

# ***ILC DR Vacuum System***

***Progress in ELOUD Task (Goal 7) for the ILC DR***

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## Required vacuum

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- The need to avoid fast ion instability leads to very demanding specifications for the vacuum in the electron damping ring [Lanfa Wang, private communication]:
  - $< 0.5$  nTorr CO in the arc cell,
  - $< 2$  nTorr CO in the wiggler cell and
  - $< 0.1$  nTorr CO in the straight section
- In the positron damping ring required vacuum level was not specified and assumed as 1 nTorr (common figure for storage rings)

## Sources of Gas in a Vacuum System

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- Thermal stimulated desorption
  - The thermal desorption rate for stainless steel, well-known as a good vacuum material, can be reduced to the level of  $10^{-12}$  Torr-l/(s-cm<sup>2</sup>) for CO after 24 hrs bake-out at 300°C and weeks of pumping.
- Photon stimulated desorption
  - Depends on many parameters as
    - Choice of material and cleaning procedure
    - Bakeout temperature and duration
    - Photon/electron/ion intensity flux, energy and integral dose.

## Sources of Gas in a Vacuum System

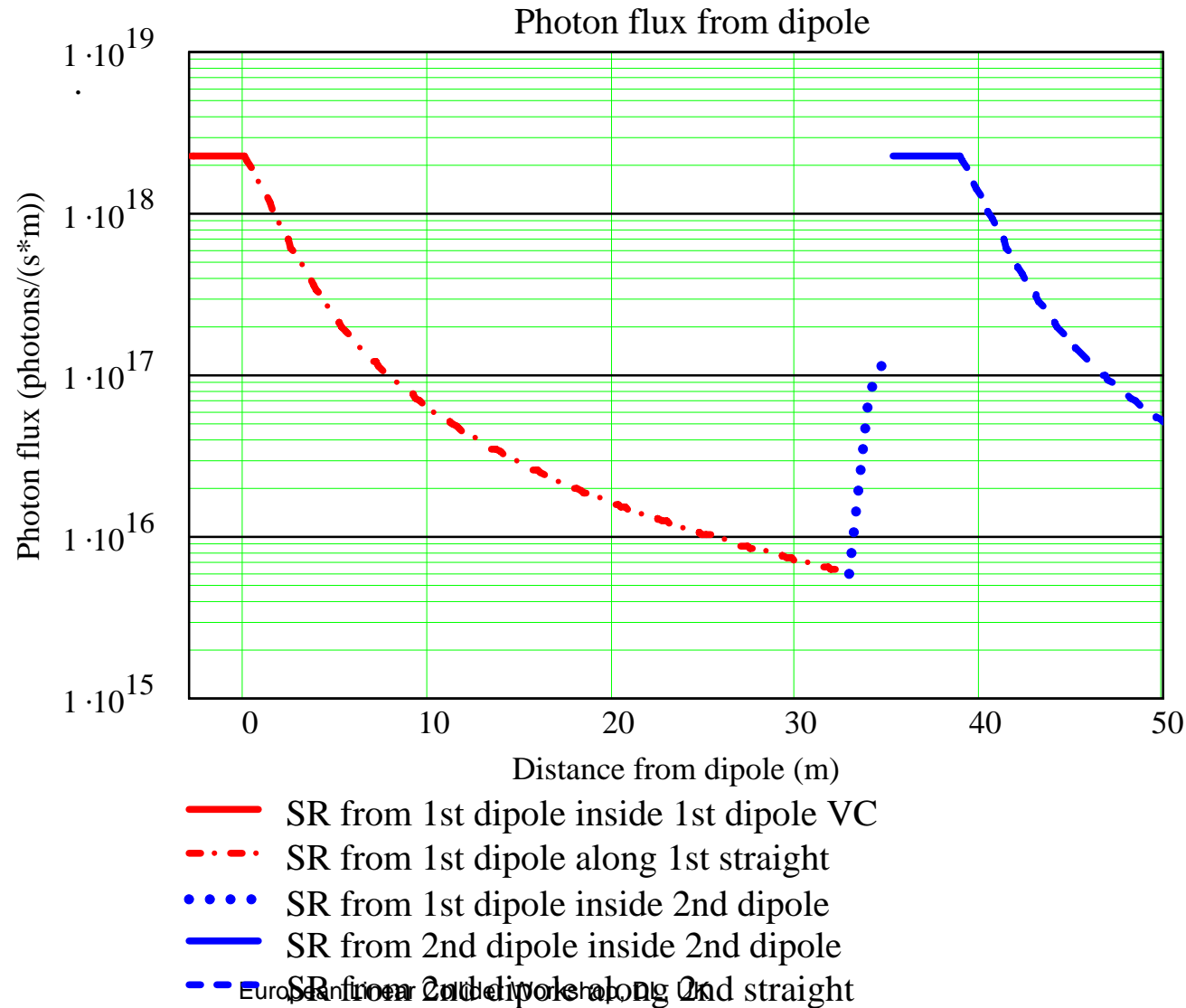
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- **Photon stimulated desorption**
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    - Choice of material and cleaning procedure
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- **Electron and ion stimulated desorption**
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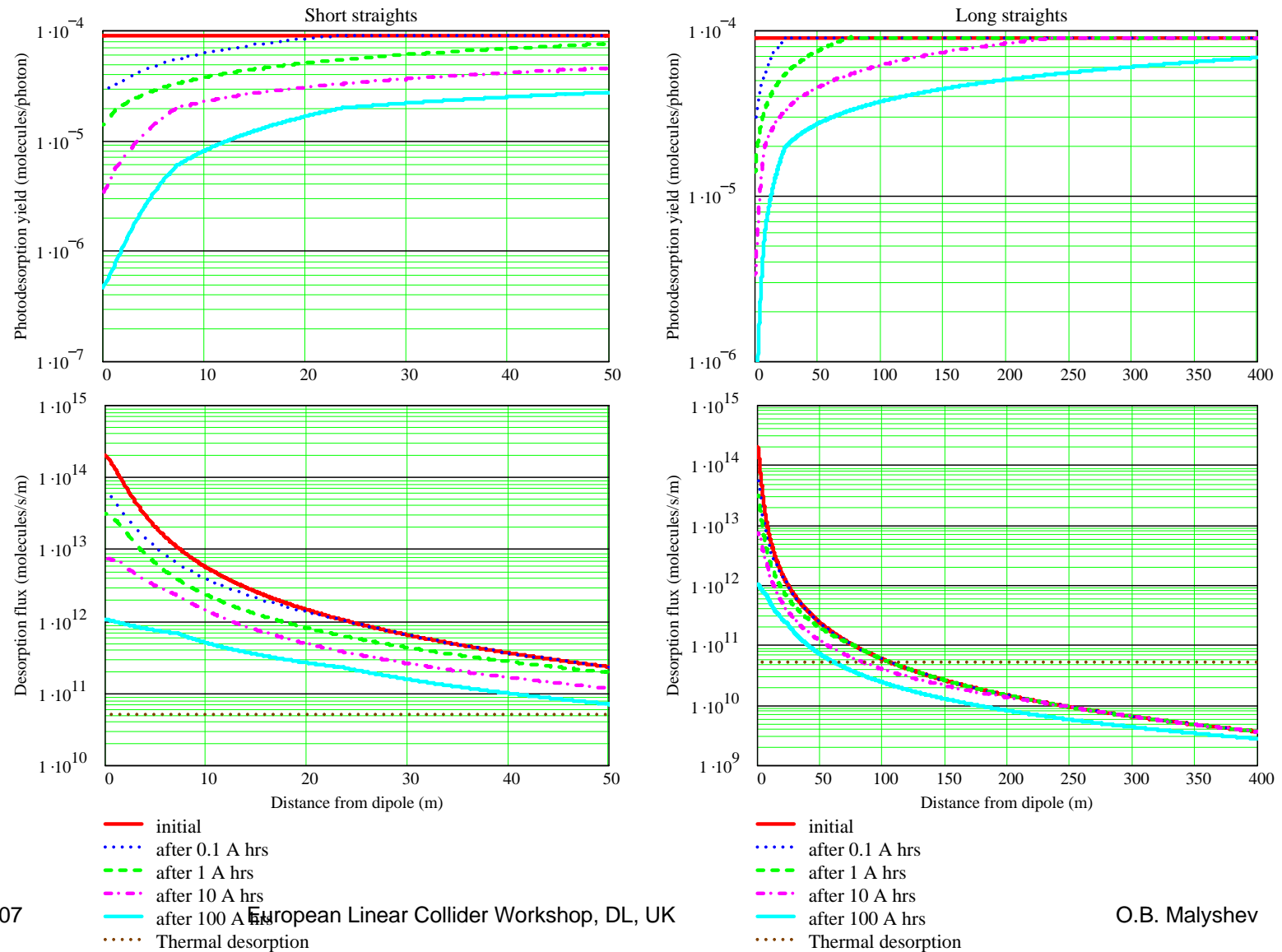
## DR & Beam Parameters

	Arc cell	Wiggler cell	Straight section
Number of dipole/wiggler cells per beamline (ring)	120	40	—
Sectorisation	12 x 5 x 2	5 x 4 x 2	2 x 404.6 m + + 110 x 32.9 m + + 10 x 58.7 m + + 16 x 43.8 m
Total arc/wiggler cell length	38.9 m – most of (58.8 m x 10 times)	6.3 m (5 wigglers in row)	1775 m
Dipole/wiggler length (pole face – pole face)	6 m	2.45 m	—
Dipole field /Wiggler peak field	0.1455 T	1.58 T	—
Dipole bend angle	$2\pi/120$	—	—
Electron beam energy	5 GeV		
Electron beam average current	0.400 A		
Chamber vertical full aperture	50 mm	46 mm	50 mm
Chamber horizontal aperture	50 mm	120 mm	50 mm
Required residual gas pressure after 100 Ahr beam conditioning	< 0.5 ntorr CO	< 2 ntorr CO	< 0.1 ntorr CO
Photon critical energy	2.4 keV	26 keV	2.4 keV after arc or 26 keV after wiggler
Photon flux (maximum)	$2.23 \cdot 10^{18}$ photons/(m·s)	$2.43 \cdot 10^{19}$ photons/(m·s)	From 0 to $2.43 \cdot 10^{19}$ photons/(m·s)

## Photon flux onto the 50-mm diameter vacuum chamber walls inside the dipoles and along the short straights

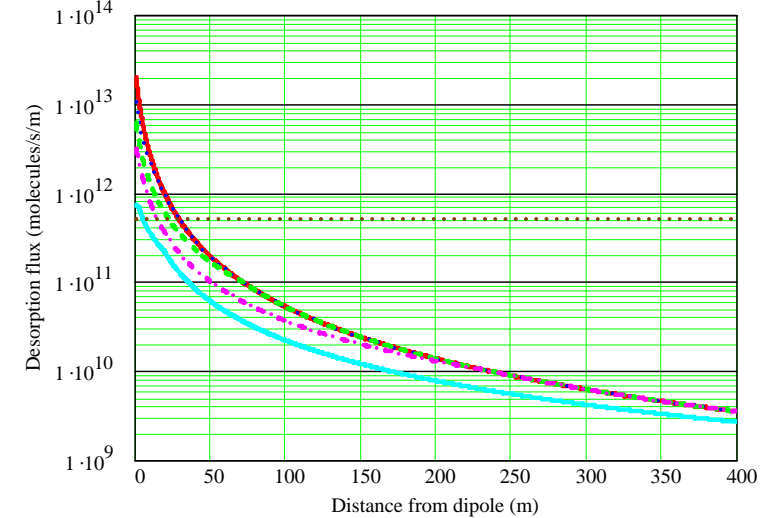
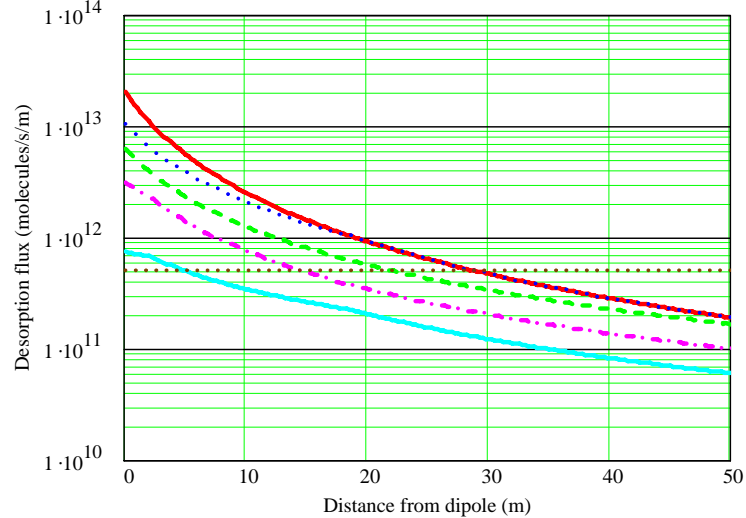
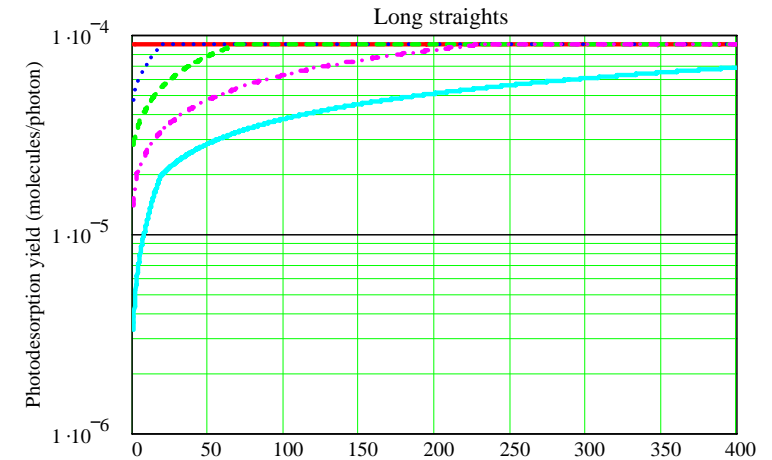
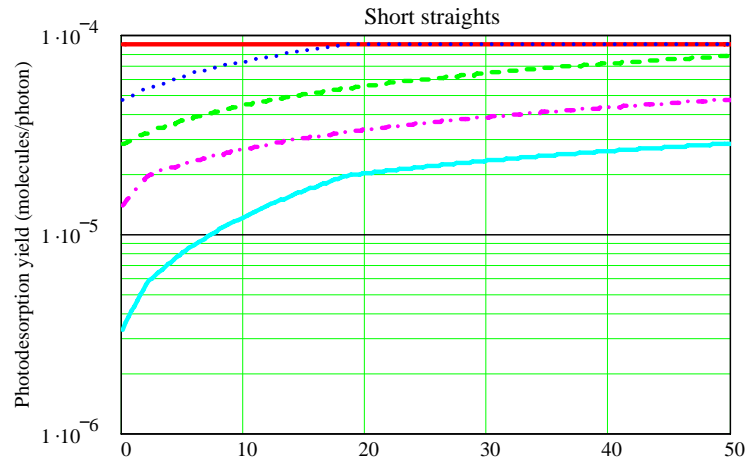
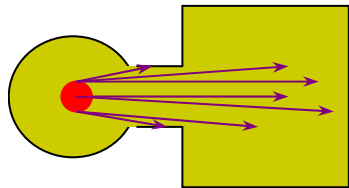


## Photodesorption yield and flux along the damping ring straights made of stainless steel *tubular vacuum chamber* and baked in-situ at 300°C for 24 hrs.



# Photodesorption yield and flux along a stainless steel vacuum chamber with an ante-chamber in the damping ring straights baked in-situ at 300°C for 24 hrs.

10% of photons hit vacuum chamber



- initial
- after 0.1 A hrs
- - - after 1 A hrs
- · - after 10 A hrs
- after 100 A hrs
- Thermal desorption

- initial
- after 0.1 A hrs
- - - after 1 A hrs
- · - after 10 A hrs
- after 100 A hrs
- Thermal desorption



# Tubular chamber vs a vacuum chamber with antechamber

- **Assumption:**
  - 90% of photons are absorbed by SR absorbers and
  - 10% of photons are distributed along the beam vacuum chamber, a gas load analysis can be performed.
- **Results:**
  - The distributed gas desorption due to 10% of photons is after 100 Ahr of beam conditioning the distributed photon stimulated desorption due to 10% of photons is the same for both designs: with and without antechamber.
  - Meanwhile, in addition to photon stimulated desorption from the chamber there is thermal outgassing (10 times larger with an ante-chamber) and photon stimulated desorption from the lumped absorber.
  - Therefore the total outgassing inside the vacuum chamber with an antechamber is larger. Hence, one can conclude that the thermal outgassing will be reduced much faster in a tubular vacuum chamber conditioned with photons than in a vacuum chamber with an ante-chamber.
- **Therefore, the ante-chamber design:**
  - does indeed increase the vacuum conductance,
  - but this does not help in reducing the outgassing.
  - After 100 Ahr of beam conditioning the total outgassing along a tubular vacuum chamber is the same or lower than that along a vacuum chamber with an antechamber, and the SR absorbers make a gas load on the pumps even larger for an antechamber design.
  - Since the antechamber design is more expensive, it worth to explore only if it is necessary to deal with other problems such as beam induced electron multipacting and electron cloud.

## TiZrV NEG coating for accelerator vacuum chambers

- A new vacuum technology for accelerators developed at CERN in recent years [i], is the use of TiZrV (NEG) coating for all inner surfaces of the vacuum chamber.
- TiZrV films have been intensively studied by vacuum groups in many different laboratories [ii].
- TiZrV coated vacuum chambers:
  - are already used in accelerators:
    - for six years at the ESRF [iii] and
    - for 4 years at ELETTRA [iv];
  - many others are just beginning (RHIC, Soleil, Diamond) or will use them in future.

[i] C. Benvenuti. Non-Evaporable Getters : from Pumping Strips to Thin Film Coatings. EPAC '98 , Stockholm, Sweden , 22 - 26 Jun 1998, pp. 200-204.

[ii] 45th IUVESTA Workshop on NEG coatings for particle accelerators and vacuum systems. 5-8 April 2006. Catania, Italy. [www.iuvsta.org](http://www.iuvsta.org).

[iii] M. Hahn and R. Kersevan. Status of NEG coating at ESRF. Proc. of 2005 Particle Accelerator Conference, Knoxville, Tennessee, pp. 422-424.

[iv] F. Mazzolini, L. Rumiz, J. Miertusova, F. Pradal. Ten years of ELETTRA vacuum system experience. Vacuum 73 (2004) 225–229.

[v] V.V. Anashin, I.R. Collins, R.V. Dostovalov, N.V. Fedorov, A.A. Krasnov, O.B. Malyshev and V.L. Ruzinov. Comparative study of photodesorption from TiZrV coated and uncoated stainless steel vacuum chambers. Vacuum 75 (2), July 2004, pp. 155-159.

## TiZrV NEG coating for accelerator vacuum chambers

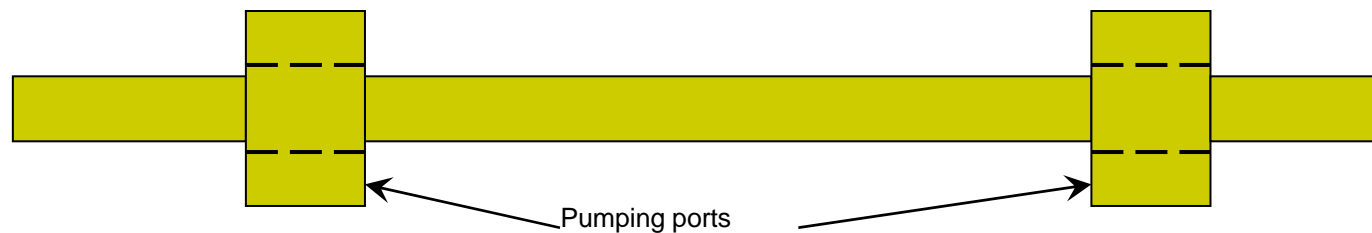
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- A 1-micron NEG coating used on a vacuum chamber made of stainless steel, copper or aluminium :
  - reduces the outgassing from the vacuum chamber walls (between 10 and 200 times less than *in-situ* baked stainless steel) and
  - introduces a distributed pumping speed, resulting in lower gas density in a beam vacuum chamber [v]. The only gases which are not pumped by such a coating are hydrocarbons and noble gases; these requires the use of other pumps, (for example, sputter ion pumps) but with much lower pumping speed.
  - The use of NEG coating requires activation, i.e. 24 hours bakeout at 180°C.
- In a positron DR the NEG coating also will play a role of an anti-multipacting coating due to low SEY.
- Thermal stimulated desorption from the NEG is negligible; the pressure inside the NEG coated chamber without SR is less than  $10^{-13}$  Torr (Helmer gauge limit)

## Pressure calculations

The average pressure can be calculated

- as a function of a distance between pumps  $L$  or
- as a function pumping speed  $S$



For two cases without or with distributed pumping speed  $C$

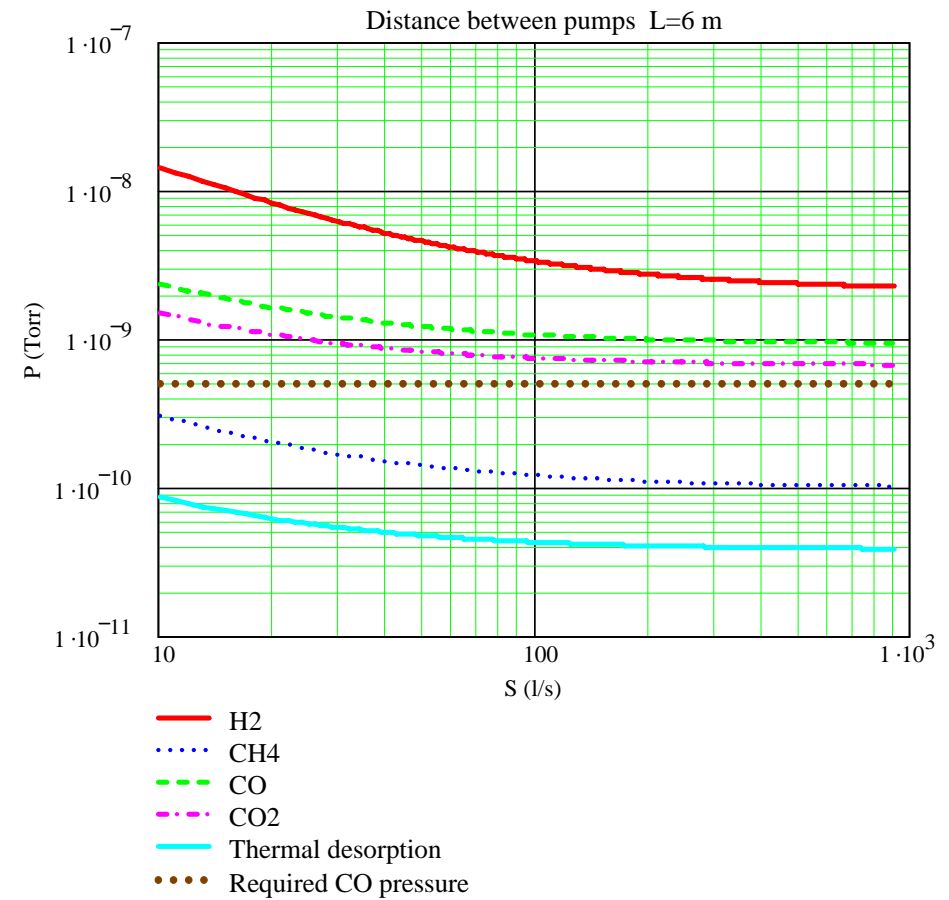
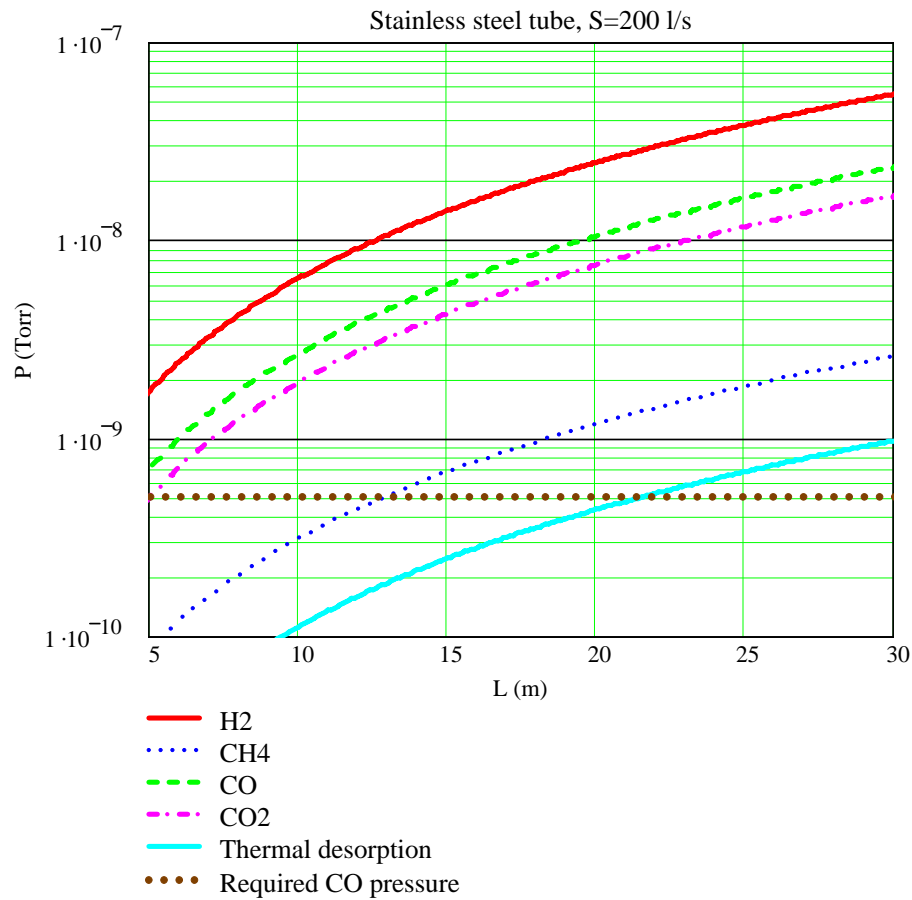
$$\langle n(L) \rangle = \eta \dot{\Gamma} \left( \frac{L}{12u} + \frac{1}{2S} \right) L$$

$$\langle n(L) \rangle = \frac{\eta \dot{\Gamma}}{\alpha C} \left( 1 - \frac{2 \tanh\left(\frac{\omega L}{2}\right)}{\omega L \left( 1 + \frac{u}{S} \omega \tanh\left(\frac{\omega L}{2}\right) \right)} \right),$$

where  $\omega = \sqrt{\alpha C / u}$

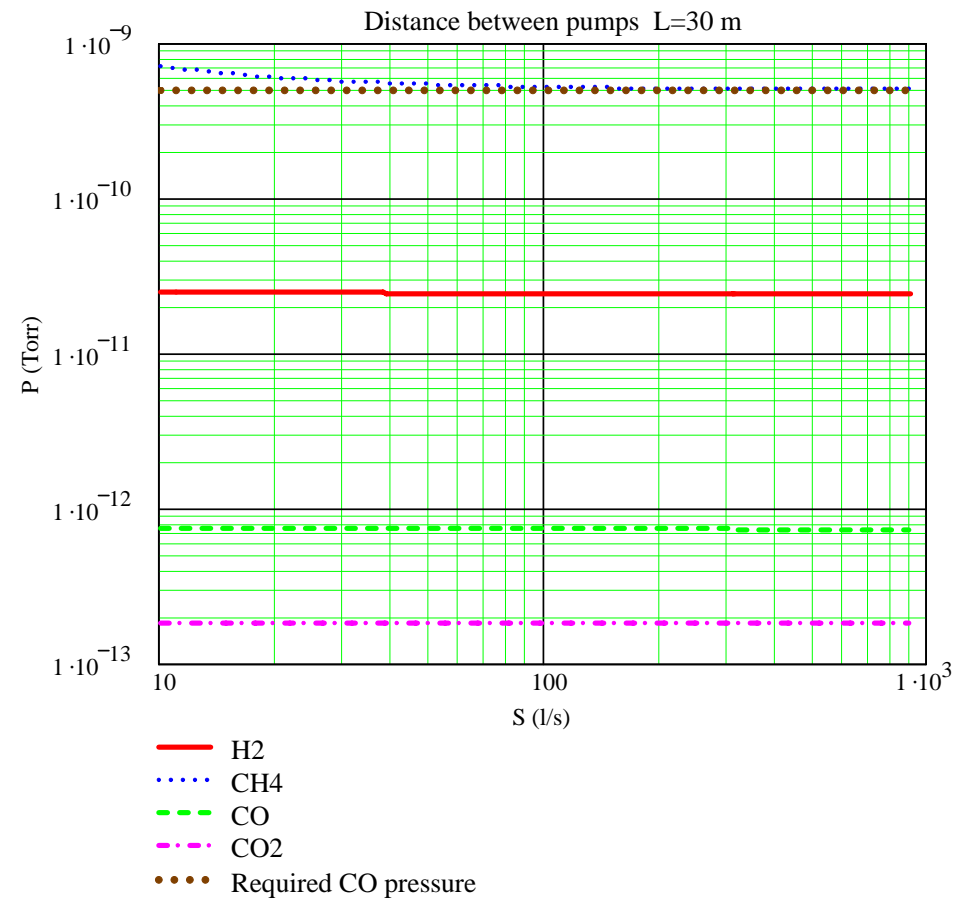
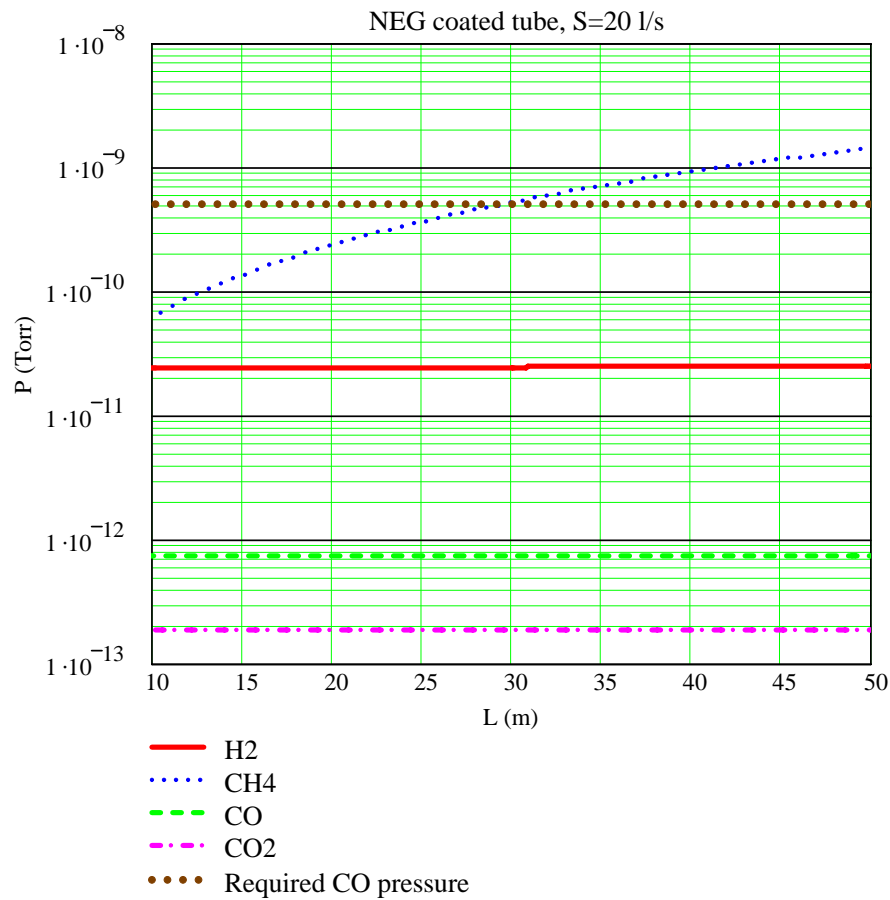
# Pressure along the arc: inside a stainless steel tube

after 100 Ahr beam conditioning:  $S_{\text{eff}} = 200$  l/s every 5 m



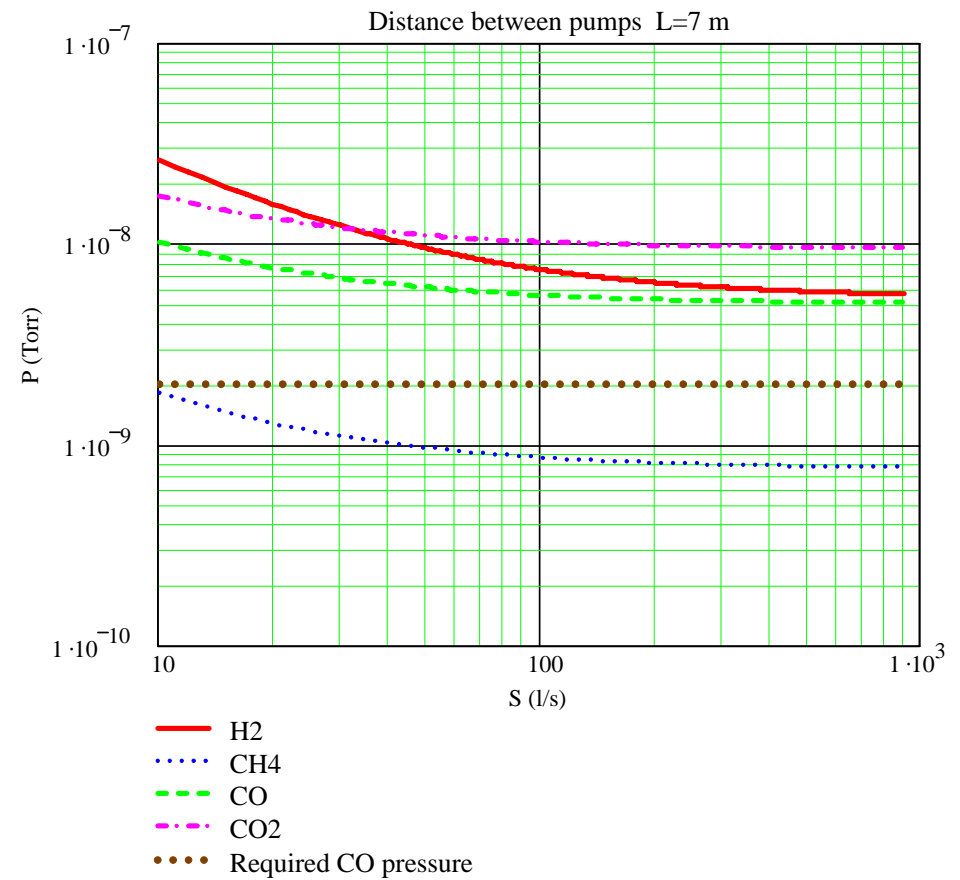
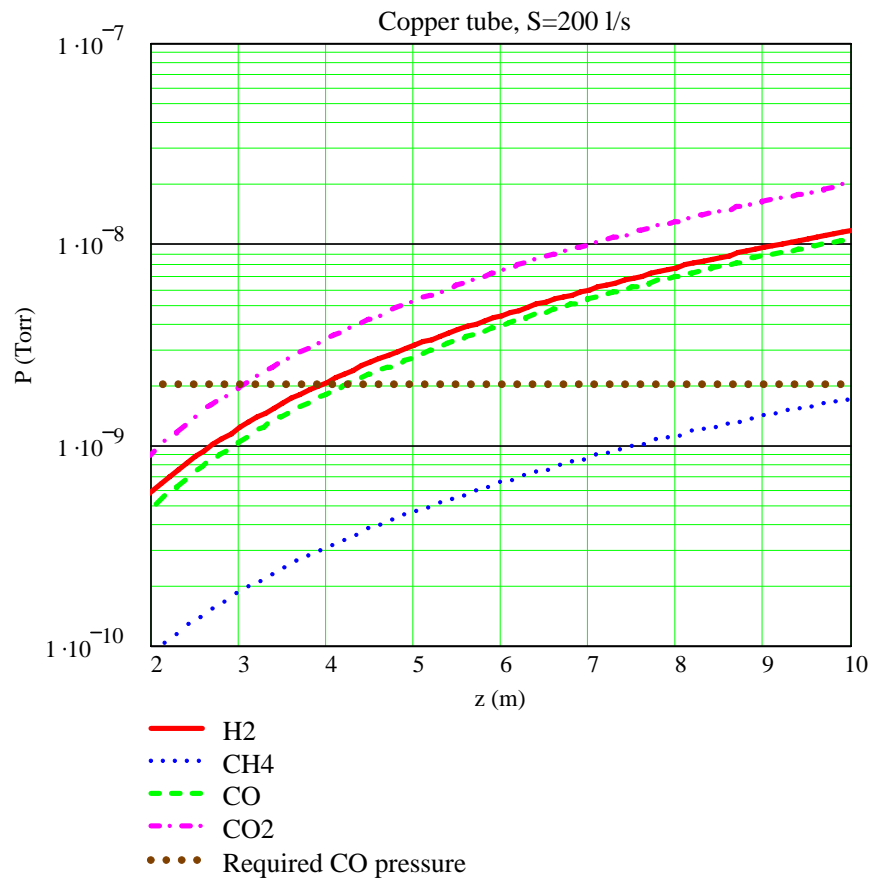
# Pressure along the arc: inside a NEG coated tube

after 100 Ahr beam conditioning:  $S_{\text{eff}} = 20 \text{ l/s}$  every 30 m



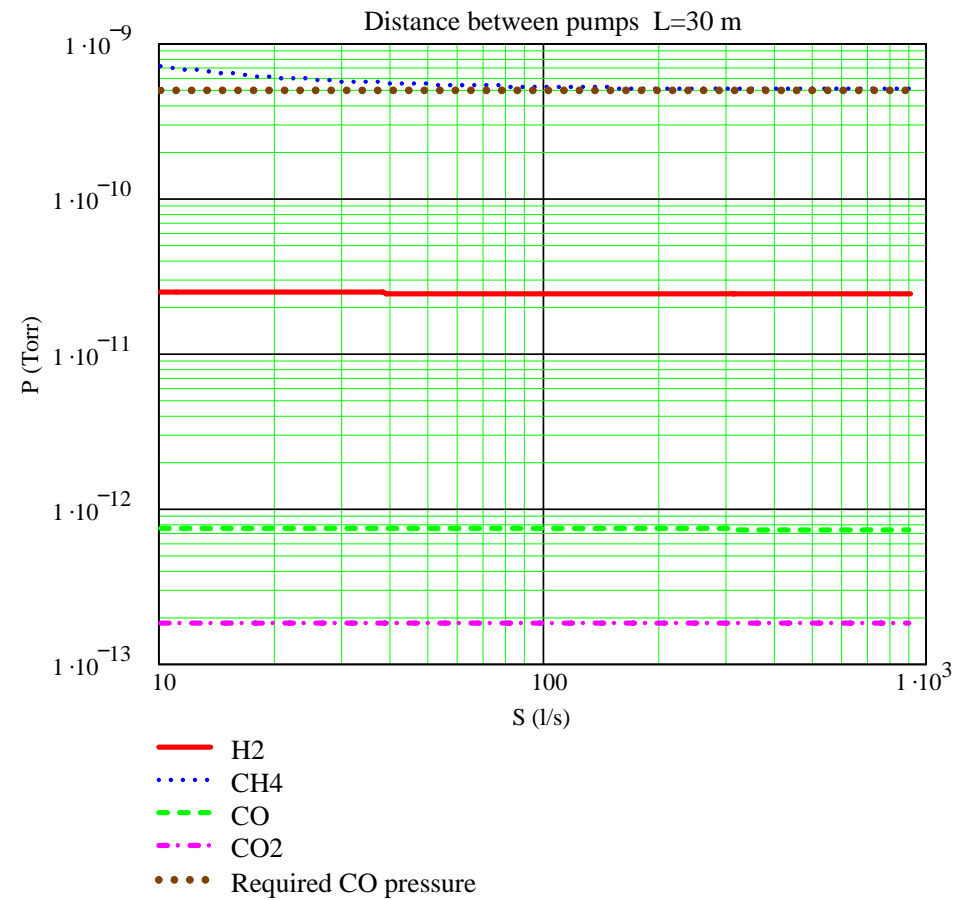
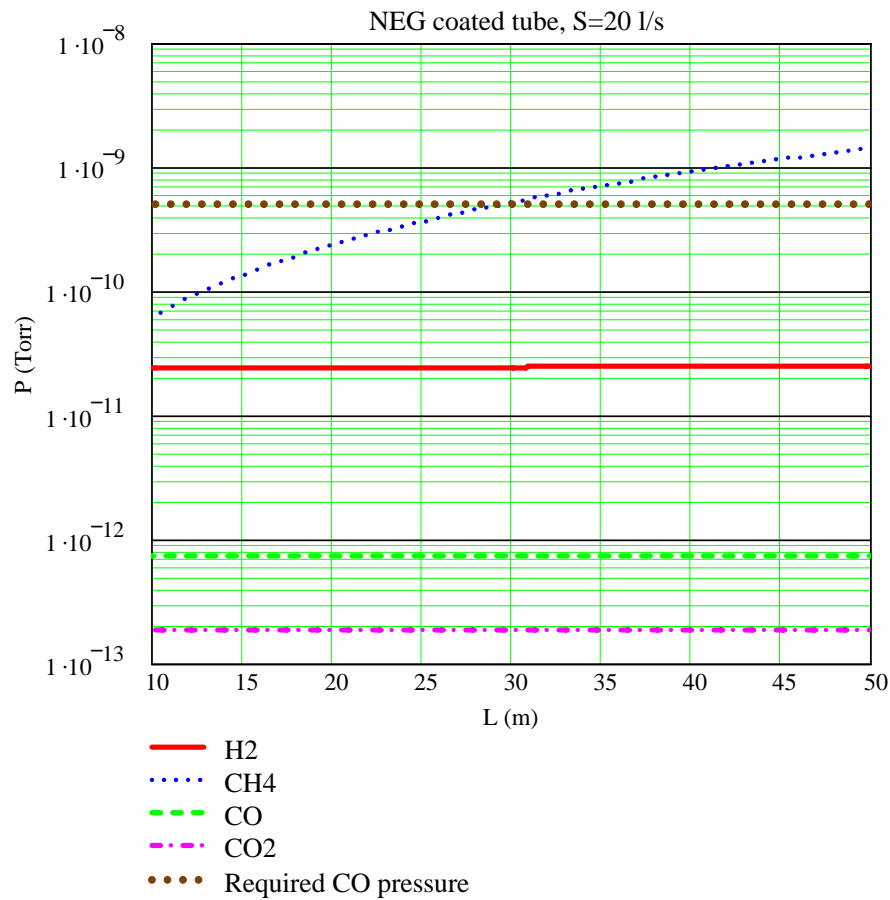
# Pressure along the wiggler VC: inside a copper tube

after 100 Ahr beam conditioning:  $S_{\text{eff}} = 200 \text{ l/s}$  every 3 m



# Pressure along the wiggler VC: inside a NEG coated tube

after 100 Ahr beam conditioning:  $S_{\text{eff}} = 20 \text{ l/s}$  every 30 m



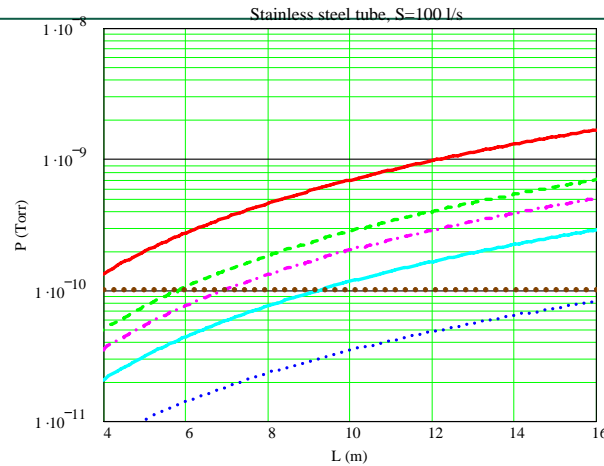


# Pressure along the stainless steel Long Straight sections

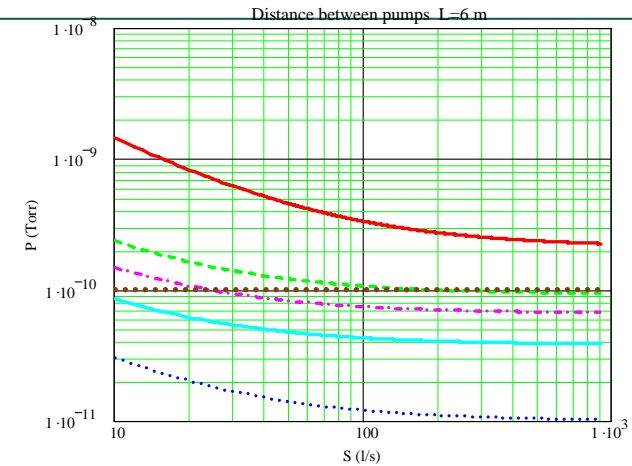
after 100 Ahr beam conditioning

40 m downstream from a dipole

$S_{\text{eff}} = 100 \text{ l/s}$  every 6 m



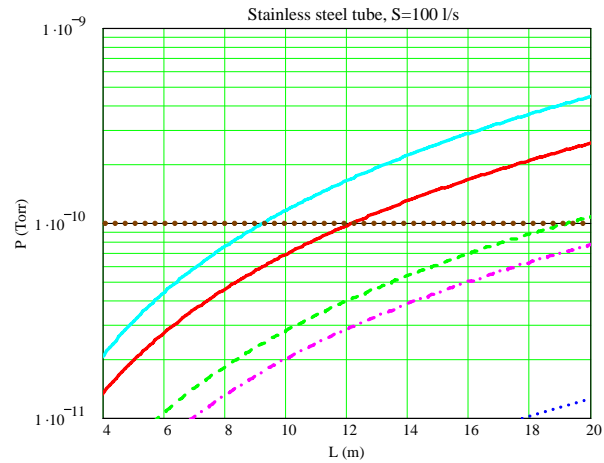
— H2  
 ..... CH4  
 - - - CO  
 - · - CO2  
 — Thermal desorption  
 ..... Required CO pressure



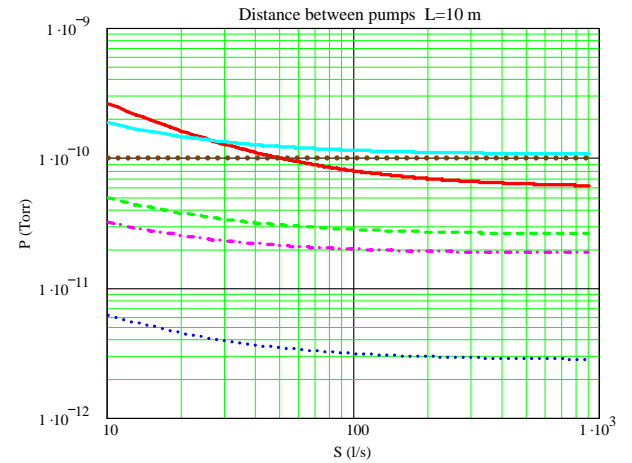
— H2  
 ..... CH4  
 - - - CO  
 - · - CO2  
 — Thermal desorption  
 ..... Required CO pressure

170 m downstream from a dipole

$S_{\text{eff}} = 100 \text{ l/s}$  every 10 m



— H2  
 ..... CH4  
 - - - CO  
 - · - CO2  
 — Thermal desorption  
 ..... Required CO pressure



— H2  
 ..... CH4  
 - - - CO  
 - · - CO2  
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 ..... Required CO pressure

# Pressure along the NEG coated Long Straight sections

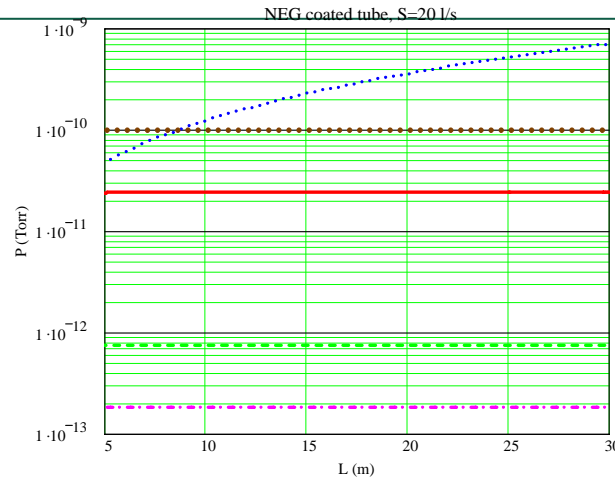
after 100 Ahr beam conditioning

40 m downstream from a dipole

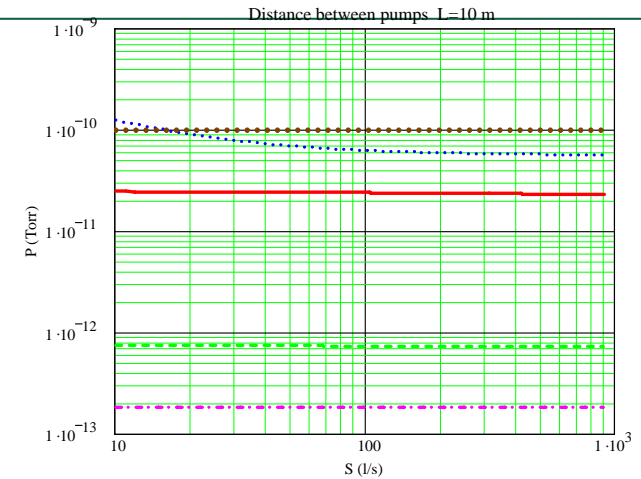
$S_{\text{eff}} = 20 \text{ l/s}$  every 10 m

170 m downstream from a dipole

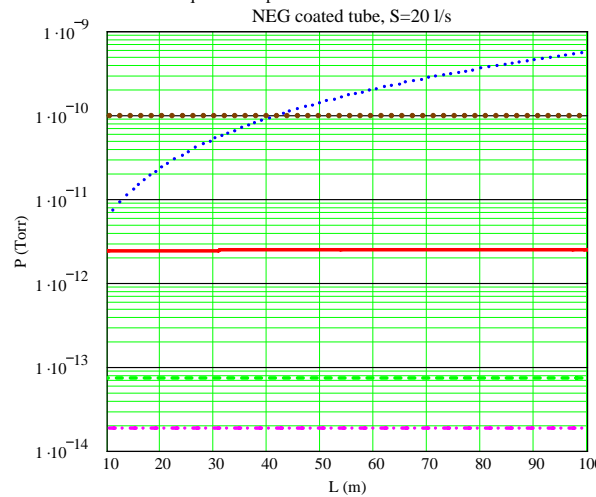
$S_{\text{eff}} = 20 \text{ l/s}$  every 40 m



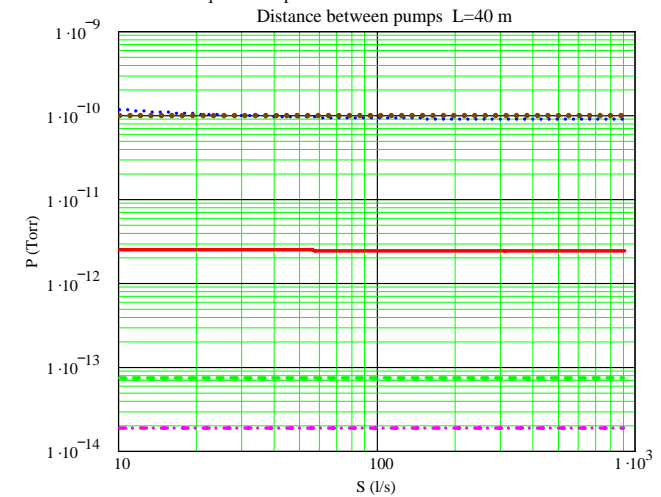
— H2  
 ..... CH4  
 - - - CO  
 - · - · CO2  
 ..... Required CO pressure



— H2  
 ..... CH4  
 - - - CO  
 - · - · CO2  
 ..... Required CO pressure



— H2  
 ..... CH4  
 - - - CO  
 - · - · CO2  
 ..... Required CO pressure



— H2  
 ..... CH4  
 - - - CO  
 - · - · CO2  
 ..... Required CO pressure

## Electron multipacting effect on vacuum

- The photon stimulated desorption is a two-step process:
  - Photoelectron emission ( $E_1 = \sim 5-10$  eV and  $E_2 = \sim E_\gamma$ ,  $PEY = \sim 0.1$  e $^-$ /  $\gamma$ )
  - Electron stimulated molecular desorption
- The electron stimulated desorption grow with electron energy and electron flux hitting the vacuum chamber.
- For example, for  $E_{e^-} = 100$  eV and  $\Gamma_{e^-} = 10^{16}$  e $^-$ /(m·s), the electron stimulated gas desorption is comparable to the photon stimulated desorption for  $\Gamma_\gamma = 10^{17}$   $\gamma$ /(m·s) (~8 m downstream dipole). I.e. the electron multipacting may affect on vacuum, new results of e-cloud modelling are required for different parts of DR.
- If the electron multipacting is significant on long straights, it will badly affect the vacuum performance as no vacuum conditioning will be done there with photons.

## Main results of the modelling

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- NEG coating of vacuum chamber along both the arcs and the wigglers as well as a few tens meters downstream of both looks to be the only possible solution to fulfil vacuum requirement for the ILC dumping ring
- Beam induces electron Multipacting (BIEM) looks to make negligible impact inside dipoles and wigglers, but it might affect on the straights vacuum design and the beam conditioning scenario. **E-cloud modelling results are needed!**
- Power dissipation from SR (and BIEM if there is any) have to be considered:
  - vacuum chamber water cooling is required in wigglers, arcs and a few tenth meters downstream of both.
  - end power absorber for SR from the wiggler (at first dipole downstream a wiggler)
- NEG coated power absorber for wiggler vacuum chamber needs to be studied experimentally.

## Ideal vacuum chamber for ILC DR

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- Round or elliptical tube
  - Cheapest from technological point of view
- No antechamber
  - Beam conditioning is most efficient
- NEG coated
  - Requires less number of pumps with less pumping speed
  - 180°C for NEG activation instead of 250-300°C bakeout
  - Choice of vacuum chamber material (stainless steel, copper and aluminium ) does not affect vacuum in this case
  - Residual gas CH<sub>4</sub> and H<sub>2</sub> (almost no CO and CO<sub>2</sub>)
- There are experimental results that NEG coated elliptical vacuum chamber might be re-activated even without baking to 180°C, just by SR.
  - Accurate experimental study is needed