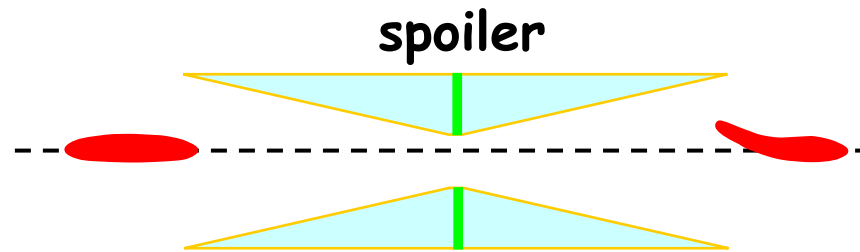


Status of Collimator Damage Studies



Nigel Watson (Birmingham)

Daresbury, 9-Jan-2007

- Aims
- Simulations
- Plans

Aims

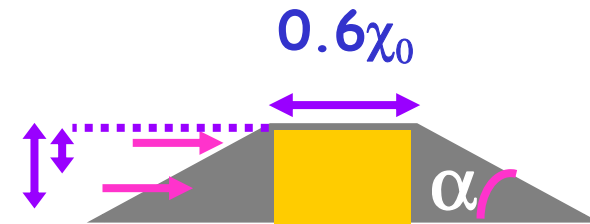
- Design of spoiler jaws (geometry and materials) to optimise performance for wakefields:
 - ▶ E.M. modelling (J.Smith)
 - ▶ T480 beam test of collimator profiles (Fernandez-Hernando)
 - ⇒ Develop data-validated ability to predict (3D) short range transverse wakes to 10% in regimes ~ ILC
 - ▶ Realistic wakefield models implemented in tracking codes (Bungau, Latina)
 - ▶ “Simple”, direct experimental measurement at ESA
- ... and beam damage
 - ▶ Fluka, Geant4, EGS simulations (Fernandez-Hernando, Bungau, Keller)
 - ▶ ANSYS (Ellwood, Greenhalgh)
 - ▶ More difficult to quantify “significant” damage
- Need to consider wakefield and damage mitigation designs together

People

- “Spoiler Wakefield and Mechanical Design” task
- Details on project web: <http://hepunx.rl.ac.uk/swmd/>
- Birmingham: N. Watson
- CCLRC: C. Beard, G. Ellwood, J. Greenhalgh, J. O'Dell, L. Fernandez
- CERN: F. Zimmermann, G. Rumolo, D. Schulte
- [DESY: I. Zagorodnov]
- Lancaster: D. Burton, N. Shales, J. Smith, A. Sopczak, R. Tucker
- Manchester: R. Barlow, A. Bungau, G. Kurevlev, R. Jones, A. Mercer
- TEMF, Darmstadt: M. Kärkkäinen, W. Müller, T. Weiland
- For ESA tests, working closely with
 - ▶ CCLRC on optics for wakefield and beam damage studies
 - ▶ SLAC for all aspects

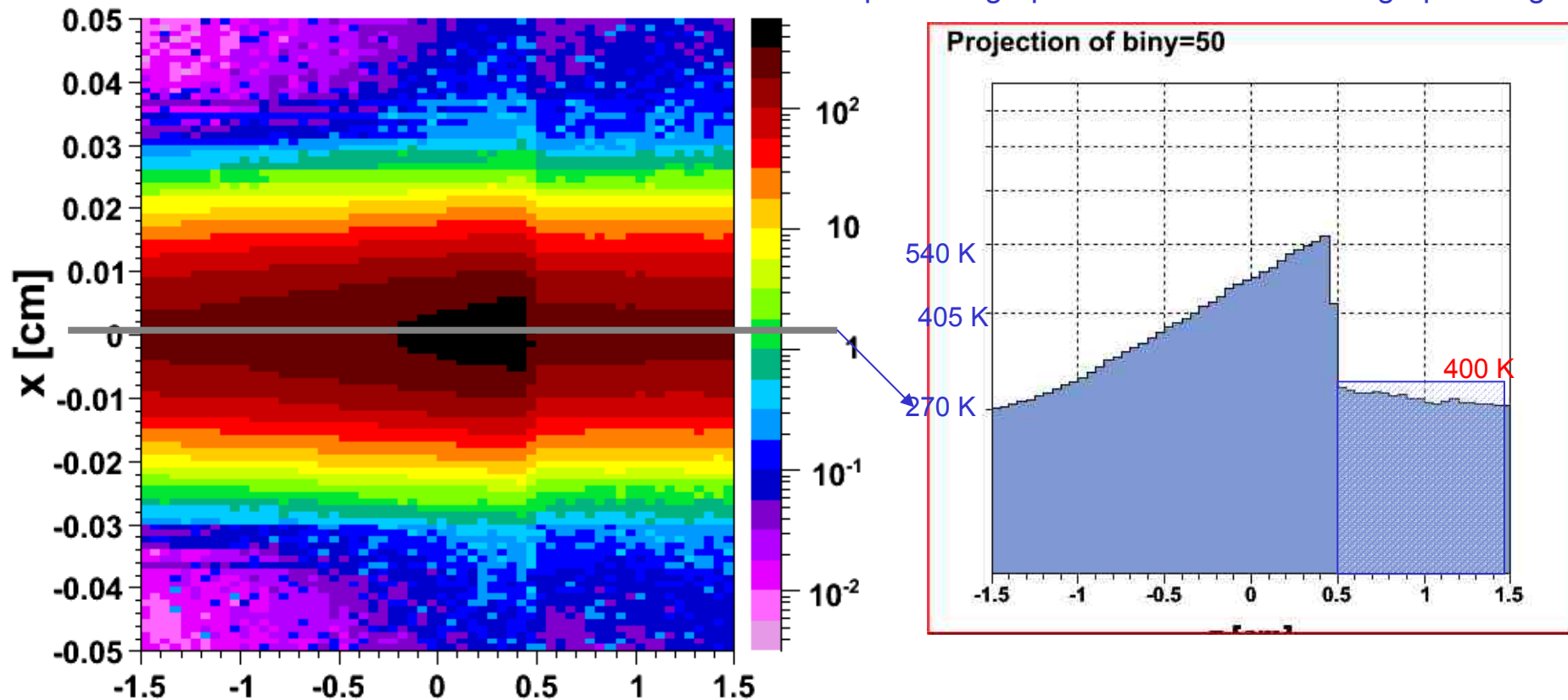
Starting point

- Long, shallow tapers ($\sim 20\text{mrad}$?), reduce short range transverse wakes
- High conductivity surface coatings
- Robust material for actual beam spoiling
- Long path length for errant beams striking spoilers
 - ▶ Large χ_0 materials (beryllium..., graphite, ...)
- Require spoilers survive at least 2 (1) bunches at 250 (500) GeV
- Design approach
 - ▶ Consider range of constructions, study relative resilience to damage (melting, fracture, stress)
 - ▶ Particularly important for beam-facing surfaces (wakefields)
 - ▶ Also within bulk (structural integrity, heat flow)
- Design external geometry for optimal wakefield performance, reduce longitudinal extent of spoiler if possible
- Use material of suitable resistivity for coating
- Design internal structure using in initial damage survey seems most appropriate.



Ti / Graphite Spoiler

Temperature data in the left only valid the Ti-alloy material. Top increase of temp. in the graphite ~400 K. Dash box: graphite region.



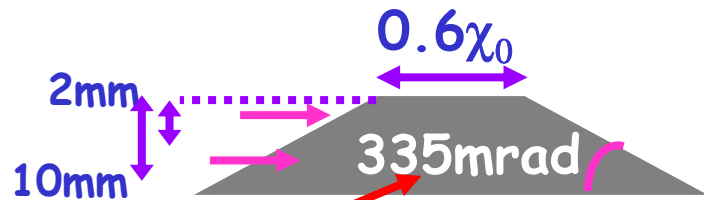
2 mm deep from top z [cm] $\Delta T_{\text{max}} = 575$ K per a bunch of $2E10$ e- at 500 GeV

Ti alloy and graphite spoiler $\sigma_x = 79.5$ μm , $\sigma_y = 6.36$ μm

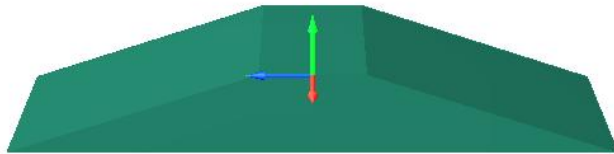
European LC Workshop / 9-Jan-2007

[L. Fernandez, ASTeC]
Nigel Watson / Birmingham

Spoilers considered include...

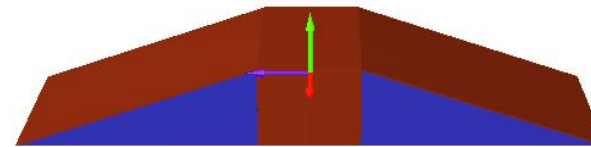


As per T480 Ti, Cu, Al



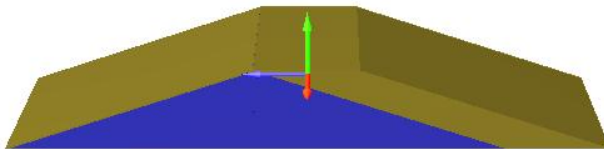
$2 \cdot 10^{10} e^-$, $E_{\text{beam}} = 250 \text{ GeV}$, $\sigma_x \times \sigma_y = 111 \times 9 \mu\text{m}^2$
 also, $E_{\text{beam}} = 500 \text{ GeV}$

Option 1: Ti/C, Ti/Be



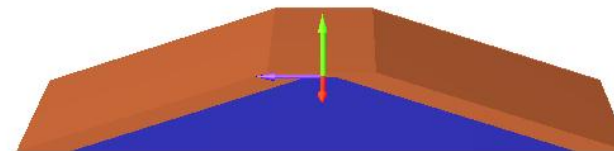
Graphite regions ■

Option 2: Ti/C, Cu/C, Al/C



0.6 X_0 of metal taper (upstream),
 1 mm thick layer of Ti alloy

Option 3: Ti/C



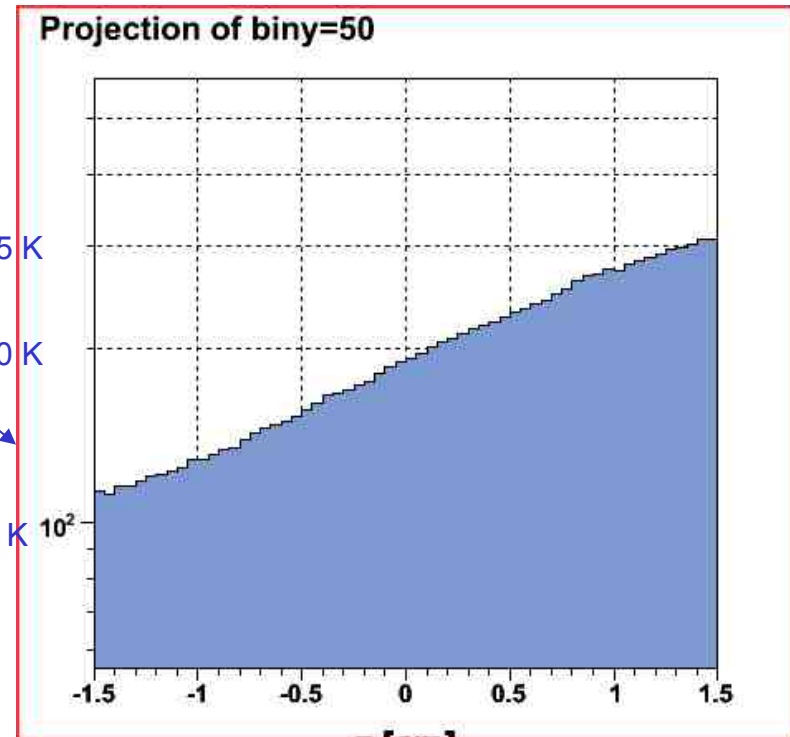
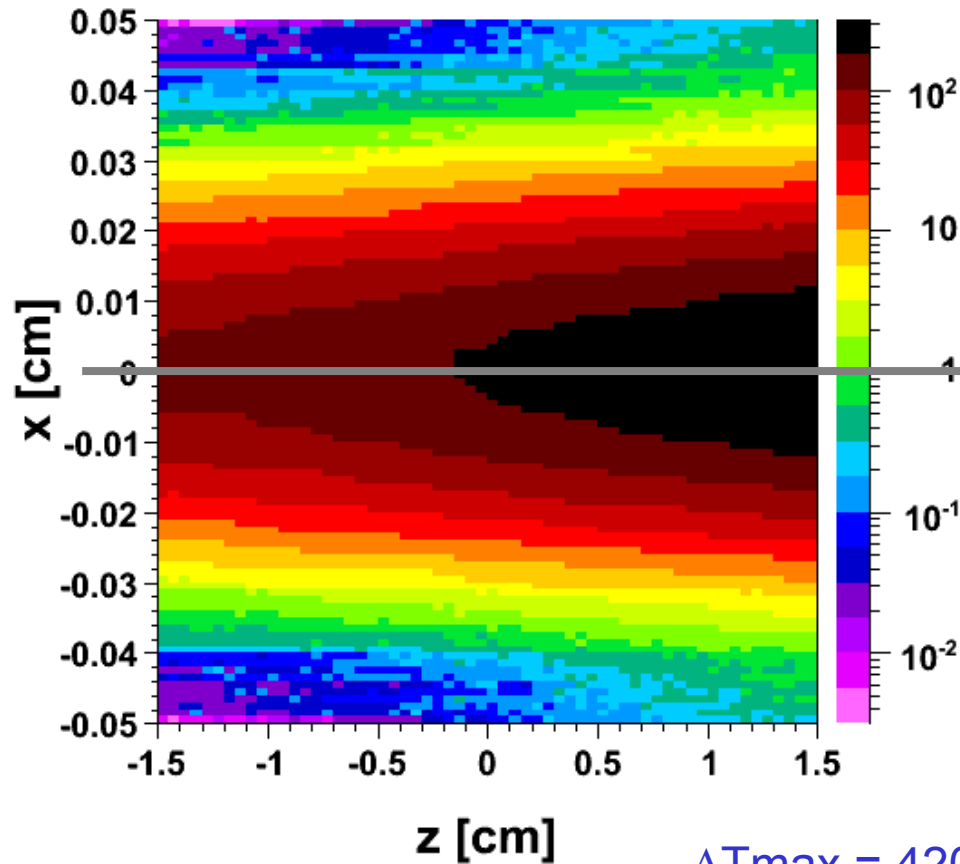
0.3 X_0 of Ti alloy upstream and
 downstream tapers

[Details, see Eurotev Reports 2006-015, -021, -034] tson / Birmingham

2 mm deep from top

250 GeV e- [GeV/cm³]

Full Ti alloy spoiler



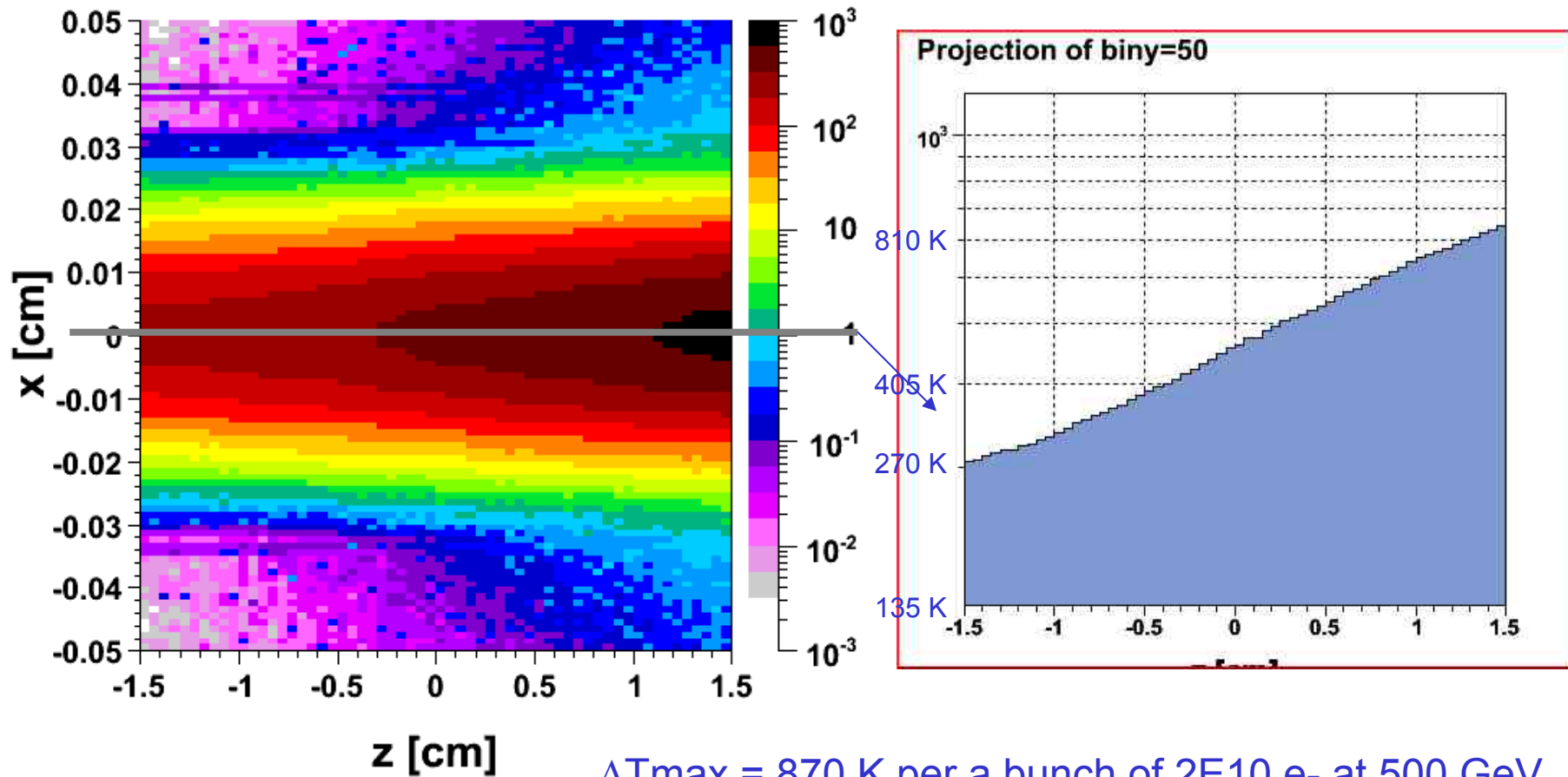
$\Delta T_{\text{max}} = 420 \text{ K}$ per a bunch of $2E10 \text{ e-}$ at 250 GeV

$\sigma_x = 111 \text{ }\mu\text{m}$, $\sigma_y = 9 \text{ }\mu\text{m}$

2 mm deep from top

500 GeV e- [GeV/cm³]

Full Ti alloy spoiler



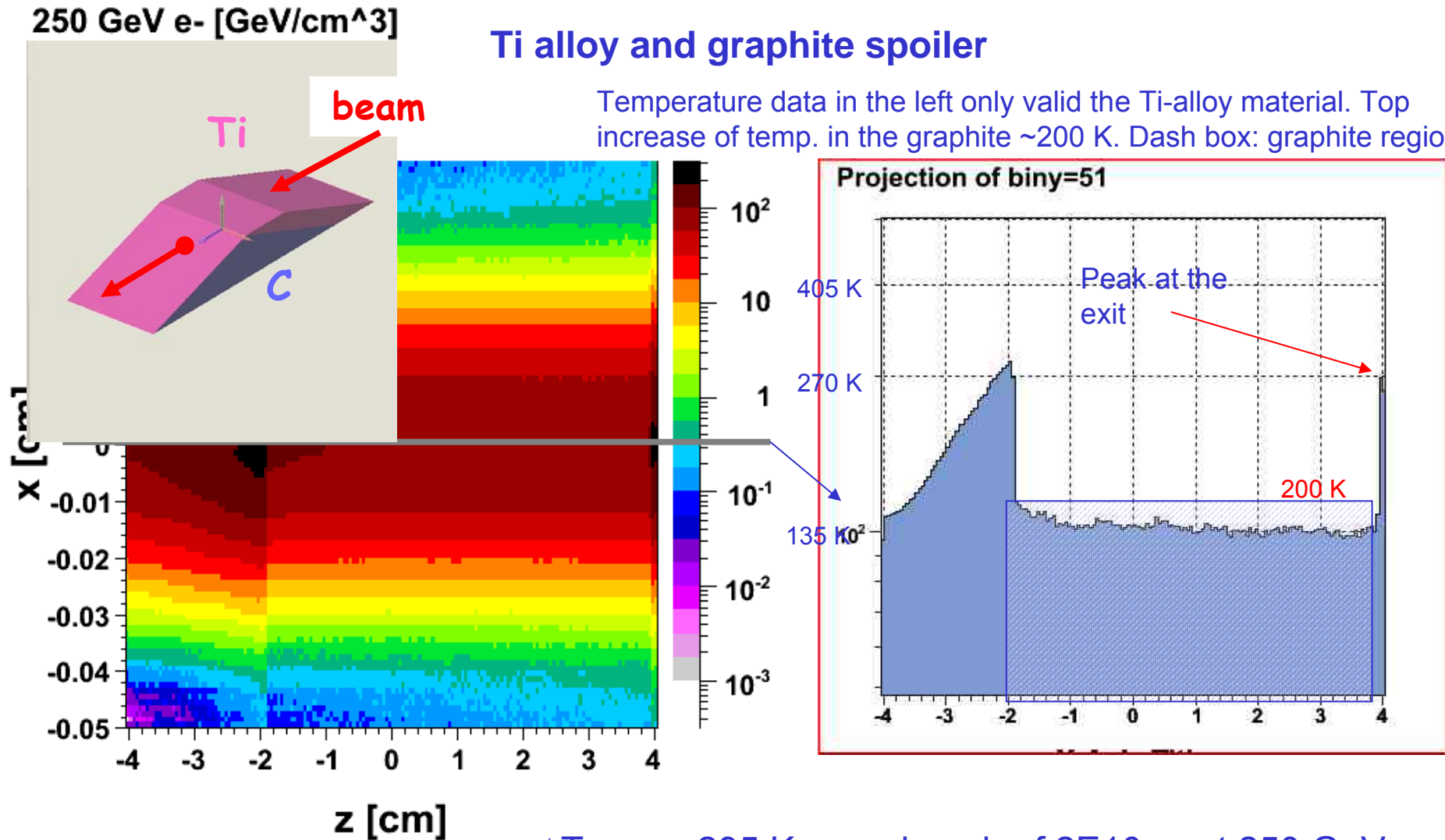
$\Delta T_{\text{max}} = 870 \text{ K}$ per a bunch of $2E10 \text{ e-}$ at 500 GeV

$\sigma_x = 79.5 \text{ }\mu\text{m}$, $\sigma_y = 6.36 \text{ }\mu\text{m}$

10 mm deep from top

Ti alloy and graphite spoiler

Temperature data in the left only valid the Ti-alloy material. Top increase of temp. in the graphite ~200 K. Dash box: graphite region.



$\Delta T_{max} = 295$ K per a bunch of $2E10$ e- at 250 GeV

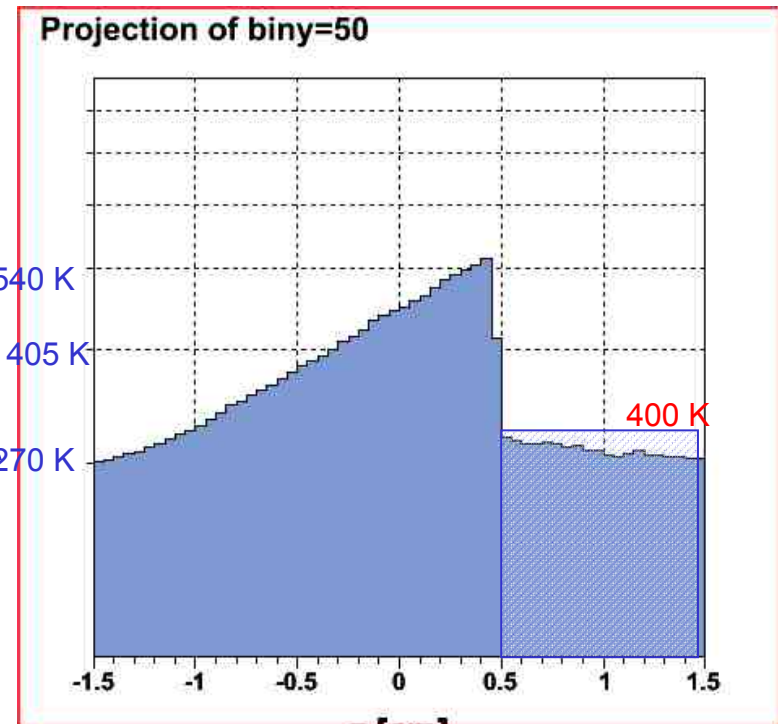
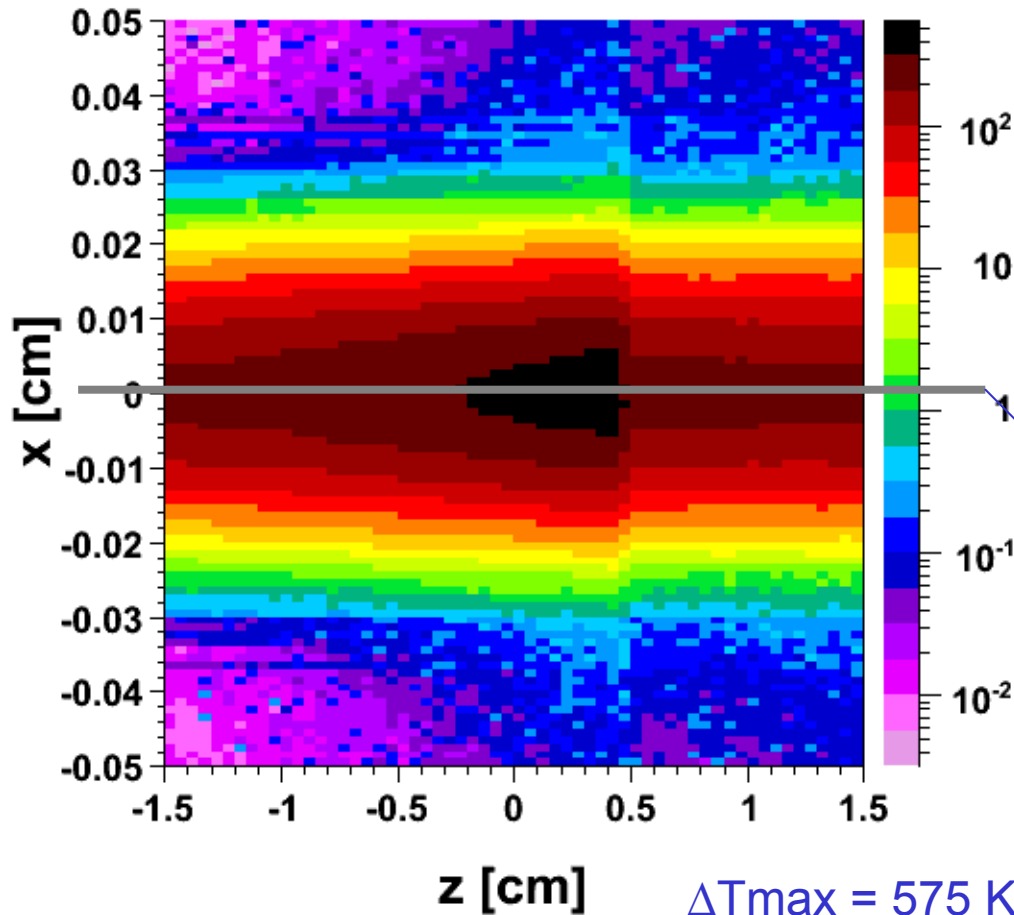
$\sigma_x = 111$ μ m, $\sigma_y = 9$ μ m

500 GeV e- [GeV/cm³]

2 mm deep from top

Ti alloy and graphite spoiler

Temperature data in the left only valid the Ti-alloy material. Top increase of temp. in the graphite ~400 K. Dash box: graphite region.



$\Delta T_{max} = 575$ K per a bunch of $2E10$ e- at 500 GeV

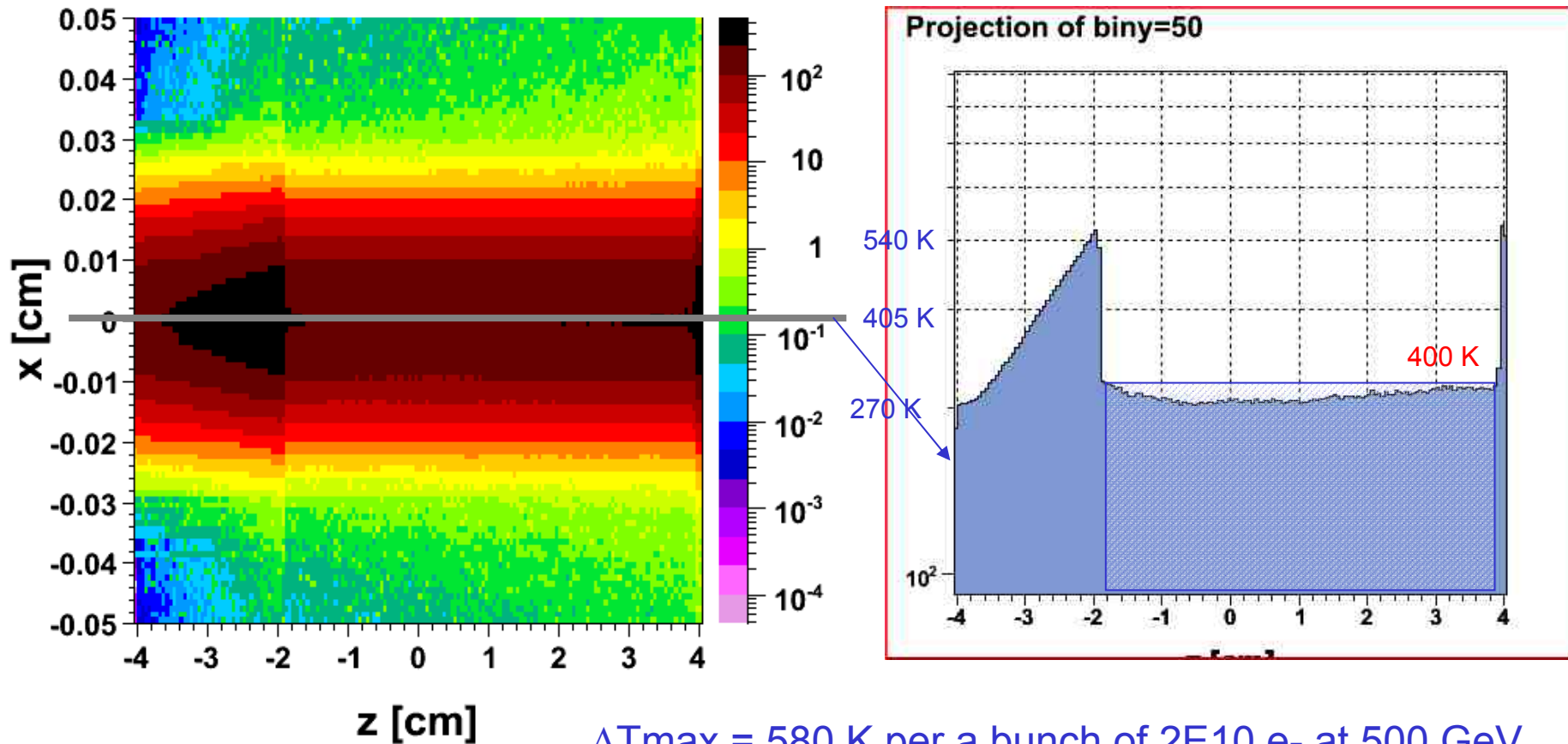
$\sigma_x = 79.5$ μ m, $\sigma_y = 6.36$ μ m

10 mm deep from top

500 GeV e- [GeV/cm³]

Ti alloy and graphite spoiler

Temperature data in the left only valid the Ti-alloy material. Top increase of temp. in the graphite ~400 K. Dash box: graphite region.

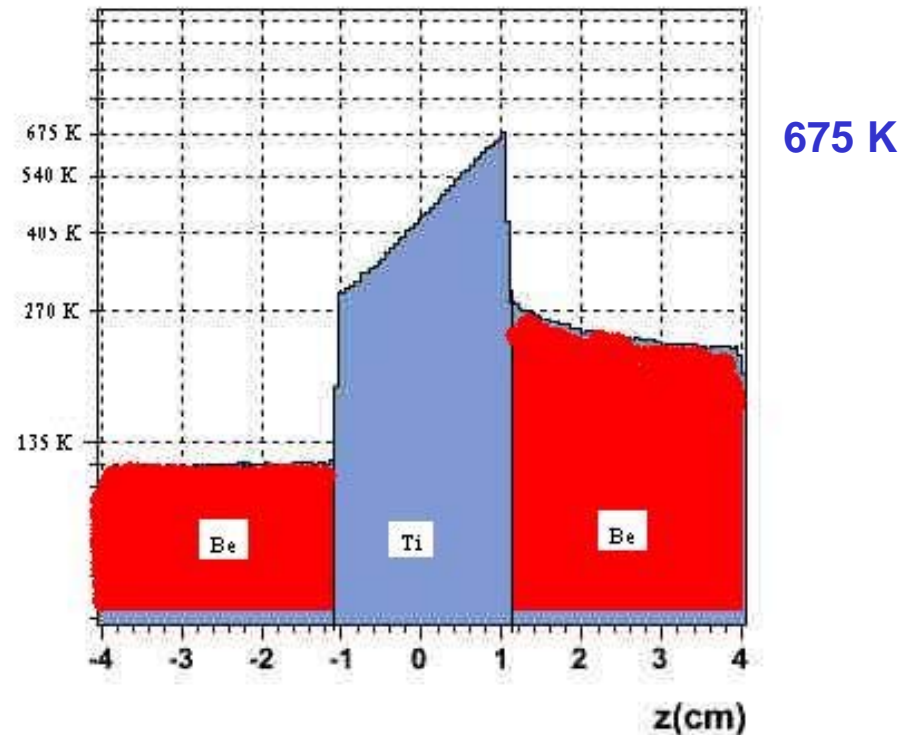
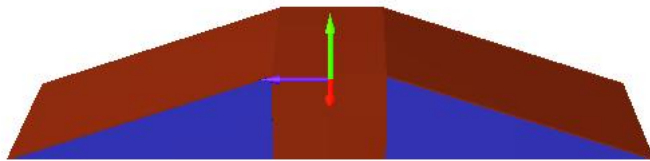


$\Delta T_{\text{max}} = 580 \text{ K}$ per a bunch of $2E10 \text{ e-}$ at 500 GeV

$\sigma_x = 79.5 \text{ }\mu\text{m}$, $\sigma_y = 6.36 \text{ }\mu\text{m}$

10 mm depth from top

Ti alloy (solid central region) and
beryllium spoiler (all tapers)



Temperature data in the left only valid the Ti-alloy material.

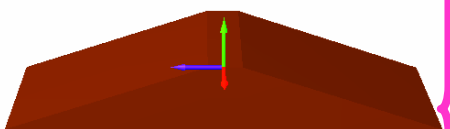
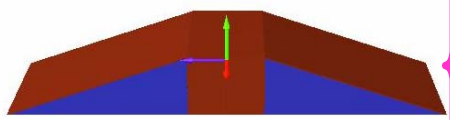
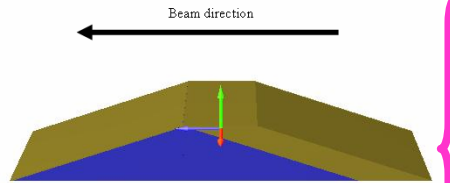
$\Delta T_{\max} = 675 \text{ K}$ per a bunch of $2E10 \text{ e}^-$ at 500 GeV

$\sigma_x = 79.5 \text{ } \mu\text{m}$, $\sigma_y = 6.36 \text{ } \mu\text{m}$

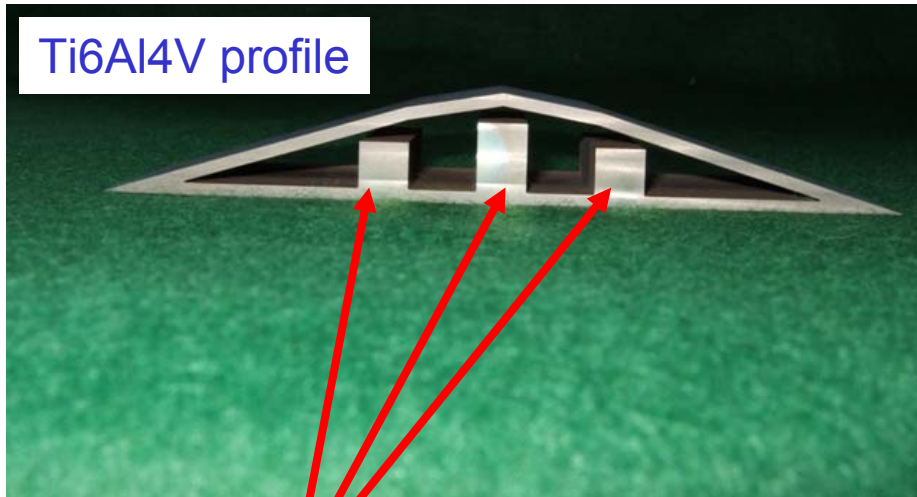
Summary of simulations

- Exceeds fracture temp.
- Exceeds melting temp.

Temperature **increase** from 1 bunch impact

		2mm depth		10mm depth	
		250 GeV e ⁻ 111×9 μm ²	500 GeV e ⁻ 79.5×6.4 μm ²	250 GeV e ⁻ 111×9 μm ²	500 GeV e ⁻ 79.5×6.4 μm ²
	Solid alloy Ti	420 K	870 K	850 K	2000 K
	Solid Al	200 K	210 K	265 K	595 K
	Solid Cu	1300 K	2700 K	2800 K	7000 K
	Graphite+Ti option 1	325 K	640 K	380 K	760 K
	Beryllium+Ti ≈ option 1	-	-	-	675 K
	Graphite+Ti option 2	290 K	575 K	295 K	580 K
	Graphite+Al option 2	170 K	350 K	175 K	370 K
	Graphite+Cu option 2	465 K	860 K	440 K	870 K
	Graphite+Ti option 3	300 K	580 K	370 K	760 K

Manufacturing study

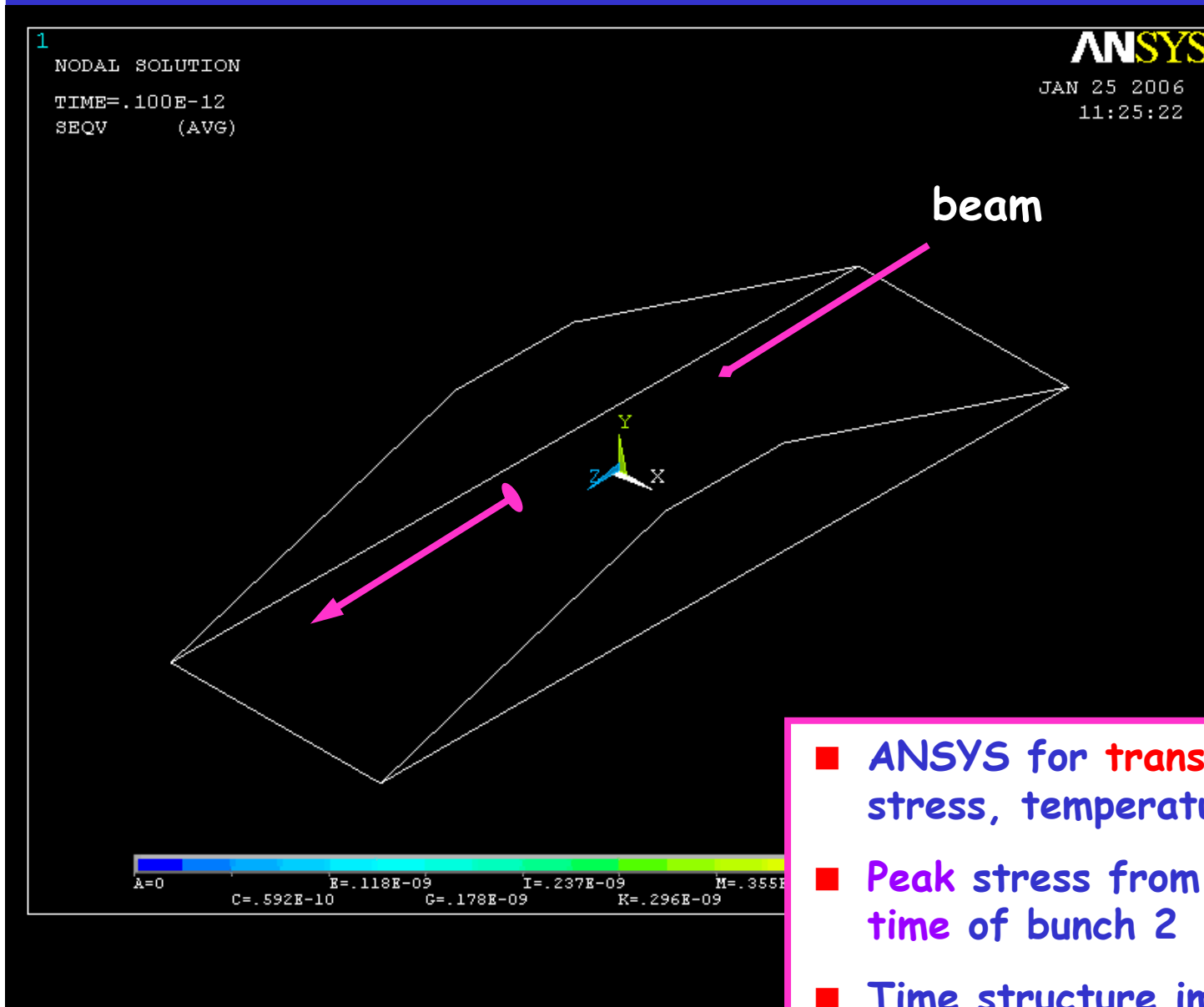


- Pillars are artefact of ESA vacuum vessel

- Ti "option 3", spoiler can survive if profile not supported by C (rigidity, uniformity of surface, taper angle)
- At 50mrad, $0.6\chi_0$ (Ti6Al4V) in z is 1mm thick layer
- Wire erosion process used, also characterise surface quality
- Importance of outer geometry optimisation from wakefield study

2 ILC bunches

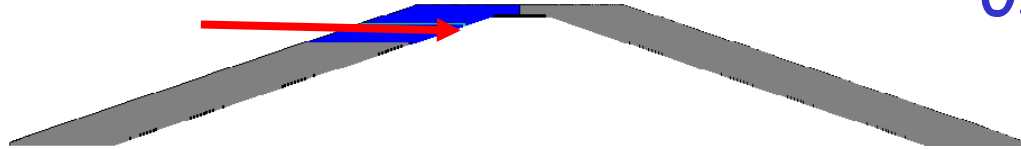
[Ellwood/RAL]



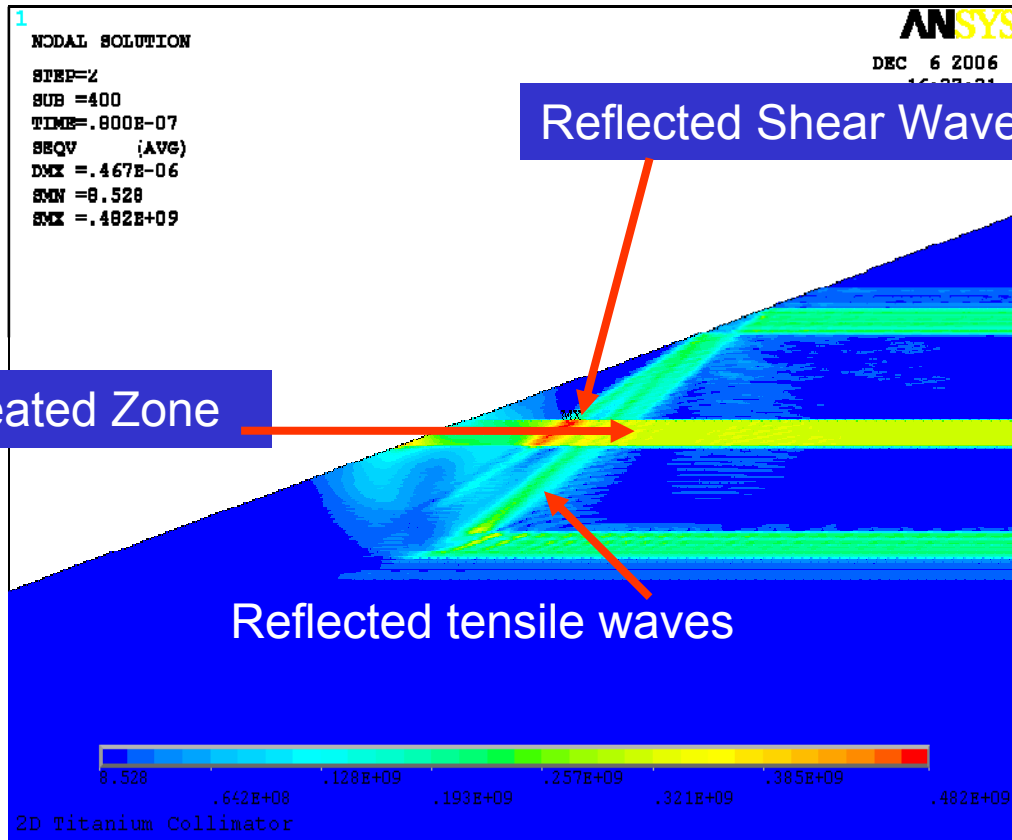
- ANSYS for **transient** mechanical stress, temperature rise
- Peak stress from bunch 1 ~ arrival time of bunch 2
- Time structure important for tests

2d shockwave study

beam



Use "option 3" spoiler with simple heated zone ~ beam dimensions



Reflected Shear Waves

Heated Zone

Reflected tensile waves

Most damage caused by reflected shear waves

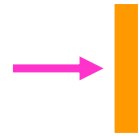
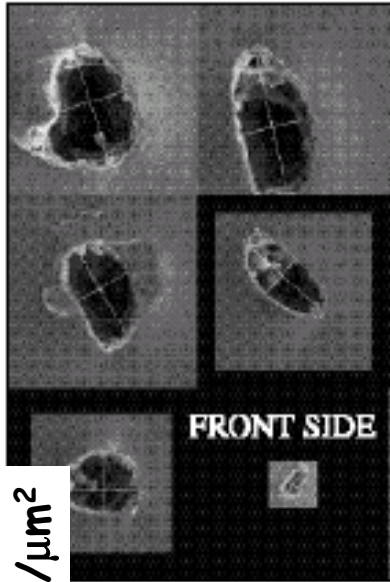
Depends on angle of incidence of reflected wave and free surface, i.e. taper angle from wakefield optimisation

Compressive waves

Code benchmarking

- Gives some confidence that our simulations are reasonable
- Simulation of existing Cu data encouraging
- Need to understand mechanical properties of Ti alloy (or Be) in rapid heating / shock regime
 - ▶ Effect of two bunch impacts
- Beam timing required for meaningful tests
 - ▶ Found single bunch/2nd bunch do need $\Delta t \sim \text{ILC}$ bunch t get useful information
 - ▶ Too low energy aflash/ttf2 for full shower development
- Considered options at FLASH, ESA,...

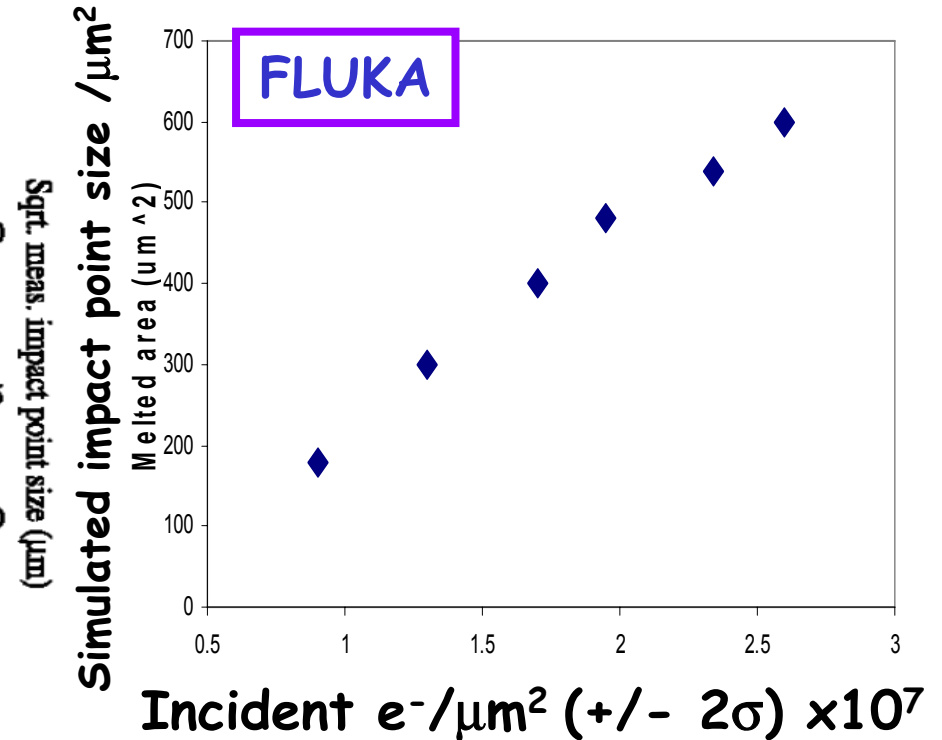
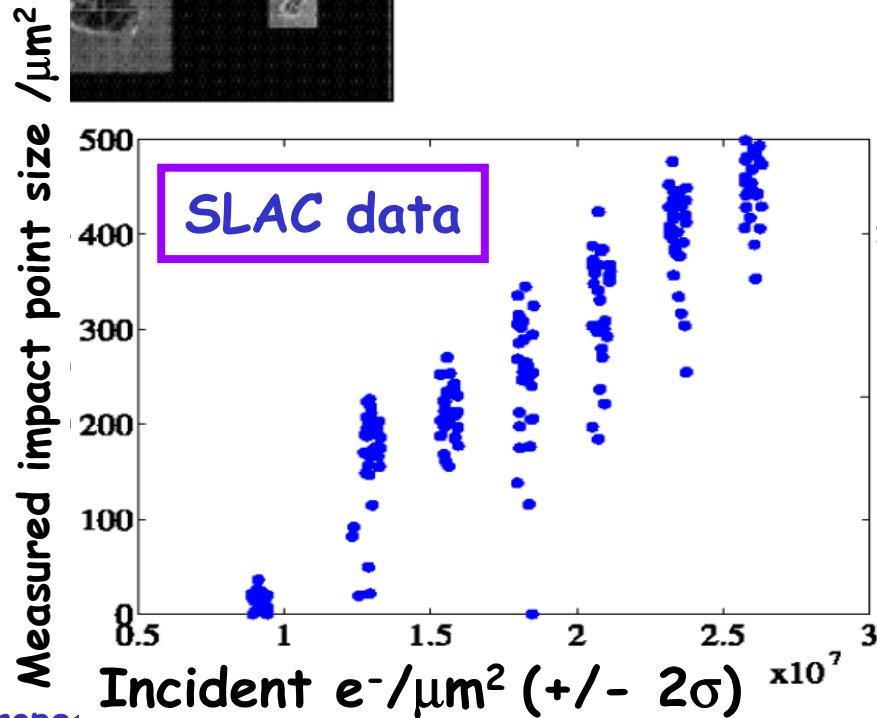
Fluka Benchmark



Observed size of beam damage hole in Cu, from FFTB

[Measurements c/o Marc Ross et al., Linac'00]

Fluka prediction of beam damage, good agreement with data (NB: evaporated vs. melted - expect data < FLUKA)



TTF

- ILC bunch spacing
 - ▶ Multiple bunch effects
- ~450 MeV
- Limited material in transfer line ($\sim 0.4\chi_0$), space in existing jig (4mm thickness)
 - ▶ Do not get significant shower development in Ti on downstream surface



σ_r [μm]	#bunches to initiate melting (melt area)	#bunches for $10 \times 10 \mu\text{m}^2$ melted area
10	3 ($26 \times 26 \mu\text{m}^2$)	-
20	9 ($8 \times 8 \mu\text{m}^2$)	10
30	18 ($1 \times 1 \mu\text{m}^2$)	20
40	30 ($1 \times 1 \mu\text{m}^2$)	35
50	45 ($1 \times 1 \mu\text{m}^2$)	52

ESA

- 28.5 GeV
- 10Hz, therefore only single pulse damage can be studied
- Would need beam focussing to $\sigma_r \sim 10 \mu\text{m}$ (typical beam size in 2006 $\sigma_x \times \sigma_y \sim 500 \times 100 \mu\text{m}^2$)
- Dispersion in ESA currently limiting

Summary & Future Plans

- Good agreement between FLUKA, GEANT4, EGS4 on energy deposited
- Resulting mechanical stresses examined with ANSYS3D
- Continue study into beam damage/materials
 - ▶ Experimental (beam?) test to reduce largest uncertainties in material properties
- Study geometries which can reduce overall length of spoilers while maintaining performance
- Means of damage detection, start engineering design of critical components
- Revisit collimation requirements for materials ($0.6\chi_0$ optimised?)
- Combine information on geometry, material, construction, to find acceptable baseline design for
 - ▶ Wakefield optimisation
 - ▶ Collimation efficiency
 - ▶ Damage mitigation