text{horizontal}} = 0.15\text{mgon}$, $\sigma_{\text{vertical}} = 0.15\text{mgon}$,
 $\sigma_{\text{distance}} = 0.015\text{mm}$
 - **Ignoring refraction**
- Network geometry assumes access to only one side of the tunnel



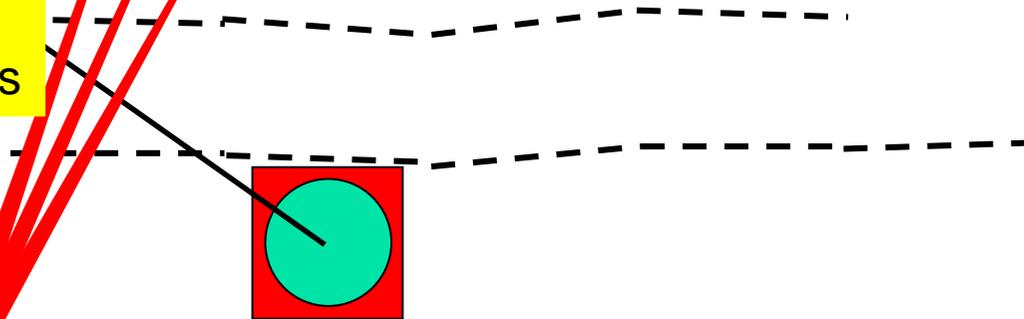
IGNORING Refraction !

Insufficient!

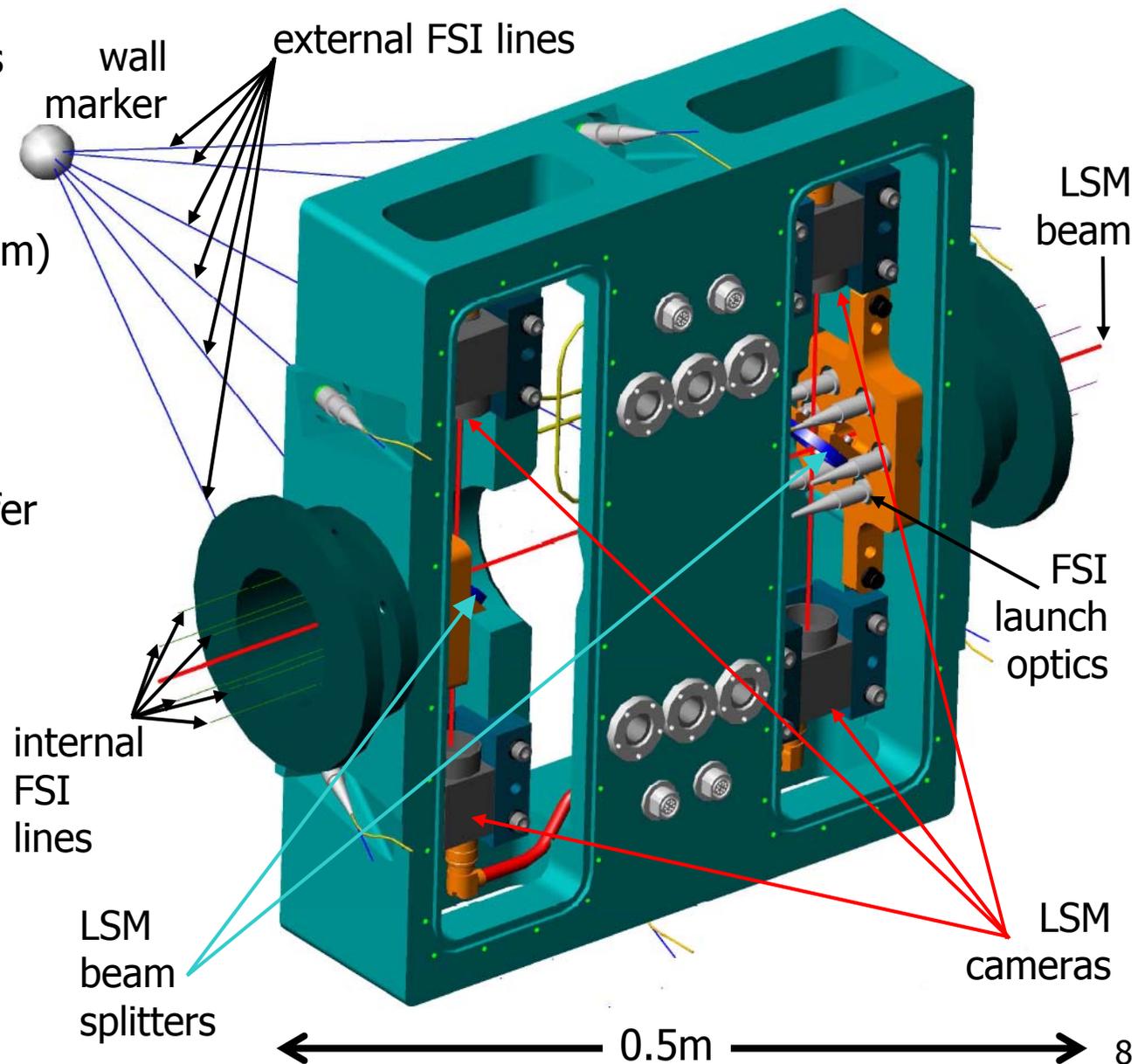




LiCAS technology for automated stake-out process



- Machined from single cast of multiple stress relieved Invar
- High precision machining of active element seats $O(10 \mu\text{m})$
- CMM survey of the entire unit and sub-assemblies
- Unit under vacuum
- Optimised heat transfer paths from CCD's to surface
- Custom vac. fibre feedthroughs
- Design maxime:
 - Stability of active element positions



■ Cost modelling of the reference survey

■ $TCO_{Ref} = R_{acc} n_{surv} L_{acc} T_{sd} (k_{sd} + C_{surv}) + I_{surv} + M_{surv}$

- TCO : Total cost of ownership
- R_{acc} : Lifetime of accelerator [years]
- n_{surv} : Number of surveys per year [1/year]
- L_{acc} : Length of beamline [km]
- T_{sd} : time required for 1 km survey [days/km]
- k_{sd} : cost per shutdown time [€/day]
- C_{surv} : cost of survey team(s) [€/day]
- I_{surv} : Investment costs for survey system [€]
- M_{surv} : Maintenance costs for survey instruments [€]

■ Global Assumptions

- $R_{\text{acc}} = 20$ [years]
- $n_{\text{surv}} = 1.2$ [1/year]
- $L_{\text{acc}} = 50$ [km]
- $k_{\text{sd}} = 800$ [k€/day] (HERA operations cost + TESLA investment cost)

■ Specific Assumptions

■ RTRS (pessimistic)

- $T_{\text{sd}} = 0.42$ [days/km]
 - 3 min per stop = 1/3 of design speed!
- $C_{\text{surv}} = 747$ [€/day]
 - (2 per team: design is 1 operator for 4 RTRS)
- $I_{\text{surv}} = 500$ [k€] per RTRS
 - excluding R&D costs
 - no automated marker placement
- $M_{\text{surv}} = 5$ [k€] per year per RTRS
 - assume twice as much as a laser tracker

■ RTRS (optimistic)

- $T_{\text{sd}} = 0.14$ [days/km]
 - 1 min per stop = design speed!
- $C_{\text{surv}} = 93$ [€/day]
 - 1 operator for 4 RTRS
- $I_{\text{surv}} = 500$ [k€] per RTRS
 - excluding R&D costs
 - including automated marker placement
- $M_{\text{surv}} = 2.5$ [k€] per year per RTRS
 - same as laser tracker

■ Classical

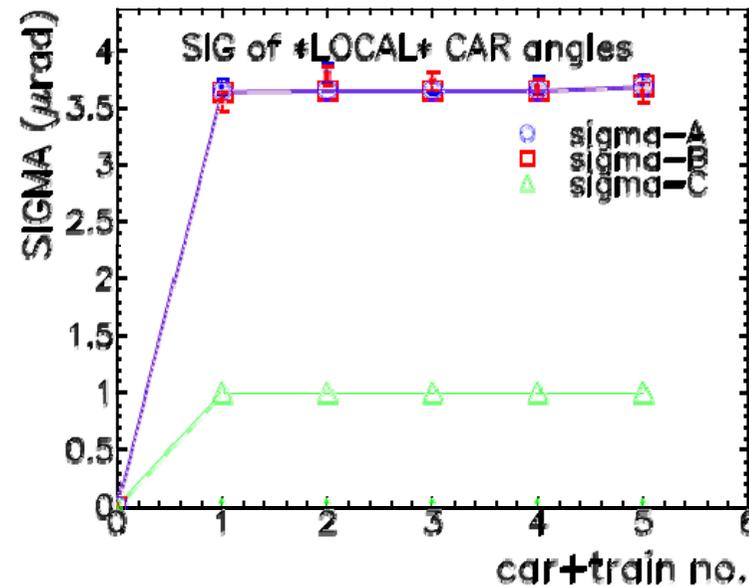
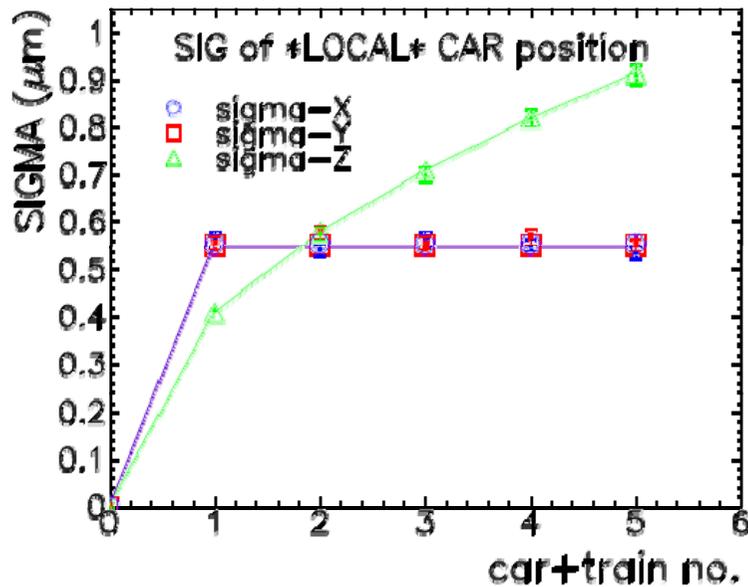
- $T_{\text{sd}} = 5$ [days/km]
 - 1 team of 3 takes that long
- $C_{\text{surv}} = 1120$ [€/day]
 - 3 per team at DESY costs
- $I_{\text{surv}} = 100$ [k€] per tracker
- $M_{\text{surv}} = 2.5$ [k€] per year per tracker

- Cost Comparison (realistic approach, finding minimum in TCO leads to very low down times of a day per year):
 - starting point: 4 RTRS is a **practical** number

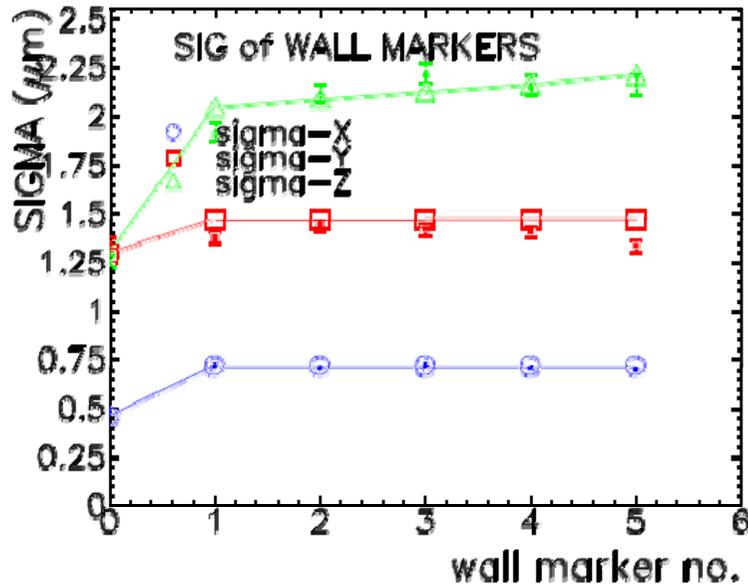
| | RTRS pessimistic | Classical matching downtime of RTRS pessimistic | RTRS optimistic | Classical matching downtime of RTRS optimistic |
|-------------------------------|----------------------------|---|---------------------------|--|
| #of teams | 4 | 47 | 4 | 142 |
| Downtime [days] | 126 | 126 | 42 | 42 |
| TCO with downtime [k€] | 103,520 | 115,841 (120%) | 35,797 | 61,804 (173%) |
| TCO without down time [k€] | 2,776 | 13,770 (496%) | 2,216 | 28,020 (1264%) |

- **Two** independent methods to predict the performance of the RTRS (for details see: Grzelak, Simulation of the LiCAS Survey System for the ILC, IWAA 2006, TH007)
 - Analytical error propagation (old)
 - describe an **opto geometrical model** of the measurement process using SIMULGEO, representing **all statistical errors** across multiple RTRS stops
 - Use **Simulgeo** in **error propagation** mode
 - produces average wall maker errors, no distributions, only **statistical errors**
 - Monte Carlo simulations (new)
 - Simulate **many** measurement **campaigns** of a known tunnel geometry using a custom **ray tracer** (generates measurements with **statistical and systematic errors**)
 - perform full reconstruction of marker positions using **Simulgeo** Model in **reconstruction** mode
 - produces **error distributions**, access to **systematics** and calibrations by varying RTRS geometry parameters between ray-tracer and Simulgeo Model

- Both techniques agree well (only short distance simulated so far)

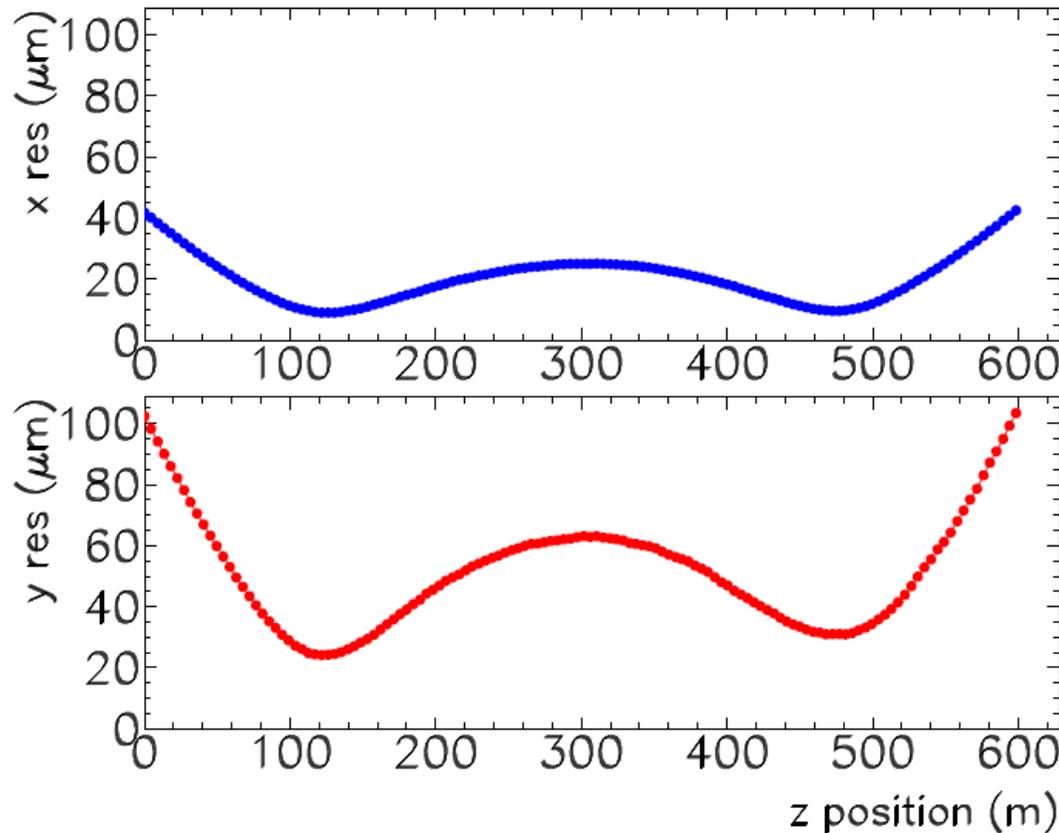


$A = \text{Rot}_X$
 $B = \text{Rot}_Y$
 $C = \text{Rot}_Z$



- assuming intrinsic resolutions:
 - CCD: $\sigma_{\text{CCD}} = 1 \mu\text{m}$
 - FSI: $\sigma_{\text{FSI}} = 1 \mu\text{m}$
- 1000 Simulgeo runs, simplified model, no errors on calib. const. (INT/EXT-FSI, CCD, BS)
- open markers: Matrix calculation (analytic)
- solid markers: Errors from Monte Carlo

■ Long distance results:



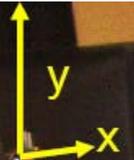
- mean deviation from straight line fits (X, Y) direction
- realistic input to the simulations of beam dynamics

- well below specification: $\sigma_x = 500\mu m$, $\sigma_y = 200\mu m$
- however: only statistical errors included
- precision between $X - Y$ can be swapped by changing the marker location (horizontal to vertical position)

LSM Test Setup

Want to remove 2-DOF from retro reflector beam walk out of the LSM measurements

Laser

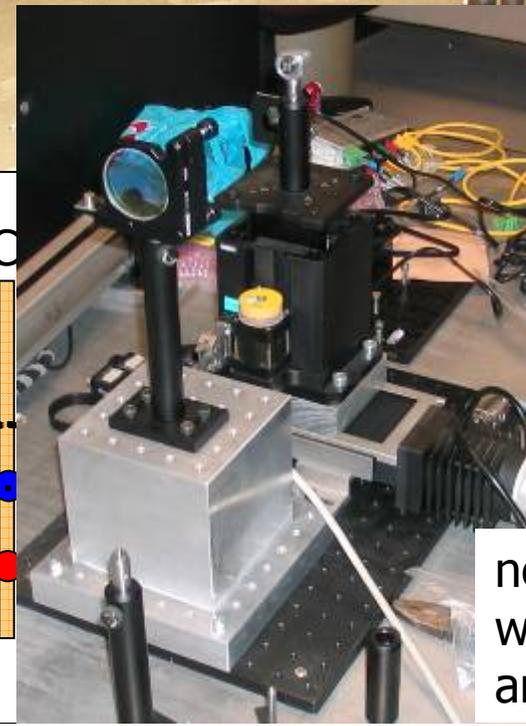
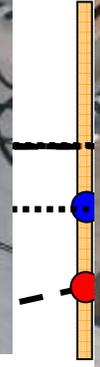


New LSM with improved DAQ and 5th motion stage

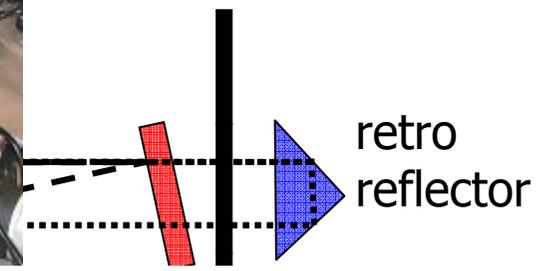
LSM L



CO

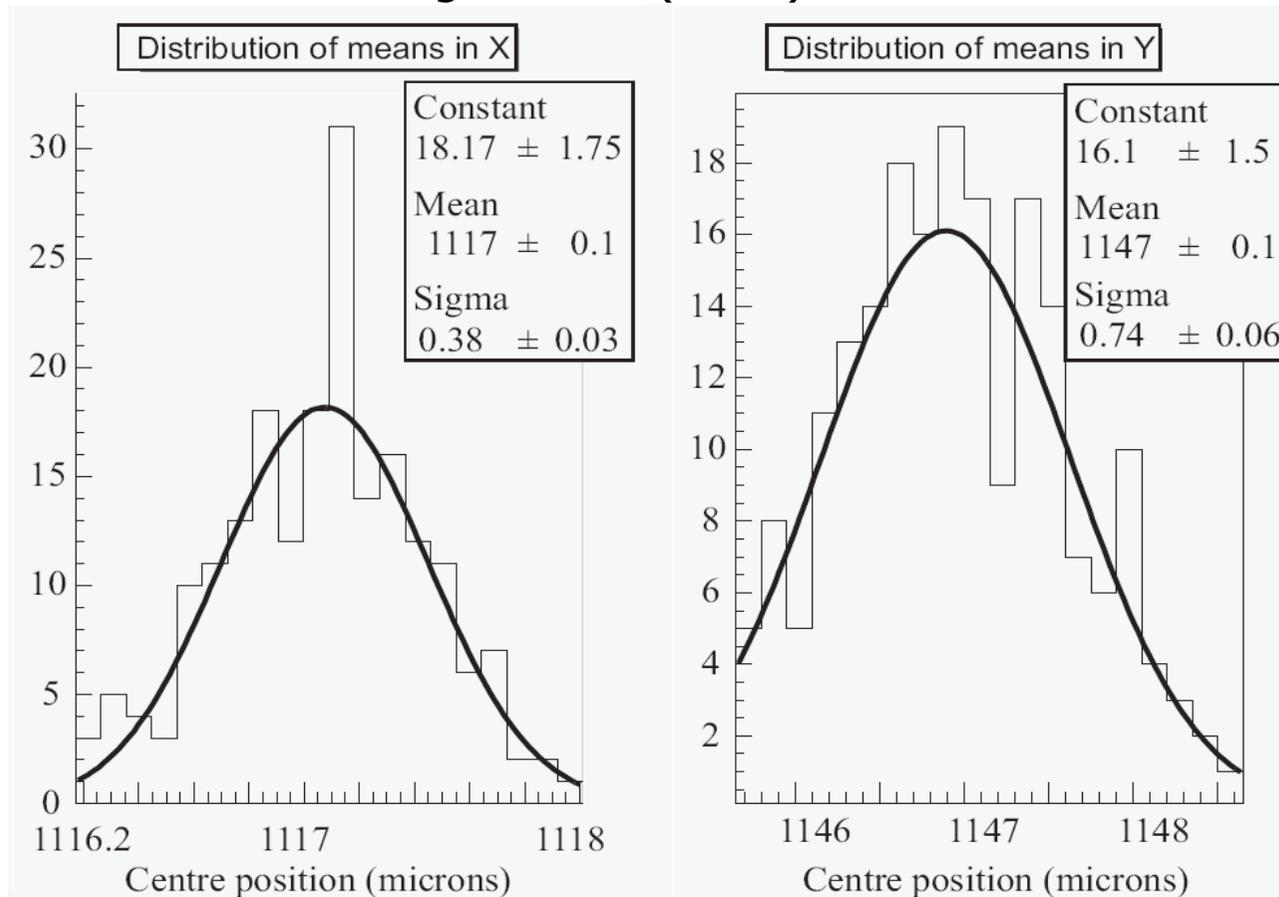


shutter

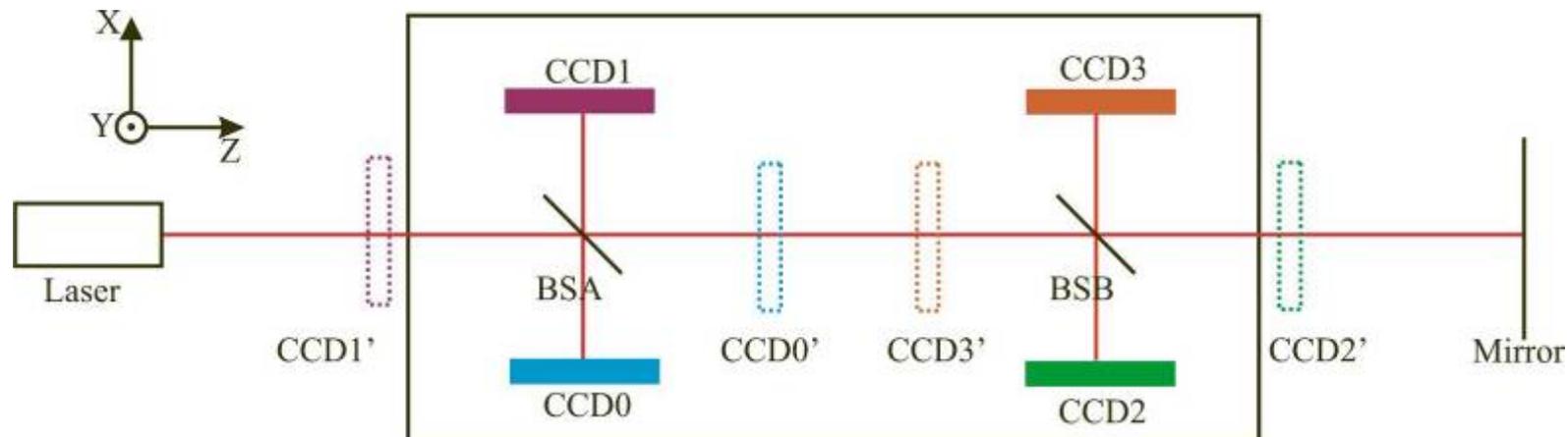


new reflector units with retro reflector and mirror for calibration

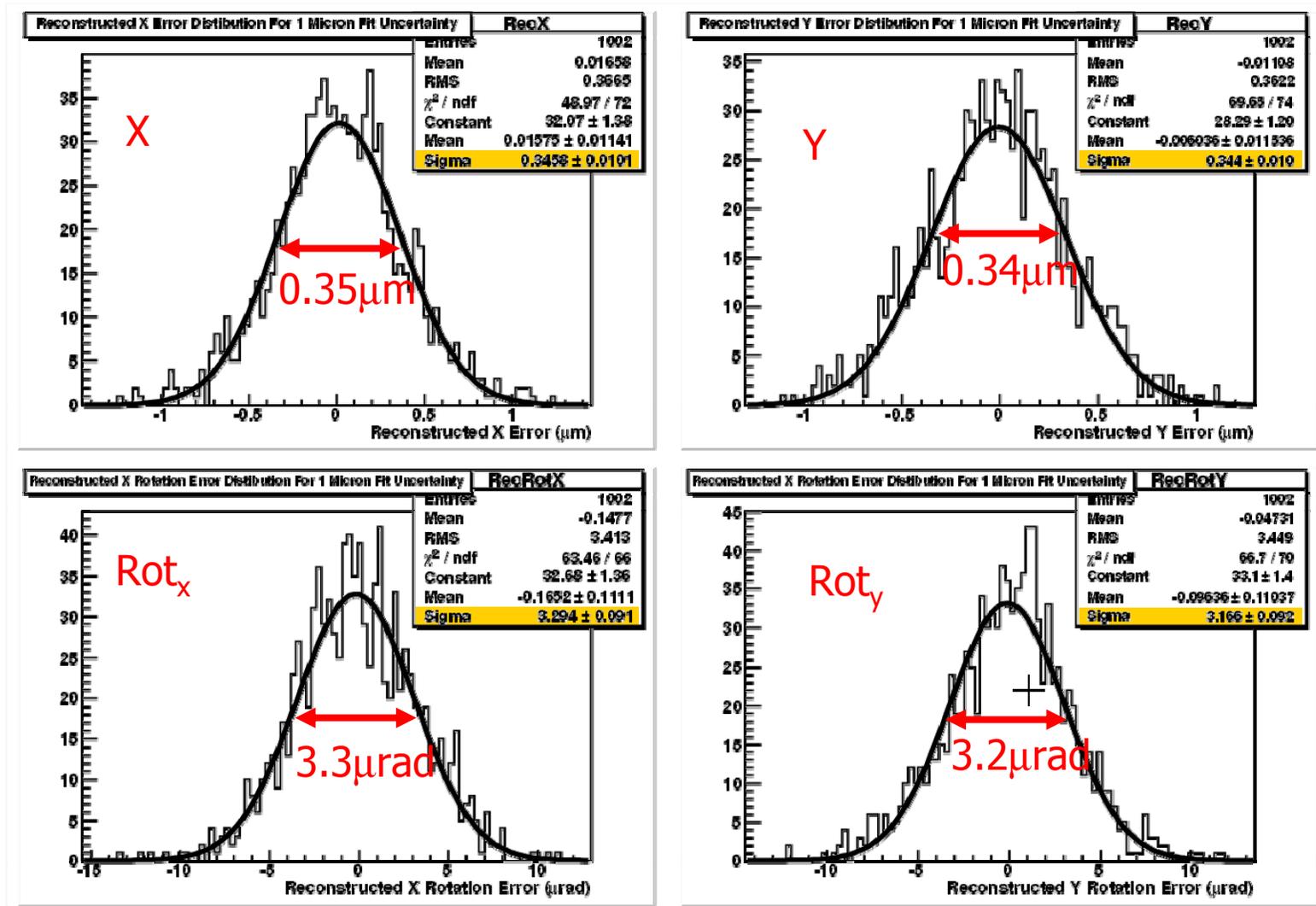
- Spot position fitting in open air (2m)
 - Fourier filtering
 - 2D Gaussian fitting
 - resolutions well below 1 micron
 - most likely limited by refraction effects in current set-up
 - Measurements in a long vacuum (RTRS) will soon be available



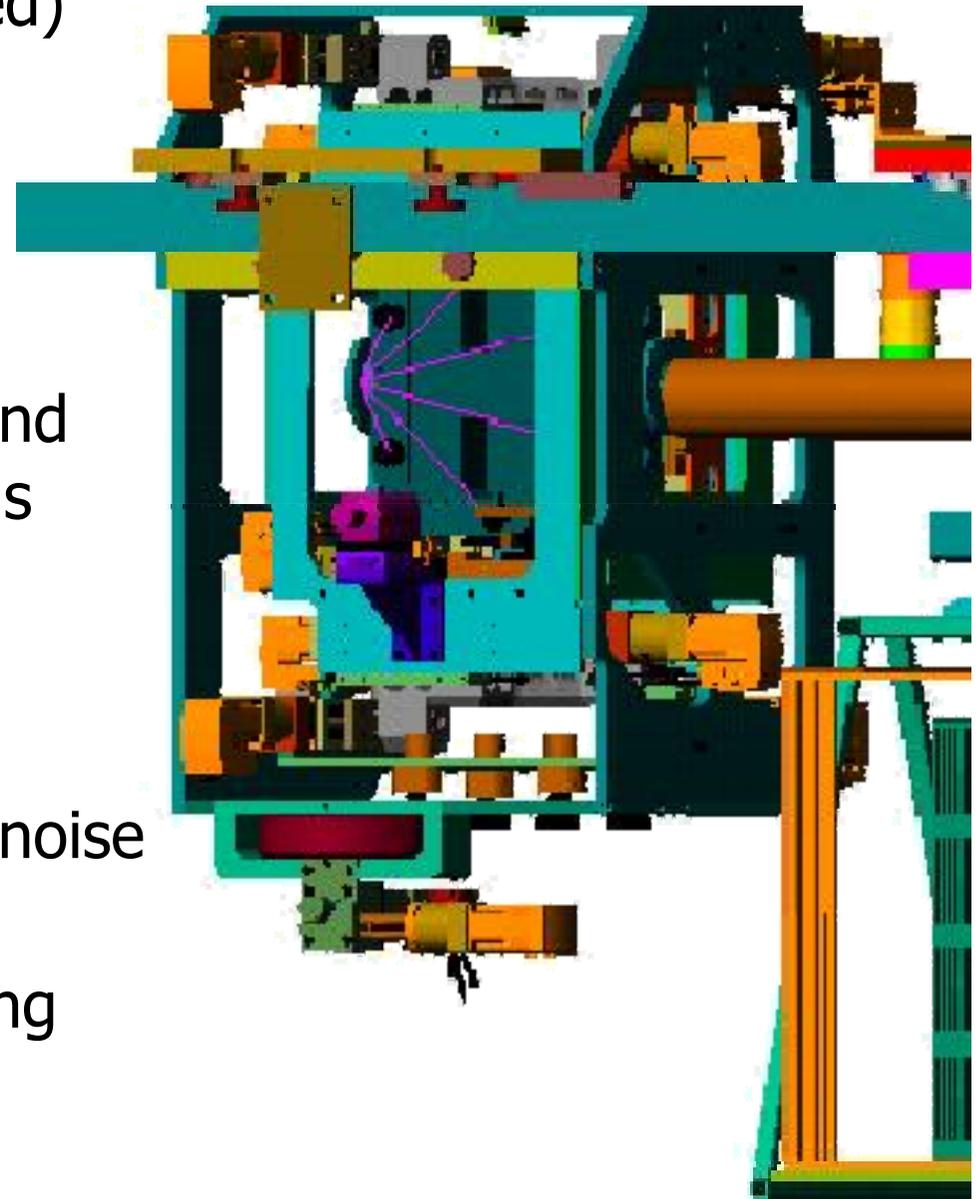
- Reconstruct co-ordinates in LSM frame **using only LSM** readout (independent of SIMULGEO reconstruction)
- **Independent** of non-LSM calibration constants
- Based on linearised model (small angles, small calibration constants, small deviations from symmetry)
- Very **fast** as it is analytical
- Can be used inside motion feedback loops to keep LSM on beam or to find beam
- Used to verify Simulgeo reconstruction code



- Sensitivity study, no calibration errors, only 1 micron spot position errors, fast linearised reconstruction

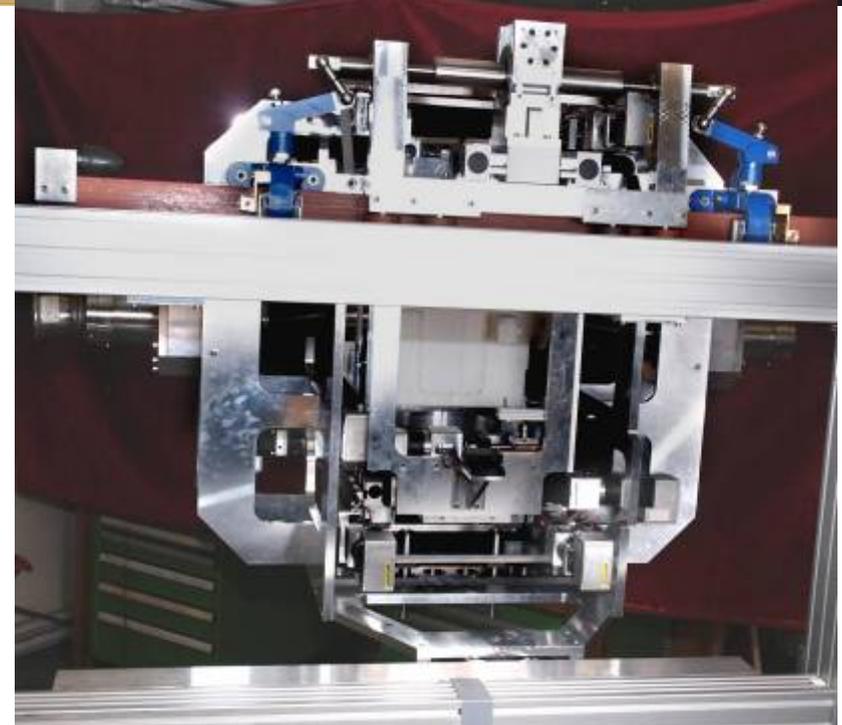
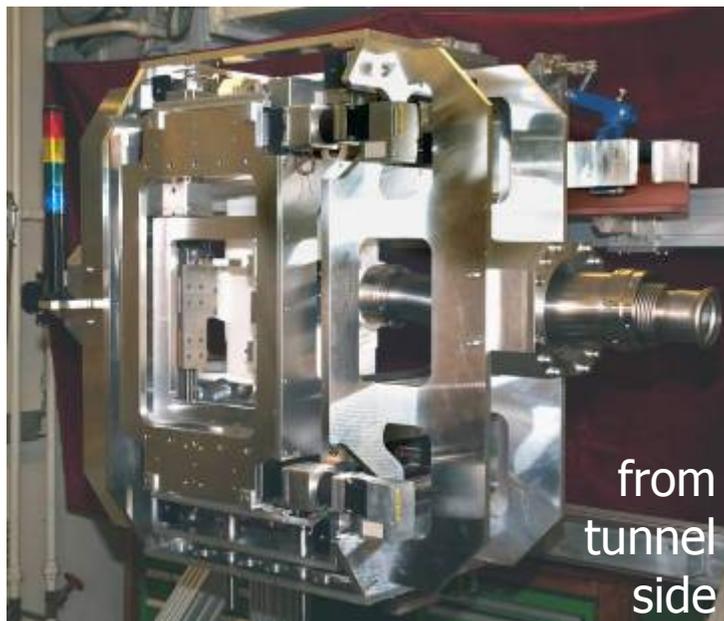
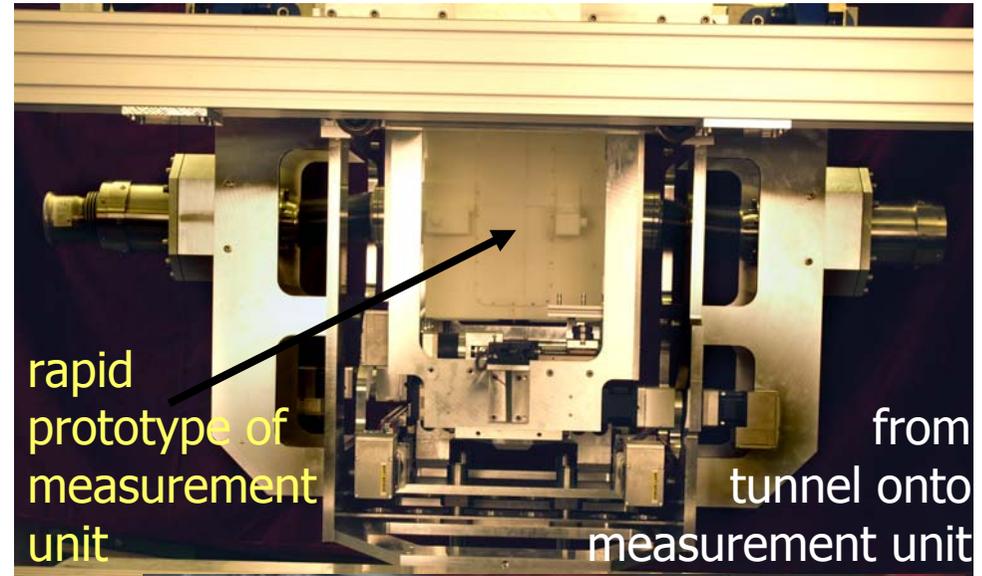
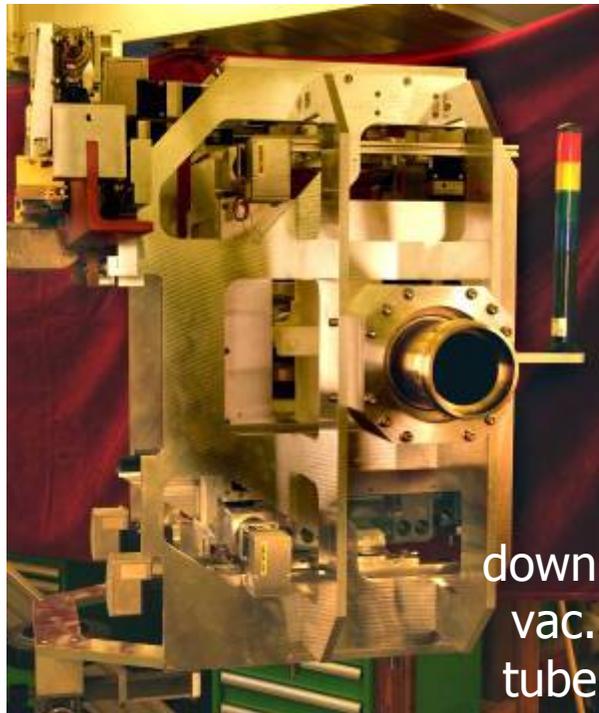


- 3 Units built at DESY (finished)
- 6 DOF for position of measurement unit to:
 - Adjust to wall marker
 - Adjust to neighbouring cars
- Total of 12 stepper motors and stages controlled via CAN-bus
- Extremely rigid frame for:
 - Position repeatability
 - Vibration stability
- Mechanical decoupling from noise in service car
- Clamps to rail while measuring



Measurement Cars

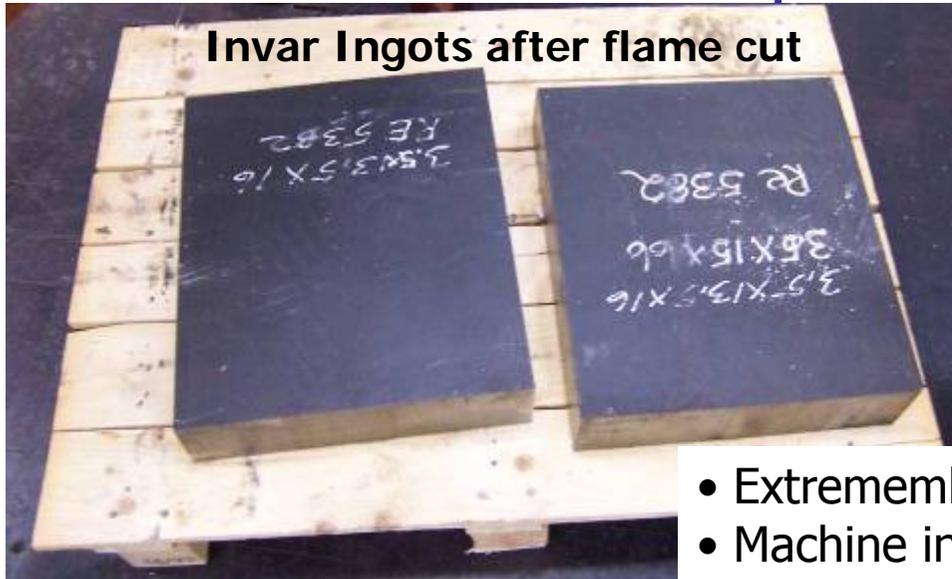
EuroTeV, Armin Reichold



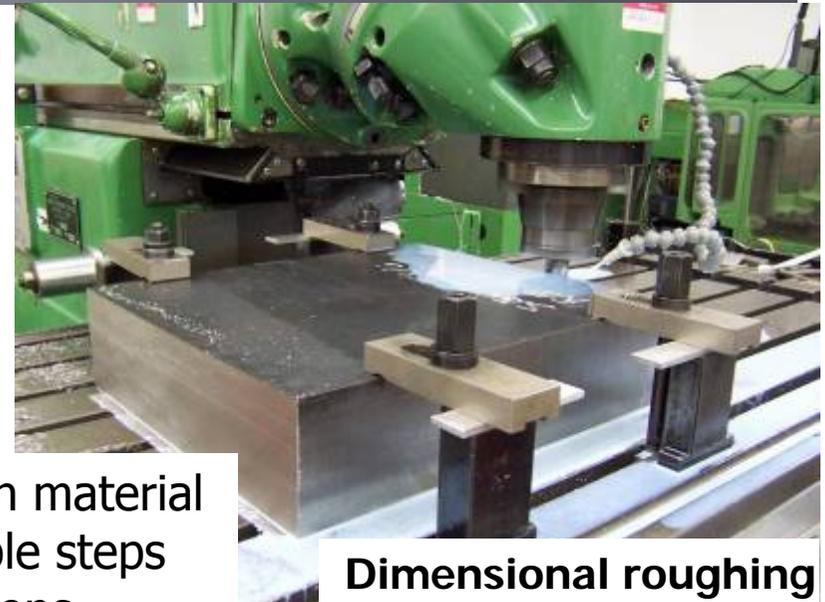
Measurement Unit production

EuroTeV, Armin Reichold

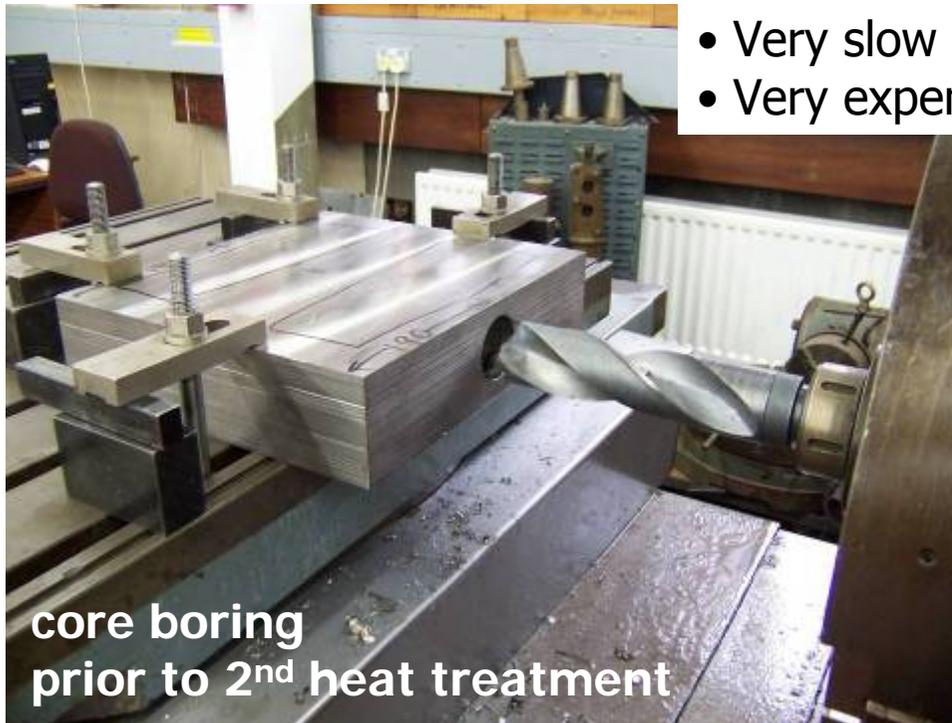
Invar Ingots after flame cut



- Extremely tough material
- Machine in multiple steps to minimise distortions
- Very slow machining speed
- Very expensive tooling



Dimensional roughing



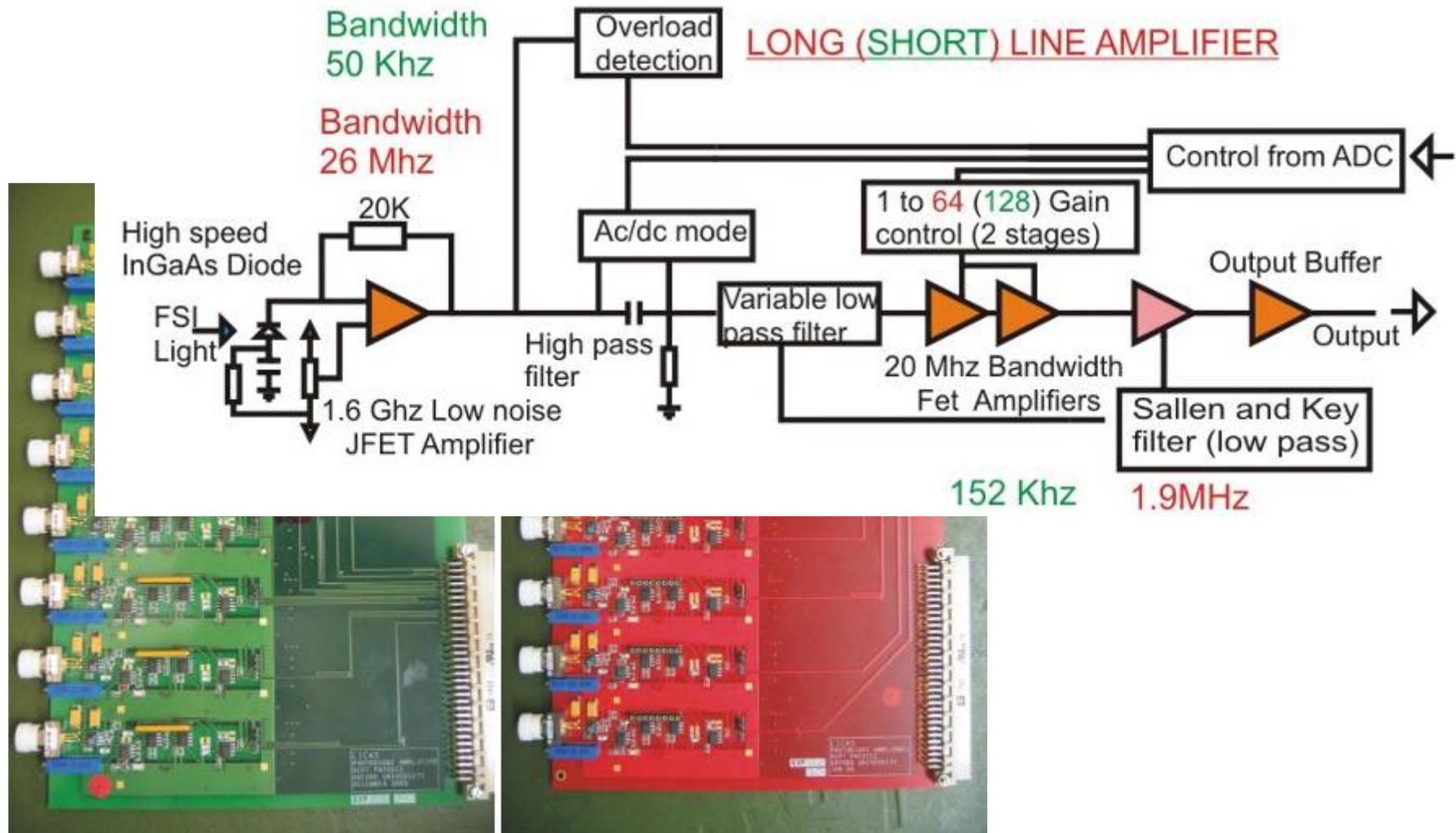
**core boring
prior to 2nd heat treatment**

**Top and bottom
precision
ground 80% of
features
machined**

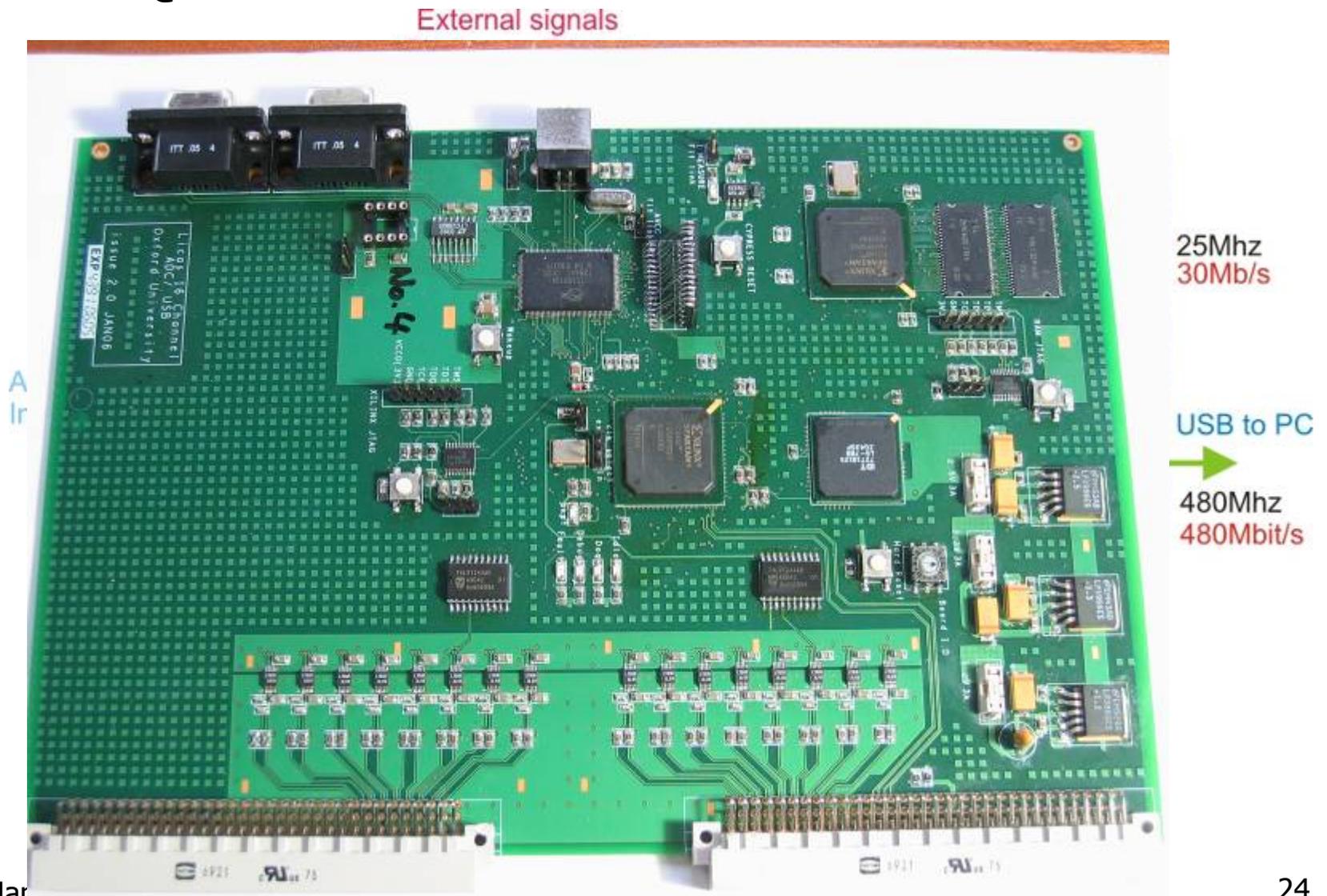


- Drive Control System
- Custom DAQ for FSI
- Commercial DAQ for LSM-CCDs
- ELMBs (Embedded Local Monitoring Boards, ATLAS) via CAN bus for auxiliaries
 - temperature
 - pressure
 - digital I/O (limit switches)
- Trigger and Clock distribution ($\Delta t < 100$ ns)
- Dual CPU, server based control computers
 - 3*service car reading all sensors (Frame grabbers, USB, CAN)
 - 1*master car controlling FSI and LSM laser systems, propulsion and safety and collating data from service cars for reconstruction (CAN, GPIB, RS485)

FSI DAQ: Photo Amplifiers



■ FSI DAQ: USB ADC board

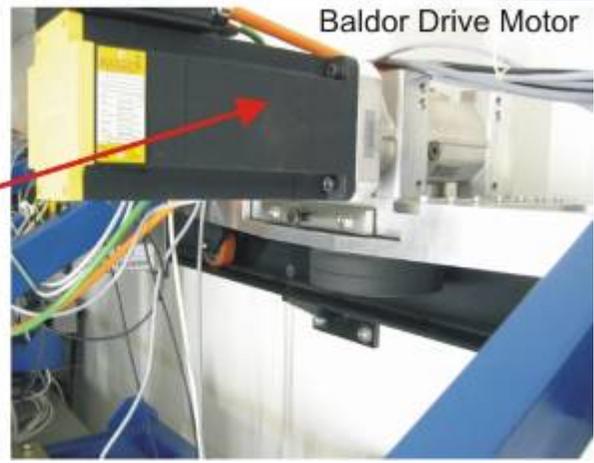
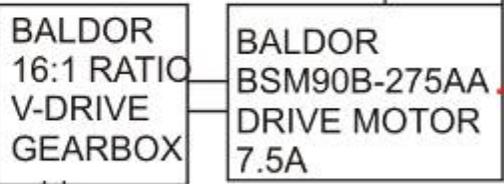
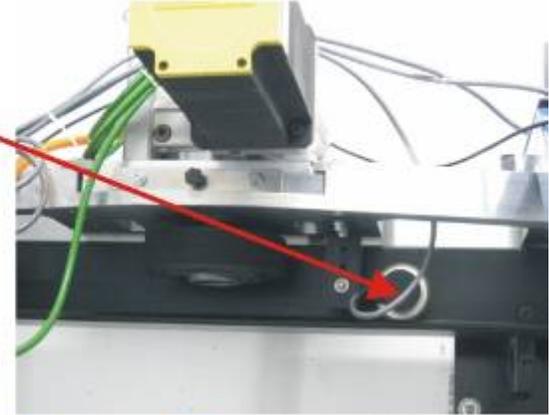
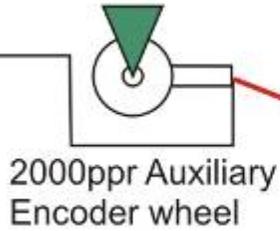
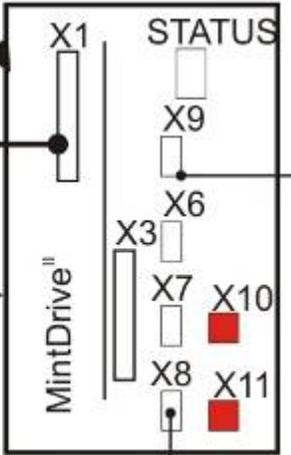




Mintdrive Motor Controller



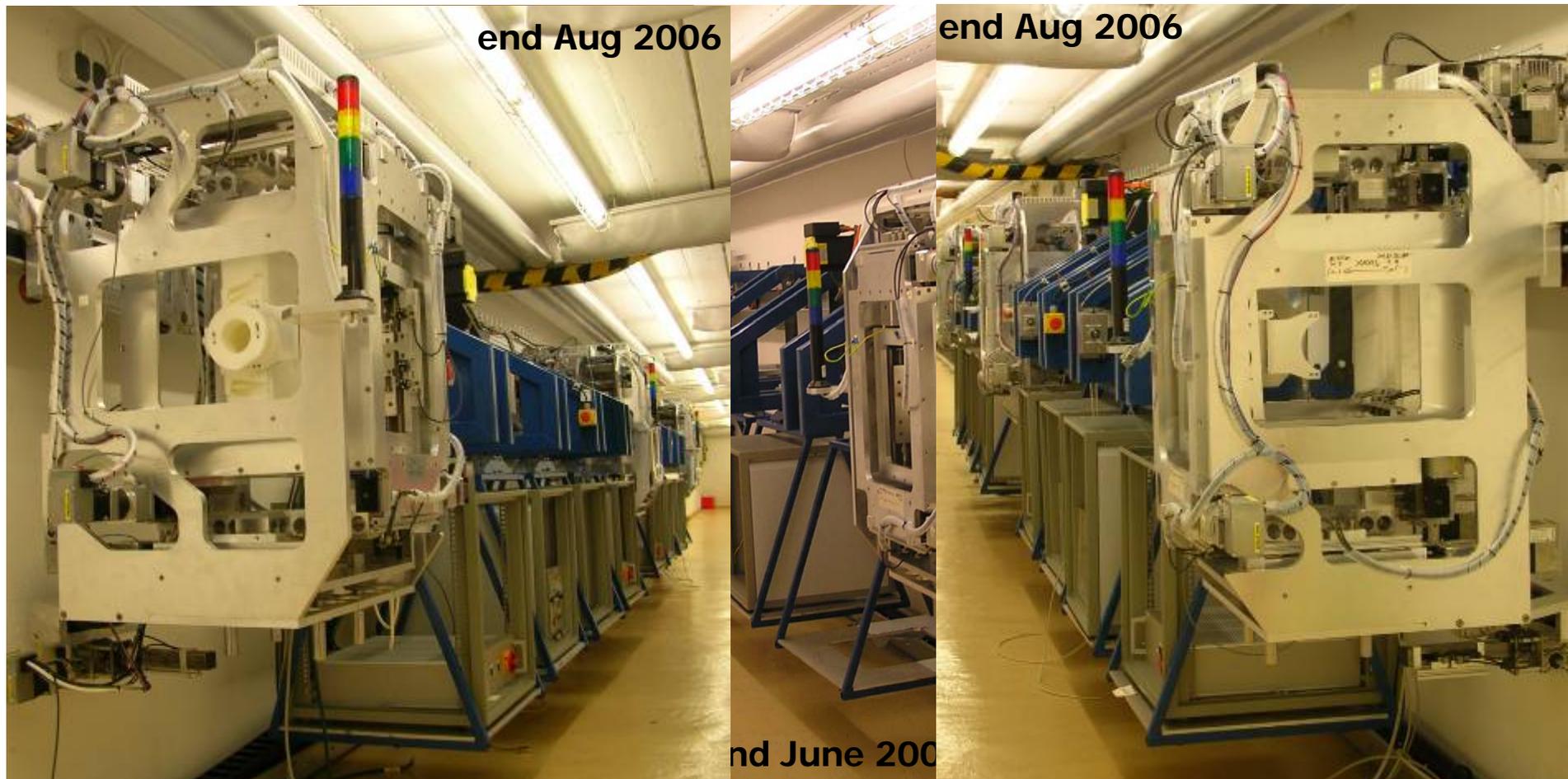
MOTOR CONTROLLER



RTRS Installation at DESY

EuroTeV, Armin Reichold

- Service, measurement and master car joined into one RTRS
- Drive system installed and operational
- Power and interlocks installed
- Motion stage systems in measurement cars operational
- Parking brakes operational
- Vacuum system 95% installed
- Infra structure complete
 - air conditioning
 - interlocks
 - networks
 - rail



- Carefull, now it moves!



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forwards...



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...and backwards!

- A LiCAS RTRS prototype is being built to try and **meet** the survey **requirements** of the ILC
- The LiCAS project is well advanced
 - Have simulated effects of random errors on resolution
 - Are now simulating systematic errors
 - Majority of the RTRS now **installed** at DESY
 - Completion of the invar **measurement units** is the main outstanding construction task
 - Expect improvements to FSI from new reference interferometers
 - Custom **DAQ** system has been built (backup slides)
 - Can **predict** the effect of survey accuracy on **ILC** Linac **performance** (backup slides)
- Calibration and determination of residual systematic errors is the **main goal** of the next year
 - FSI reference length to be traced to **frequency standard**
 - system calibration to be achieved by
 - **as built** measurements using CMM and Smart-Scope
 - **in-situ** consistency fits to monitored differential motion
- Estimates of the reference survey cost strongly favour the RTRS over classical survey methods

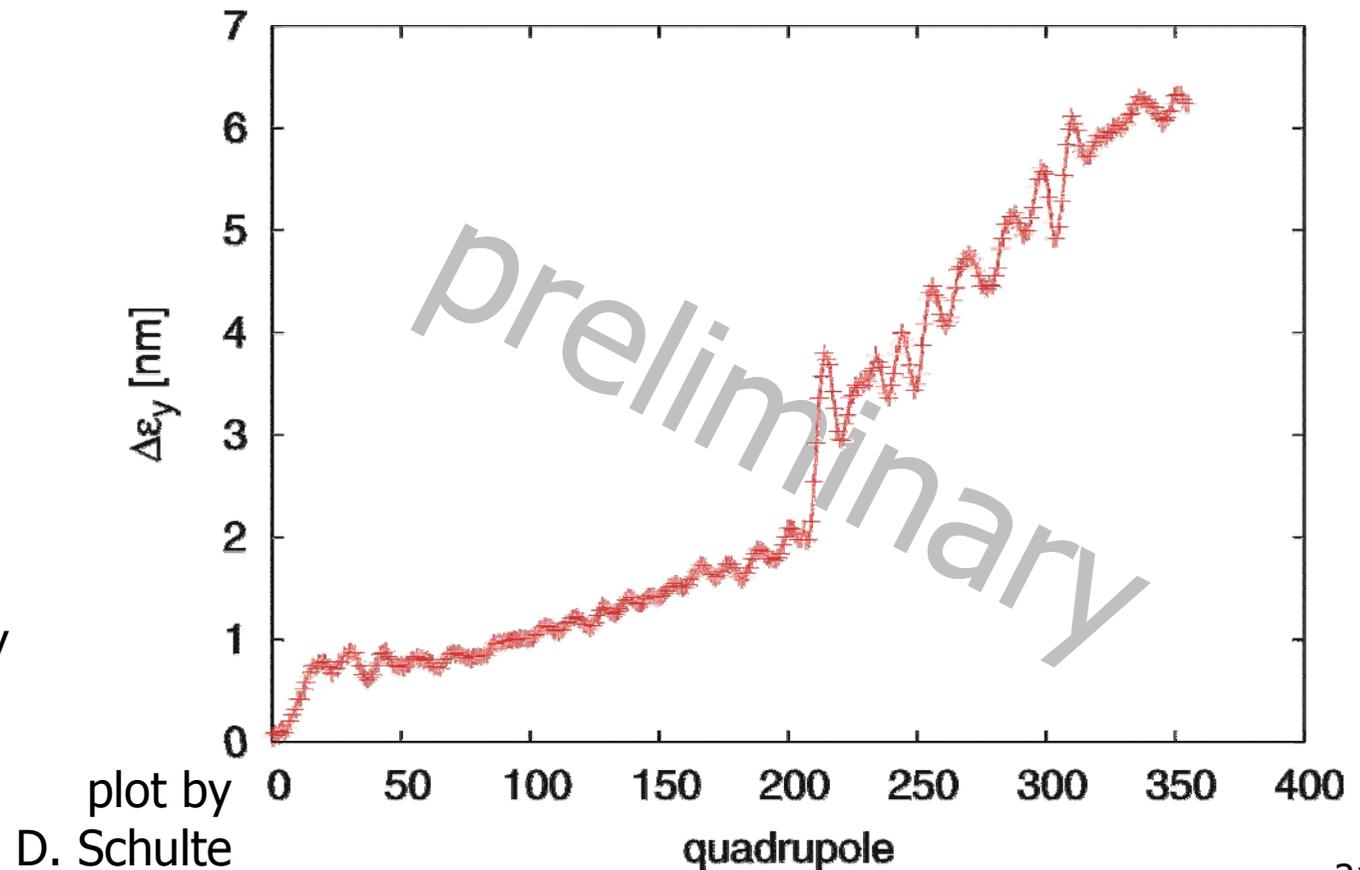
The End

Thank you for your attention

Backup Slides

- Interface from performance simulations to PLACET (RWALK_licas_sim)
- Simulate positions of all accelerator components as expected after LiCAS survey
- Feed this back into PLACET to study emittance growth

- Emittance growth vs. Quadrupole number
- Long range Licas survey errors only
- ongoing study



- Do we need to know the reference interferometer OPD OPD_{ref} on an absolute scale?
 - Yes, because
 - we want to use comparisons with other systems for system calibration
 - we want to be able to maintain the scale over the ILC project life time O(20-30 years)
 - Note: OPD_{ref} is approximately 10m
- How accurately do we need to know L_{ref} ?
 - More accurate than the resolution of the technique (better than 1 μm , say 0.5 μm)
 - Accurate enough to be able to use a single phase measurement at a reference wavelength to fine tune the length, i.e. we know the order number (much better than 1.5 μm , say 0.1 μm)
 - Accurate enough to be able to see creep or drift over reasonably short time scales (say 50 nm)

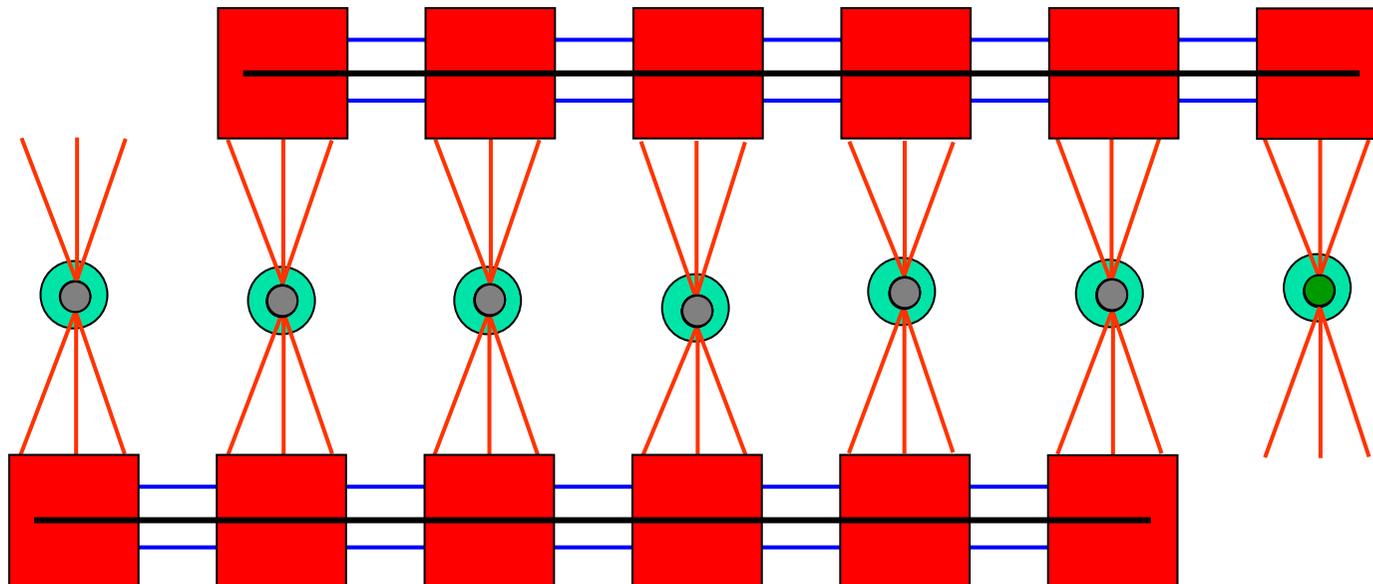
- Saturated acetylene absorption cell (NPL) can define $\Delta\lambda/\lambda$ to $O(10^{-10})$ for **many lines** in the $1.5 \mu\text{m}$ region if scanned slowly
- Build passively stabilised etalon with
 - high finesse of few 10^3 and
 - FSR $\approx O(10)$ GHz and
 - peak(s) close to absorption feature(s)
- At few GHz/s (slow) scan laser linearly through etalon and absorption cell
 - \rightarrow measure FSR to $O(10^{-9})$
- Directly afterwards (within passive stabilisation time) perform fast FSI scan through reference interferometer and etalon simultaneously
 - \rightarrow measure the frequency change $\Delta\nu_{FSI}$ across part of FSI scan to $O(10^{-8})$
- Determine total phase advance $\Delta\Phi_{ref}$ generated by reference interferometer during $\Delta\nu_{FSI}$ by phase extraction methods to $O(10^{-8})$
- From knowledge of $\Delta\nu_{FSI}$ and $\Delta\Phi_{ref}$ obtain OPD_{ref} to $O(\text{few } 10^{-8})$ corresponding to few 0.1 mm .

- If OPD_{ref} is known to $O(0.1 \text{ micron})$
- and comparison to a wavelength standard can be made regular enough for drift not to destroy knowledge of the order number
- then a very short scan (AOM) around any well known single wavelength can reveal the phase and thus OPD_{ref}
- A variety of derivatives of the above method are possible
- We are looking for advice on this.

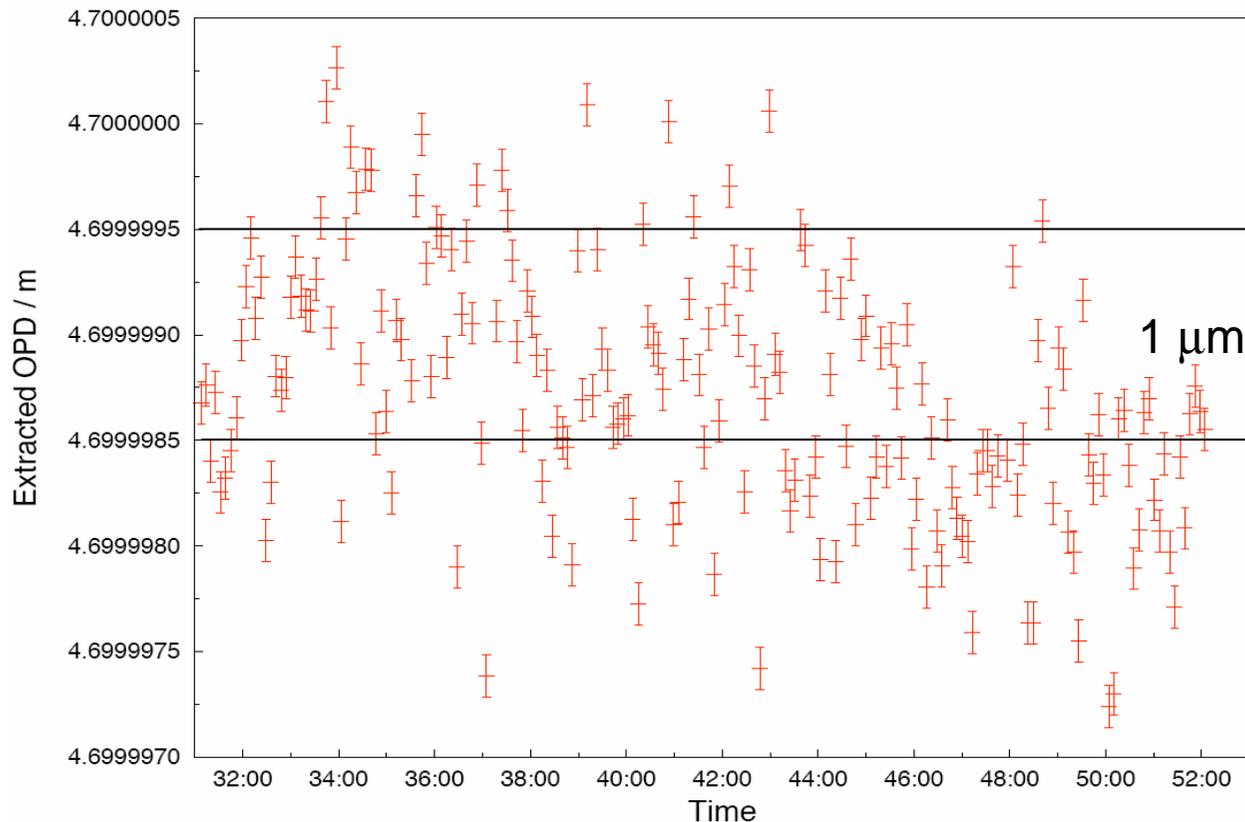
- Reconstruction of wall marker positions depends on the geometry of the measurement units
- This problem partially factorises into
 1. geometry of LSM to get
 - unit's transverse offsets and
 - transverse angles (pitch, yaw) wrt. LSM beam
 2. geometry of internal FSI system to get
 - distance between units and
 - relative transverse angles
 - shared problem between two units, one for launch other for reflectors
 3. geometry of external FSI system to
 - measure 3D co-ordinates of wall markers wrt. unit's external FSI system
 4. orientation of tilt sensors to determine roll
 5. relative co-ordinates of the 4 sub-systems

- As built measurements:
 - perform highly accurate CNC production to reduce size of calibration constants to $O(10 \mu\text{m})$
 - verify built at all stages with CMM and Smart-Scope (for CCD location) to obtain approximately $5 \mu\text{m}$ 3D co-ordinates to final assembly
 - sub-assemblies (i.e. cameras with holders, pellicle holders, etc.) are measured before and after insertion to unit

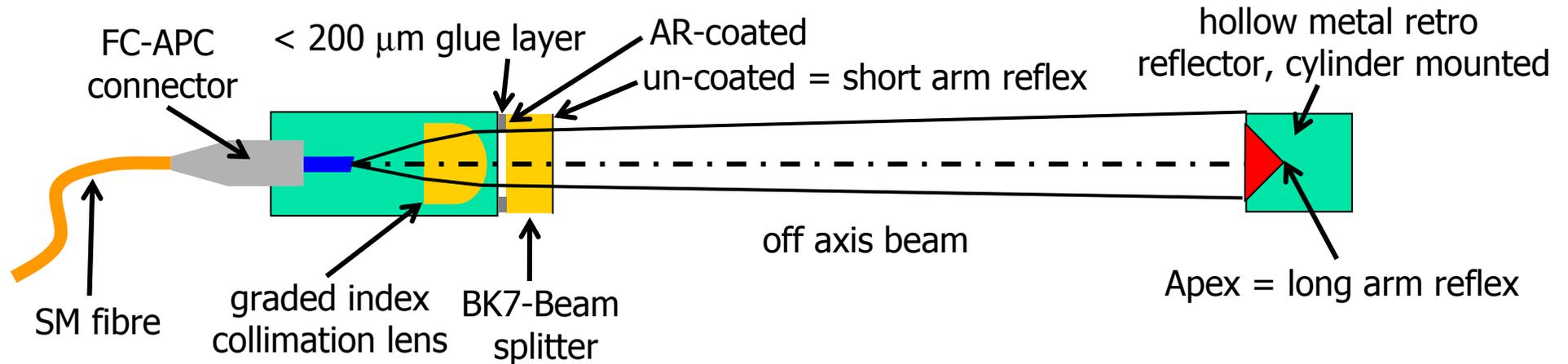
- In-situ geometry calibration:
 - fully assemble RTRS to operational state
 - during one measurement stop (all elements inside dynamic range, all measurements active)
 - move one measurement unit in many steps across its dynamic range keeping roll close to zero of tilt sensor
 - monitor differential 6D motion with as many laser trackers (maybe 3D-arm, slow?) as possible
 - reconstruct the motion using the RTRS assuming
 - wall markers do not move
 - two other cars do not move
 - vary the calibration constants of each subsystem until the reconstructed moves fit best to the monitored ones
 - this can give entire relative geometry of LSM
 - and entire external FSI system relative geometry
 - and partial relative geometry of the internal FSI system
 - repeat the above for all units
 - change units into all possible different locations and repeat again
 - rotate units by 180 degrees in pitch and repeat again



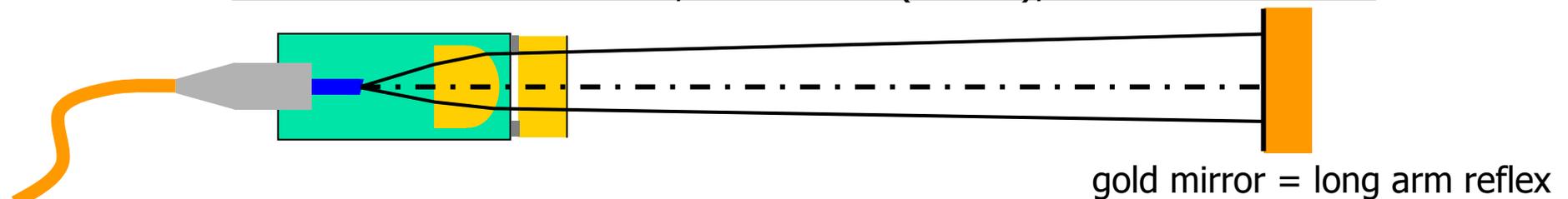
- Using **old** Michelson style **reference interferometer**
- Passive thermal shield, operates in air, no expansion compensation, steel table
- Expect large improvements from new ref. & evac measurement interferometer
- OPD measured over **25 min**
- No offline corrections for thermal expansion
- OPD = $4.6999989 \pm \underline{5.94 \times 10^{-7} \text{ m}}$



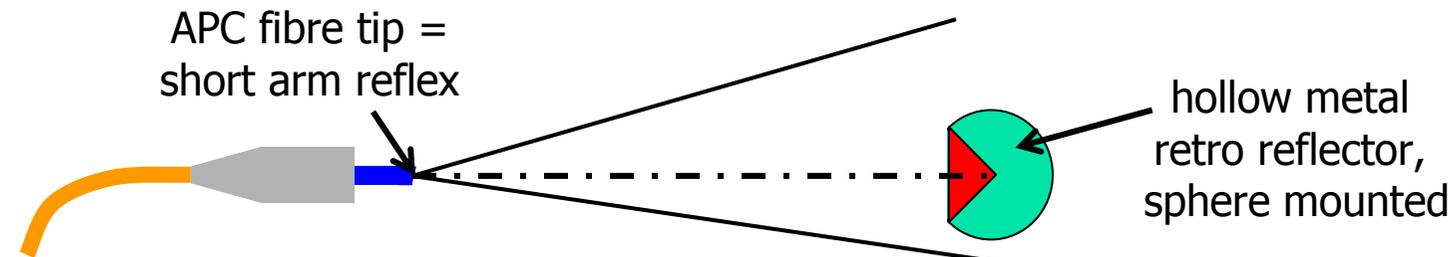
Long line measurement interferometer, OPD \approx 5m, surface to point



Reference interferometer, OPD=10m (folded), surface to surface

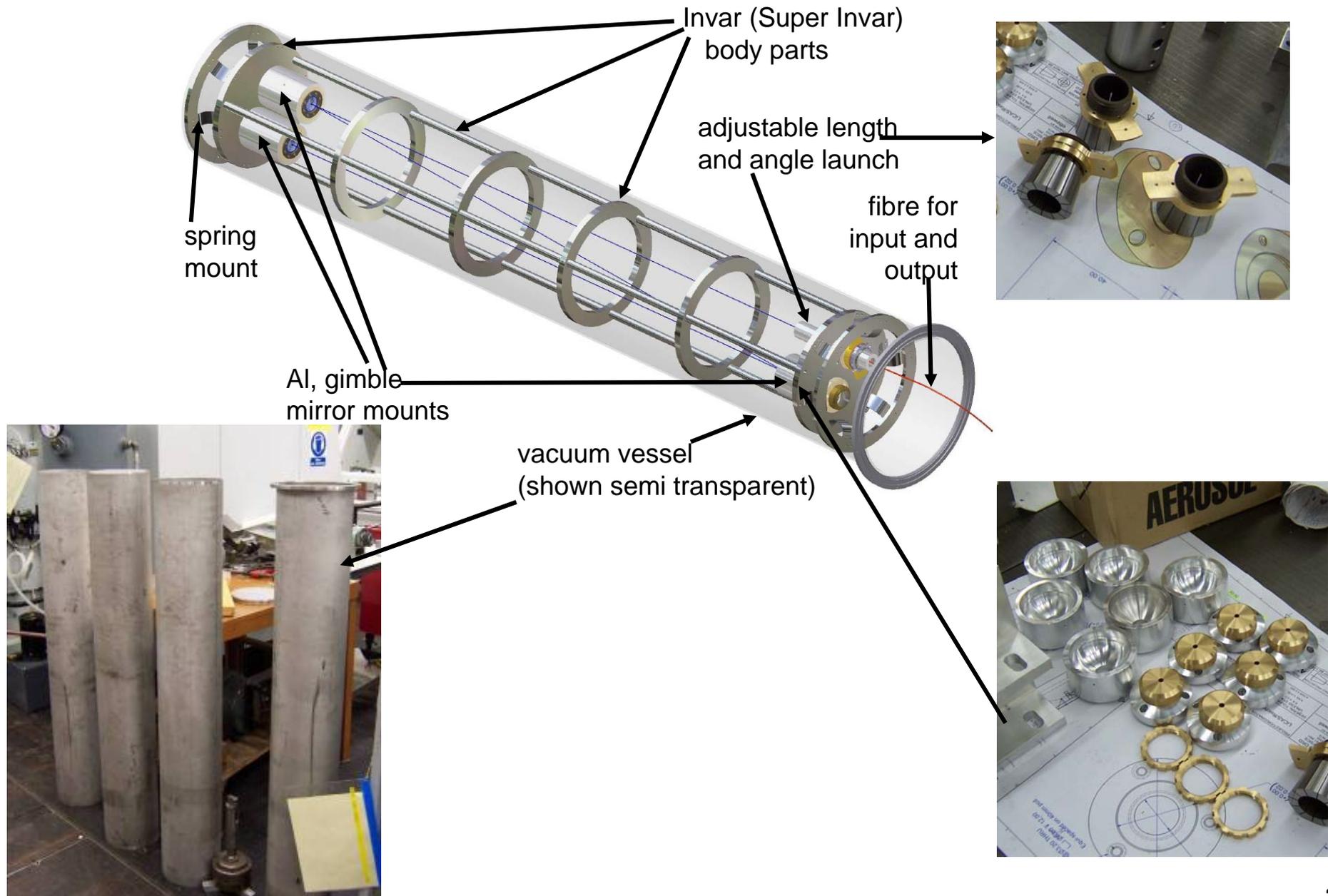


Short line measurement interferometer, OPD \approx 0.5m, point to point



Reference Interferometers

EuroTeV, Armin Reichold



Daresbury, 6 Jan 2007

- Oxford drive tests on 25m rail test stand
- 3 service + 1 master car + 3 "dummy" measurement cars as loading
- Developed torque synchronisation software
- Three schemes tested
- Finishing touches to be done when operational at DESY



- Cost Comparison (brute force cost minimisation):
 - starting point: find minimum of TCO with downtime

| | RTRS pessimistic, min TCO (with down time cost) | Classical matching downtime of RTRS pessimistic | Classical min TCO (with down time cost) | RTRS optimistic, min TCO (with down time cost) | Classical matching downtime of RTRS optimistic | Classical min TCO (with down time cost) |
|-------------------------------|--|--|---|---|--|---|
| #of teams | 26 | 308 | 179 | 16 | 522 | 179 |
| Downtime [days] | 19 | 19 | 34 | 11 | 11 | 34 |
| TCO with downtime [k€] | 41,375 | 68,496 (166%) | 60,371 (146%) | 17,211 | 94,210 (547%) | 60,371 (351%) |
| TCO without down time [k€] | 15,976 | 52,920 (331%) | 33,570 (210%) | 8,816 | 85,020 (964%) | 33,570 (381%) |

- Downtime **too low** (<parasitically available downtime)