# THE STATUS OF POSITRON SOURSE DEVELOPMENT AT CORNELL

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# **ACTIVITIES**

### √ CODE FOR POSITRON CONVERSION (UNDULATOR → LINAC → further on)

Choice of undulator parameters → main issue

Choice of target dimensions

Choice of collection optics parameters

### **√ UNDULATOR DESIGN** (main activity)

Undulators with period 10 and 12 mm having 8 mm aperture (tested)

Designed undulators with aperture 1/4" (7mm magnetic core)

#### TARGET DESIGN (in addition to Livermore, SLAC, Daresbury

Rotating Tungsten target (including new sandwich type)

Liquid metal target: Bi-Pb or Hg

#### **COLLECTION OPTICS DESIGN**

Lithium lens

Solenoid

#### **√** COLLIMATORS

Collimator for gammas

Collimators for full power beam

#### **√ PERTURBATION OF EMITTANCE AND POLARIZATION**

Perturbation of emittance in regular part

Polarization handling

#### **√ UNDULATOR CHICANE**

Minimal possible parallel shift

#### **√ COMBINING SCHEME**

Two-target scheme

These positions not closed finally

# **CODE FOR POSITRON CONVERSION**

Undulator → target → focusing → post acceleration Written in 1986-1987; restored in 2007

#### PROGRAM KONN

T.A. Vsevelezhskaya, A.A. Mikhaffichenko

Monte-Carlo simulation of positron conversion

Energy of the beam;

Length of undulator;

Undulator period M= $L/\lambda_{y}$ ;

K-factor;

Emittance;

Betu-function;

Number of harmonics (four);

Number of positrons to be generated;

Target:

Distance to the undulator

Thickess:

Dimneter of turget;

Material;

Diameter of hole at center;

Step of calculation

Acceleration

Distance to the lens:

Length of structure;

Gradient;

Diameter of collimator at the entrance;

Equivalent of collimator

Diameter of irices;

External notenoidal field;

Further phase volume captured;

Litinm Lens:

Distance to the target;

Length;

Diameter;

Thicness of flanges;

Material of flanges;

Gradient;

Step of calculations;

CALCULATES at every stage:

Efficiency in given phase volume;

Polarization in given phase volume;

Beam dimensions;

Phase-space distributions;

Beam lengthening;

Energy spread within phase space;

Interactive code; Solenoidal lens will be added soon

Particles described by 2D array (matrix). One parameter numerates particles, the other one numerates properties associated with each particle: energy, polarization, angles to axes

Code has ~1400 rows;

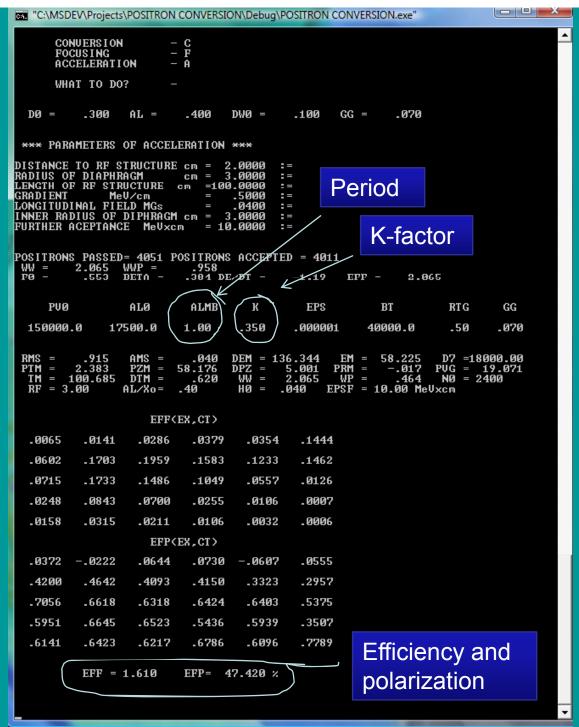
Will be added solenoidal lens;

Will be added more graphics;

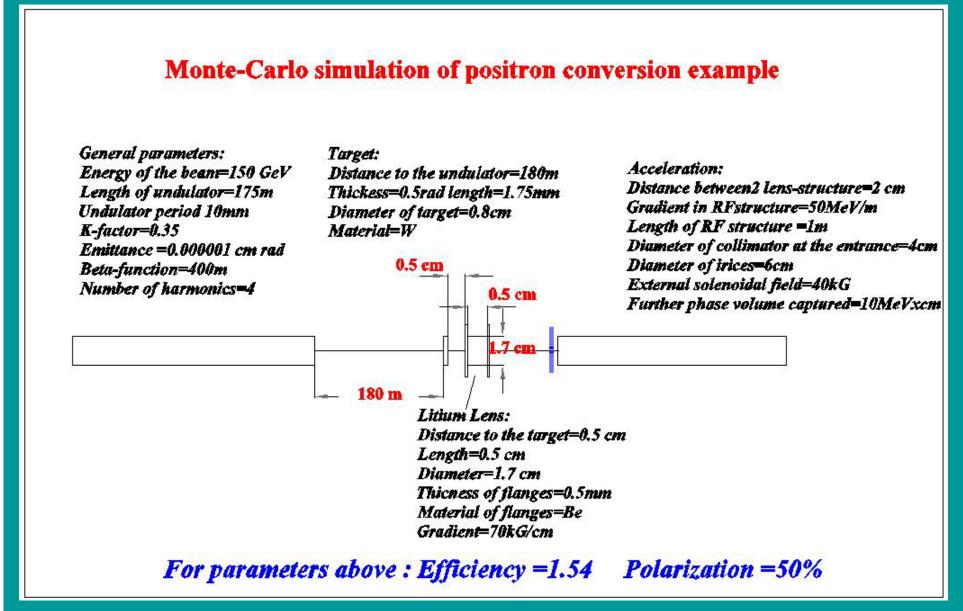
Possibility for the file exchange with graphical and statistical Codes (JMP);

Possibility for the file exchange with PARMELA;

Few seconds for any new variant



## Parameters optimized with KONN



So K-factor can be small, K<0.4, what brings a lot of relief to all elements of system

## Modeling of E-166 experiment

Phase space right after the target

```
- - X
"C:\MSDEV\Projects\POSITRON CONVERSION\Debug\POSITRON CONVERSION.exe"
        WHAT TO DO?
   *** SYSTEM PARAMETERS ***
INITIAL MOMENTA ,MeV
                                 =150000.0 :=49000
LENGTH OF UNDULATOR,cm = 17500.0 :=100
K FACTOR
                                        .350 :=.17
PERIOD OF ONDULATOR. cm = 1.000 :=.254
DISTANCE TO THE TARGET = 18000.0 :=3200
RADIUS OF TARGET, cm =
                                        .500 :=.15
RADIUS OF HOLE
EMITTANCE, cmxrad
BETTA-FUNCTION,
                         = .000 :=
= 1.000E-06:=
cm = 40000.0 :=4000
LENGTH OF TARGET/Xo
                                 = .400 :=.5
STEP OF CALCULATION =
HARMONICS INDEX 0; <5 =
NUMB.OF PART ON 1 H =24
                                       .100
 TOTAL NUMBER OF PHOTONS = MAX ENERGY OF QUANTA = GAMMA =
   POSITRONS ACCEPTED = 5000
                                        POSITRONS GENERATED = 30820
ENERGY OF QUANTA = 8.741 BETA = 1.274 EFF = .003 PU0 = 49000.0

LENGTH OF UNDUL. = 100.0 PERIOD = .25 PT2 = .03 EPT = .0000010

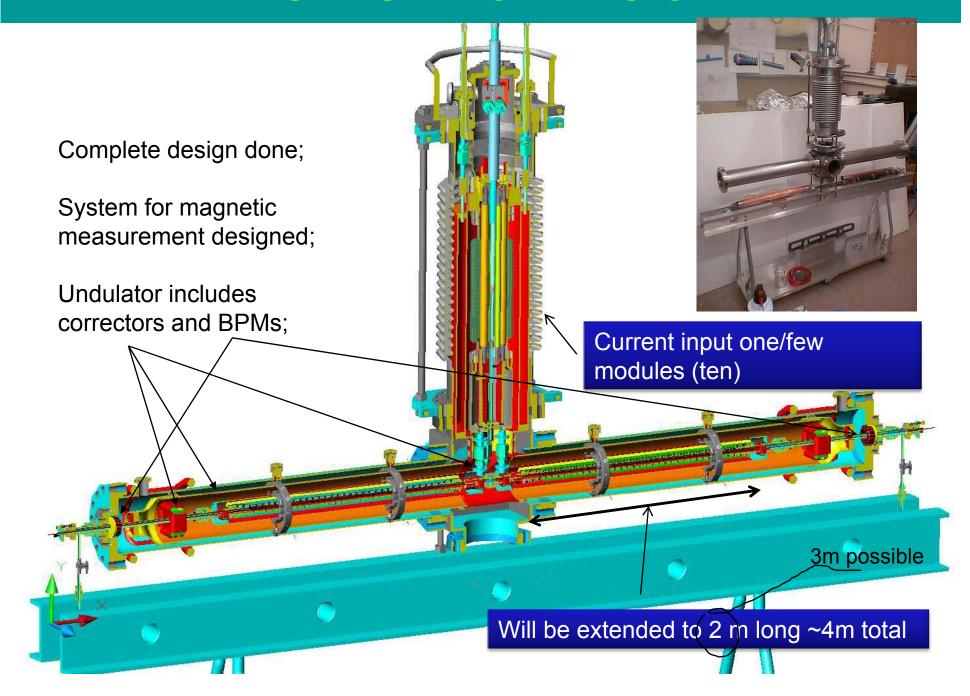
BT = 4000.0 RTG = .15 F0 = -.091 RMS = 1.138 AMS = .894

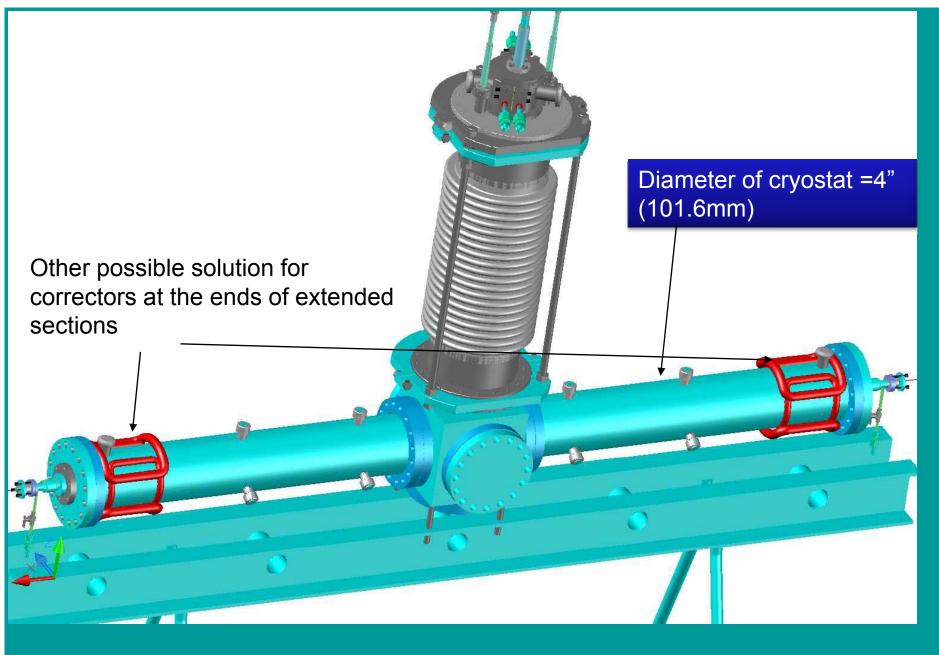
XU = .072 NUMBER OF PARTICLES BY FIRST HARMONIC = 2400

PHOTONS/e = 1.014 GAMMA = 95890.4
                           EFF(EX,CT)
   .0000
             .0000
                        .0000
                                              .0001
                                                         .0001
                                   .0001
   .0001
             .0001
                        .0002
                                   .0002
                                              .0002
                                                         .0003
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                                              .0002
                                                         .0004
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                        .0000
                                   .0000
                                              .0001
                                                         .0002
   .0000
             .0000
                        .0000
                                   .0000
                                              .0000
                                                         .0000
                           EFP(EX,CT)
   -.0336
           -.0927
                        .0143
                                 -.0414
                                            -.0172
                                                      -.0734
              .4170
   .4099
                         4039
                                   .3911
                                              .3971
                                                         .2796
              .7675
                         7085
   .7835
                                   .7309
                                              .7255
                                                         .6872
   .8858
             .8004
                         .8221
                                   .8011
                                              .8528
                                                         .8420
                         .7001
                                   .6678
   .6790
             .6925
                                              .7615
                                                         .7450
```

Dependence of polarization seen in experiment

# **UNDULATOR DESIGN**





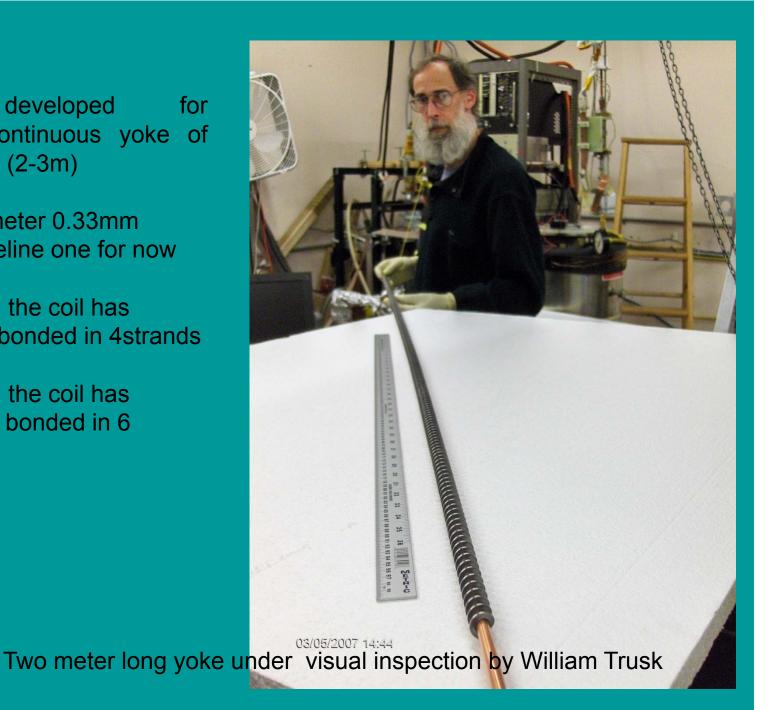
Cryostat expandable; shown with the terminals for Hall probe insertion; Field distribution will be measured in this cryostat; will be tested with beam

developed Technology for fabrication of continuous yoke of necessary length (2-3m)

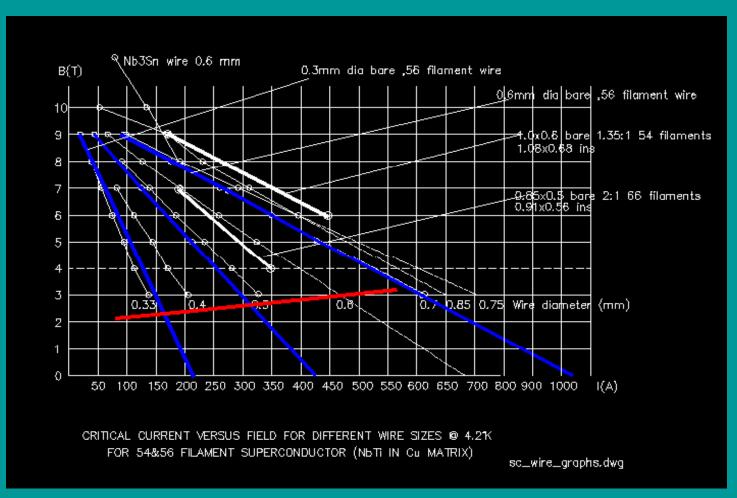
Wire having diameter 0.33mm chosen as a baseline one for now

For 10mm period the coil has 8(z)x11(r) wires; bonded in 4strands

For 12mm period the coil has 12(z)x12(r) wires bonded in 6 strands

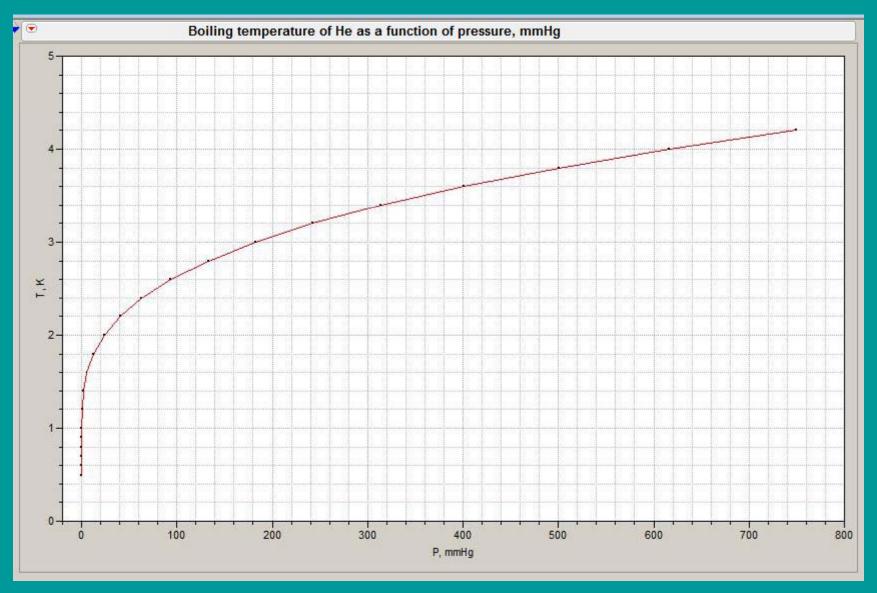


## Wires for undulator



All new wire is a 56 filaments with SC to Cu ratio 1:0.9 We switched to 0.3 mm bare from 0.6 bare Wounding with bonded tape of four and six wires in parallel

# Operation at lower pressure of He



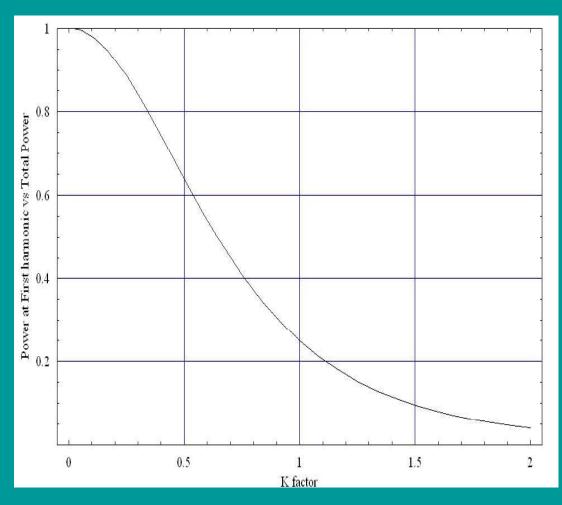
Dewar sealed and used for low pressure experiments; two oil pumps deliver vacuum down to -24"Hg with Helium level covering the undulator

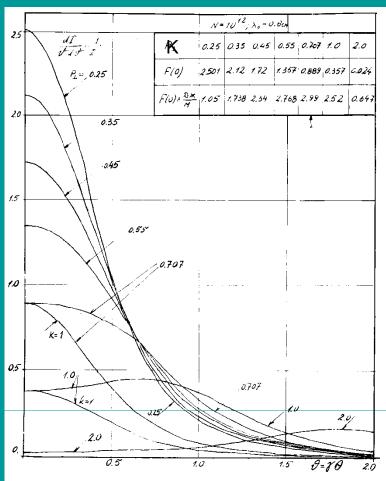
## For Dewar pumped down -24"Hg (-609.6mmHg), the temperature ≈ 3 °K



Measured excitation curve for undulator with 8mm aperture, wire-0.33 mm, 56 filaments Random point; spread of amplitudes~5%

# No need for K factor to be high This is useful for higher polarization





Ratio of Power radiated at first harmonics to the all power in all angles

Angular distribution of intensity of radiation for different K

# **ILC Beam parameters**

 $ge_x$ =8 10<sup>-6</sup> m rad -high edge  $ge_y$ =8 10<sup>-8</sup> m rad -high edge  $b_v$  ~200 m

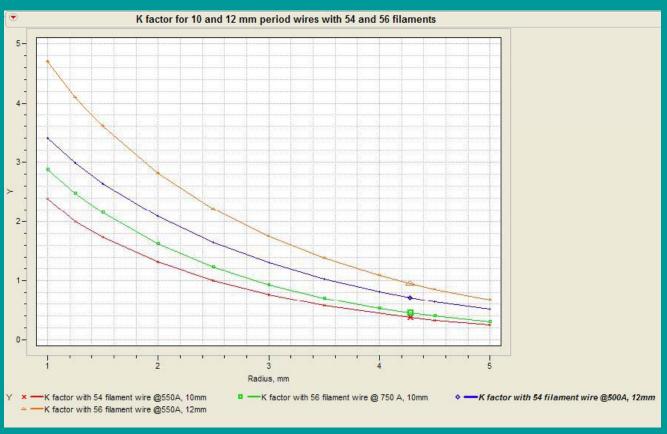
Angular spread in radiation	$\alpha \sim \sqrt{1+K^2}/\gamma$	$3 \cdot 10^{-6} \ (K=1)$
Angular spread in beam, vert.	$y' \cong \pm \sqrt{\gamma \varepsilon_z / \beta \gamma}$	$3.5 \cdot 10^{-8}$
Angular spread in beam, rad.	$y' \cong \pm \sqrt{\gamma \varepsilon_z / \beta \gamma}$	$3.5 \cdot 10^{-7}$
Radius of helix	$a \cong \lambda_u K / \gamma$	$5 \cdot 10^{-7} cm \ (K=1)$
Beam size, vertical	$\sqrt{\langle y^2 \rangle} \cong 2 \times \sqrt{\gamma \varepsilon_y \beta / \gamma}$	$1.4 \cdot 10^{-3} cm$
Beam size, radial	$\sqrt{\langle x^2 \rangle} \cong 2 \times \sqrt{\gamma \varepsilon_x \beta / \gamma}$	$1.4 \cdot 10^{-2} cm$

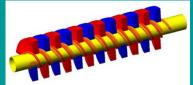
50 sigma ~7 mm; At the beginning of operation one can expect emittance degradation

That is why we have chosen as big aperture as possible -- Ø8 mm clear.

This 8 mm diameter allows K~0.4-0.5

# K factor as function of radius of undulator chamber

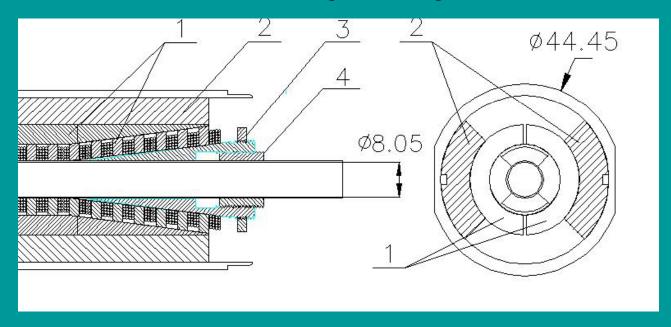




NbTi wire 56 filaments demonstrate best properties

Sectioning coil in radial direction allows further enhancement

# End region design



Details of design. 1–Iron yoke, 2–Copper collar, 3, 4–trimming Iron nuts. Inner diameter of Copper vacuum chamber is 8mm clear.



Period kept even

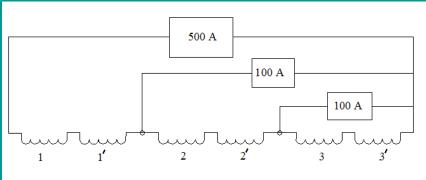


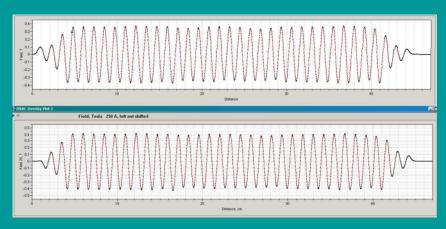
We developed simplified tapering allowing smooth end without diameter expansion

# Sectioned coils for undulators









10 mm undulator operated with two PS 500+50 A; 4x6 wires (0.6mm in diam. bare) Undulator 12 mm feed with one PS;

In a future there will be <3 PS for coils sectioned in radial direction

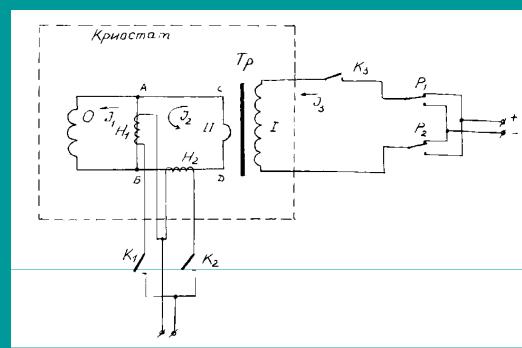
## **Identification of losses in joints**

Tested SC transformer scheme to identify time decay (losses in joints)

For undulator with 36 turns decay time found to be ~400 sec (5joints)

This defines the resistance to be  $<1E-15\Omega$ 

This scheme used in 1986 to feed SC undulator

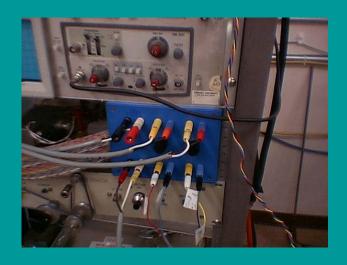


Scheme allows to work with captured flux



SC transformer with keys

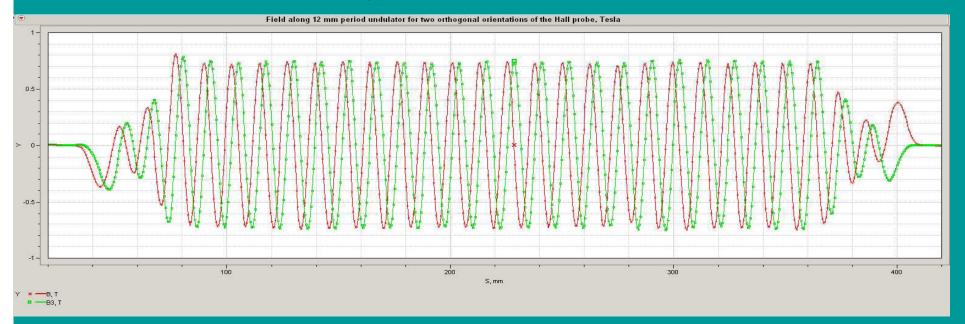


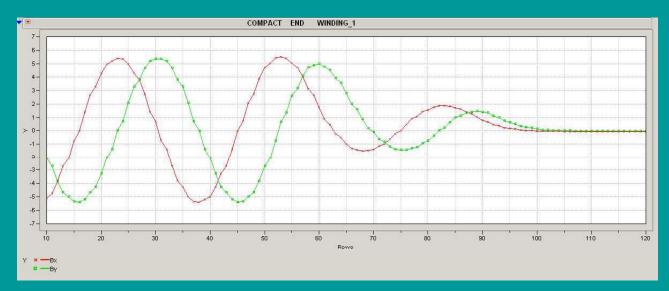


Distribution box for switches

SC transformer installation— at the left

# Typical field distribution





Simplified tapering

#### Undulators tested so far

## Aperture available for the beam is 8 mm in Ø clear

### **OFC vacuum chamber, RF smoothness**

SC wire	54 filaments	56 filaments	56 filaments	56 filaments
# layers	5*	6*	11***	9** (12***) +sectioning
λ=10 mm @ <i>300 °K</i>	K=0.36 tested	K=0.42 tested	K=0.467 tested	K≈0.5 (calculated)
λ=12 mm@ <i>300 °K</i>	K=0.72 tested	K=0.83 tested		K≈1 (calculated)

\*) Wire – Ø0.6 mm bare

\*\*) Wire – Ø0.4 mm bare

\*\*\*) Wire – Ø0.3 mm bare

## For aperture diam. 1/4" we expect for period 10mm K=0.7; for period 12mm K=1.2



Two sections of 45 cm long each will be measured in cryostat to the end of this year; The plan is to test it with the beam at Cornell ERL test module setup.

4m long prototype will be assembled in general to the end of 2007, Field distribution will be measured earlier in 2008

# **TARGET DESIGN**

Ti rotating wheel target is under development at Livermore, SLAC, Daresbury.

# We are looking for some other guarantied solutions

Ti needle target

Liquid metal target with Pb/Bi or Hg

Spinning compact W disk

Sandwich type target with W+Ti → New

Together

FlePDE model calculates temperature and pressure according equations

$$\nabla(k\nabla T) + \dot{Q} = \rho c_V \dot{T}$$

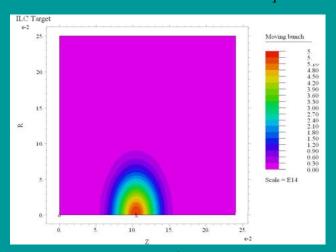
$$\dot{P} - \nabla(c_0^2 \nabla P) = \frac{\Gamma}{V_0} \dot{Q}$$
Implemented pressure block
$$\dot{Q} = \sum_i \frac{2cQ_{bunch}}{\pi\sqrt{\pi}\sigma_z\sigma_{\perp\gamma}^2 l_T} \frac{z}{l_T} \exp\left(-\frac{(z+z_0-c(t-i\cdot i_0))^2}{\sigma_z^2}\right) \cdot \exp\left(-\frac{r^2}{\sigma_{\perp\gamma}^2}\right)$$

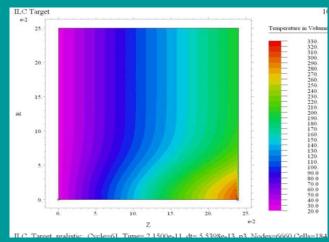
The thermal pressure  $p_T$  can be expressed

$$p_T = \boldsymbol{\Gamma}(V) \frac{c_V T}{V} = \boldsymbol{\Gamma}(V) \frac{\boldsymbol{\varepsilon}_T}{V}$$

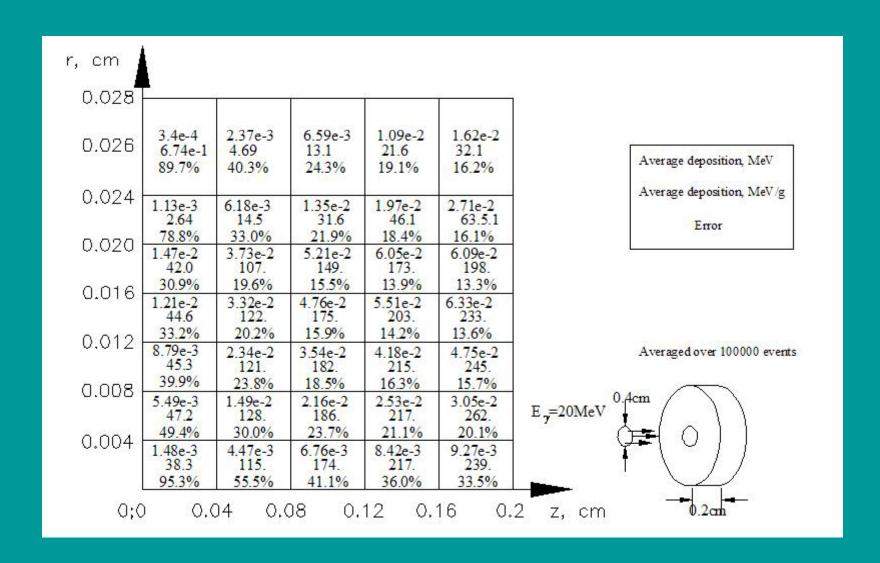
where  $\Gamma(V) = V/c_V(\partial P/\partial T_V)$  characterizing the ratio of the thermal pressure to the

specific thermal energy  $\epsilon_T/V$  called Grüneisen coefficient.





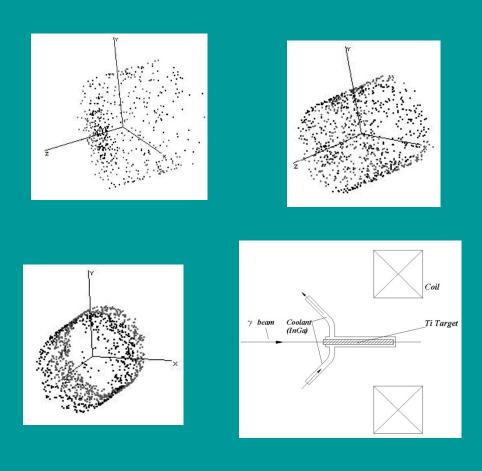
Instant position of the bunch moving in the target, at the left. Isotherms right after the bunch passage, at the right.

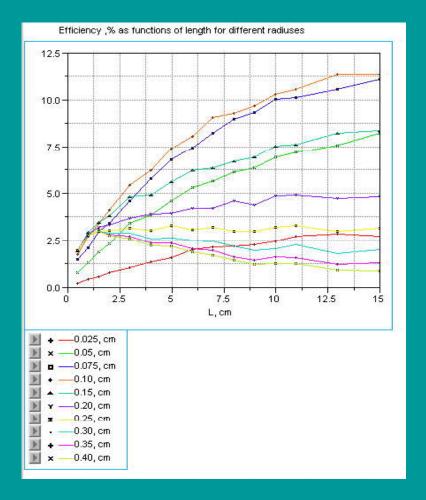


A.D.Bukin, A.A.Mikhailichenko," Optimized Target Strategy for Polarized Electrons and Positrons Production for Linear Collider". (IYF) BUDKER INP 92-76, Novosibirsk, 1992.

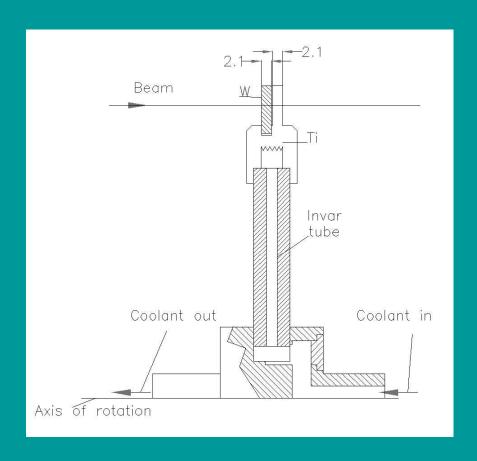
# Needle type target made from Ti

We are using numerically available codes to evaluate efficiency. Cylindrical target example





# Sandwich type target concept (earlier design) First layer (at the entrance is W, the last fraction might be Ti



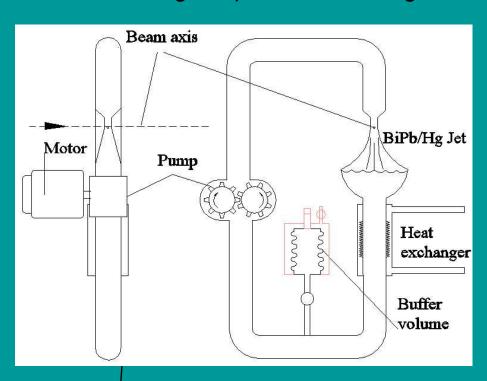


By this one can expect more compact design

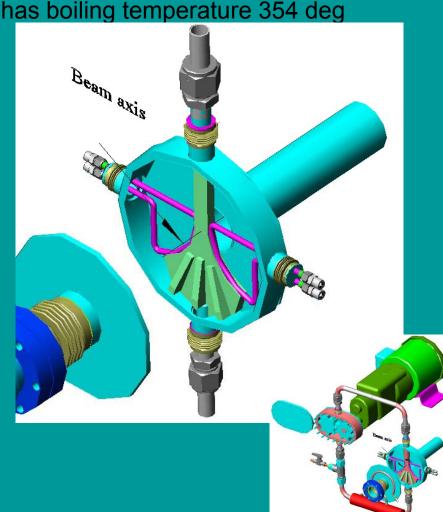
# **Liquid metal target**

High Z metals could be used here such as Bi-Pb, Mercury. InGa alloy also can be used here if filled with W powder.

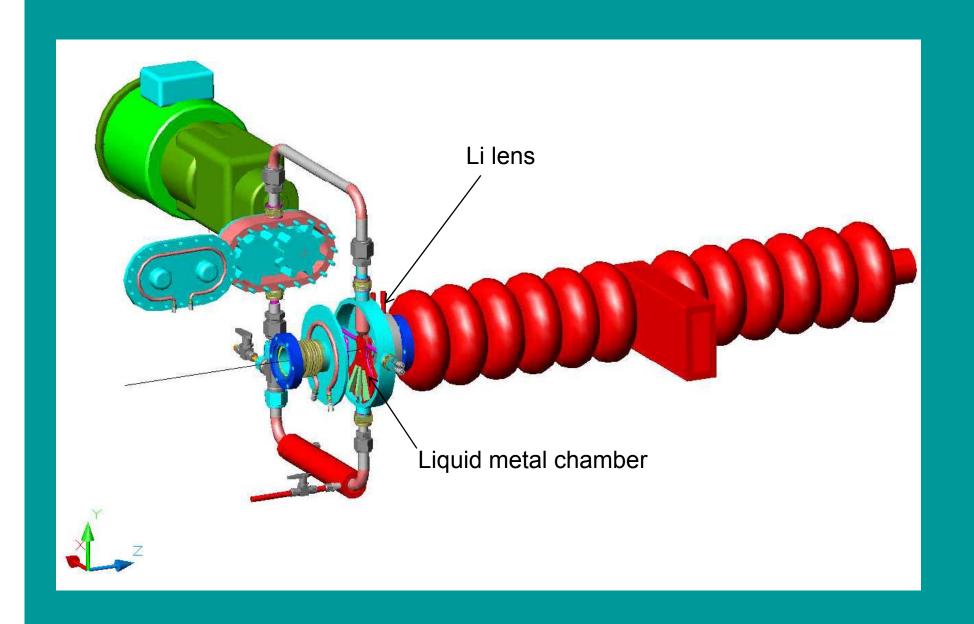
BiPb has melting temperature 154 deg C. Hg has boiling temperature 354 deg



Gear pump. Hg Jet velocity~10m/s
Calculations show absolute feasibility of this approach

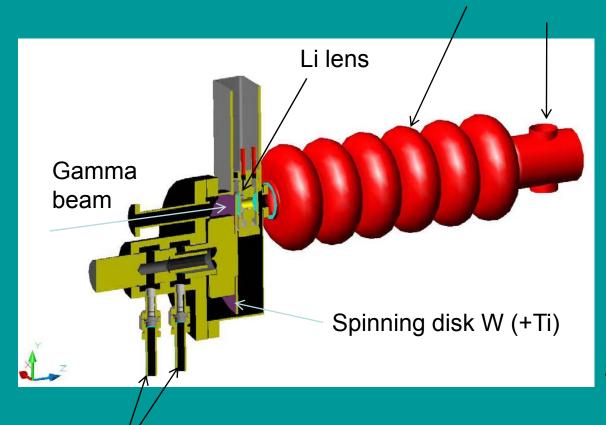


# Conversion unit with liquid metal target and Lithium lens (described below)

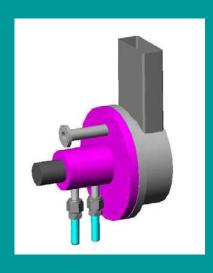


# Conversion unit on a basis of spinning W(+Ti) and Lithium lens

RF structure; input-far from the target side



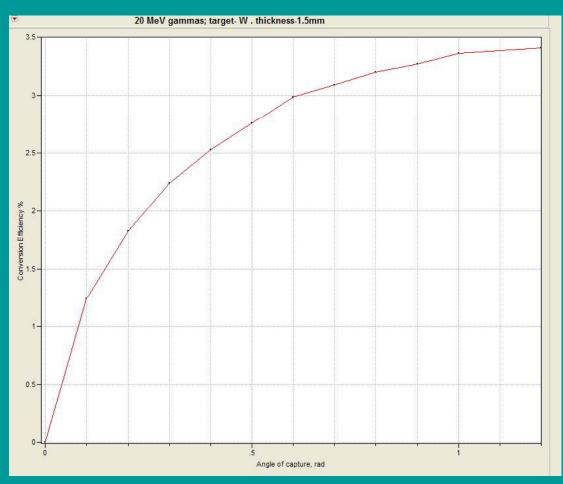
Coolant

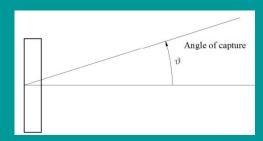


Size ~30cm in diameter

# **COLLECTION OPTICS DESIGN**

Efficiency= N<sub>e+</sub> /N<sub>gammas</sub>





Angle shown~0.3 rad

Target – Tungsten (W)

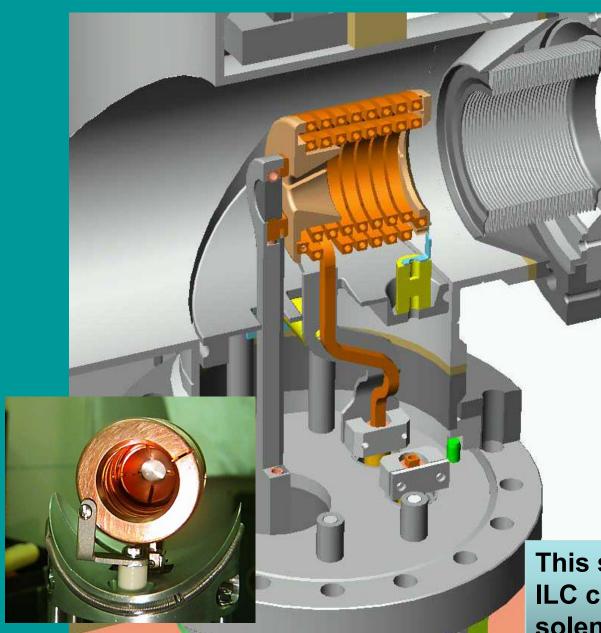
Thickness – 1.5 mm

20 MeV photons

Particles from 10 to 19 MeV only

Efficiency as function of capturing angle; within this angle the particles are captured by collection optics

## Many different systems possible here. Shown is Cornell positron capturing system



Efficiency of positron accumulation in CESR with system turned on/off changes 5 times;

This design introduced in 2000; it doubled positron accumulation in CESR, coming to 100 mA/min anytime (R=100m)

This serves as a prototype for ILC capturing system with solenoid (see below)

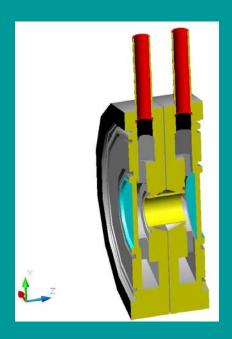
### Lithium lens basics

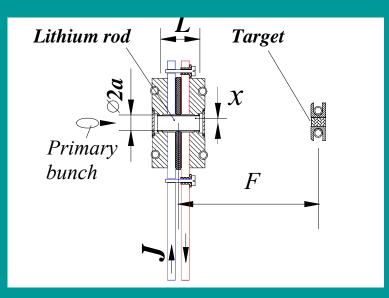
If steady current *I* runs through the round conductor having radius *a*, its azimuthal magnetic field inside the rod could be described as

$$H_{\vartheta}(r) = \frac{0.4\pi Ir}{2\pi a^2}$$

where magnetic field is measured in Gs, a –in cm, I –in Amperes. Current density comes to  $j_s = I / \pi a^2$  The particle, passed through the rod, will get the transverse kick

$$\alpha \cong \frac{H(x) \cdot L}{(HR)} \cong \frac{0.2ILx}{a^2 \cdot (HR)}$$





This picture drawn for the focusing of electron beam to the target

So the focal distance could be defined as the following

$$F \cong \frac{a^2 \cdot (HR)}{0.2IL}$$

If the focal distance is given, the current required could be found as

$$I \cong \frac{a^2 \cdot (HR)}{0.2FL}$$

For the primary electron beam of say, 20  $MeV(HR) \cong 66kGcm$ , Suggesting F=0.5 cm, L=2cm, a=0.5cm

$$I \cong \frac{0.5^2 \cdot 66}{0.2 \cdot 0.5 \cdot 2} = 83.25 kA$$

Scattering of the beam in a Lithium rod target could be estimated as  $\sqrt{<\theta^2>} \cong \frac{13.6 MeV}{pc} \sqrt{\frac{t_{Xo}}{X_{Li}}}$  where  $X_{e\!f\!f}$  —is an effective radiation length of Lithium,  $X_{Li} = 83.3 g / cm^2$  (or 156 cm),  $t_{Xo}$  —is the thickness of the rod in  $g/cm^2$ .  $\sqrt{<\theta^2>} \cong \frac{13.6}{20} \sqrt{\frac{2}{156}} \cong 0.077$  rad

Resistance of the 1 cm long 1 cm in diameter Lithium rod could be estimated as

$$R = \rho L / \pi a_{.}^{2} \cong 1.44 \cdot 10^{-5} \cdot 2 / \pi / 0.5^{2} \cong 3.7 \cdot 10^{-5}$$
 Ohm.

the instant power dissipation in the rod as big as  $P = I^2 \cdot R \cong 83.25^2 \cdot 10^6 \cdot 3.7 \cdot 10^{-5} = 2.5 \cdot 10^5$  W

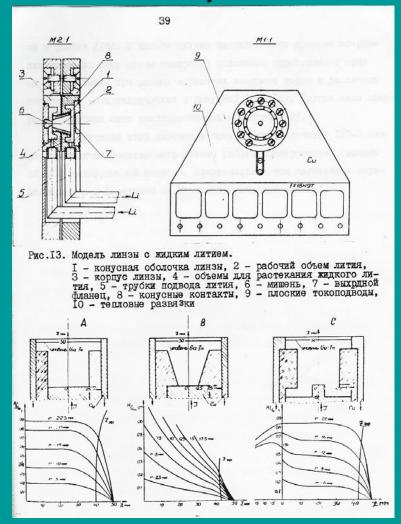
If the pulse lasts for au seconds with repetition rate f, Hz, then the average power dissipation will be  $< P >= J^2 \cdot R \cdot f au$ 

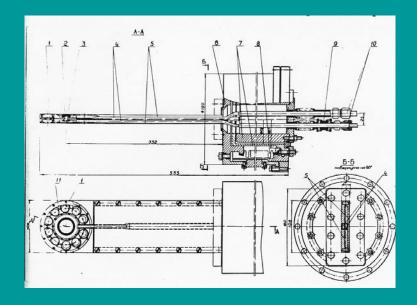
. For 
$$f$$
=5 $Hz$ ,  $\tau \cong 2ms$  the last goes to  $\langle P \rangle = 2.5 \cdot 10^5 \cdot 5 \cdot 2 \cdot 10^{-3} \cong$  2.5  $kW$ 

This is much, much easier, than for focusing of (anti) protons.

## T.A. Vsevolojskaja, A.A. Mikhailichenko, G.I. Silvestrov, A.D. Cherniakin

"To the Conversion System for Generation of Polarized Beams in VLEPP", BINP, 1986





1-ex-centric contact pushers;2-conic lens body; 3-W target; 4-Ti tubing for LI supply; 5-flat current leads; 6-vacuum chamber; 7-coaxial fraction of current leads; 8-bellows; 9-ceramic insulators; 10-conical gasket; 11-set of ex-centric pushers.

Field measured in liquid Gallium model.

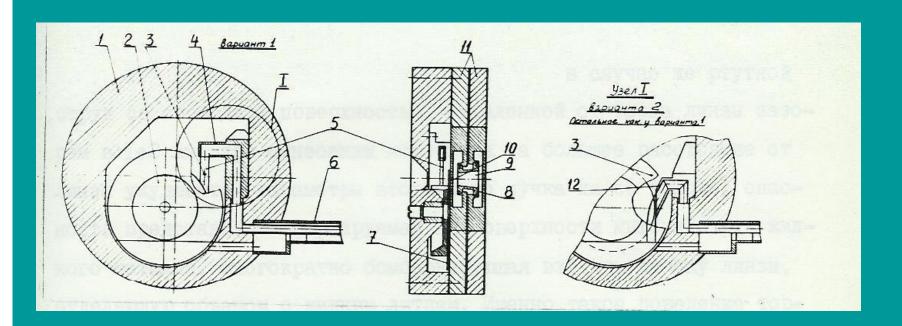
A-cylindrical lens with homogenous current leads supply at the end

B- conical lens with the same current feed

C –lens with cylindrical target at the entrance flange

## The same report

Two possibilities were considered at the time: 1-Mercury jet 2-W disc spin by Gallium Just reminding, that for VLEPP project the beam with 10<sup>12</sup> electrons/positrons was used



Variant 1-Mercury jet, Variant 2-spinning W disc, 1-case, 2-disc, 3-beam axis, 4-feeding tube for Hg, 5-Hg jet, 6-tubes, 7-Protective Ti disc, 8-Lithium lens container, 9-Liothium volume, 10- entrance flange of the lens, 11-current leads, 12-Ga jet nozzle.

Energy deposition in Be flanges is going by secondary particles (positrons and electrons) is  $\delta E \sim 2 \ MeV cm^2/g$ , Secondary beam diameter  $d \approx 1 \ cm^2$ . Area illuminated is going to be S=1/4  $\pi d^2 \approx 0.4 \ cm^2$ . Volume density of Be is  $\rho \approx 1.8 \ g/cm^3$ , for thickness 0.5 mm Energy deposited in a material of flange going to be

$$\Delta E \approx \delta E \cdot \rho \cdot t/1 cm \approx 2 \cdot 1.8 \cdot 0.05 \approx 0.2 MeV$$
 per particle

So the total energy deposited by train of  $n_b$  bunches with population N each, comes to

$$E_{tot} \cong \Delta E \times N \times n_b \times e$$
 Joules,

where *e* stands for the charge of electron. The last expression goes to be

$$E_{tot} \cong 1.8 J.$$
 Although e defocused

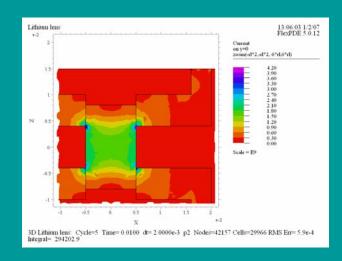
Factor reflecting spare particles,  $\sim 1.5-2$ , factor two- reflecting equal amount of electrons and positrons and, finally, factor reflecting enciency of capturing ( $\sim 30\%$ ). So the final number comes to  $\rightarrow \approx 21J$ .

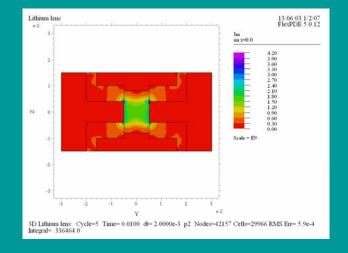
Temperature gain by heat capacity of Be  $C_v \approx 1.82 \ J/g/degC$  comes to

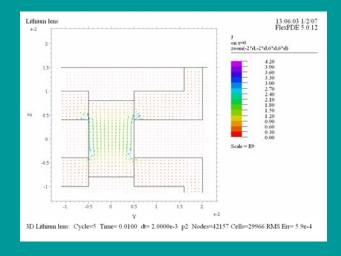
$$\Delta T \cong \frac{E_{tot}}{mC_v} \cong \frac{E_{tot}}{\rho SlC_v} \cong \frac{21}{1.8 \times 1.82 \times 0.05 \times 0.2} \cong 660 \text{ deg.}$$

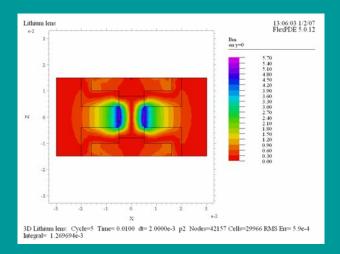
One needs to add the initial temperature which is above melting point of Lithium, coming to maximal temperature ~850-900 deg. Meanwhile the melting temperature of Be is 1278 deg, so it withstands.

### Recent calculation of Lithium lens done with FlexPDE® code

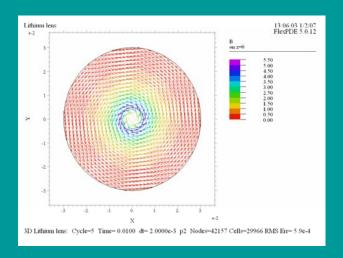


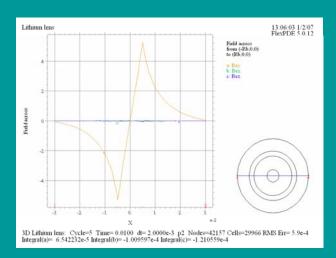


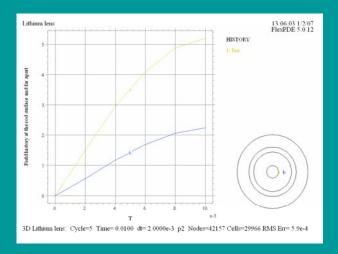


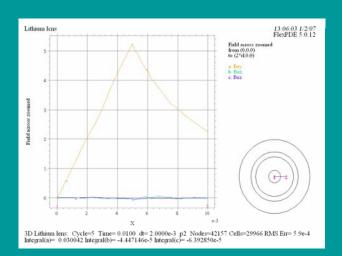


### Spatial field distribution over time (cinema)







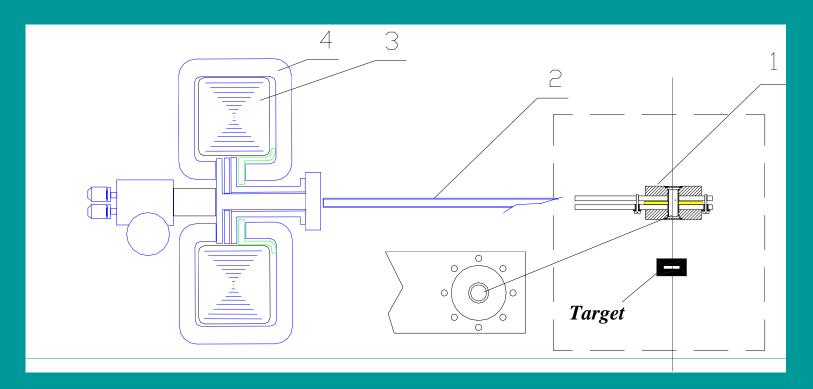


Power dissipated per pulse goes to 0.6 kJ for the current ~135 kA and time duration half sin wave with period 40 msec

Energy stored -21.6 J so reactive component is low.

(Dissipation for time from zero to 10 msec is 0.3 kJ)

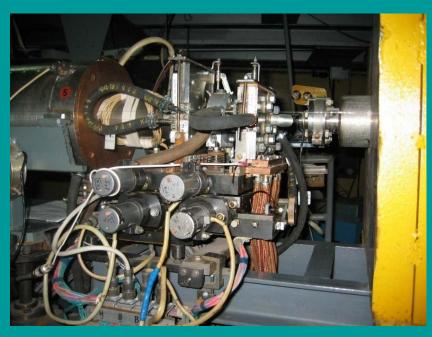
Feeding with 5<sup>th</sup> harmonic allows making current flat.



The transformer with Lithium Lens (example). 1-fixture, 2-flat coaxial line, 3-transformer yoke, 4-cable windings. Lens with a current duct could be removable from the beam path.

### Doublet of Lithium lenses in Novosibirsk BINP

Photo- courtesy of Yu Shatunov





First lens is used for focusing of primary 250 MeV electron beam onto the W target,

Second lens installed after the target and collects positrons at ~150MeV

Number of particles in pulse ~2E+11; ~0.7Hz operation (defined by the beam cooling in Damping Ring)

Lenses shown served ~30 Years without serious problem (!)

### Li lens resume

Utilization of Lithium lens allows Tungsten survival under condition required by ILC with  $N_e \sim 2x10^{10}$  with moderate  $K \sim 0.3$ -0.4 and do not require big-size spinning rim (or disc). Thin W target allows better functioning of collection optics (less depth of focusing).

Liquid targets as Pb/Bi or even Hg allows further increase of positron yield.

Lithium lens (and x-lens) is well developed technique.

Usage of Li lens allows drastic increase in accumulation rate, low K-factor.

Field is strictly limited by the surface of the lens from the target side.

Plan is to repeat optimization of the cone angle in Li rod.

### Solenoidal lens instead of Li lens

One can equalize the focal length of the Lithium lens and the solenoidal one

$$\frac{1}{f} \cong \frac{GL}{(HR)} = \frac{\int H_{\parallel}^{2}(s)ds}{4(HR)^{2}} \qquad \int H_{\parallel}^{2}ds \equiv H_{\parallel \max}^{2} \cdot L \cdot \eta = 4(HR)GL$$

where (HR) = pc/300 stands for magnetic rigidity.

Typically longitudinal continuity  $L\eta \approx 1.5 \div 2D$ , where D stands for diameter of solenoidal lens. The Lithium lens has the length L=0.5cm. Diameter of solenoidal lens is something about 5 cm, then for HR) =100 kGcm (for 30 MeV particles), one can obtain

$$H_{\parallel \text{max}}^2(s) = \frac{4 \cdot 150 \cdot 100}{15} = 4000 \text{ kG}^2$$

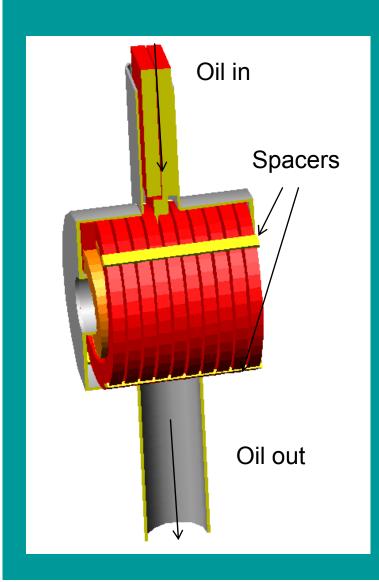
So the maximal field comes to  $H_{\parallel \text{max}} \cong 63\text{kG}$  (for 30MeV particles)

For generation of such field the amount of Ampere-turns required goes to be

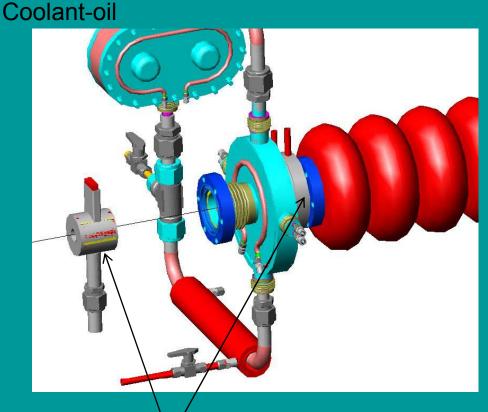
$$nJ \cong \frac{H_{\parallel \text{max}} \Lambda}{0.4\pi \cdot n}$$
 262 kAxturns (again, for 30 MeV particles)

No flux concentrator possible for 1 msec; skin~3-4mm

Solenoidal lens could be designed with dimensions ~ a bit larger than the Lithium lens



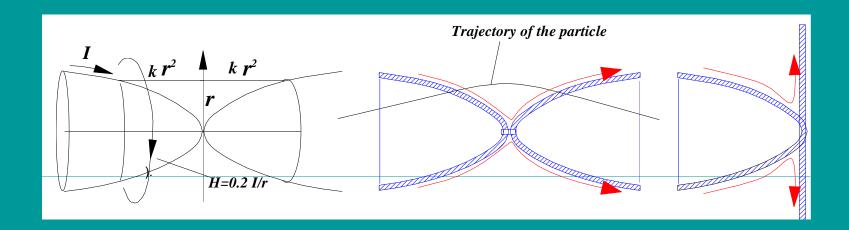
For the number of turns =20, current in one turn goes to  $I_1\sim15$  kA during~10msec duty time; Two harmonics for feeding current. Conductor cross-section~ 5x10mm<sup>2</sup>;



Lenses in comparison; for Li lens current leads are not shown

### Other focusing possibilities to be mentioned

Other short –focusing elements-such as horn, can be used here as well. Design also was done, horn lens, so called x-lens was at service for positron capture for may years at BINP (G. Budker, G. Silvestrov)



So the device has ideal dependence for linear focusing. The focal distance of this lens goes to  $F = \frac{(HR)}{0.4 Ik}$ .

As the particles here going through material of the horn, it manufactured usually from Aluminum (  $X_{Al} = 24.3g/cm^2 [\cong 9cm]$  ) or Beryllium (  $X_{Be} \cong 66g/cm^2 [\cong 35.8cm]$  ).

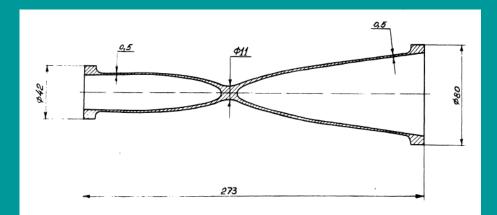


Fig. 2a Special profile of the "linear" lens.

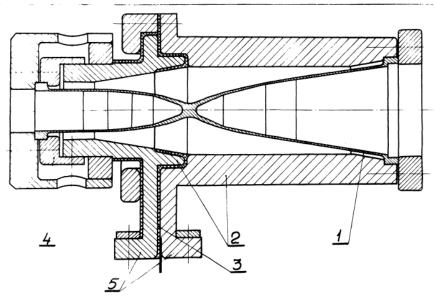


Fig. 2b Sectional view of the "linear" lens

- 1 lens body
  2 coaxial conductor
  3 insulation
- 4 damping device for demountable contact
- 5 flat conductor for connection to the transformer.

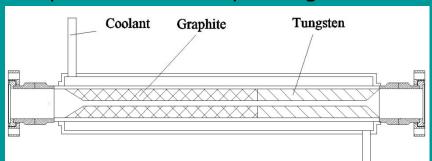
# **COLLIMATORS**

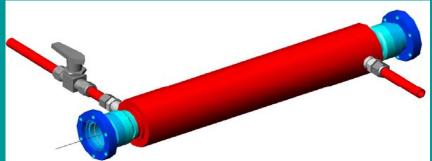
- **√** Collimator for gammas
- **√** Collimators for full power primary beam

 See A.Mikhailichenko, "Collimators for ILC", PAC 2006, European Particle Accelerator Conference (EPAC 06), Edinburgh, Scotland, 26-30 Jun 2006. Proceedings, pp.807-809

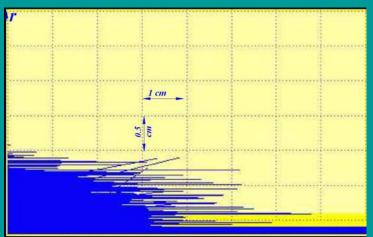
### **Collimator for gammas**

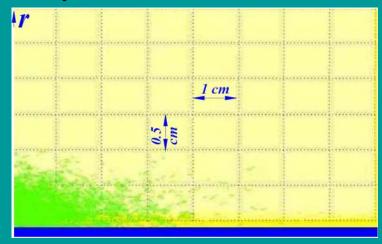
Pyrolytic Graphite (PG) is used here. The purpose of it is to increase the beam diameter, before entering to the W part. Vacuum outgassing is negligible for this material. Heat conductivity ~300 W/m-oK is comparable with meals. *Beryllium* is also possible here, depending on task.





Transverse dimensions defined by Moliere radius



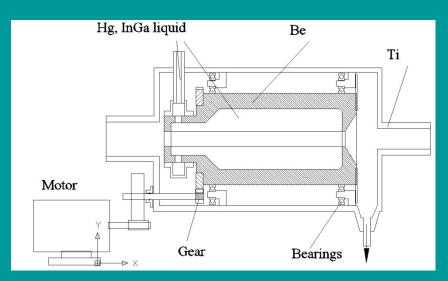


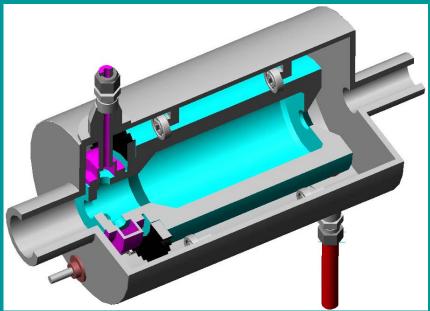
Gamma-beam.  $s_g$ = 0.5cm, diameter of the hole (blue strip at the bottom) d=2 mm. Energy of gamma-beam coming from the left is 20 MeV.

Positron component of cascade

# **High power collimator**

This a liquid metal one. Liquid formed a cylinder as result of rotation and centrifugal force





High average power collimator. Beam is coming from the right.

# PERTURBATION OF EMITTANCE AND POLARIZATION

 See A.Mikhailichenko, CBN 06-1, Cornell
 LEPP, 2006.

Fragment from CBN 06-1

#### Kinematical perturbations due to multiple scattering in a target

Let us consider the possible effect of kinematical depolarization associated with rotation of spin vector while particle experience multiple scattering in media of target before leaving. Typically polarized positron carries out  $\simeq (0.5\text{-}1)\hbar\omega$  -energy of gamma quanta. As positrons/electrons created have longitudinal polarization, it is good to have assurance that during scattering in material of target polarization is not lost. Each act of scattering is Coulomb scattering in field of nuclei. So BMT equation describing the spin  $\vec{\zeta}$  motion in electrical field of nuclei looks like

$$\frac{d\vec{\zeta}}{dt} = \frac{e}{mc^2 \gamma} \left\{ G\gamma + \frac{\gamma}{\gamma + 1} \right\} \cdot \vec{\zeta} \times \left( \vec{E} \times \vec{v} \right), \tag{A16}$$

where  $\vec{E} \sim Ze\vec{r}/r^3$  stands for repulsive (for positrons) electrical field of nuclei, factor  $G = \frac{g-2}{2} \cong 1.1596 \times 10^{-3} \approx \frac{\alpha}{2\pi}$ . Deviation of momentum is simply  $d\vec{p}/dt = e\vec{E}$ .

So the spin equation becomes

$$\frac{d\vec{\zeta}}{dt} = \frac{1}{mc^2 \gamma} \left\{ G\gamma + \frac{\gamma}{\gamma + 1} \right\} \cdot \vec{\zeta} \times \left( \frac{d\vec{p}}{dt} \times \vec{v} \right). \tag{A17}$$

We neglected variation of energy of particle during the act of scattering, so  $\frac{d\vec{p}}{dt} \cong m\gamma \frac{d\vec{v}}{dt}$  and vector  $\vec{p}$  just changes its direction. Introducing normalized velocity as usual  $\vec{\beta} = \vec{v}/c$ , equation of spin motion finally comes to the following

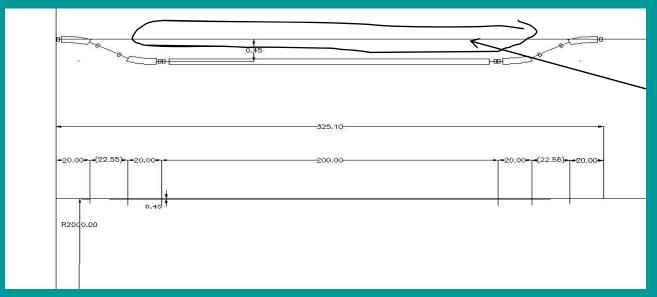
$$\frac{d\vec{\zeta}}{dt} = \left\{ G\gamma + \frac{\gamma}{\gamma + 1} \right\} \cdot \vec{\zeta} \times (\dot{\vec{\beta}} \times \vec{\beta}) = \left\{ G\gamma + \frac{\gamma}{\gamma + 1} \right\} \cdot \vec{\zeta} \times \frac{d\vec{\phi}}{dt}, \tag{A18}$$

where  $\varphi$  stands for the scattering angle and the vector  $\underline{d} \varphi / \underline{dt}$  directed normally to the scattering plane. For intermediate energy of our interest  $\gamma \sim 40$ , so the term in bracket  $\sim 1$  and, finally

$$\frac{d\vec{\zeta}}{dt} \cong \vec{\zeta} \times \frac{d\vec{\boldsymbol{\varphi}}}{dt}.$$
 (A19)

The last equation means that spin rotates to the same angle as the scattering one, i.e. spin follows the particle trajectory.

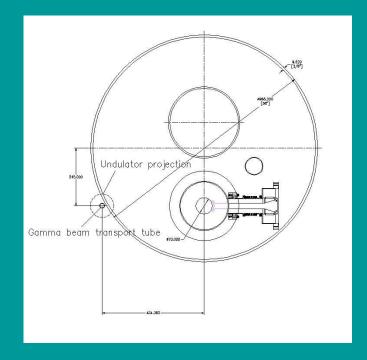
# **UNDULATOR CHICANE**



This space can be used for accelerator -"keep alive" source

[1] V.V. Vladimirsky, D.G. Koshkarev, "The Achromatic Bending Magnet System", Instr. Exp. Tech., (USSR), (English Translation) N6, 770(1958).

[2] T.A.Vsevolojskaya, A.A.Mikhailichenko, G.I Silvestrov, A.N. Cherniakin, "To the Project of Conversion System for Obtaining Polarized Beams at VLEPP Complex", unpublished internal report BINP, Novosibirsk, 1986.



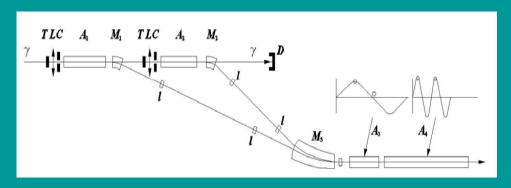
# **COMBINING SCHEME**

After the first target only 13% of photons are lost. So it is possible to install second target and collect positrons from this second target.

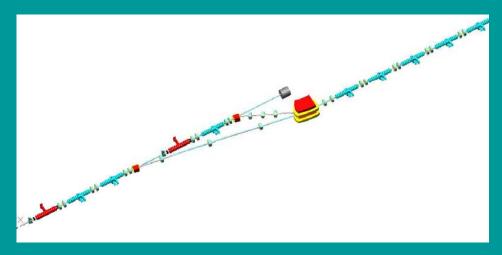
Combining in longitudinal phase space could be arranged easily in the same RF separatrix in damping ring.

Additional feed back system will be required for fast dump of coherent motion.

This combining can help in reduction of power deposition in target if each target made thinner, than optimal.



Energy provided by acceleration structures A1 and A2 are slightly different, A1>A2.



Combining scheme allows ~double positron yield and cut in half the length of undulator

## CONCLUSIONS

Restored start to end code for Monte-Carlo simulation of conversion; Confirmed low K factor possible here; K<0.4 with period 10 mm

For 500 GeV, a conversion system requires more efforts; one solution is to move the system as a whole to a new 150 GeV point.

Tested 10 and 12 mm period undulators, aperture 8 mm, ~40 cm each; Reached K=0.467 for 10 mm period with for 56 filament wire diameter 0.33mm; Longitudinal field profile measured; Reached K=0.83 for 12 mm period undulator wire 0.63mm;

Pumping of Helium was tested, gain >10%;

Radial sectioning will be implemented in the following models

### Our calculations show that these parameters satisfy ILC

4-m long Undulator module fabrication and its test is a priority job→ end 2007;

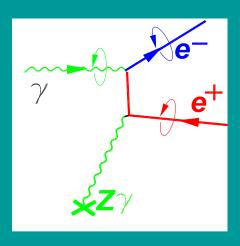
Helical iron yokes of 3 m long obtained from industry;

Wire 0.33 used for latest model; strands x4(used) and by x6 (obtained).

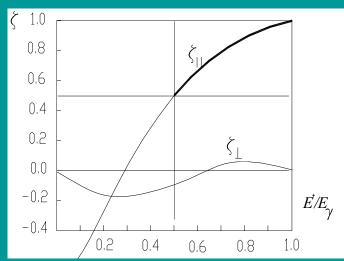
Designed undulator with 6.35mm aperture, K~0.7 for 10mm; and K~1.2 for 12mm

Target, collection optics and spin handling are in scope of our interest.

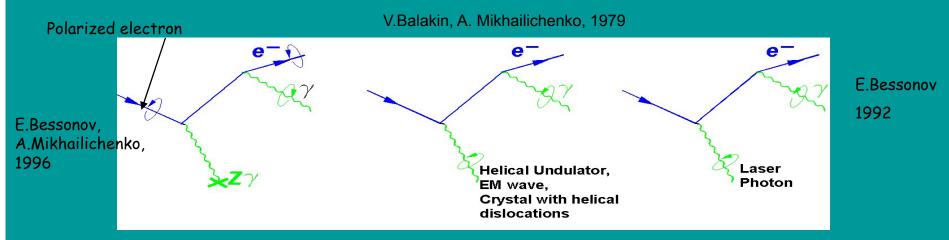
# Polarized e<sup>±</sup> production



The way to create circularly polarized positron, left. Crossdiagram is not shown. At the right-the graph of longitudinal polarization - as function of particle's fractional energy



### The way to create circularly polarized photon



Polarization of positrons is a result of positron selection by energy

$$\vec{\zeta} = \xi_2 \cdot \left[ f(E_+, E_-) \cdot \vec{n}_{\parallel} + g(E_+, E_-) \cdot \vec{n}_{\perp} \right] = \vec{\zeta}_{\parallel} + \vec{\zeta}_{\perp}$$

# Two-year Budget, in then-year K\$

Item	9/07- 8/08	9/08- 8/09	Total
Other Professionals	31.0	32.55	63.55
Graduate Students	21.8	23.762	45.562
Undergraduate Students	5.0	5.250	10.25
Total salaries and Wages	57.8	61.562	119.362
Fringe Benefits	10.23	10.742	20.972
Total Salaries, Wages and Fringe Benefits	68.03	72.304	140.334
Equipment	25	49	74
Travel and transportation	7.5	7.5	15
Materials and Supplies	30	45	75
Other direct costs	19.528	21.286	40.814
Subcontract	0	0	0
Total direct costs	153.33	195.089	345.147
Indirect costs	62.263	73.634	135.897
Total direct and indirect costs	212.321	268.723	481.044