

SECOND INTERNATIONAL ACCELERATOR SCHOOL FOR LINEAR COLLIDERS

October 1 -10, 2007 ~ Ettore Majorana Center, Erice (Sicily), Italy



Topics

Linear Collider Basics • Super Conducting & Warm RF Technology • Beam Dynamics of Collider Linac & Damping Rings • ILC and Its Major Systems • CLIC • Detectors and Physics

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Deadline for online application: June 1, 2007
<http://www.linearcollider.org/school/2007/>

Number of students is limited
Students will receive financial aid, including travel

Lecture 7

Beam Delivery & beam-beam

Andrei Seryi
SLAC



Fermilab

PPARC



IN2P3



HER



SLAC



ELAN





Linear Collider – two main challenges

- **Energy** – need to reach at least 500 GeV CM as a start

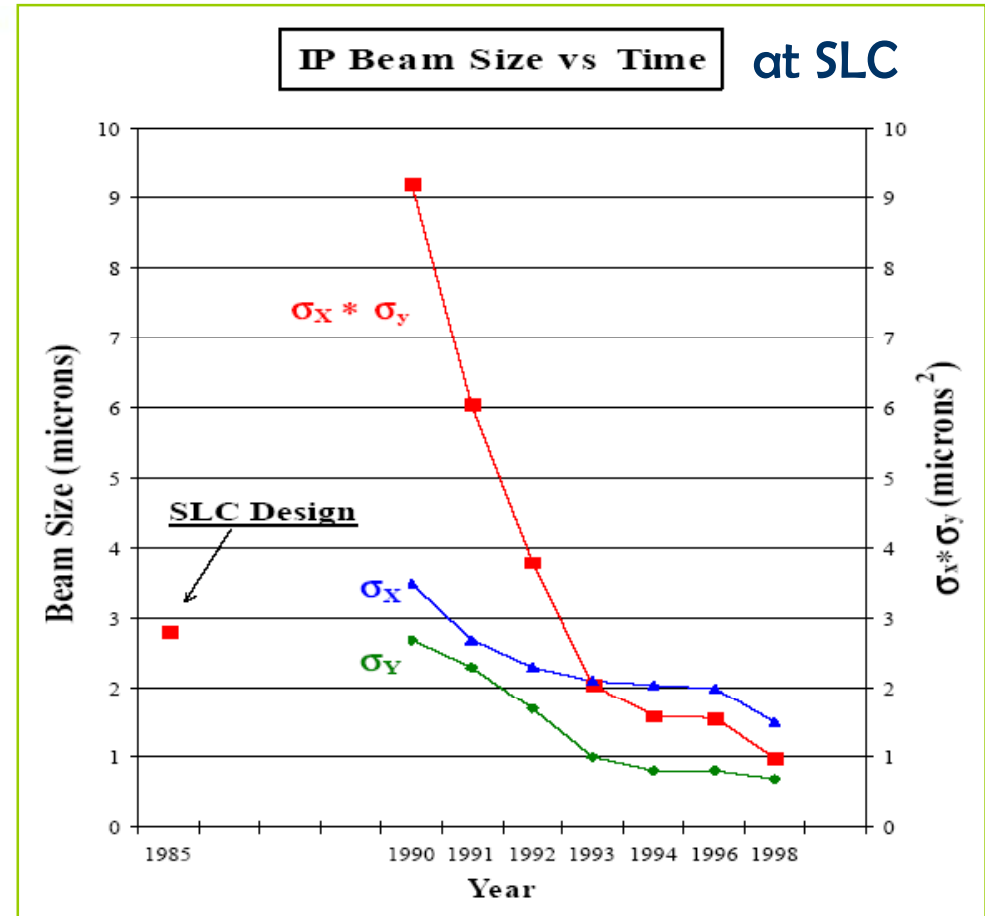


- **Luminosity** – need to reach 10^{34} level



The Luminosity Challenge

- Must jump by a Factor of 10000 in Luminosity !!! (from what is achieved in the only so far linear collider SLC)
- Many improvements, to ensure this : generation of smaller emittances, their better preservation, ...
- Including better focusing, dealing with beam-beam, safely removing beams after collision and better stability



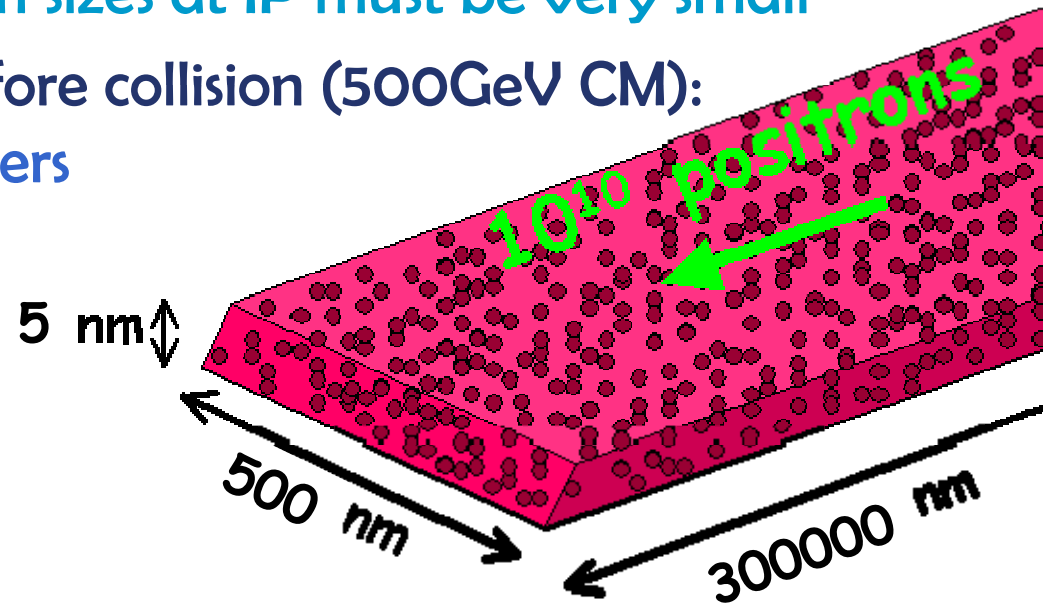
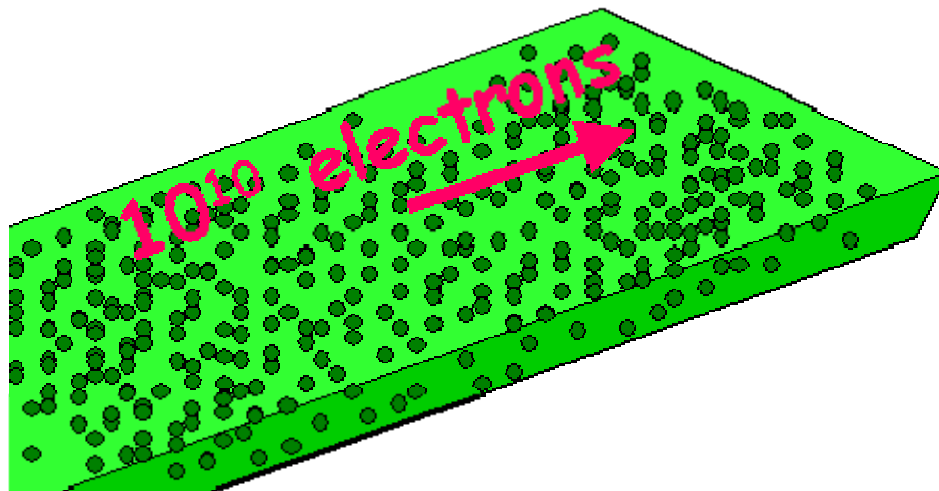


How to get Luminosity

- To increase probability of direct e^+e^- collisions (luminosity) and birth of new particles, beam sizes at IP must be very small
- E.g., ILC beam sizes just before collision (500GeV CM):
500 * 5 * 300000 nanometers

(x y z)

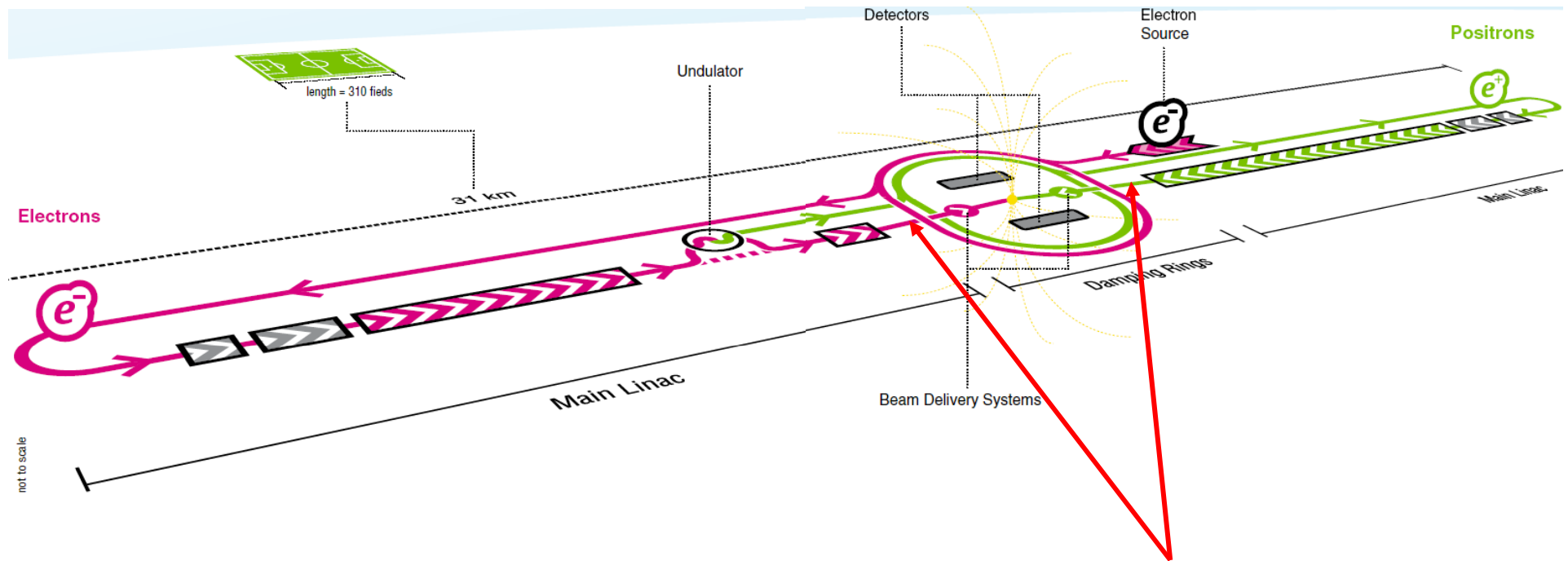
↑
Vertical size
is smallest



$$L = \frac{f_{rep}}{4\pi} \frac{n_b N^2}{\sigma_x \sigma_y} H_D$$



BDS: from end of linac to IP, to dumps

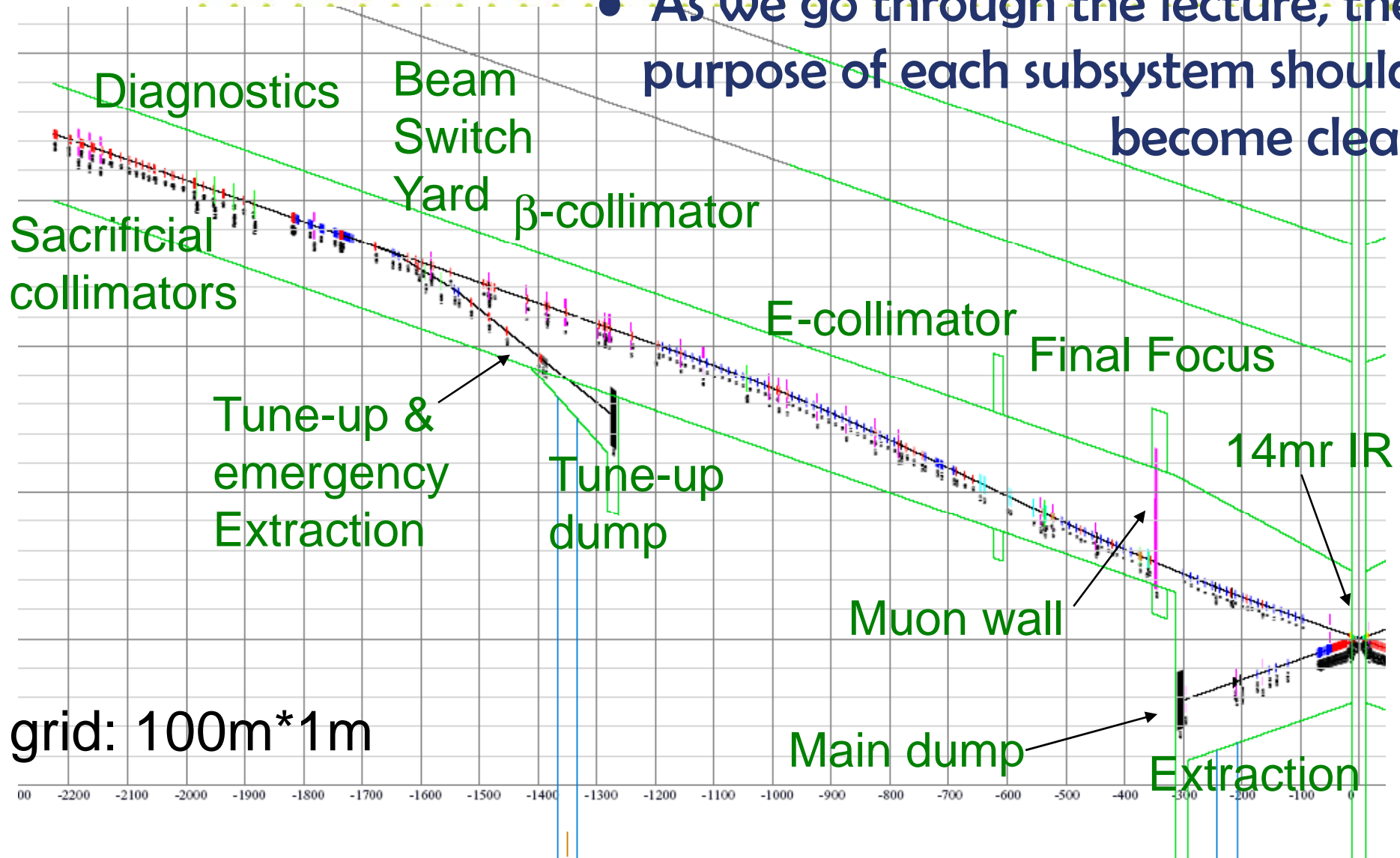


Beam Delivery System (BDS)



Beam Delivery subsystems

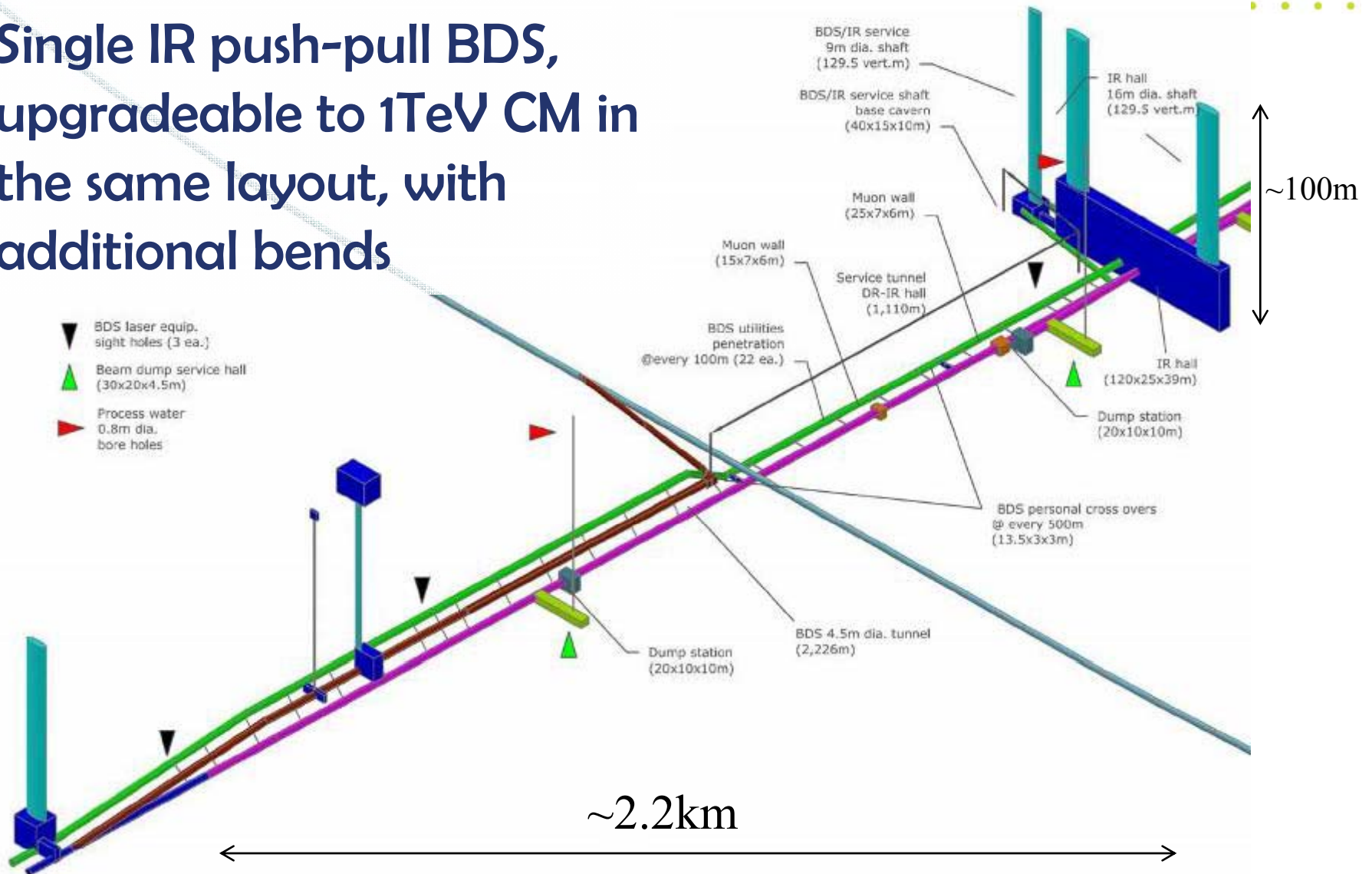
- As we go through the lecture, the purpose of each subsystem should become clear





Layout of Beam Delivery tunnels

- Single IR push-pull BDS, upgradeable to 1TeV CM in the same layout, with additional bends





Beam Delivery System challenges



- measure the linac beam and match it into the final focus
- remove any large amplitude particles (beam-halo) from the linac to minimize background in the detectors
- measure and monitor the key physics parameters such as energy and polarization before and after the collisions
- ensure that the extremely small beams collide optimally at the IP
- protect the beamline and detector against mis-steered beams from the main linacs and safely extract them to beam dump
- provide possibility for two detectors to utilize single IP with efficient and rapid switch-over



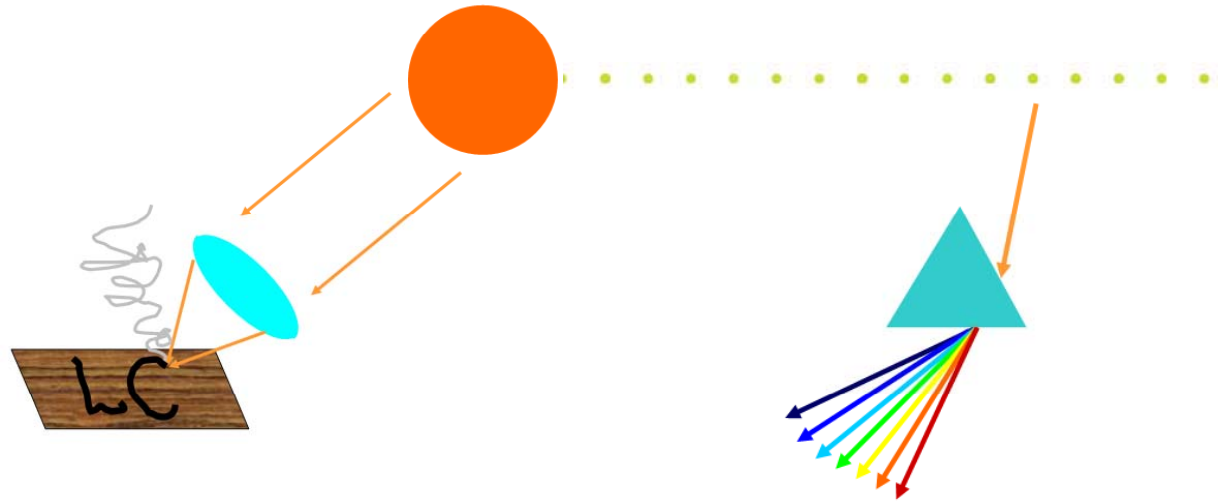
Parameters of ILC BDS

Length (linac exit to IP distance)/side	m	2226
Length of main (tune-up) extraction line	m	300 (467)
Max Energy/beam (with more magnets)	GeV	250 (500)
Distance from IP to first quad, L^*	m	3.5-(4.5)
Crossing angle at the IP	mrad	14
Nominal beam size at IP, σ^* , x/y	nm	655/5.7
Nominal beam divergence at IP, θ^* , x/y	μrad	31/14
Nominal beta-function at IP, β^* , x/y	mm	21/0.4
Nominal bunch length, σ_z	μm	300
Nominal disruption parameters, x/y		0.162/18.5
Nominal bunch population, N		2×10^{10}
Max beam power at main and tune-up dumps	MW	18
Preferred entrance train to train jitter	σ	< 0.5
Preferred entrance bunch to bunch jitter	σ	< 0.1
Typical nominal collimation depth, x/y		8-10/60
Vacuum pressure level, near/far from IP	nTorr	1/50

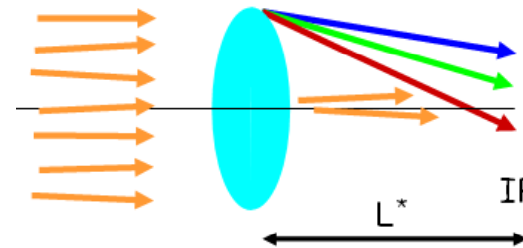


Factor driving BDS design

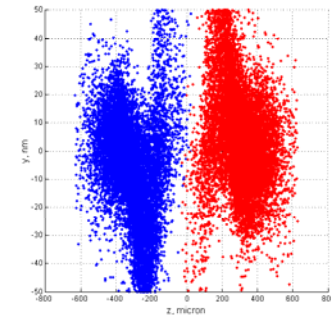
- Strong focusing



- Chromaticity



- Beam-beam effects



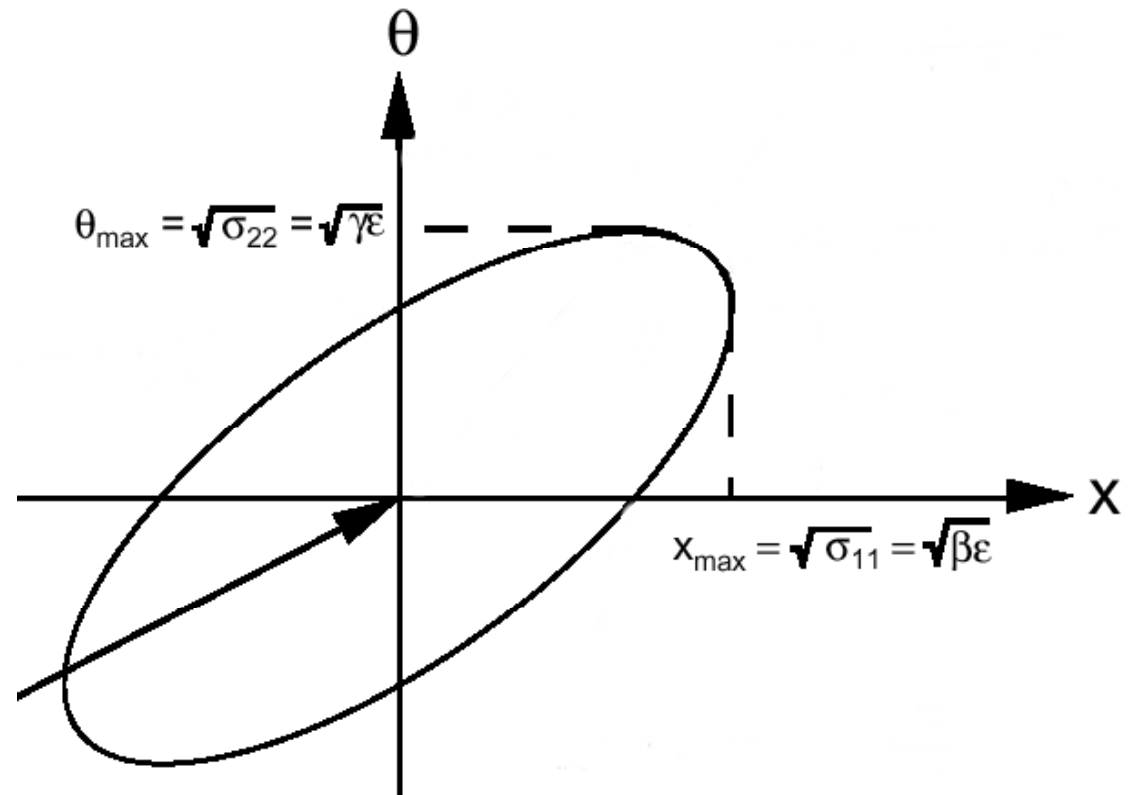
- Synchrotron radiation

– let's consider some of this in more details



Recall couple of definitions

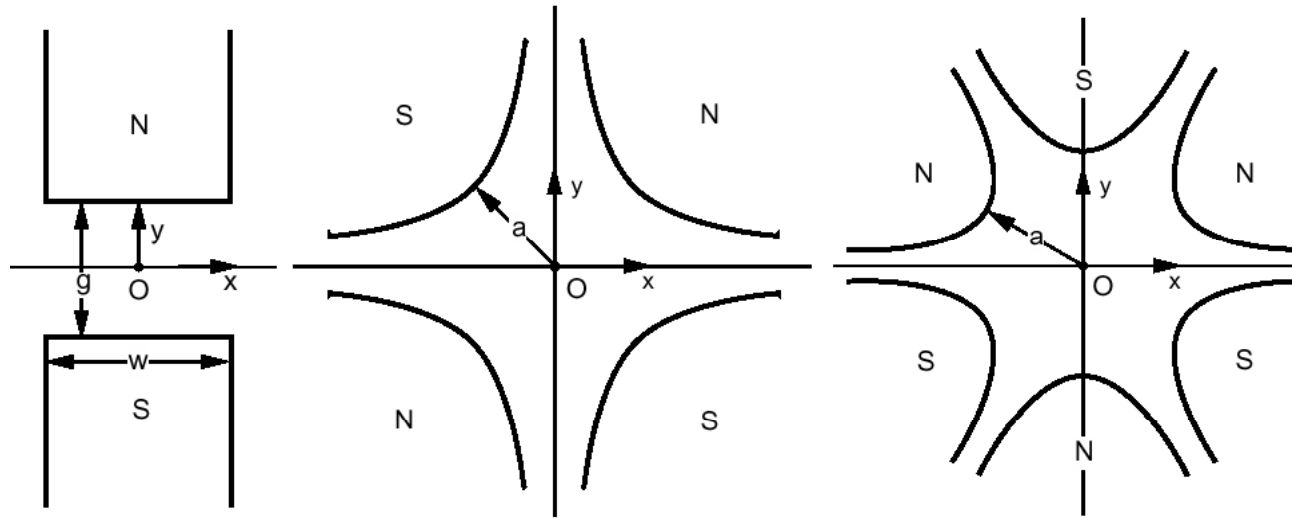
- Beta function β characterize optics
- Emittance ε is phase space volume of the beam
- Beam size: $(\varepsilon \beta)^{1/2}$
- Divergence: $(\varepsilon/\beta)^{1/2}$



- Focusing makes the beam ellipse rotate with “betatron frequency”
- Phase of ellipse is called “betatron phase”



What we use to handle the beam



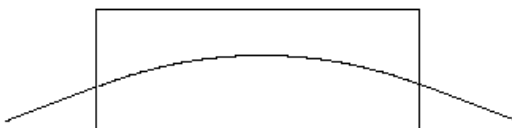
DIPOLE

QUADRUPOLE

SEXTUPOLE

Etc...

Just bend the trajectory



Focus in one plane,
defocus in another:

$$\begin{aligned} x' &= x' + G x \\ y' &= y' - G y \end{aligned}$$

Second order
effect:

$$\begin{aligned} x' &= x' + S (x^2 - y^2) \\ y' &= y' - S 2xy \end{aligned}$$

Here x is transverse coordinate, x' is angle



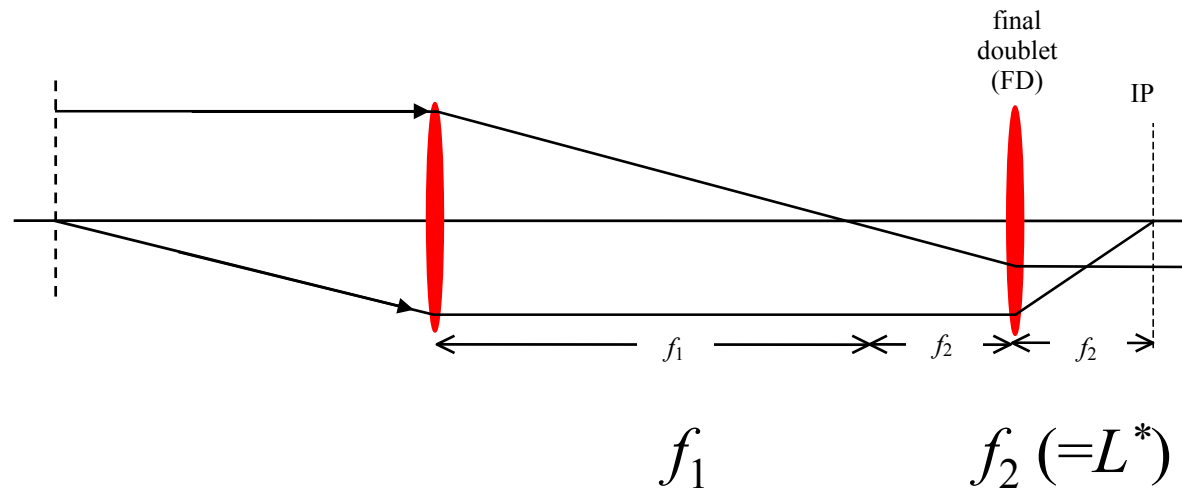
Optics building block: telescope

Essential part of final focus is final telescope. It “demagnify” the incoming beam ellipse to a smaller size. Matrix transformation of such telescope is diagonal:

$$R_{X,Y} = \begin{pmatrix} -1/M_{X,Y} & 0 \\ 0 & -M_{X,Y} \end{pmatrix}$$

A minimal number of quadrupoles, to construct a telescope with arbitrary demagnification factors, is four.

If there would be no energy spread in the beam, a telescope could serve as your final focus (or two telescopes chained together).



Use telescope optics to demagnify beam by factor $m = f1/f2 = f1/L^*$

Matrix formalism for beam transport:

$$x_i^{out} = R_{ij} x_j^{in}$$

$$x_i = \begin{pmatrix} x \\ x' \\ y \\ y' \\ \Delta l \\ \delta \end{pmatrix}$$

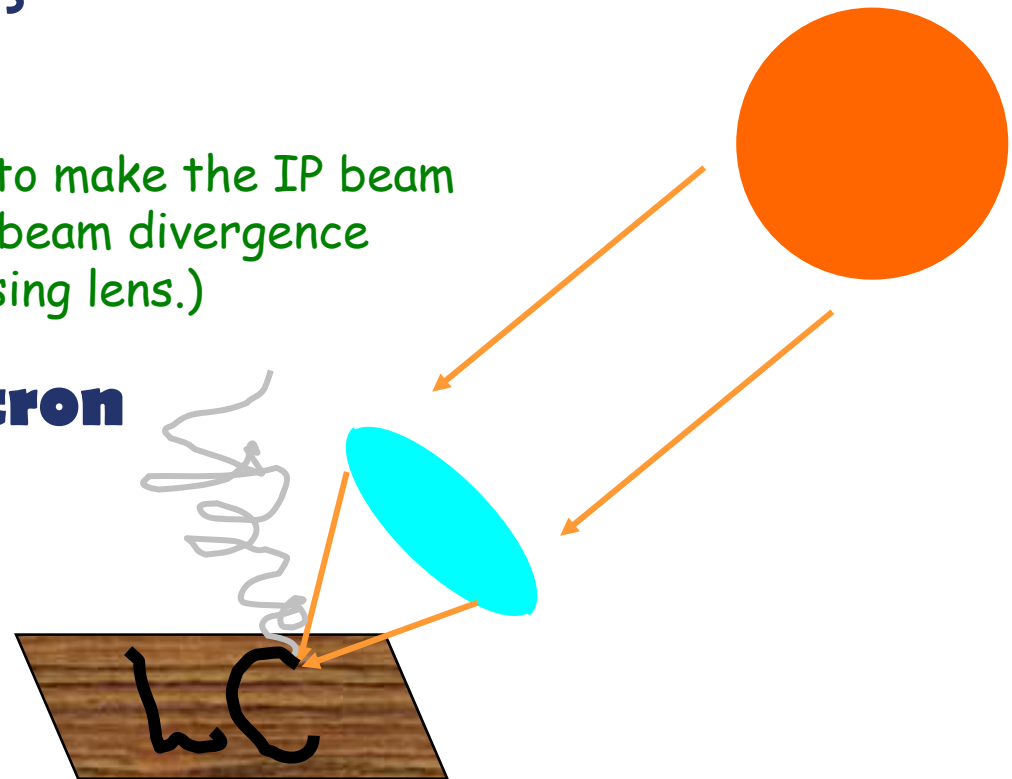


How to focus the beam to a smallest spot?

- If you ever played with a lens trying to burn a picture on a wood under bright sun, then you know that one needs a strong and big lens

(The emittance ϵ is constant, so, to make the IP beam size $(\epsilon \beta)^{1/2}$ small, you need large beam divergence at the IP $(\epsilon / \beta)^{1/2}$ i.e. short-focusing lens.)

- It is very similar for **electron** or **positron** beams
- But one have to use **magnets**





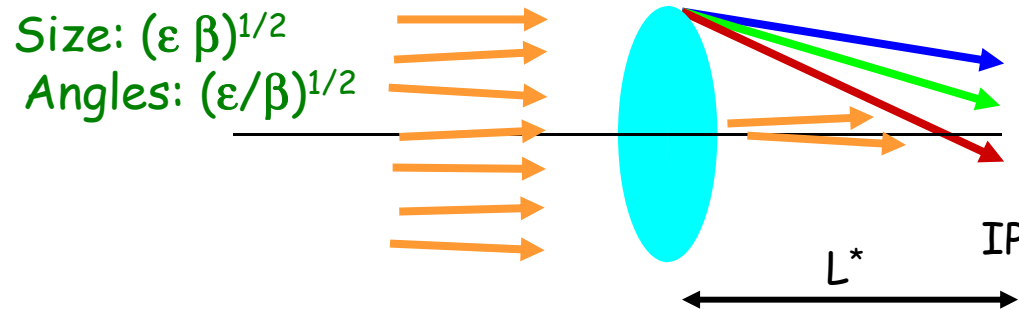
Why nonlinear elements

- As sun **light** contains different colors, **electron beam** has energy spread and get dispersed and distorted => **chromatic aberrations**
- For **light**, one uses lenses made from different materials to compensate chromatic aberrations
- Chromatic compensation for particle beams is done with **nonlinear** magnets
 - Problem: Nonlinear elements create **geometric** aberrations
- The **task** of **Final Focus system** (FF) is to focus the beam to required size and compensate aberrations





How to focus to a smallest size and how big is chromaticity in FF?



Size at IP:
 $L^* (\epsilon/\beta)^{1/2}$
+ $(\epsilon \beta)^{1/2} \sigma_E$

Beta at IP:
 $L^* (\epsilon/\beta)^{1/2} = (\epsilon \beta^*)^{1/2}$
 $\Rightarrow \beta^* = L^{*2}/\beta$

Chromatic dilution:
 $(\epsilon \beta)^{1/2} \sigma_E / (\epsilon \beta^*)^{1/2}$
 $= \sigma_E L^*/\beta^*$

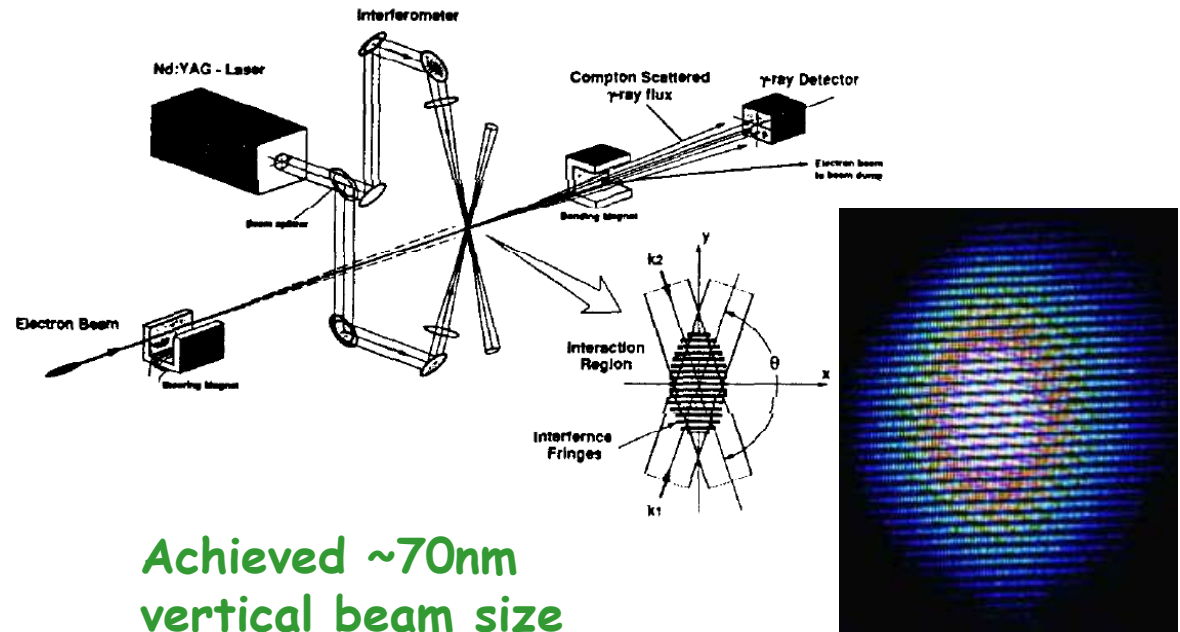
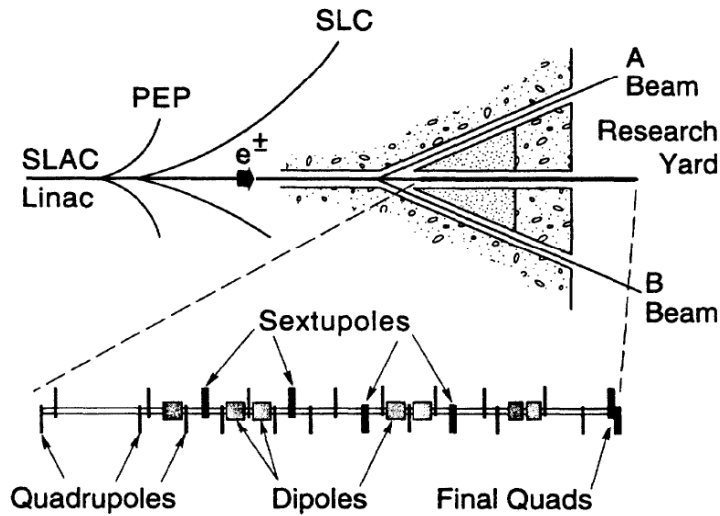
- The final lens need to be the strongest
 - (two lenses for both x and y => “Final Doublet” or FD)
- FD determines chromaticity of FF
- Chromatic dilution of the beam size is $\Delta\sigma/\sigma \sim \sigma_E L^*/\beta^*$

Typical: σ_E -- energy spread in the beam ~ 0.002-0.01
 L^* -- distance from FD to IP ~ 3 - 5 m
 β^* -- beta function in IP ~ 0.4 - 0.1 mm

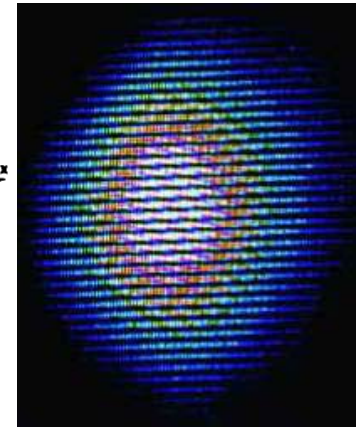
- For typical parameters, $\Delta\sigma/\sigma \sim 15-500$ too big !
- => Chromaticity of FF need to be compensated



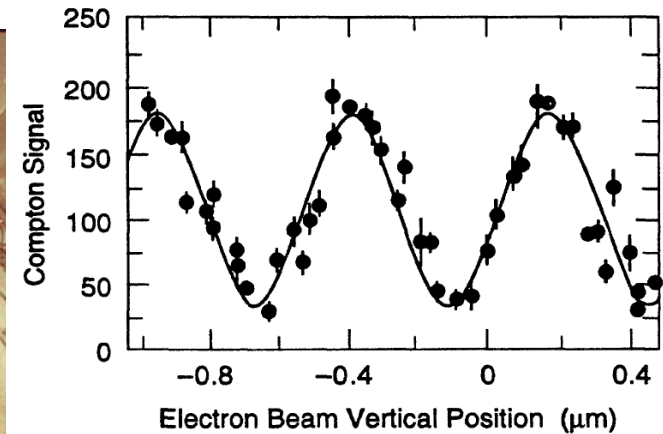
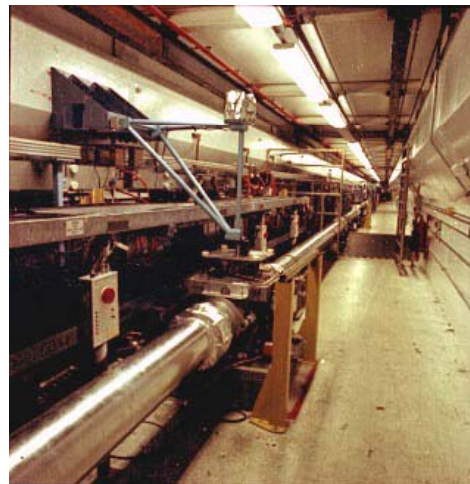
Final Focus Test Beam



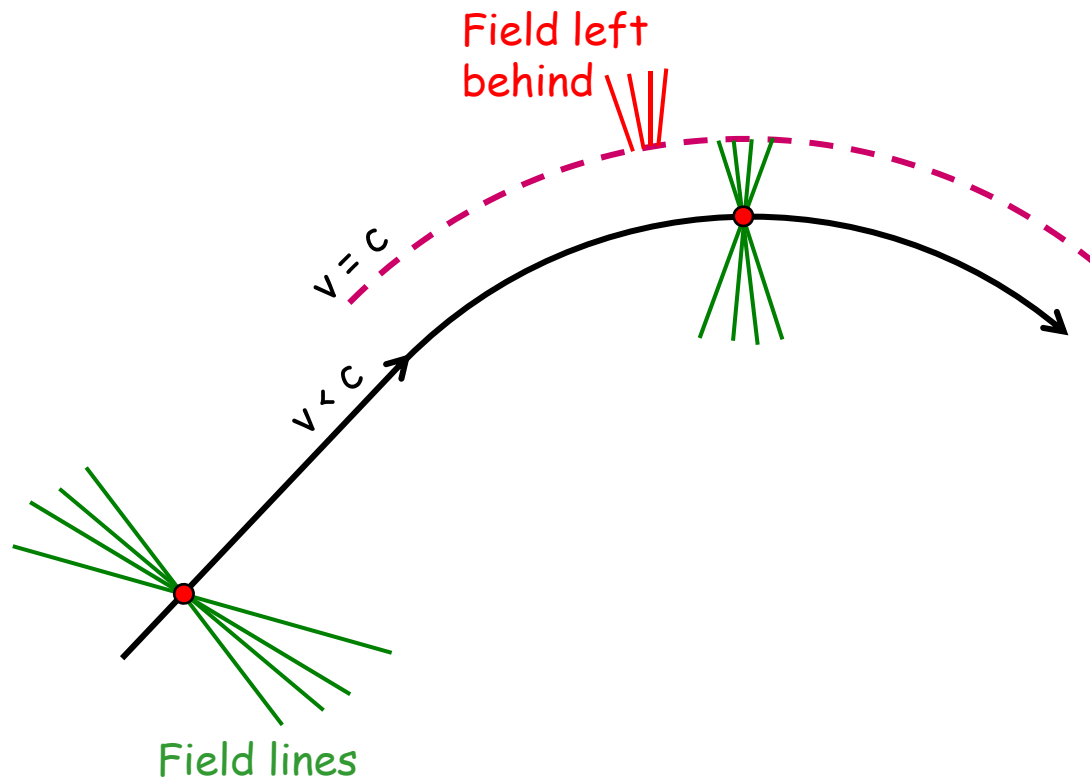
Achieved ~70nm vertical beam size



BDS: 18



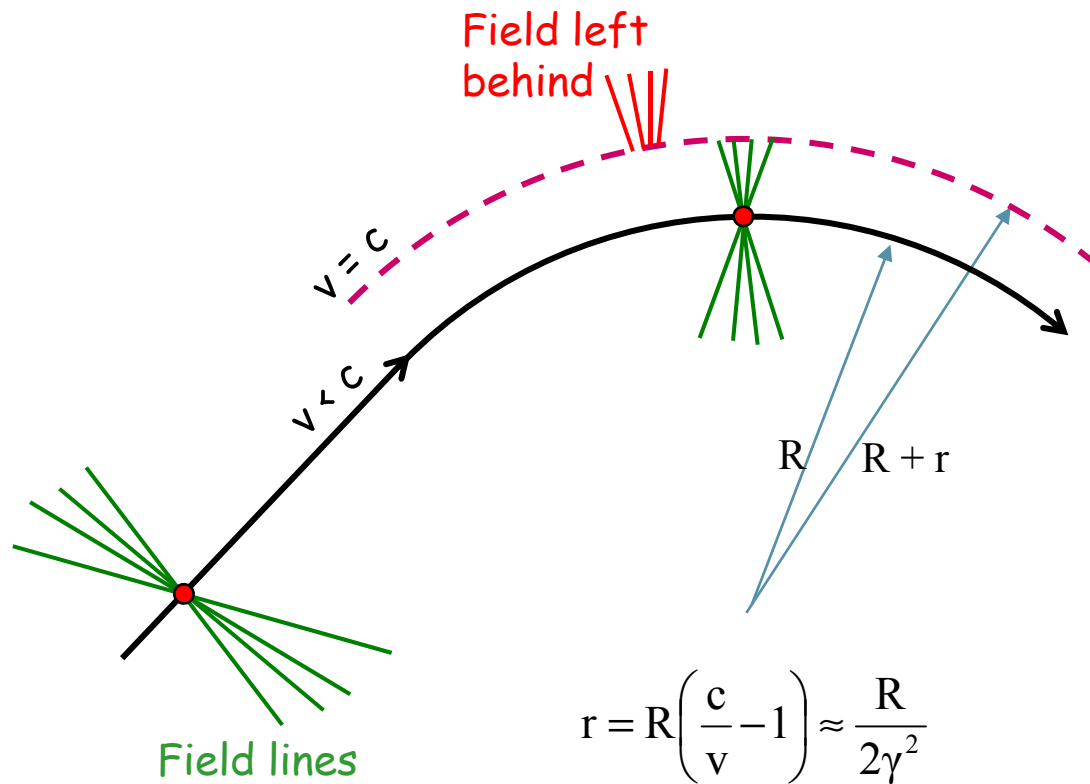
Synchrotron Radiation in FF magnets



Energy spread caused by SR in bends and quads is also a major driving factor of FF design

- Bends are needed for compensation of chromaticity
- SR causes increase of energy spread which may perturb compensation of chromaticity
- Bends need to be long and weak, especially at high energy
- SR in FD quads is also harmful (Oide effect) and may limit the achievable beam size

Let's estimate SR power



Energy in the field left behind (radiated !):

$$W \approx \int E^2 dV$$

The field $E \approx \frac{e}{r^2}$ the volume $V \approx r^2 dS$

Energy loss per unit length:

$$\frac{dW}{dS} \approx E^2 r^2 \approx \left(\frac{e}{r^2} \right)^2 r^2$$

Substitute $r \approx \frac{R}{2\gamma^2}$ and get an estimate:

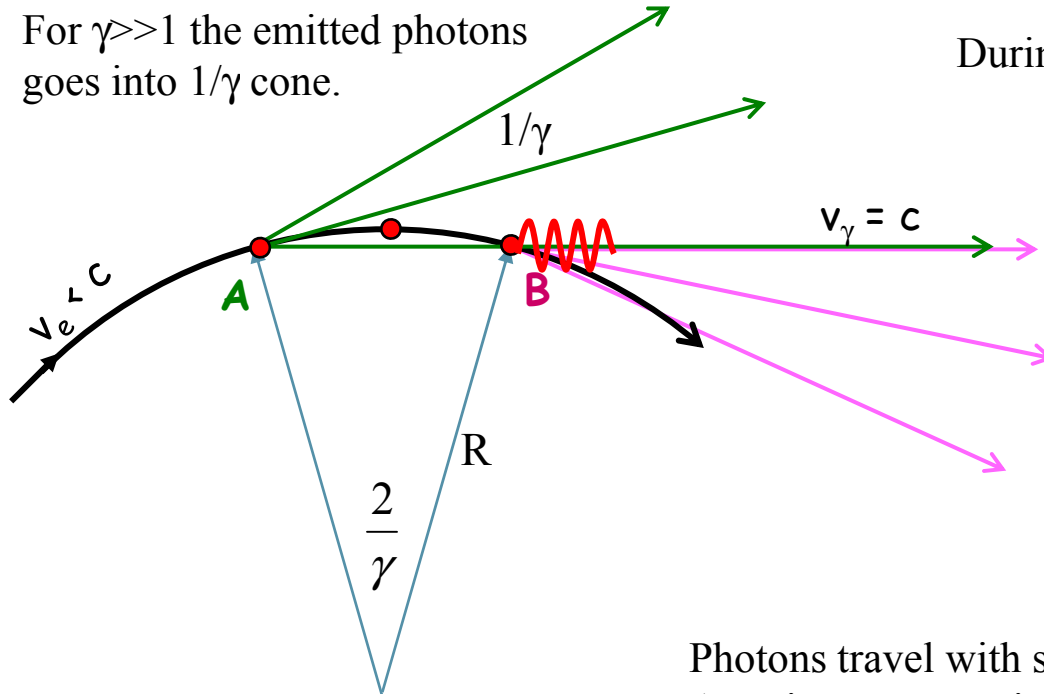
$$\boxed{\frac{dW}{dS} \approx \frac{e^2 \gamma^4}{R^2}}$$

Compare with exact formula: $\frac{dW}{dS} = \frac{2}{3} \frac{e^2 \gamma^4}{R^2}$



Let's estimate typical frequency of SR photons

For $\gamma \gg 1$ the emitted photons goes into $1/\gamma$ cone.



During what time Δt the observer will see the photons?



Photons emitted during travel along the $2R/\gamma$ arc will be observed.

Photons travel with speed c , while particles with v .

At point B, separation between photons and particles is

$$dS \approx \frac{2R}{\gamma} \left(1 - \frac{v}{c}\right)$$

Therefore, observer will see photons during $\Delta t \approx \frac{dS}{c} \approx \frac{2R}{c\gamma} (1 - \beta) \approx \frac{R}{c\gamma^3}$

Estimation of characteristic frequency

$$\omega_c \approx \frac{1}{\Delta t} \approx \frac{c\gamma^3}{R}$$

Compare with exact formula: $\omega_c = \frac{3}{2} \frac{c\gamma^3}{R}$



Let's estimate energy spread growth due to SR

We estimated the rate of energy loss : $\frac{dW}{dS} \approx \frac{e^2 \gamma^4}{R^2}$ And the characteristic frequency $\omega_c \approx \frac{c \gamma^3}{R}$

The photon energy $\varepsilon_c = \hbar \omega_c \approx \frac{\gamma^3 \hbar c}{R} = \frac{\gamma^3}{R} \lambda_e mc^2$ where $r_e = \frac{e^2}{mc^2}$ $\alpha = \frac{e^2}{\hbar c}$ $\lambda_e = \frac{r_e}{\alpha}$

Number of photons emitted per unit length $\frac{dN}{dS} \approx \frac{1}{\varepsilon_c} \frac{dW}{dS} \approx \frac{\alpha \gamma}{R}$ (per angle θ : $N \approx \alpha \gamma \theta$)

The energy spread $\Delta E/E$ will grow due to statistical fluctuations (\sqrt{N}) of the number of emitted photons :

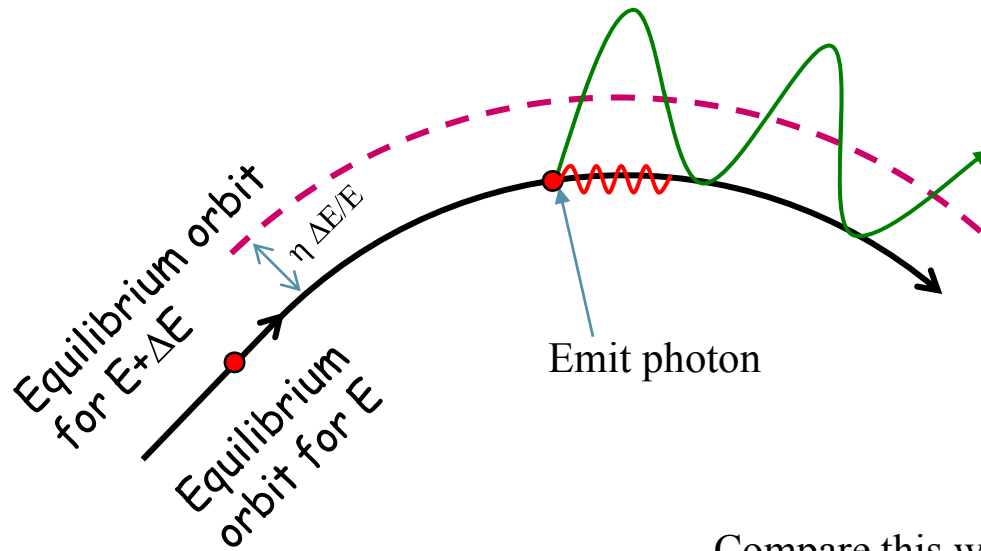
$$\frac{d((\Delta E/E)^2)}{dS} \approx \varepsilon_c^2 \frac{dN}{dS} \frac{1}{(\gamma mc^2)^2}$$

Which gives: $\frac{d((\Delta E/E)^2)}{dS} \approx \frac{r_e \lambda_e \gamma^5}{R^3}$

Compare with exact formula: $\frac{d((\Delta E/E)^2)}{dS} = \frac{55}{24\sqrt{3}} \frac{r_e \lambda_e \gamma^5}{R^3}$



Let's estimate emittance growth rate due to SR



Dispersion function η shows how equilibrium orbit shifts when energy changes

When a photon is emitted, the particle starts to oscillate around new equilibrium orbit

Amplitude of oscillation is $\Delta x \approx \eta \Delta E/E$

Compare this with betatron beam size: $\sigma_x = (\epsilon_x \beta_x)^{1/2}$

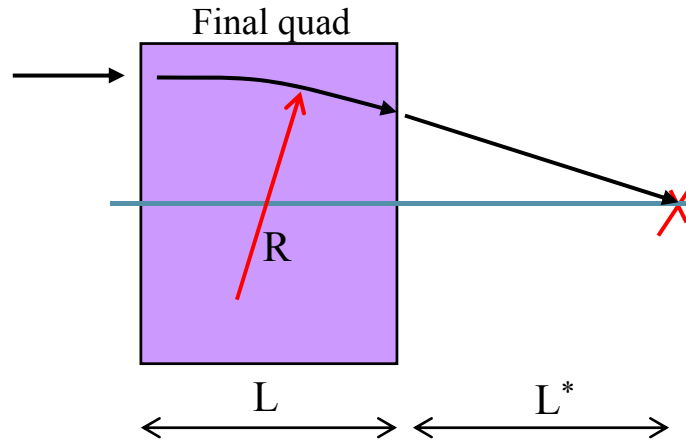
And write emittance growth: $\Delta \epsilon_x \approx \frac{\Delta x^2}{\beta}$

Resulting estimation for emittance growth: $\frac{d\epsilon_x}{dS} \approx \frac{\eta^2}{\beta_x} \frac{d((\Delta E/E)^2)}{dS} \approx \frac{\eta^2}{\beta_x} \frac{r_e \lambda_e \gamma^5}{R^3}$

Compare with exact formula (which also takes into account the derivatives): $\frac{d\epsilon_x}{dS} = \frac{(\eta^2 + (\beta_x \eta' - \beta_x' \eta / 2)^2)}{\beta_x} \frac{55}{24\sqrt{3}} \frac{r_e \lambda_e \gamma^5}{R^3}$
 $= \mathcal{H}$



Let's apply SR formulae to estimate Oide effect (SR in FD)



IP divergence:

$$\theta^* = \sqrt{\varepsilon/\beta^*}$$

IP size:

$$\sigma^* = \sqrt{\varepsilon \beta^*}$$

Energy spread obtained in the quad:

$$\left(\frac{\Delta E}{E}\right)^2 \approx \frac{r_e \lambda_e \gamma^5 L}{R^3}$$

Radius of curvature of the trajectory: $R = L / \theta^*$

Growth of the IP beam size: $\sigma^2 \approx \sigma_0^2 + (L^* \theta^*)^2 \left(\frac{\Delta E}{E}\right)^2$

Which gives $\sigma^2 \approx \varepsilon \beta^* + C_1 \left(\frac{L^*}{L}\right)^2 r_e \lambda_e \gamma^5 \left(\frac{\varepsilon}{\beta^*}\right)^{5/2}$ (where C_1 is ~ 7 (depend on FD params.))

This achieve minimum possible value:

$$\sigma_{\min} \approx 1.35 C_1^{1/7} \left(\frac{L^*}{L}\right)^{2/7} (r_e \lambda_e)^{1/7} (\gamma \varepsilon)^{5/7}$$

When beta* is:

$$\beta_{\text{optimal}} \approx 1.29 C_1^{2/7} \left(\frac{L^*}{L}\right)^{4/7} (r_e \lambda_e)^{2/7} \gamma (\gamma \varepsilon)^{3/7}$$

Note that beam distribution at IP will be non-Gaussian. Usually need to use tracking to estimate impact on luminosity. Note also that optimal β may be smaller than the σ_z (i.e cannot be used).



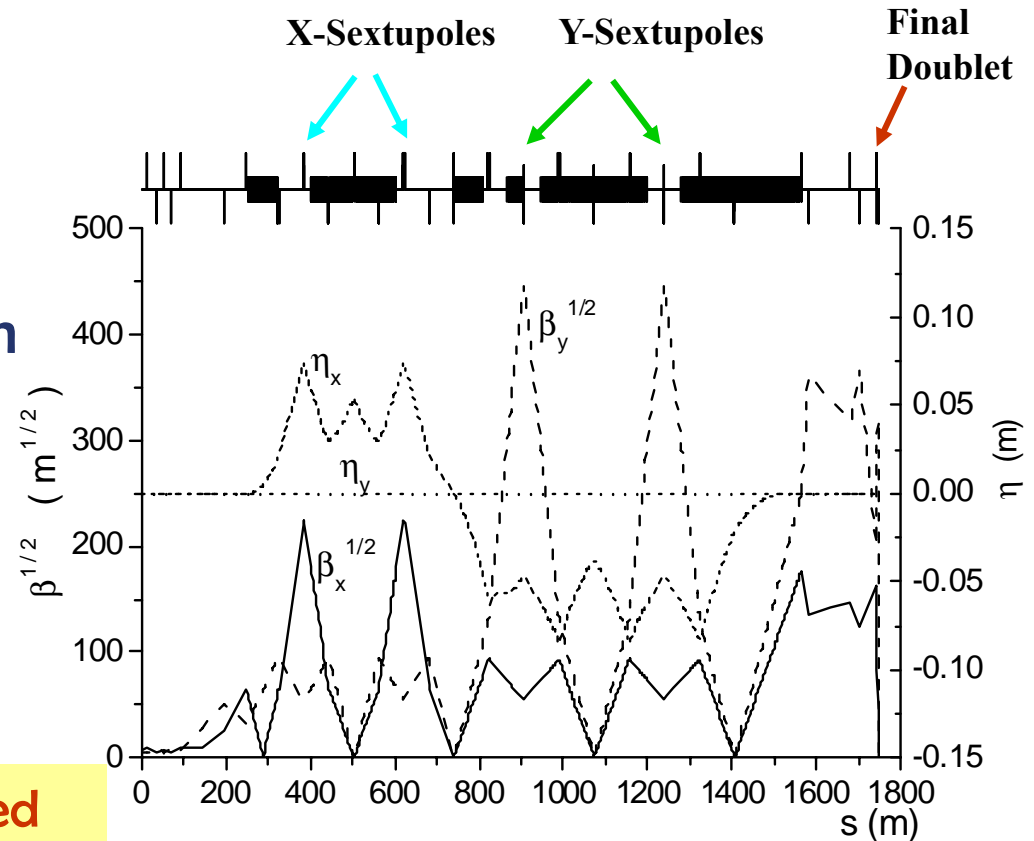
FF with non-local chromaticity compensation

- Chromaticity is compensated by sextupoles in dedicated sections
- Geometrical aberrations are canceled by using sextupoles in pairs with $M = -1$

Chromaticity arise at FD but pre-compensated 1000m upstream

Problems:

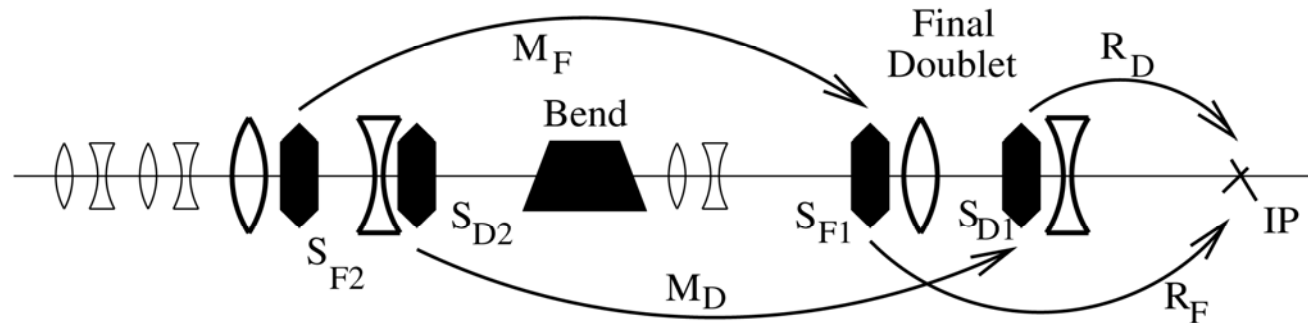
- Chromaticity not locally compensated
 - Compensation of aberrations is not ideal since $M \neq -1$ for off energy particles
 - Large aberrations for beam tails
 - ...



Traditional FF

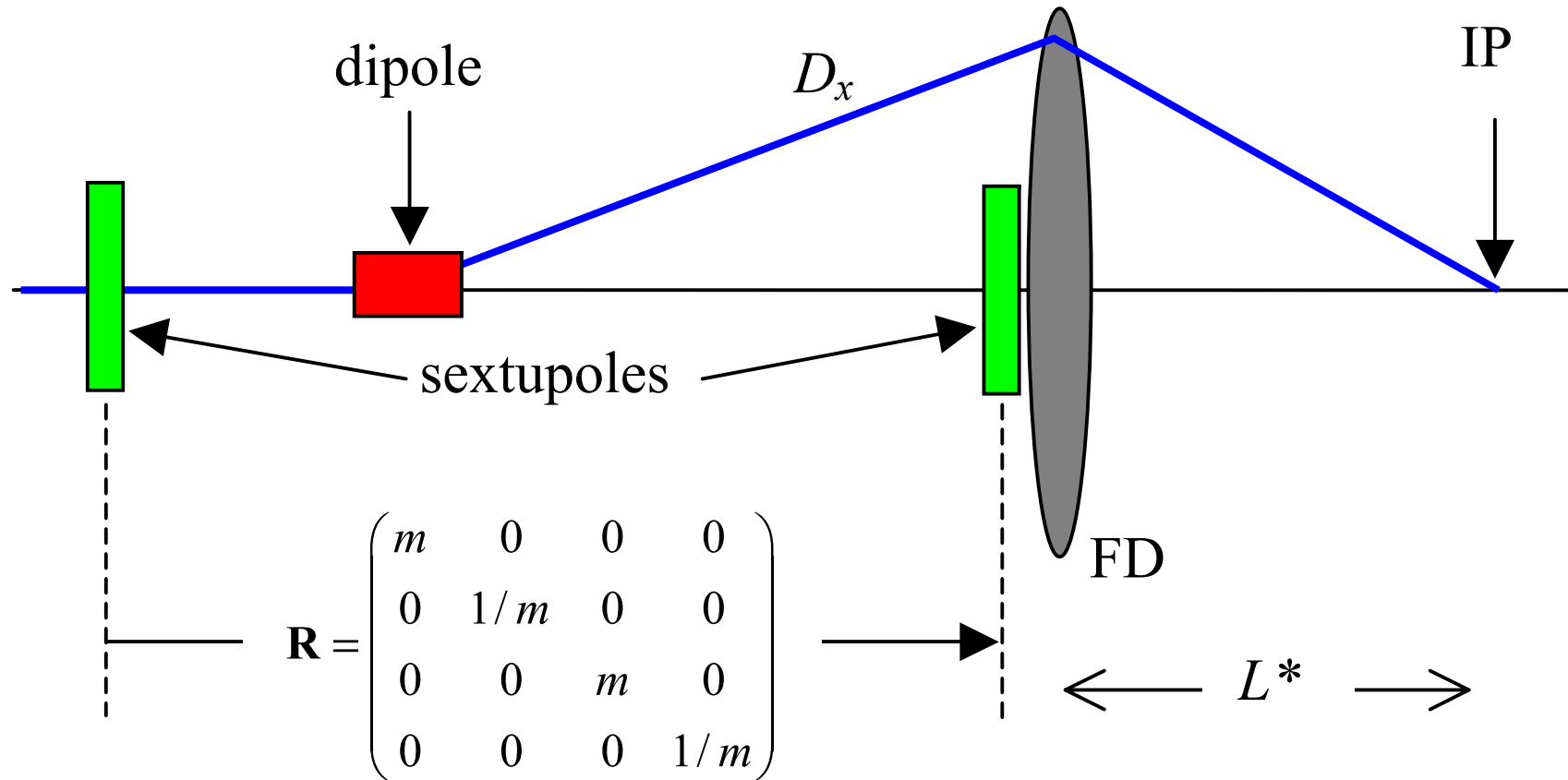


FF with local chromatic correction



- **Chromaticity** is cancelled locally by two sextupoles interleaved with FD, a bend upstream generates dispersion across FD
- **Geometric aberrations** of the FD sextupoles are cancelled by two more sextupoles placed in phase with them and upstream of the bend

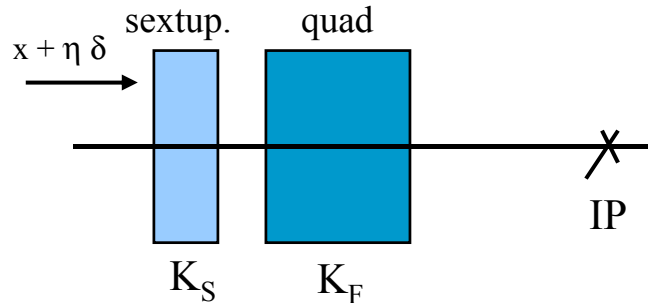
Local chromatic correction



- The value of dispersion in FD is usually chosen so that it does not increase the beam size in FD by more than 10-20% for typical beam energy spread



Chromatic correction in FD



- Straightforward in Y plane
- a bit tricky in X plane:

Quad: $\Delta x' = \frac{K_F}{(1+\delta)}(x + \eta\delta) \Rightarrow K_F(-\delta x - \eta\delta^2)$

Sextupole: $\Delta x' = \frac{K_S}{2}(x + \eta\delta)^2 \Rightarrow K_S\eta\left(\delta x + \frac{\eta\delta^2}{2}\right)$

$\Delta x' = \frac{K_F}{(1+\delta)}(x + \eta\delta) + \frac{K_{\beta\text{-match}}}{(1+\delta)}x \Rightarrow 2K_F\left(-\delta x - \frac{\eta\delta^2}{2}\right)$

$K_{\beta\text{-match}} = K_F \quad K_S = \frac{2K_F}{\eta}$

chromaticity

Second order dispersion

If we require $K_S\eta = K_F$ to cancel FD chromaticity, then half of the **second order dispersion** remains.

Solution:
The β -matching section produces as much X chromaticity as the FD, so the X sextupoles run twice stronger and cancel the **second order dispersion** as well.



Definitions of chromaticity

1st : TRANSPORT

Storage Rings: chromaticity defined as a change of the betatron tunes versus energy.

In single path beamlines, it is more convenient to use other definitions.

$$\mathbf{x}_i = \begin{pmatrix} x \\ x' \\ y \\ y' \\ \Delta l \\ \delta \end{pmatrix} \quad \mathbf{x}_i^{\text{out}} = \mathbf{R}_{ij} \mathbf{x}_j^{\text{in}}$$

The second, third, and so on terms are included in a similar manner:

$$\mathbf{x}_i^{\text{out}} = \mathbf{R}_{ij} \mathbf{x}_j^{\text{in}} + \mathbf{T}_{ijk} \mathbf{x}_j^{\text{in}} \mathbf{x}_k^{\text{in}} + \mathbf{U}_{ijkn} \mathbf{x}_j^{\text{in}} \mathbf{x}_k^{\text{in}} \mathbf{x}_n^{\text{in}} + \dots$$

In FF design, we usually call ‘chromaticity’ the second order elements T_{126} and T_{346} . All other high order terms are just ‘aberrations’, purely chromatic (as T_{166} , which is second order dispersion), or chromo-geometric (as U_{32446}).



Definitions of chromaticity

2nd : W functions

Lets assume that betatron motion without energy offset is described by twiss functions α_1 and β_1 and with energy offset δ by functions α_2 and β_2

Let's define chromatic function \mathbf{W} (for each plane) as $\mathbf{W} = (iA + B)/2$ where $i = \sqrt{-1}$

And where:
$$B = \frac{\beta_2 - \beta_1}{\delta (\beta_2 \cdot \beta_1)^{1/2}} \approx \frac{\Delta\beta}{\delta \beta} \quad \text{and} \quad A = \frac{\alpha_2\beta_1 - \alpha_1\beta_2}{\delta (\beta_2 \cdot \beta_1)^{1/2}} \approx \frac{\Delta\alpha}{\delta} - \frac{\alpha}{\beta} \frac{\Delta\beta}{\delta}$$

Using familiar formulae $\frac{d\beta}{ds} = -2\alpha$ and $\frac{d\alpha}{ds} = K \cdot \beta - \frac{(1 + \alpha^2)}{\beta}$ where $K = \frac{e}{pc} \frac{dB_y}{dx}$

And introducing $\Delta K = \frac{K(\delta(-K(0))}{\delta} \approx -K$ we obtain the equation for \mathbf{W} evolution:

Can you show this?

$$\frac{d\mathbf{W}}{ds} = \frac{2i}{\beta} \mathbf{W} + \frac{i}{2} \beta \Delta K$$

knowing that the betatron phase is $\frac{d\Phi}{ds} = \frac{1}{\beta}$

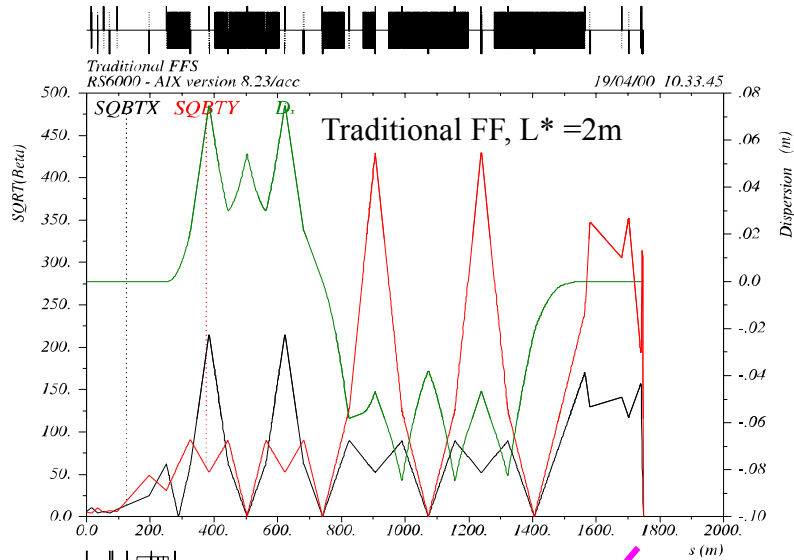
can see that if $\Delta K=0$, then \mathbf{W} rotates with double betatron frequency and stays constant in amplitude. In quadrupoles or sextupoles, only imaginary part changes.

Show that if in a final defocusing lens $\alpha=0$, then it gives $\Delta W=L^*/(2\beta^*)$

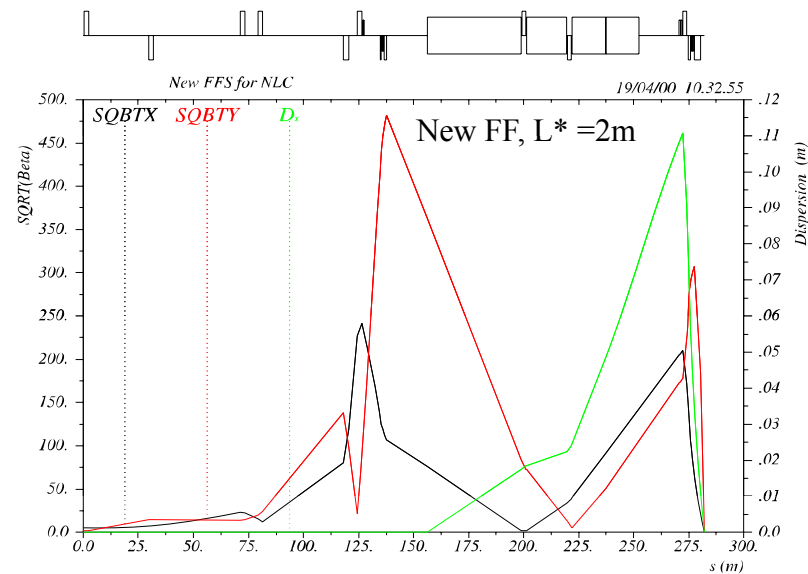
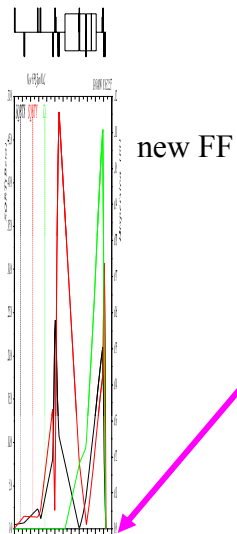
Show that if T_{346} is zeroed at the IP, the W_y is also zero. Use approximation $\Delta R_{34}=T_{346}^*\delta$, use $R_{34}=(\beta\beta_0)^{1/2} \sin(\Delta\Phi)$, and the twiss equation for $d\alpha/d\Phi$.



Compare FF designs

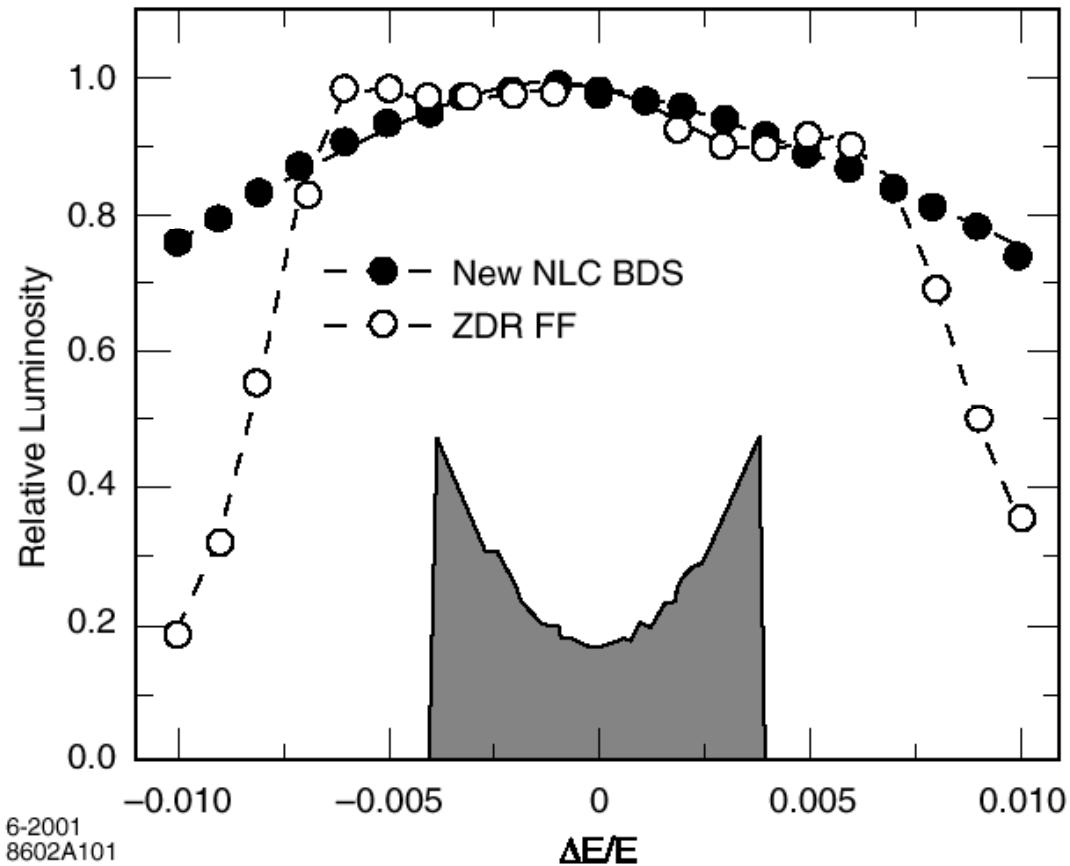


FF with local chromaticity compensation with the same performance can be ~300m long, i.e. 6 times shorter





IP bandwidth

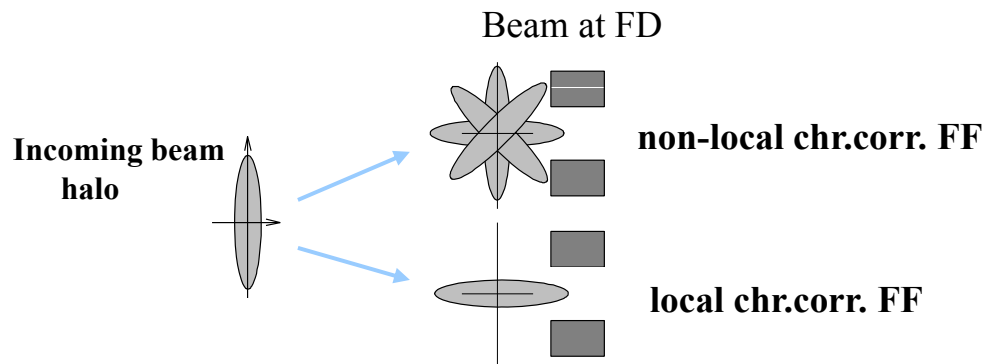
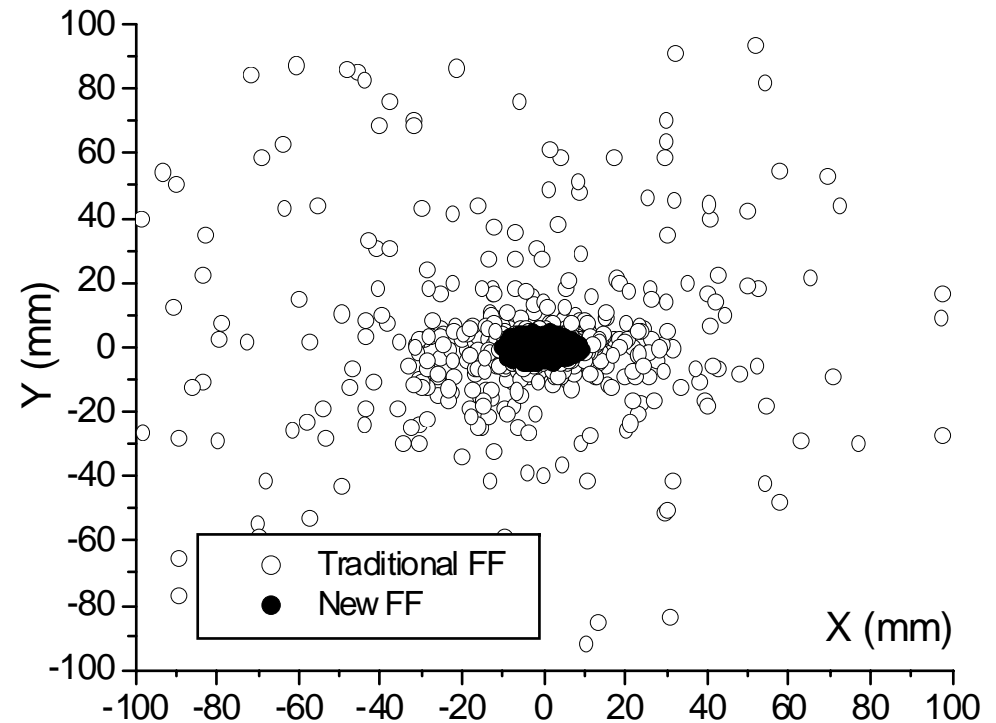


Bandwidth of FF with local chromaticity correction can be better than for system with non-local correction



Aberrations & halo generation in FF

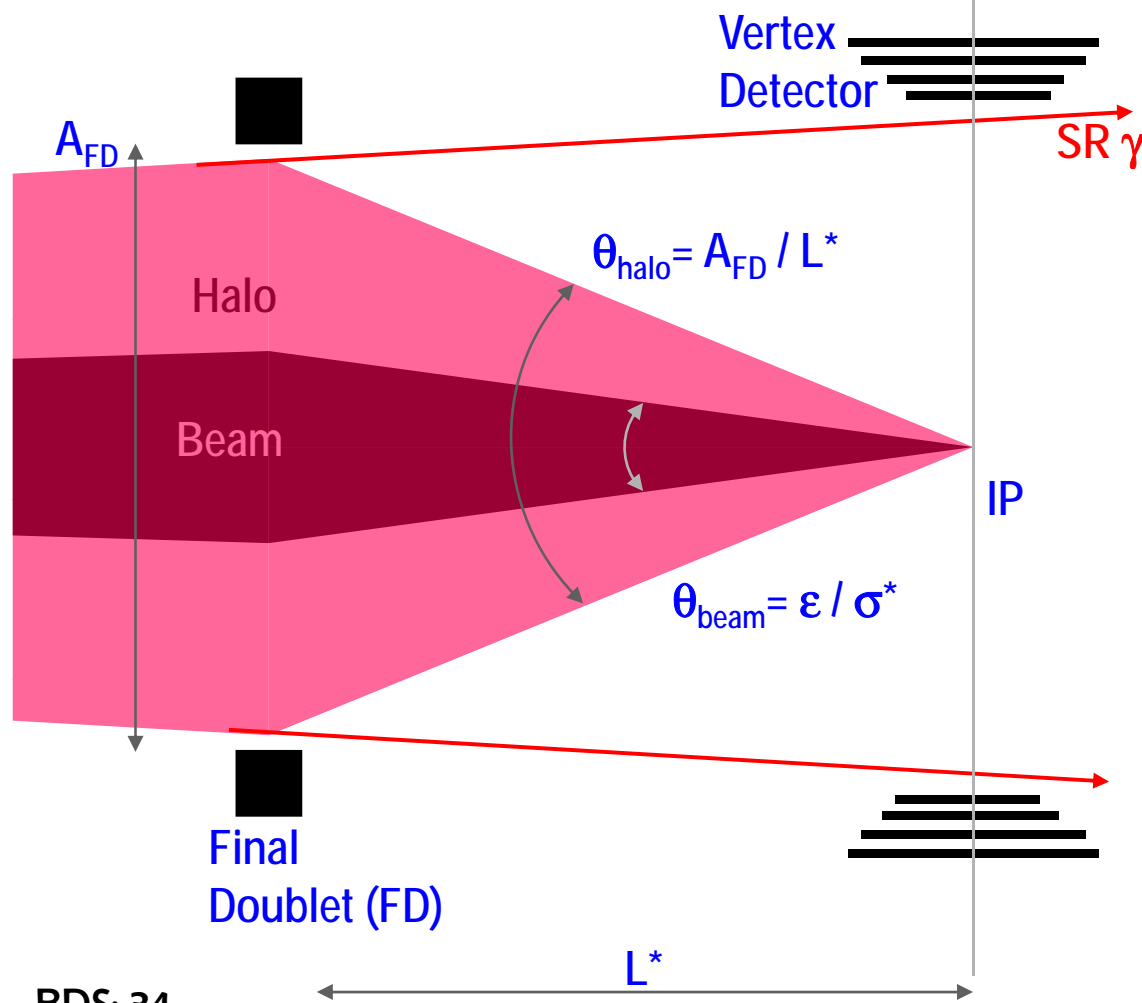
- FF with non-local chr. corr. generate beam tails due to aberrations and it does not preserve betatron phase of halo particles
- FF with local chr. corr. has much less aberrations and it does not mix phases particles



**Halo beam at the FD entrance.
Incoming beam is ~ 100 times larger than nominal beam**

Beam halo & collimation

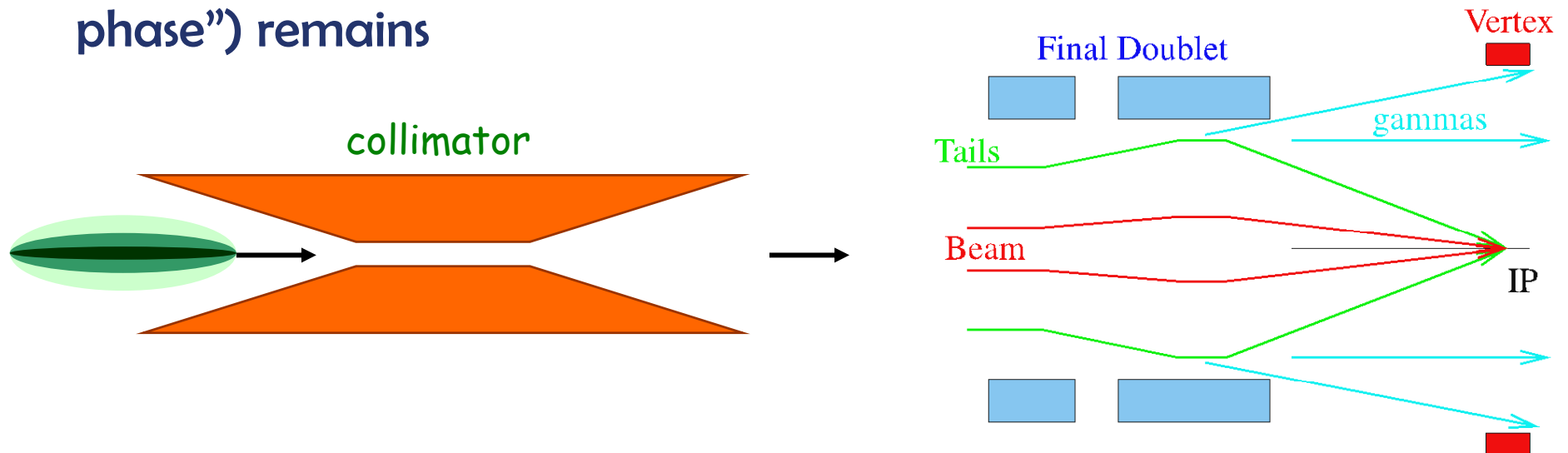
- Even if final focus does not generate beam halo itself, the halo may come from upstream and need to be collimated



- Halo must be collimated upstream in such a way that SR γ & halo e^+ do not touch VX and FD
- => VX aperture needs to be somewhat larger than FD aperture
- Exit aperture is larger than FD or VX aperture
- Beam convergence depend on parameters, the halo convergence is fixed for given geometry
=> $\theta_{halo} / \theta_{beam}$ (collimation depth) becomes tighter with larger L^* or smaller IP beam size
- Tighter collimation => MPS issues, collimation wake-fields, higher muon flux from collimators, etc.

More details on collimation

- Collimators has to be placed far from IP, to minimize background
- Ratio of beam/halo size at FD and collimator (placed in “FD phase”) remains

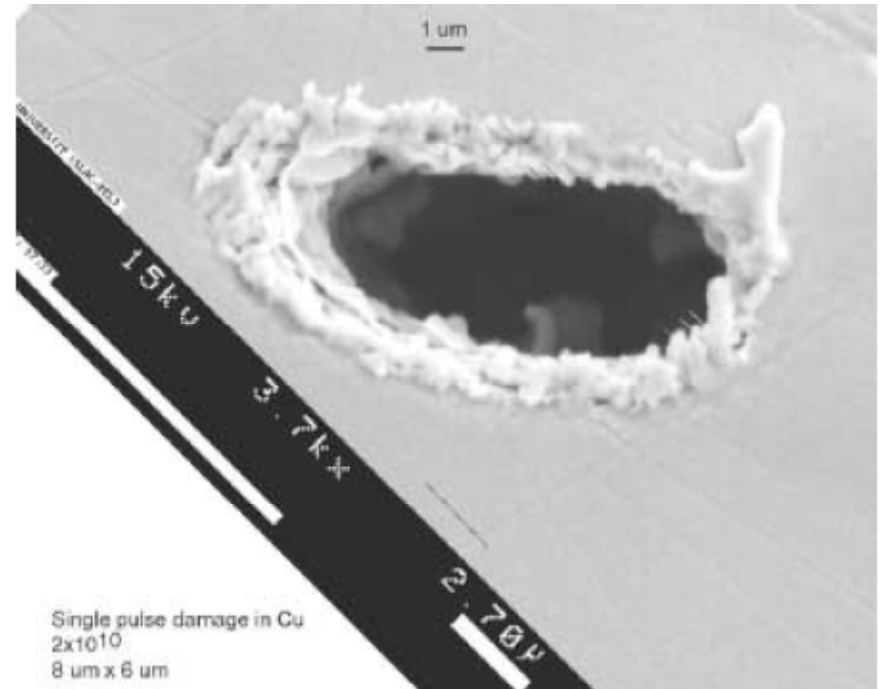


- Collimation depth (esp. in x) can be only ~10 or even less
- It is not unlikely that not only halo ($1e^{-3}$ – $1e^{-6}$ of the beam) but full errant bunch(s) would hit the collimator



MPS and collimation design

- The beam is very small => single bunch can punch a hole => the need for MPS (machine protection system)
- Damage may be due to
 - electromagnetic shower damage (need several radiation lengths to develop)
 - direct ionization loss ($\sim 1.5 \text{ MeV/g/cm}^2$ for most materials)
- Mitigation of collimator damage
 - using spoiler-absorber pairs
 - thin (0.5-1 rl) spoiler followed by thick ($\sim 20 \text{ rl}$) absorber
 - increase of beam size at spoilers
 - MPS divert the beam to emergency extraction as soon as possible

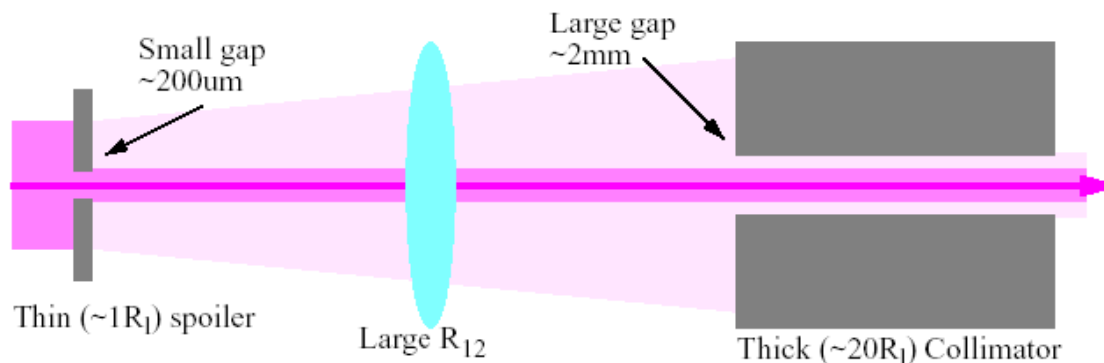


Picture from beam damage experiment at FFTB. The beam was 30 GeV, $3\text{-}20 \times 10^9$ e⁻, 1 mm bunch length, $s \sim 45\text{-}200 \mu\text{m}^2$. Test sample is Cu, 1.4 mm thick. Damage was observed for densities $> 7 \times 10^{14}$ e⁻/cm². Picture is for 6×10^{15} e⁻/cm²



Spoiler-Absorber & spoiler design

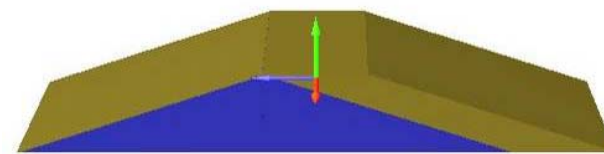
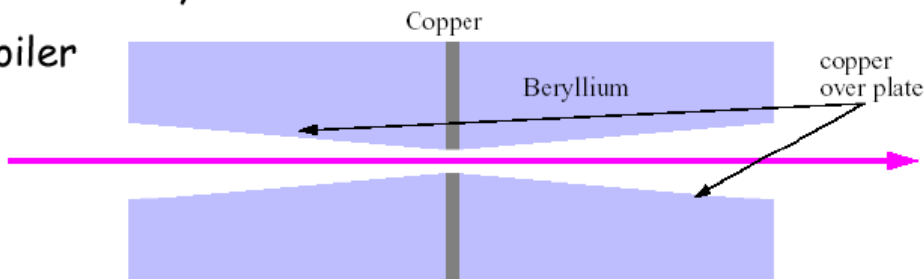
Spoiler / Absorber Scheme



Thin spoiler increases beam divergence and size at the thick absorber already sufficiently large. Absorber is away from the beam and contributes much less to wakefields.

Tapered low resistivity surface for wakefields

Thin hi-Z spoiler



Recently considered design:
0.6 Xo of Ti alloy leading taper (gold), graphite (blue), 1 mm thick layer of Ti alloy

Need the spoiler thickness increase rapidly, but need that surface to increase gradually, to minimize wakefields. The radiation length for Cu is 1.4cm and for Be is 35cm. So, Be is invisible to beam in terms of losses. Thin one micron coating over Be provides smooth surface for wakes.



Spoiler damage

Spoiler material properties and temperature rise due to a single bunch of 1.25×10^{10} electrons within a beam spot with $\sigma_x = \sigma_y = 3.16 \mu\text{m}$.

	Be	C	Al	Ti	Cu	Fe
Radiation Length (cm)	35.7	21.7	9.0	3.7	1.4	1.8
dE/dx_{min} (MeV cm ⁻¹)	3.1	3.6	4.4	7.2	12.8	11.6
Specific Heat, C_p (J cm ⁻³ °C ⁻¹)	3.3	1.9	2.5	2.4	3.5	3.8
Melting Point, T_{melt} (°C)	1280	3600	660	1800	1080	1530
Stress Limit, T_{stress} (°C)	150	2500	140	770	180	135
Temperature Rise, ΔT (°C)	2350	4740	4403	7506	9150	7637
$\Delta T / T_{melt}$	1.8	1.3	6.7	4.2	8.5	5.0
$\Delta T / 4T_{stress}$	3.9	0.36	7.9	2.4	12.7	14.1

Temperature rise for thin spoilers (ignoring shower buildup and increase of specific heat with temperature):

$$\Delta T = \frac{0.393N}{\pi\sigma_x\sigma_y} \frac{dE/dx_{min}}{C_p}$$

The stress limit based on tensile strength, modulus of elasticity and coefficient of thermal expansion. Sudden T rise create local stresses. When ΔT exceed stress limit, micro-fractures can develop. If ΔT exceeds $4T_{stress}$, the shock wave may cause material to delaminate. Thus, allowed ΔT is either the melting point or four time stress limit at which the material will fail catastrophically.



Survivable and consumable spoilers

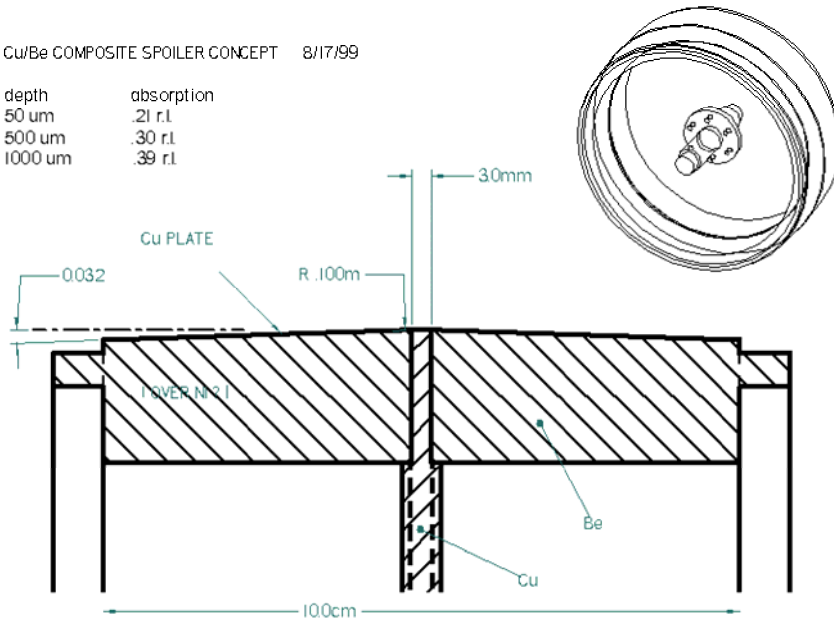
- A critical parameter is number of bunches $\#N$ that MPS will let through to the spoiler before sending the rest of the train to emergency extraction
- If it is practical to increase the beam size at spoilers so that spoilers survive $\#N$ bunches, then they are survivable
- Otherwise, spoilers must be consumable or renewable



Renewable spoilers

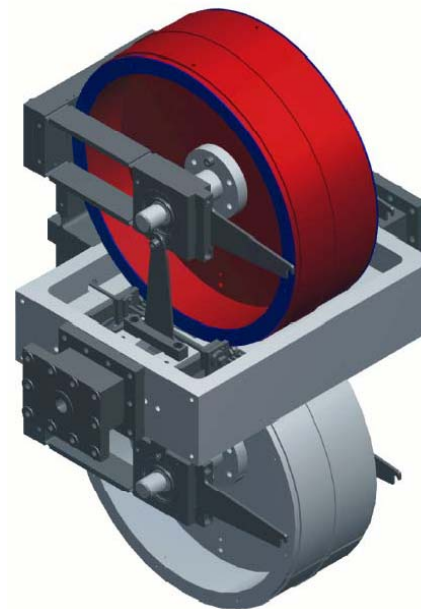
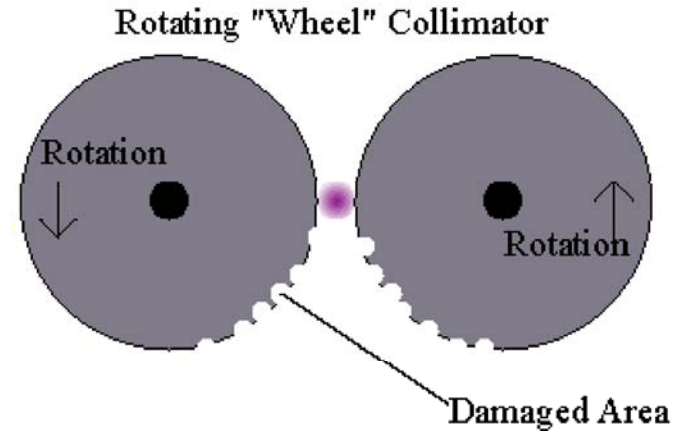
Cu/Be COMPOSITE SPOILER CONCEPT 8/17/99

depth	absorption
50 um	.21 r.l
500 um	.30 r.l
1000 um	.39 r.l



This design was essential for NLC, where short inter-bunch spacing made it impractical to use survivable spoilers.

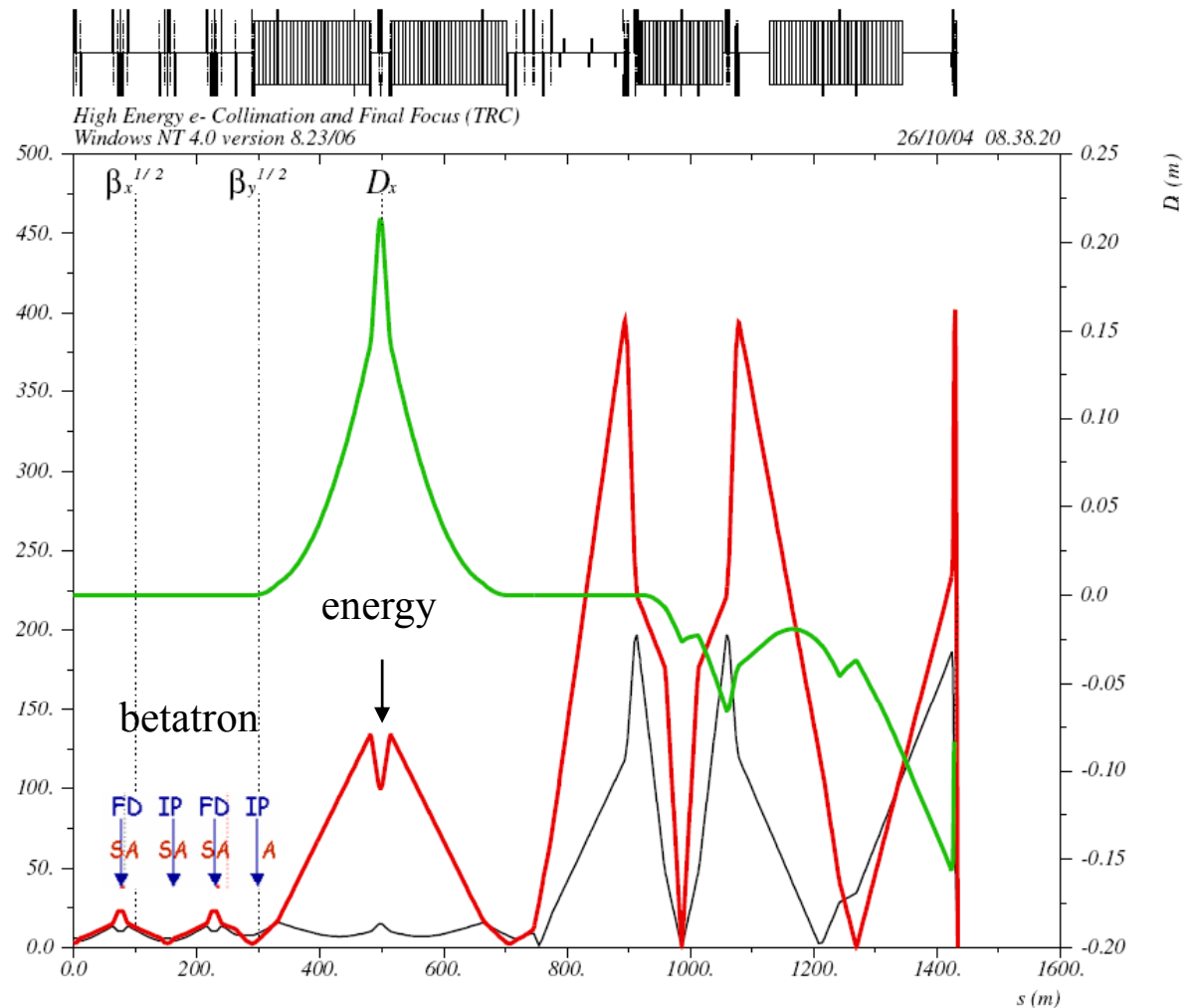
This concept is now being applied to LHC collimator system.





BDS with renewable spoilers

- Location of spoiler and absorbers is shown
- Collimators were placed both at FD betatron phase and at IP phase
- Two spoilers per FD and IP phase
- Energy collimator is placed in the region with large dispersion
- Secondary clean-up collimators located in FF part
- Tail folding octupoles (see below) are include

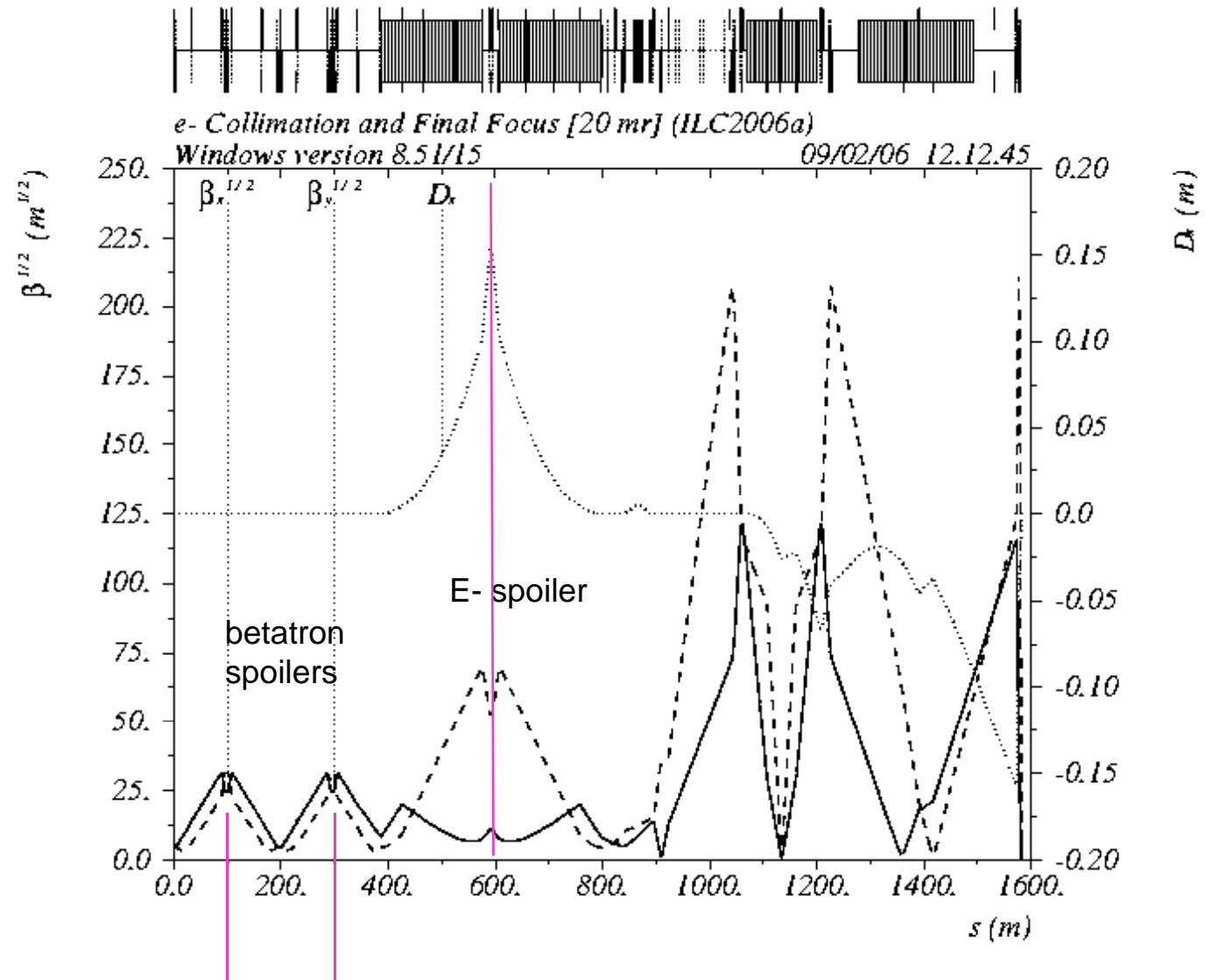


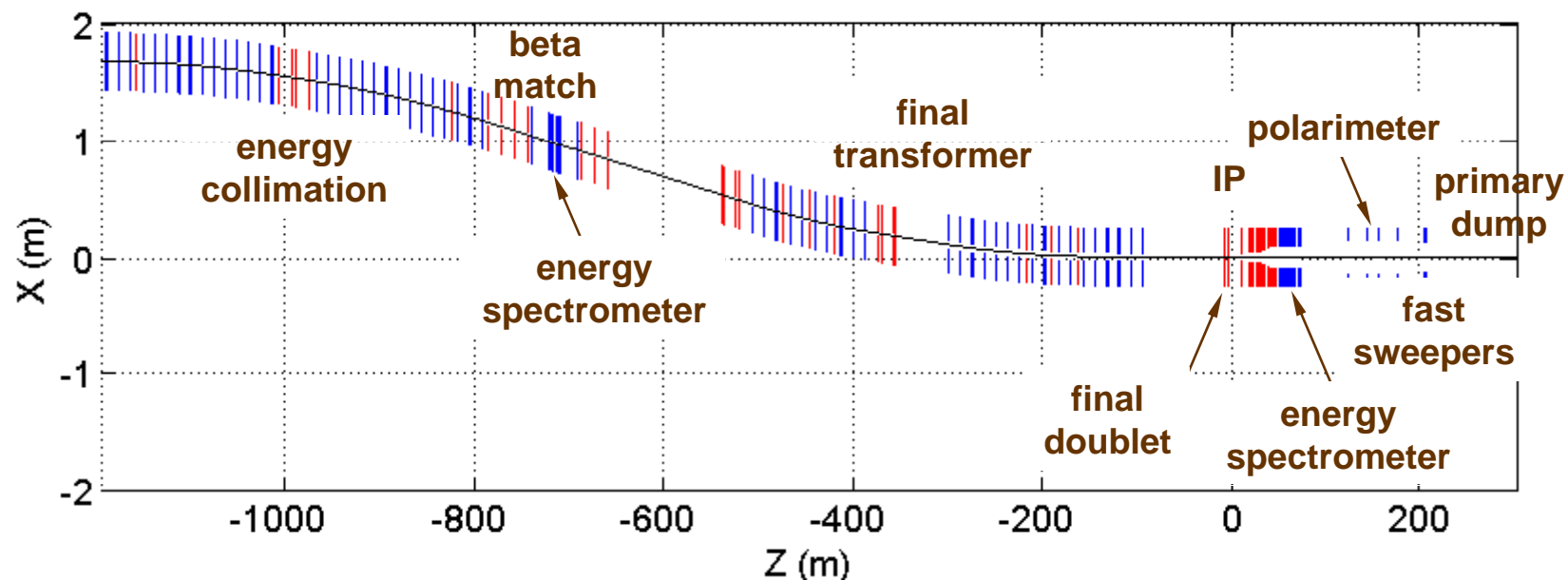
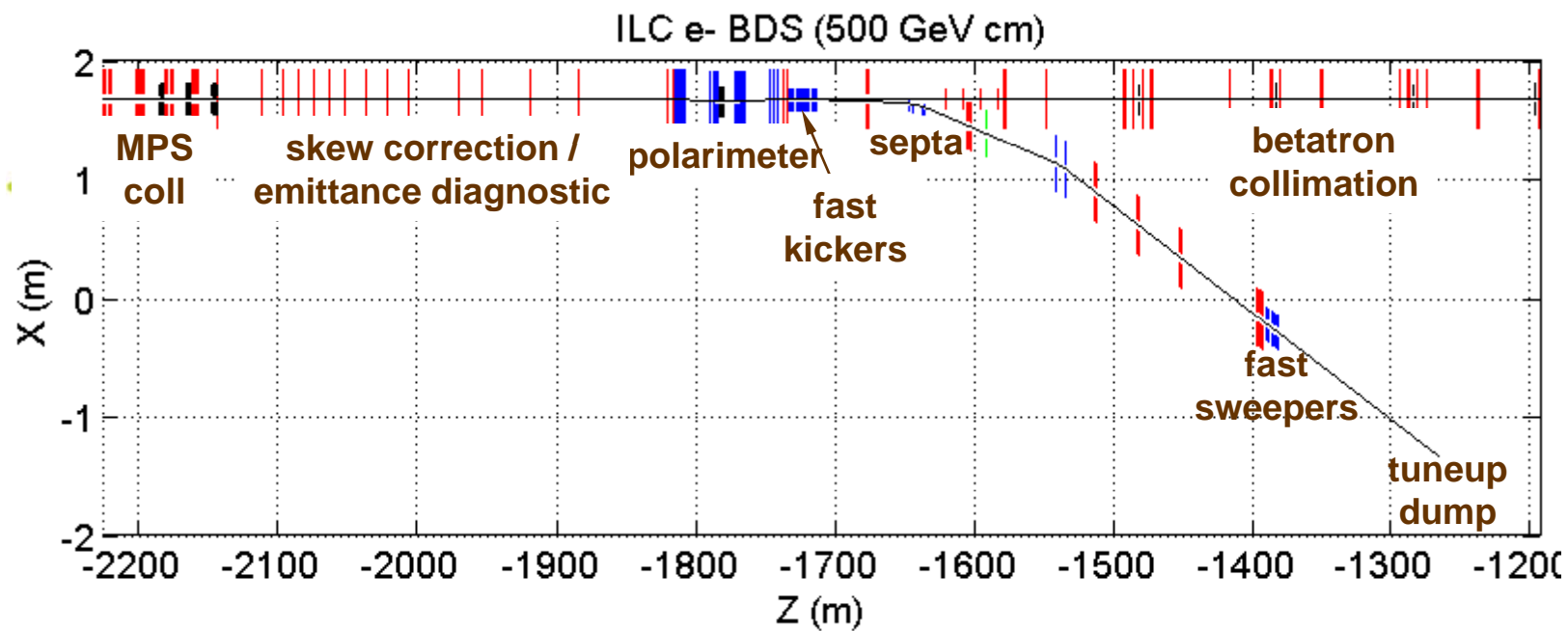
- Beam Delivery System Optics, an earlier version with consumable spoilers



ILC FF & Collimation

- Betatron spoilers survive up to two bunches
- E-spoiler survive several bunches
- One spoiler per FD or IP phase

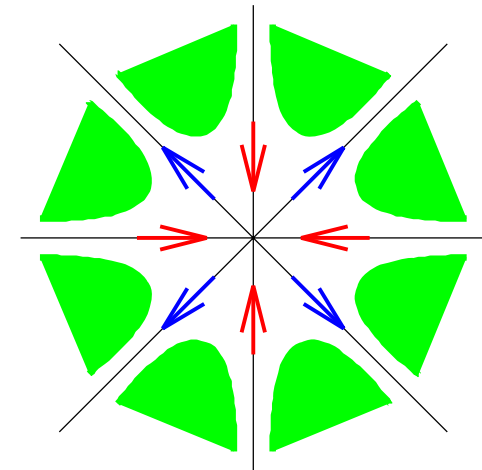






Nonlinear handling of beam tails in ILC BDS

- **Can we ameliorate the incoming beam tails to relax the required collimation depth?**
- One wants to **focus beam tails** but not to change the core of the beam
 - use **nonlinear** elements
- **Several** nonlinear elements needs to be **combined** to provide **focusing in all directions**
 - (analogy with **strong focusing by FODO**)
- **Octupole Doublets (OD)** can be used for **nonlinear tail folding** in ILC FF



Single octupole focus in planes and defocus on diagonals.

An octupole doublet can focus in all directions !



Strong focusing by octupoles

- **Two octupoles** of different sign separated by **drift** provide **focusing in all directions** for parallel beam:

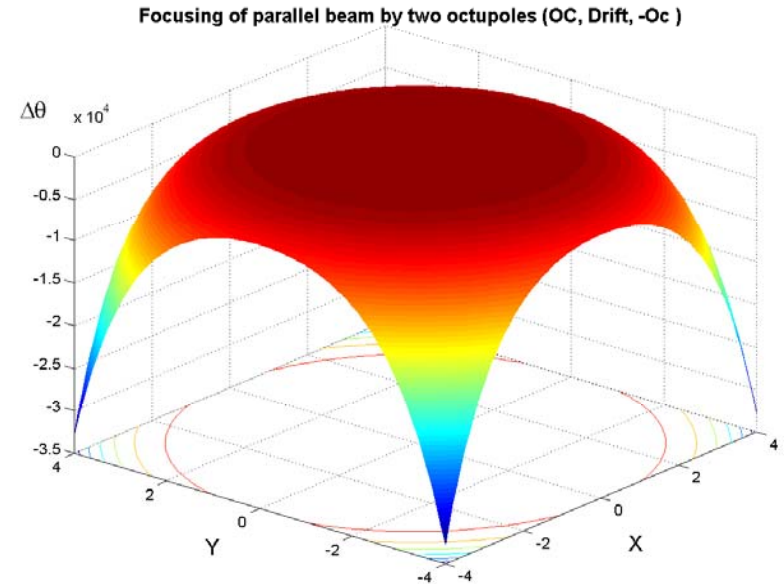
$$\Delta\theta = \alpha r^3 e^{-i3\varphi} - \left(\alpha r^3 e^{i3\varphi} (1 + \alpha r^2 L e^{-i4\varphi})^3 \right)^*$$

$$x + iy = r e^{i\varphi}$$

$$\Delta\theta \approx -3\alpha^2 r^5 e^{i\varphi} - 3\alpha^3 r^7 L^2 e^{i5\varphi}$$

Focusing in
all directions

Next nonlinear term
focusing – defocusing
depends on φ



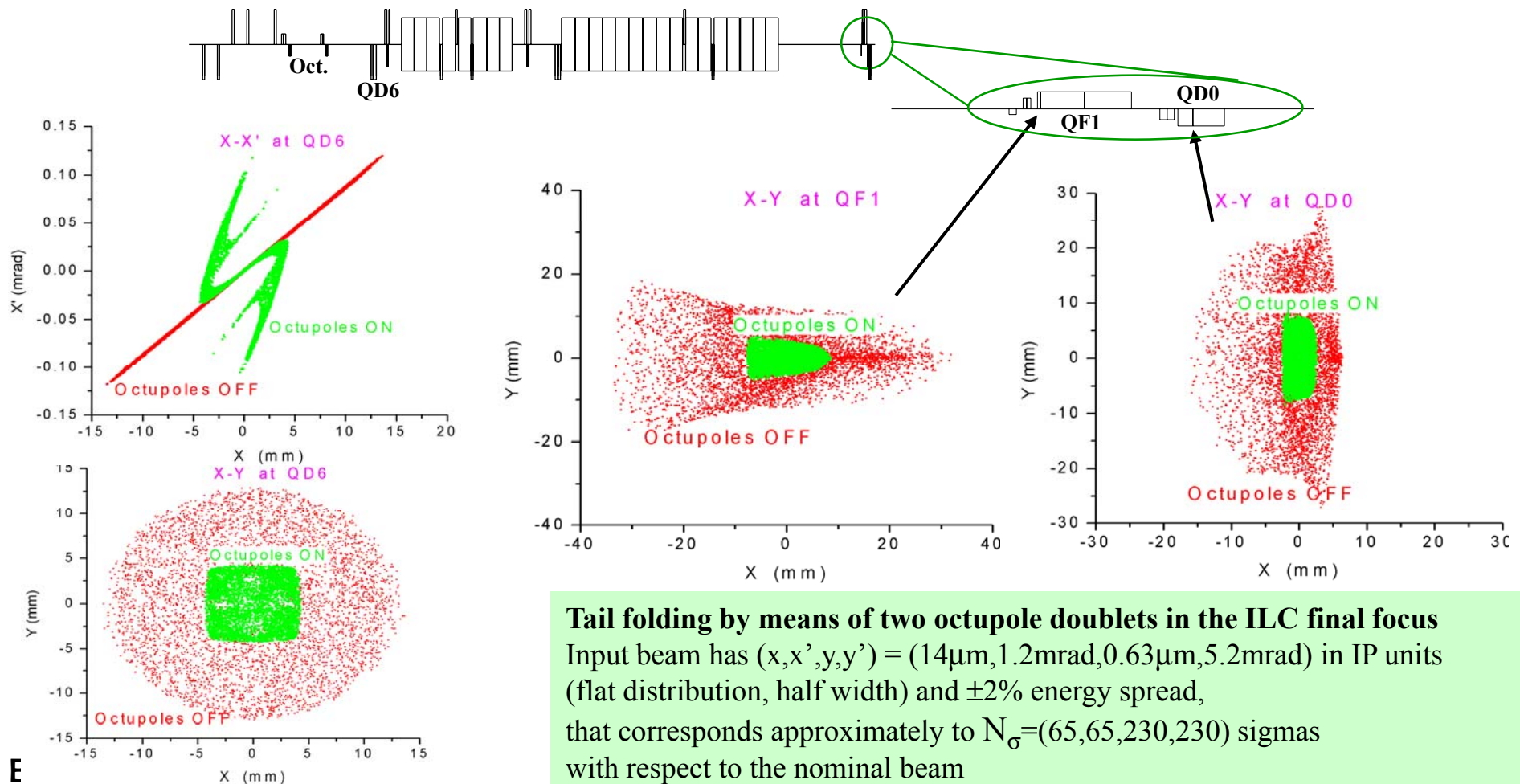
Effect of octupole doublet (Oc,Drift,-Oc) on parallel beam, $\Delta\Theta(x,y)$.

- For this to work, the beam should have **small angles**, i.e. it should be parallel or **diverging**



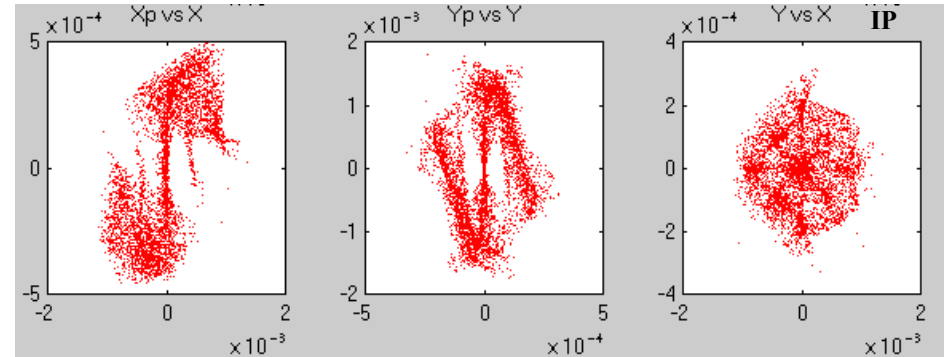
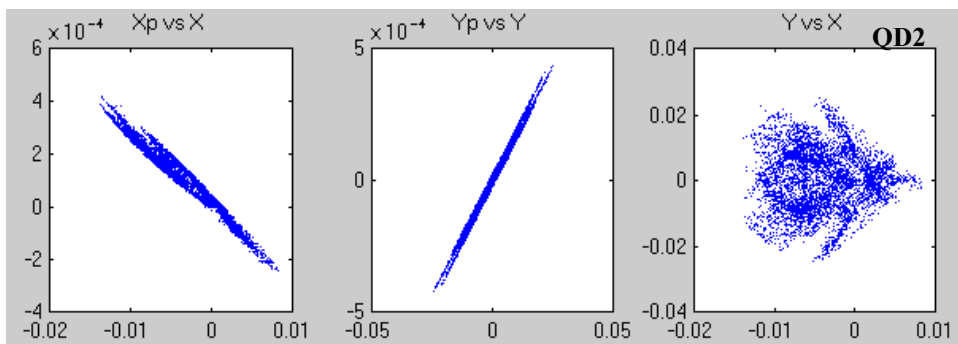
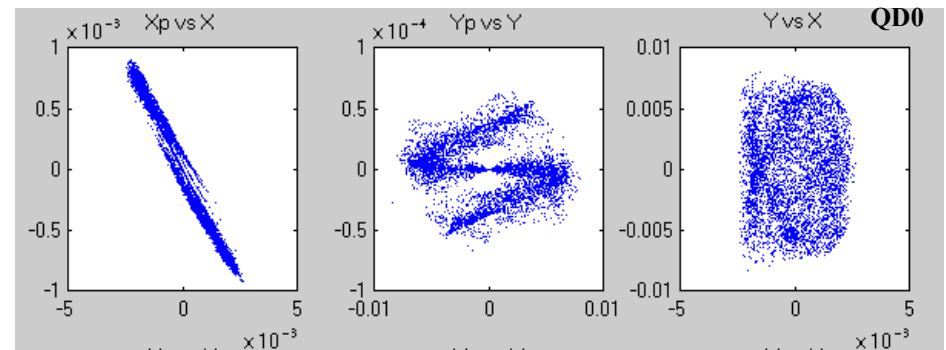
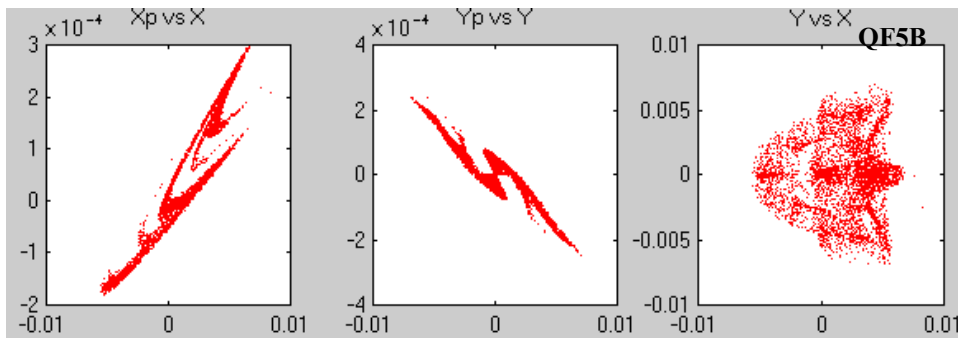
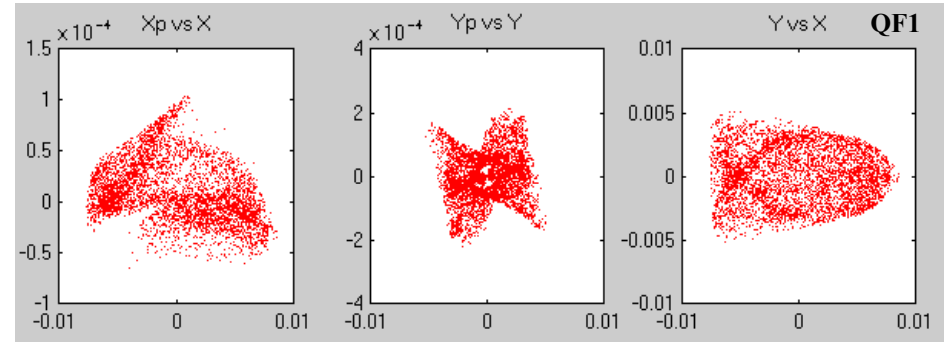
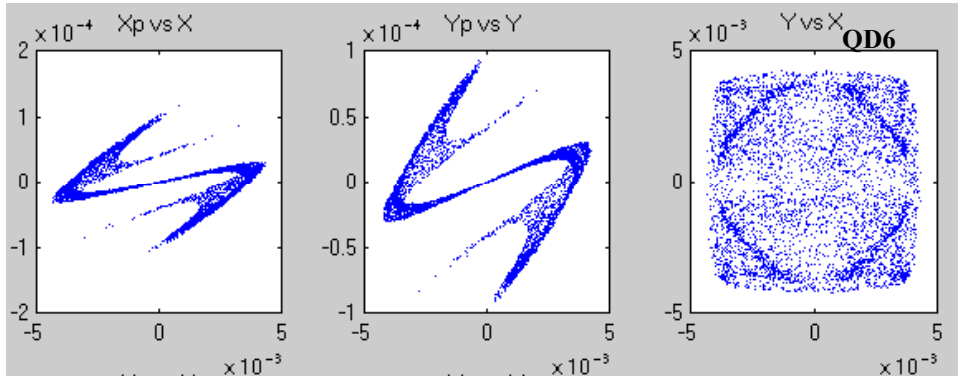
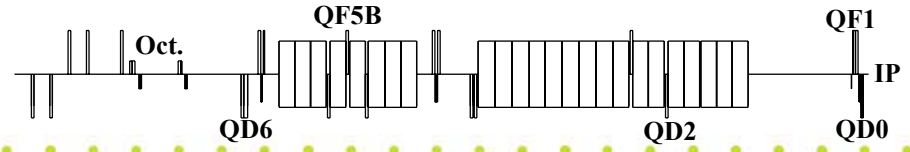
Tail folding in ILC FF

- **Two octupole doublets give tail folding by ~ 4 times in terms of beam size in FD**
- **This can lead to relaxing collimation requirements by \sim a factor of 4**

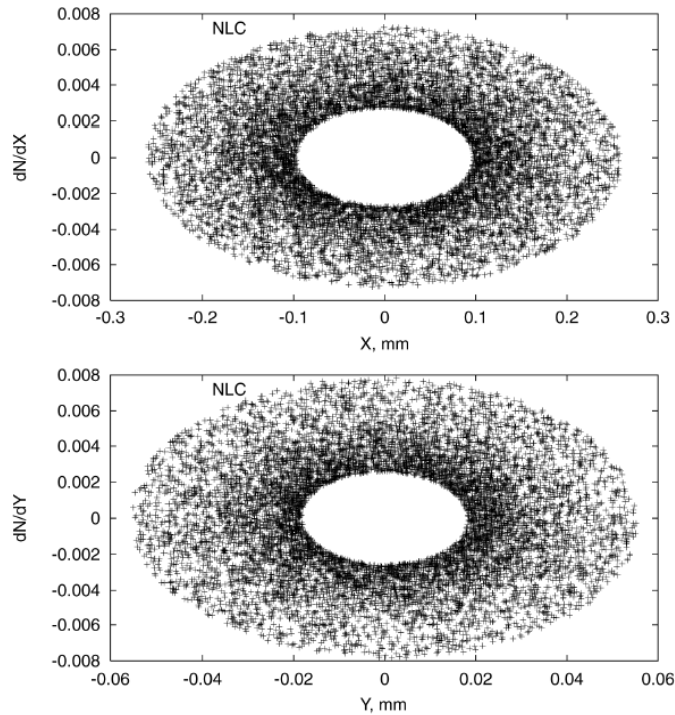




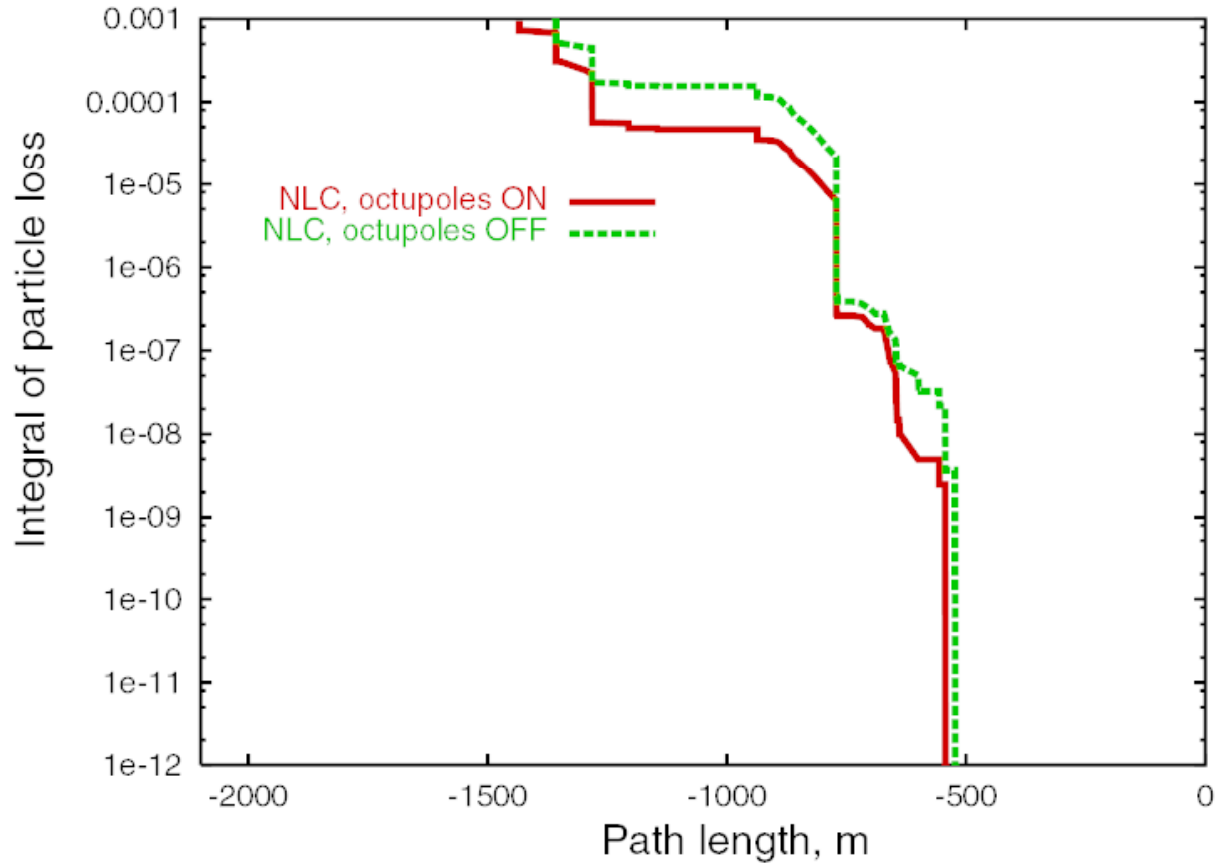
Tail folding *or Origami Zoo*



ilc Halo collimation



Assumed halo sizes. Halo population is 0.001 of the main beam.



Assuming 0.001 halo, beam losses along the beamline behave nicely, and SR photon losses occur only on dedicated masks

Smallest gaps are ± 0.6 mm with tail folding Octupoles and ± 0.2 mm without them.



Collimator wakes

- Effect from offset of the beam at the collimator:

$$\Delta y' = K y$$

- Assume that beam jitter is a fixed fraction of the beam size

$$\frac{\Delta y'}{\sigma_{y'}} = K \frac{\sigma_y}{\sigma_{y'}} \frac{y}{\sigma_y}$$

- Jitter amplification factor

$$A_\beta = K \frac{\sigma_y}{\sigma_{y'}}$$

For locations with $\alpha=0 \Rightarrow$

$$A_\beta = K \beta$$

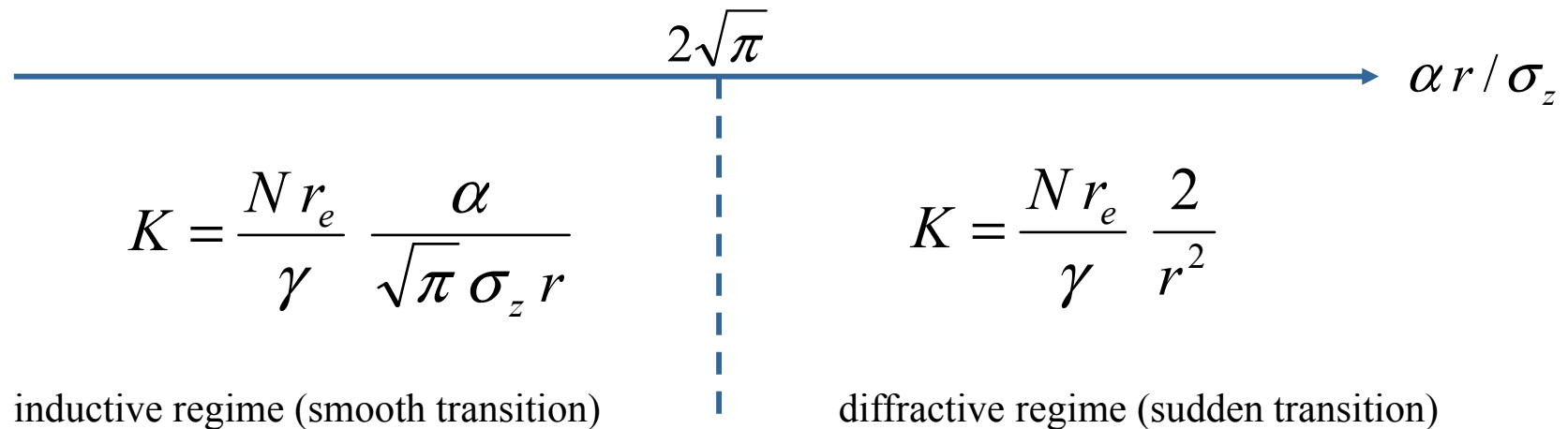
- If jitter is fraction of size in all planes, and y & y' not correlated, the fractional incoming jitter increases by

$$\sqrt{1 + A_\beta^2}$$



Wakes for tapered collimators

- Circular collimators



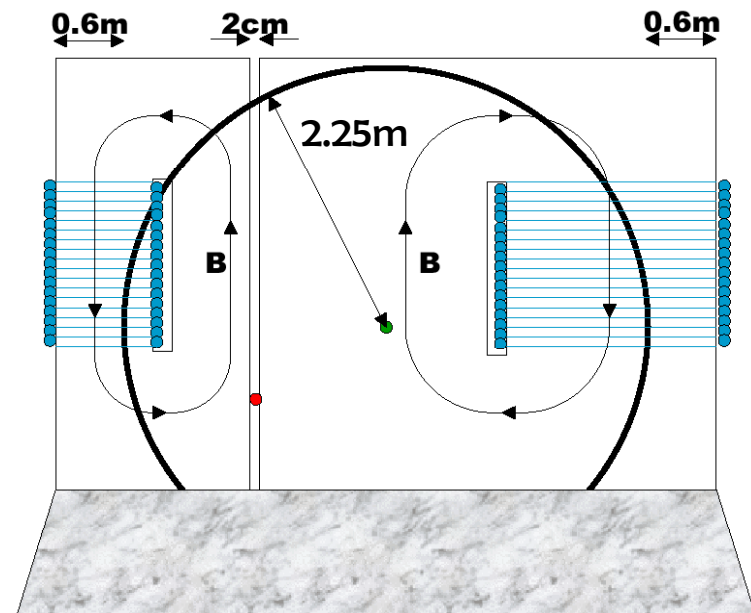
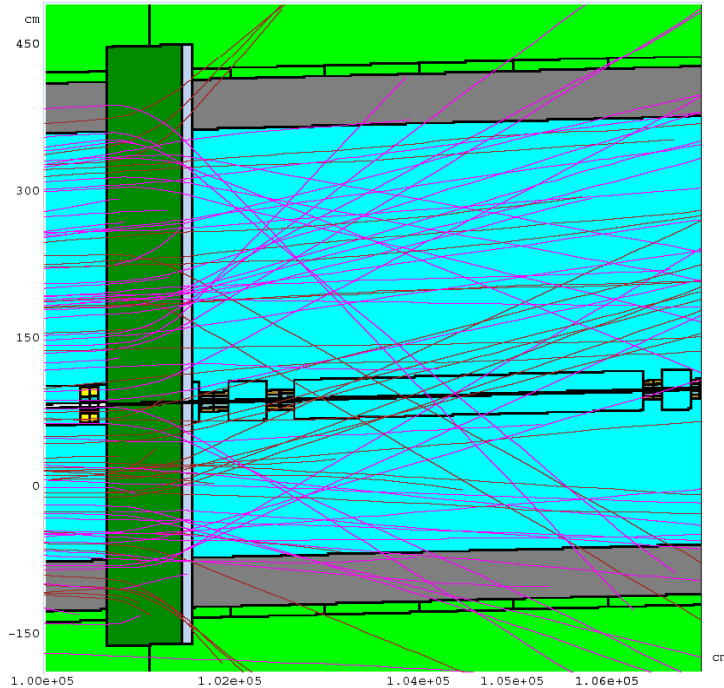
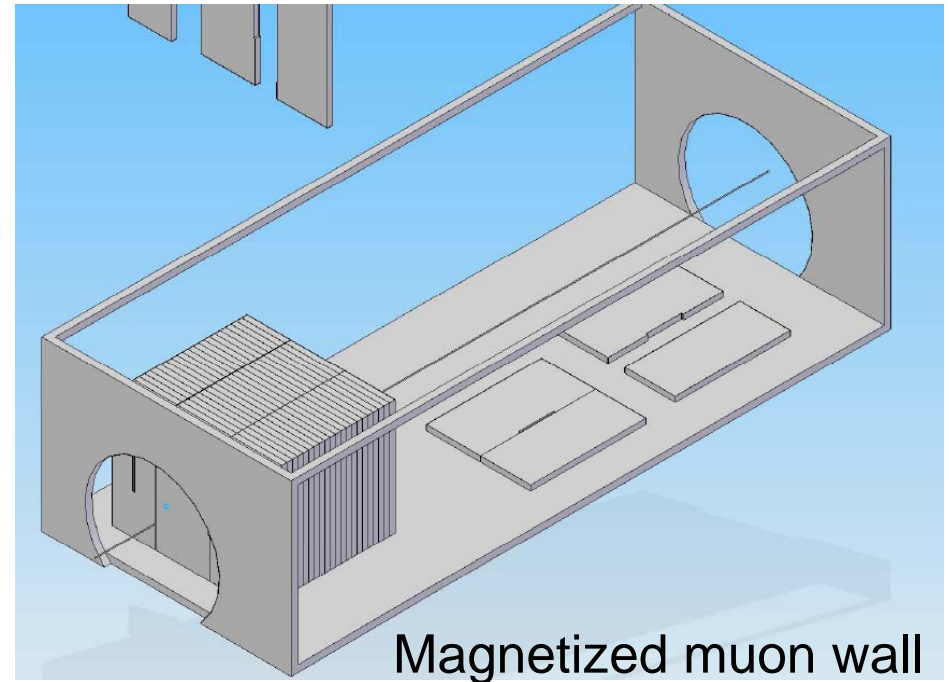
- where α is tapering angle, r is half gap

Following P.Tenenbaum, LCC-101 and G.Stupakov, PAC2001



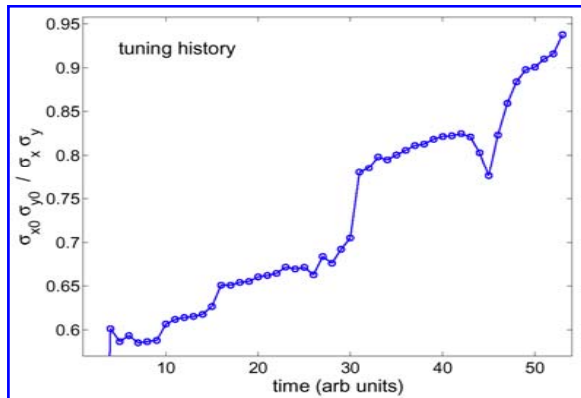
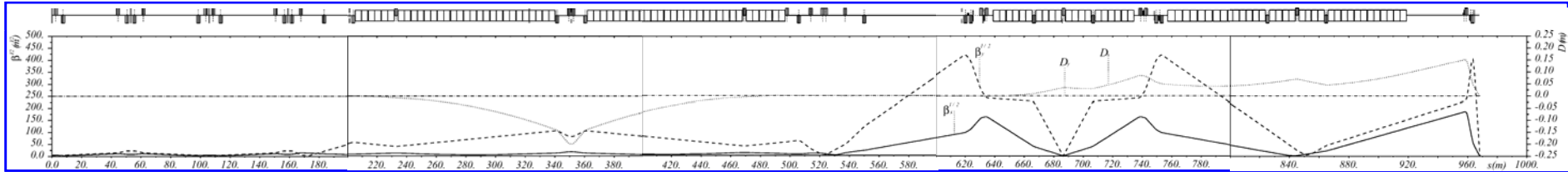
Dealing with muons in BDS

- Muons are produced during collimation
- Muon walls, installed ~300m from IP, reduce muon background in the detectors

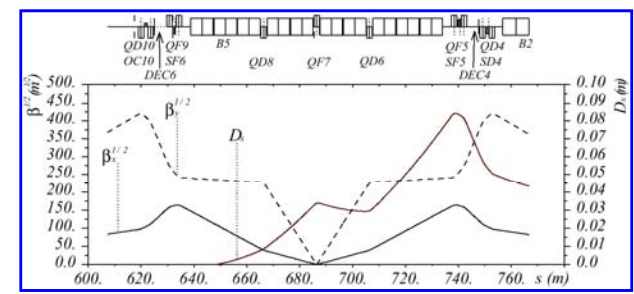
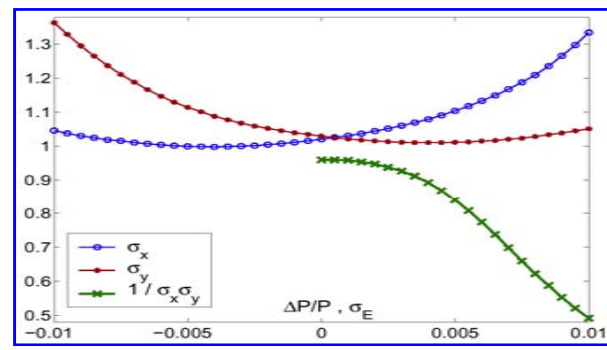
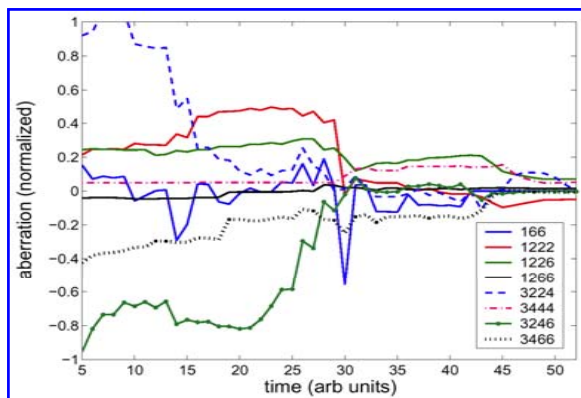
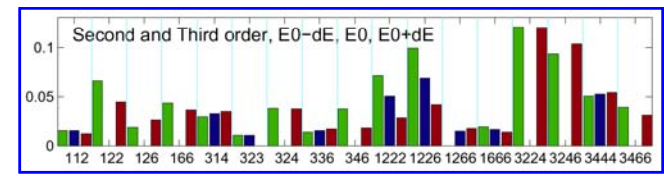
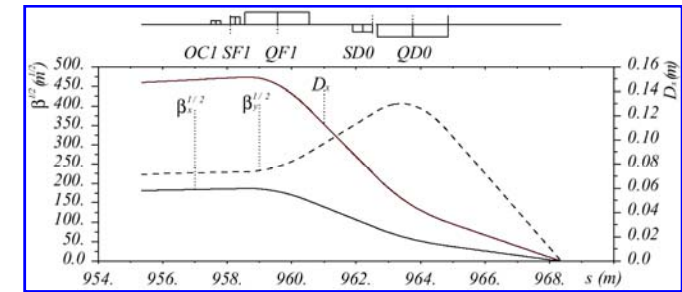




BDS design methods & examples



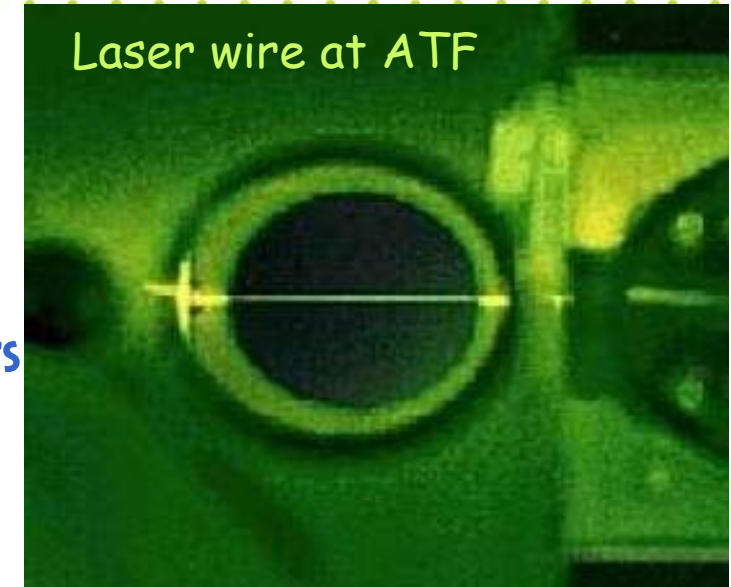
Example of a 2nd IR BDS optics for ILC; design history; location of design knobs





In a practical situation ...

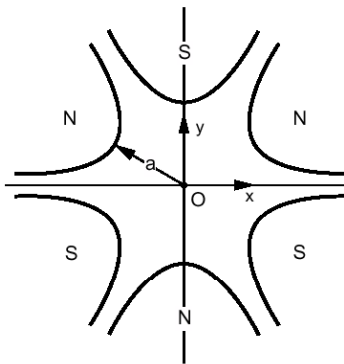
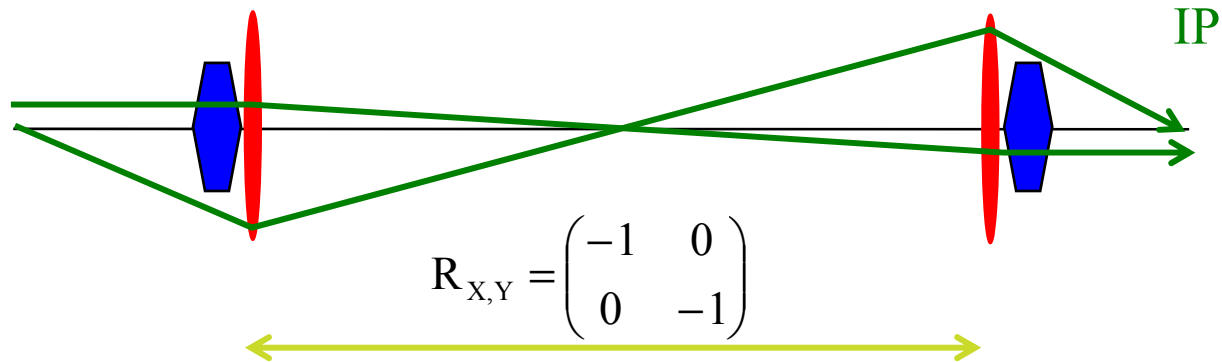
- While **designing** the FF, one has a **total control**
- When the system is built, one has just limited number of observable parameters (measured orbit position, beam size measured in several locations)
- The system, however, may initially have **errors** (errors of strength of the elements, transverse misalignments) and initial aberrations may be large
- **Tuning** of FF is done by optimization of “**knobs**” (strength, position of group of elements) chosen to affect some particular aberrations
- Experience in SLC FF and FFTB, and simulations with new FF give confidence that this is possible



Laser wire at ATF

Laser wire will be a tool for tuning and diagnostic of FF

Sextupole knobs for BDS tuning



SEXTUPOLE

Second order effect:

$$\begin{aligned} x' &= x' + S (x^2 - y^2) \\ y' &= y' - S 2xy \end{aligned}$$

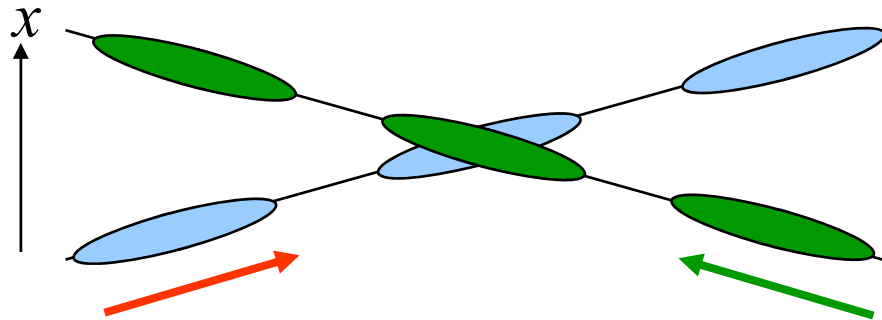
- Combining offsets of sextupoles (symmetrical or anti-symmetrical in X or Y), one can produce the following corrections at the IP

- waist shift
- coupling
- dispersion

To create these knobs, sextupole placed on movers

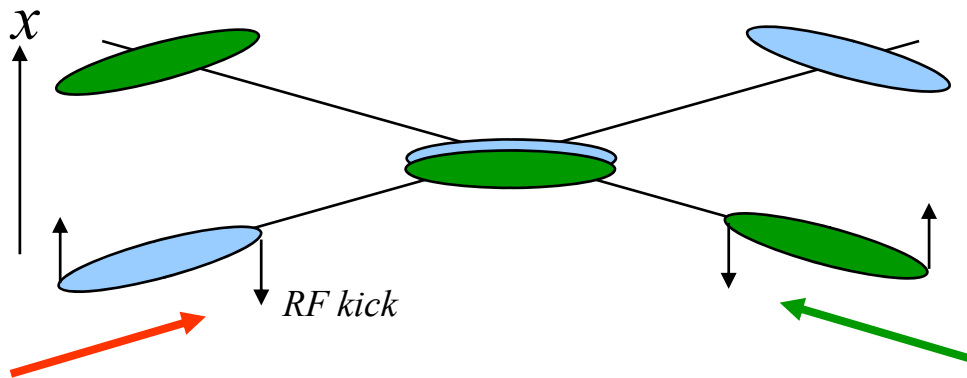


Crab crossing

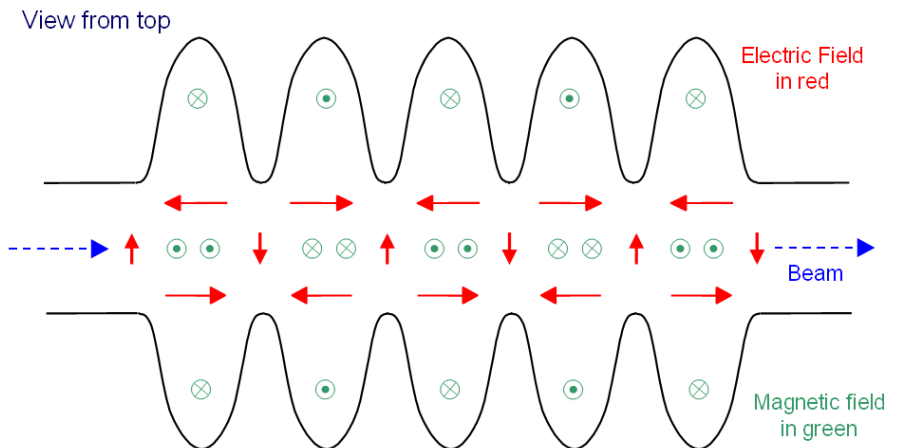


With crossing angle θ_c , the projected x-size is $(\sigma_x^2 + \theta_c^2 \sigma_z^2)^{0.5} \sim \theta_c \sigma_z \sim 4\mu\text{m}$

→ several time reduction in L without corrections



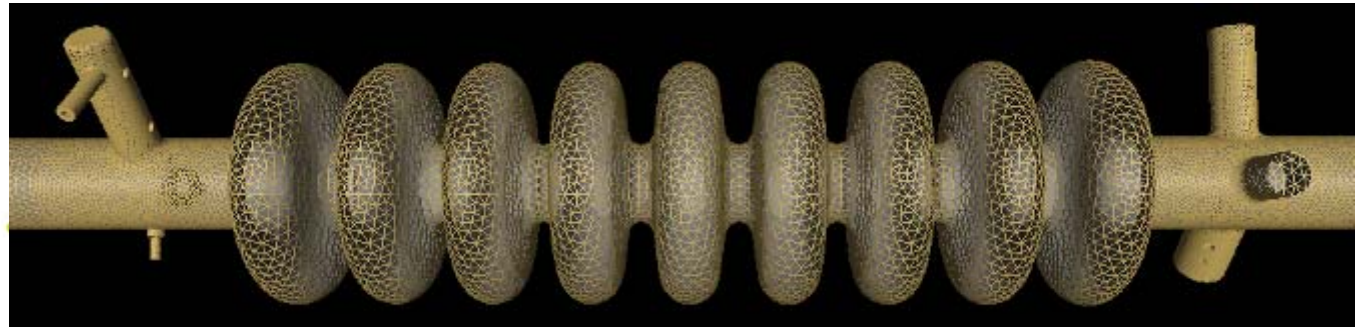
Use transverse (crab) RF cavity to 'tilt' the bunch at IP



For a crab cavity the bunch centre is at the cell centre when E is maximum and B is zero



Crab cavity design

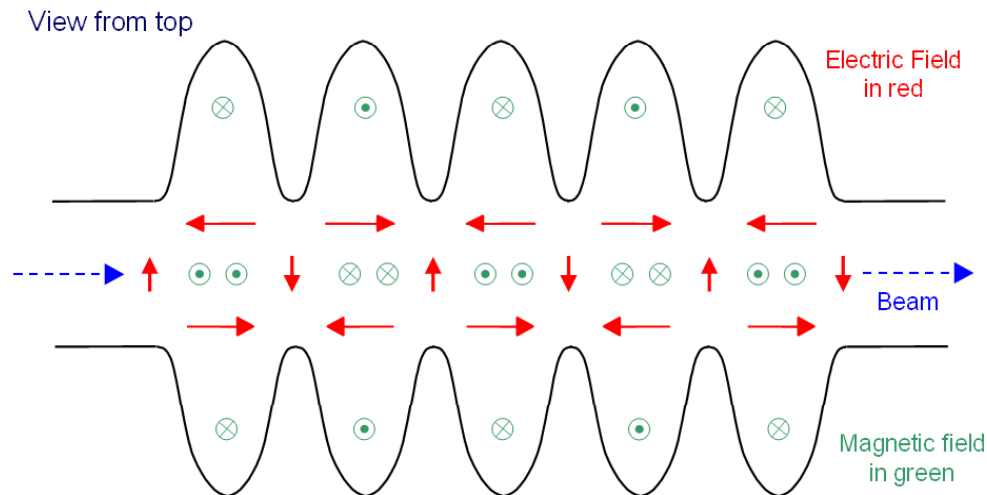


FNAL 3.9GHz 9-cell cavity in Opega3p. *K.Ko, et al*

- Prototypes of crab cavity built at FNAL and 3d RF models
- Design & prototypes been done by UK-FNAL-SLAC collaboration



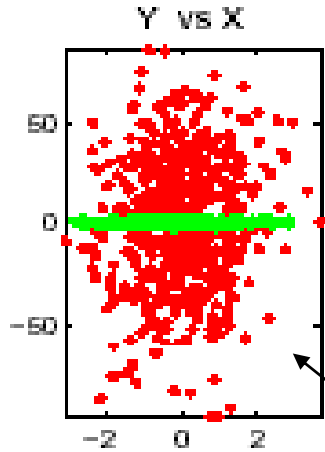
3.9GHz cavity achieved 7.5 MV/m (FNAL)



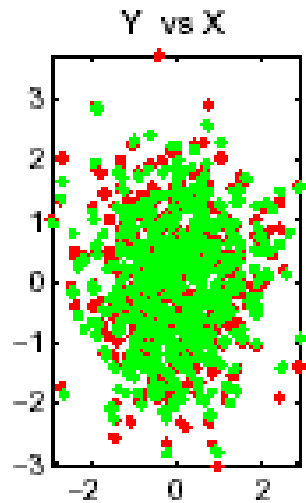
TM110 Dipole mode cavity

For a crab cavity the bunch centre is at the cell centre when E is maximum and B is zero

IR coupling compensation



without compensation
 $\sigma_y / \sigma_y(0) = 32$

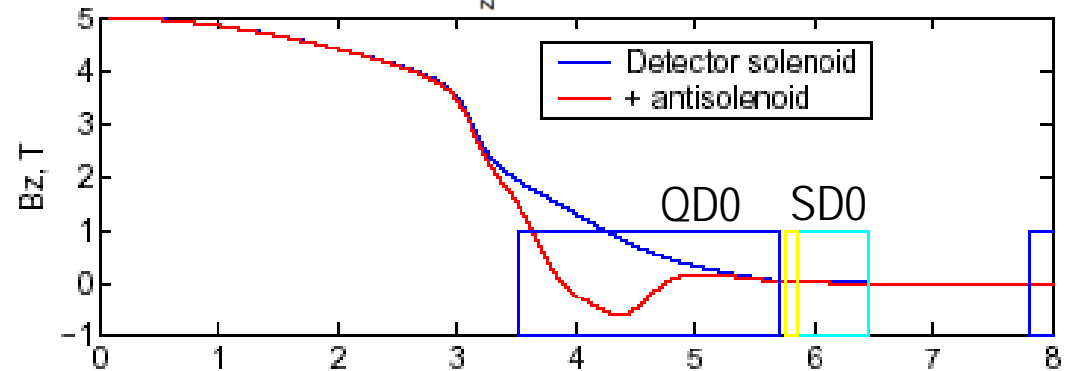
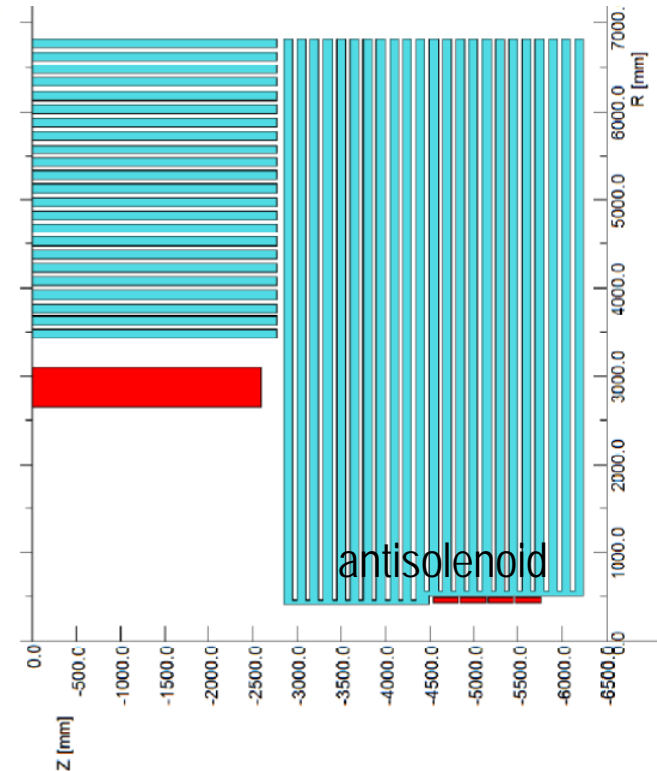


with compensation by antisolenoid
 $\sigma_y / \sigma_y(0) < 1.01$

BDS: 58

When detector solenoid overlaps QD0, coupling between y & x' and y & E causes large (30 – 190 times) increase of IP size (green=detector solenoid OFF, red=ON)

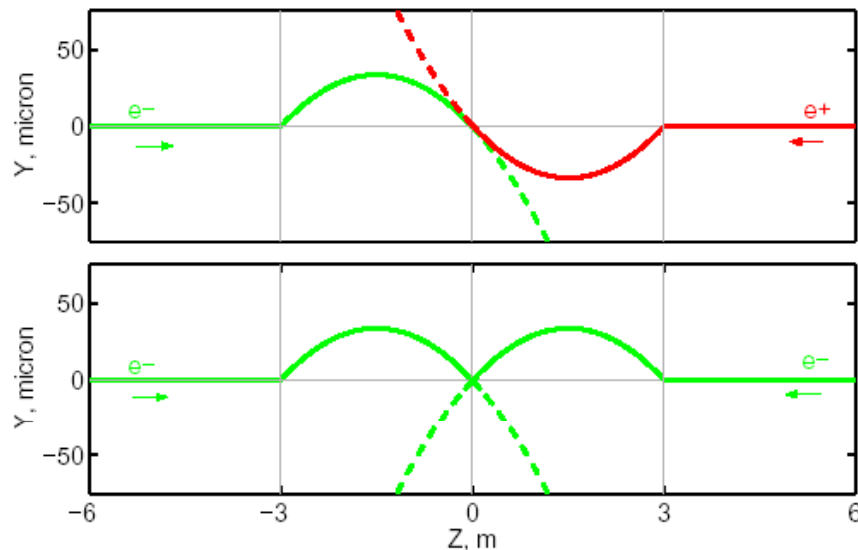
Even though traditional use of skew quads could reduce the effect, the local compensation of the fringe field (with a little skew tuning) is the most efficient way to ensure correction over wide range of beam energies



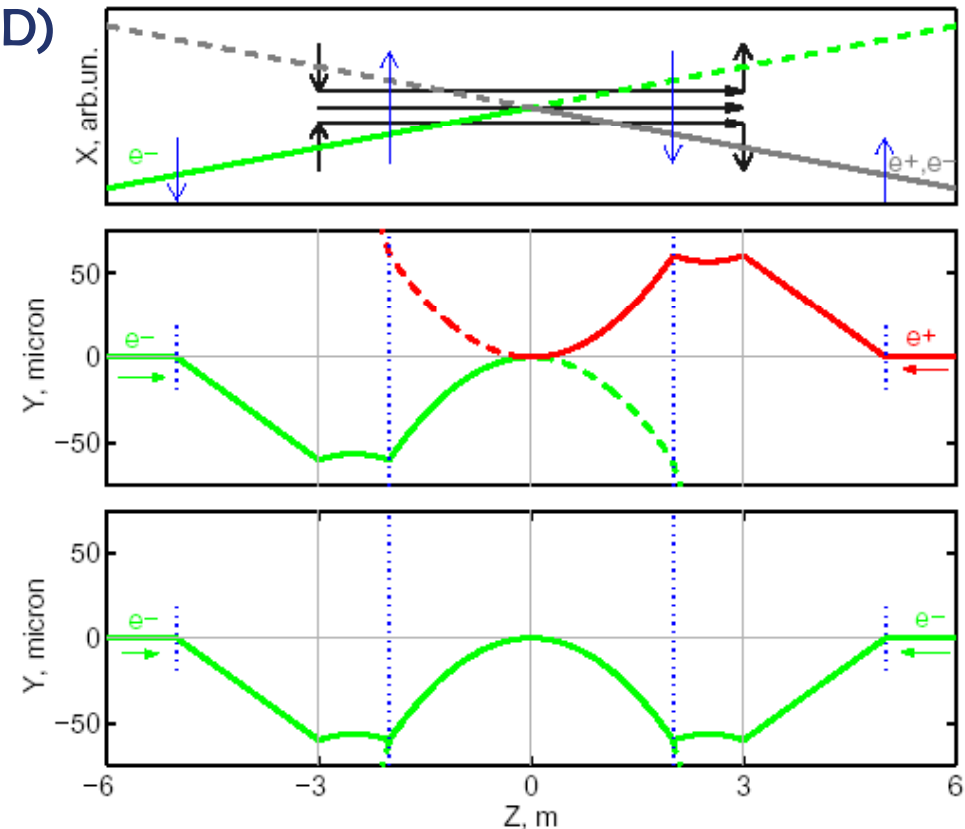


Detector Integrated Dipole

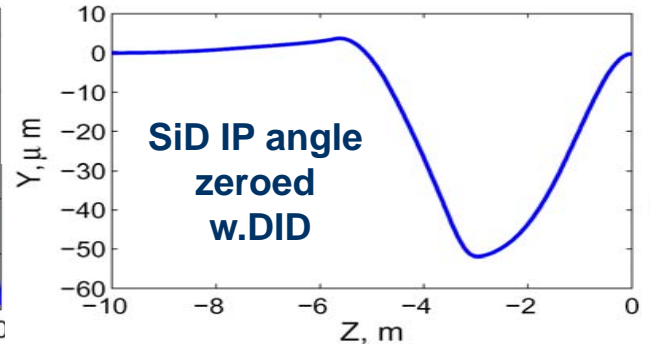
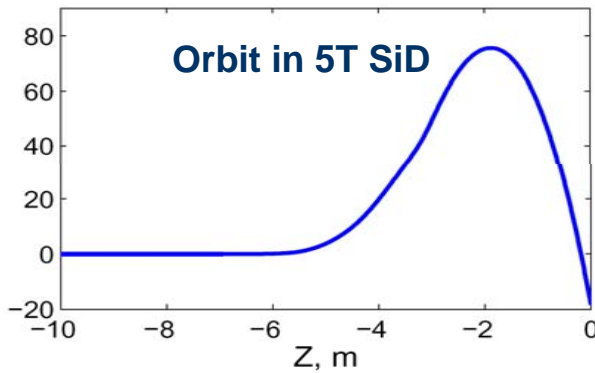
- With a crossing angle, when beams cross solenoid field, vertical orbit arise
- For e^+e^- the orbit is anti-symmetrical and beams still collide head-on
- If the vertical angle is undesirable (to preserve spin orientation or the e^-e^- luminosity), it can be compensated locally with DID
- Alternatively, negative polarity of DID may be useful to reduce angular spread of beam-beam pairs (anti-DID)



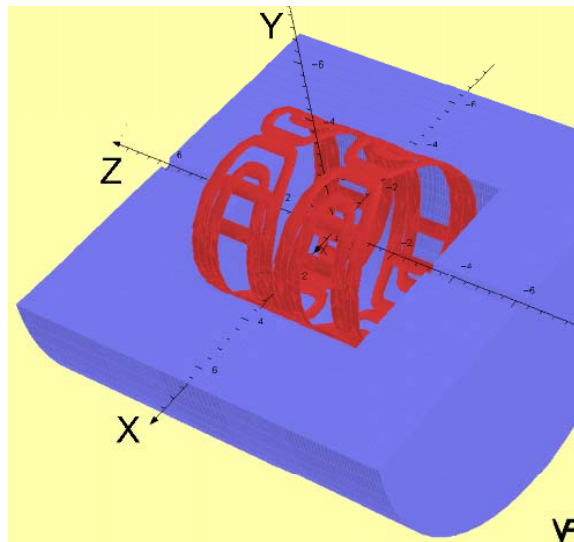
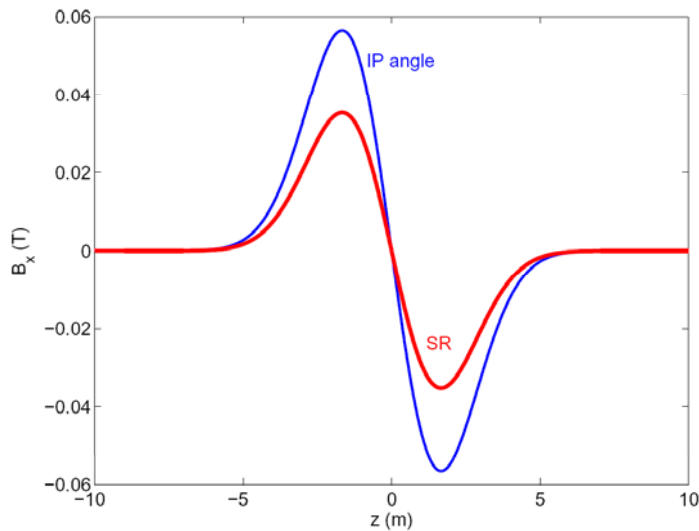
BDS: 59



Use of DID or anti-DID



DID field shape and scheme



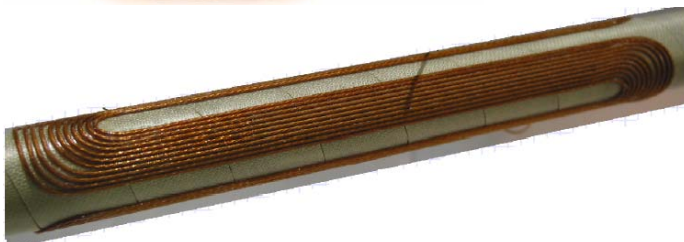
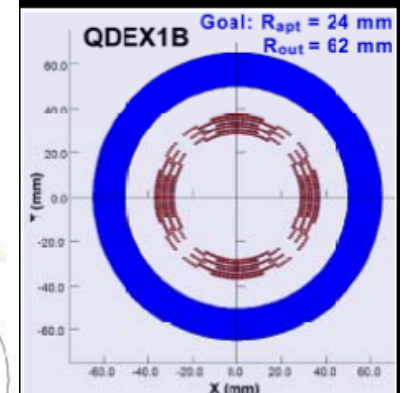
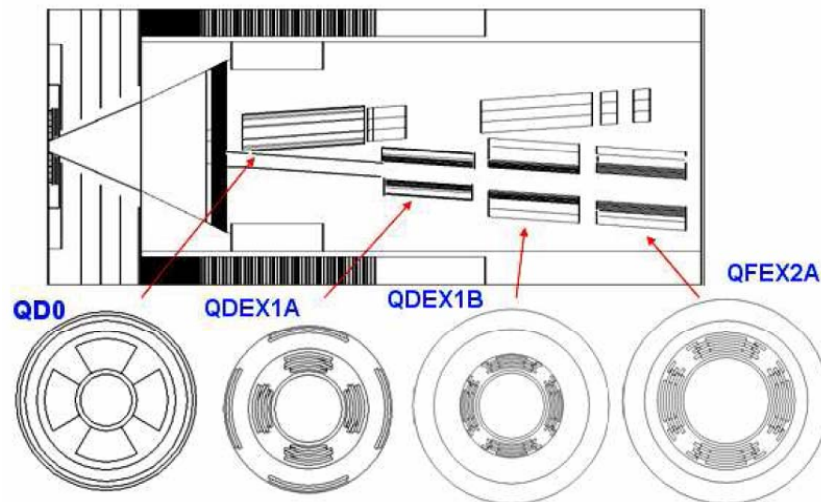
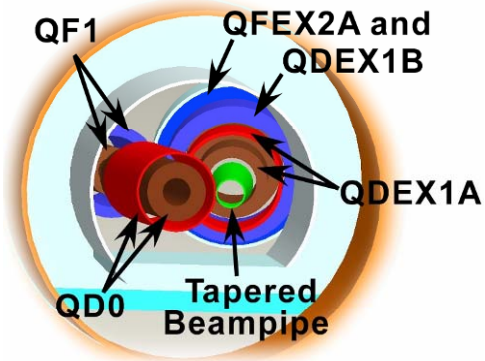
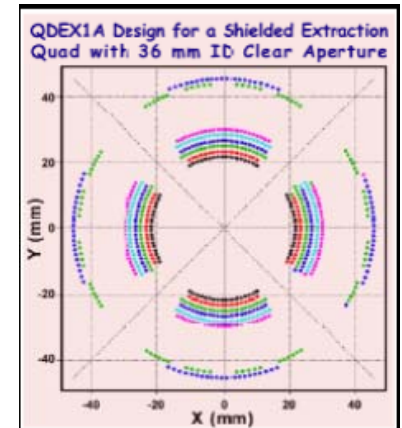
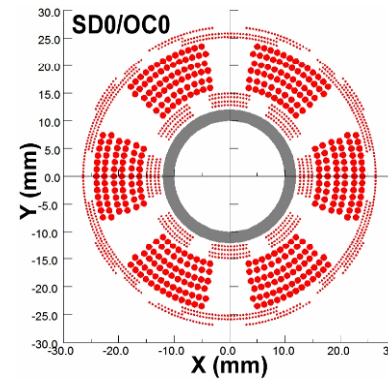
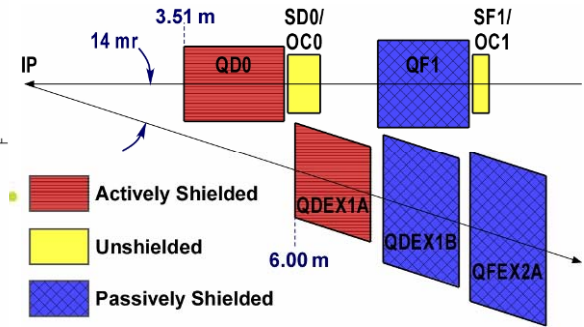
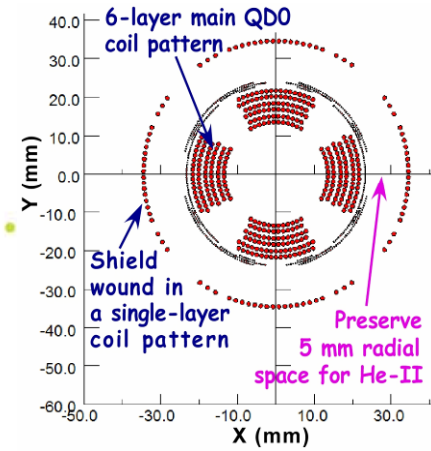
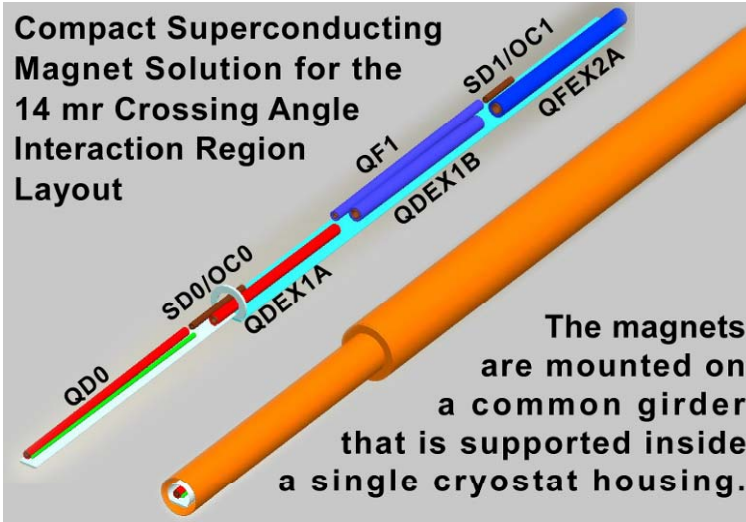
DID case

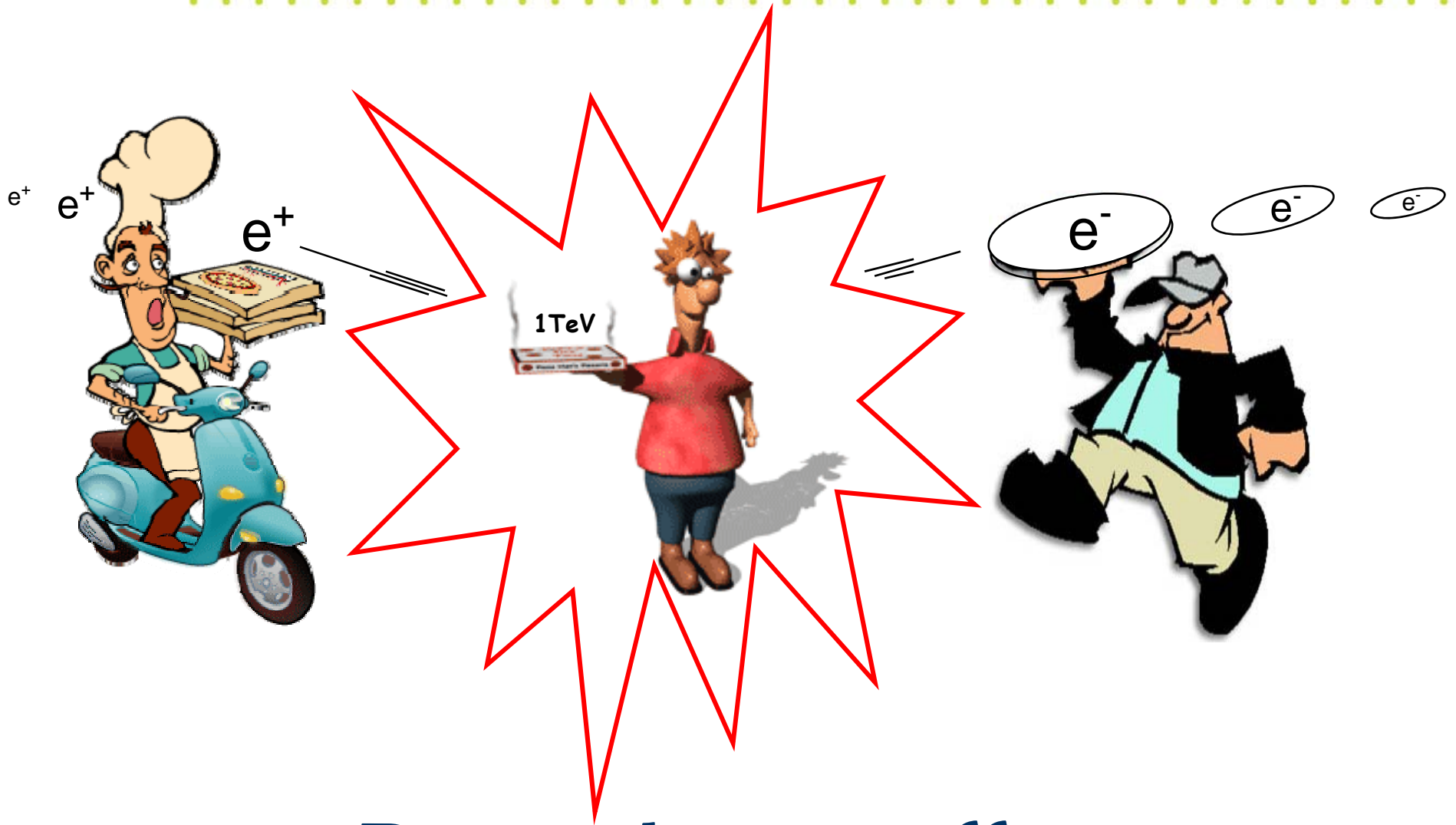
- The negative polarity of DID is also possible (called anti-DID)
- In this case the vertical angle at the IP is somewhat increased, but the background conditions due to low energy pairs (see below) and are improved



14 mrad IR

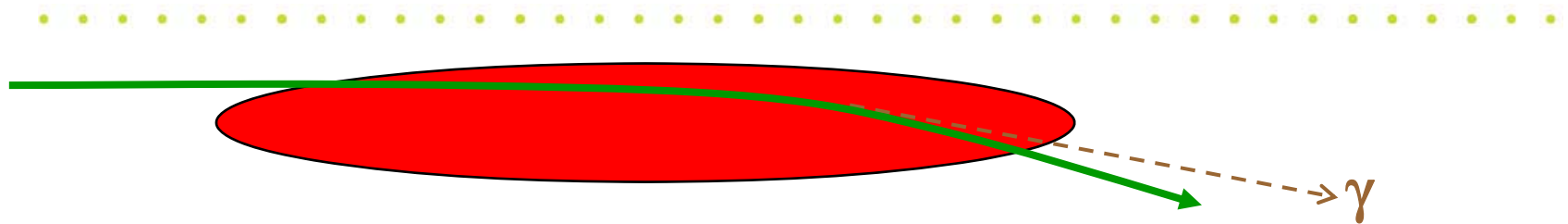
Compact Superconducting Magnet Solution for the 14 mr Crossing Angle Interaction Region Layout





Beam-beam effects

Beam-beam interactions



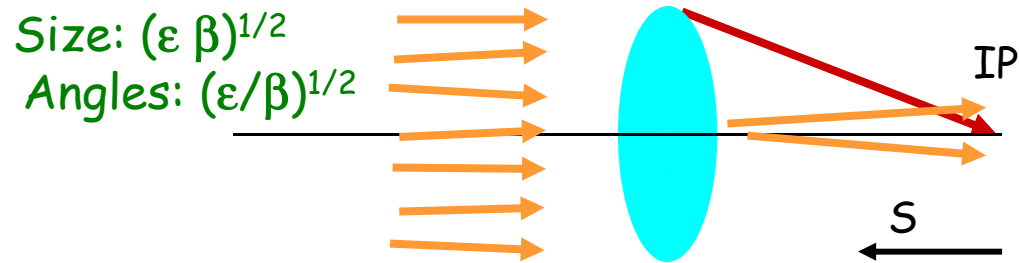
- **Transverse fields of ultra-relativistic bunch**
 - focus the incoming beam (electric and magnetic force add)
 - reduction of beam cross-section leads to more luminosity
 - H_D - the luminosity enhancement factor
 - bending of the trajectories leads to emission of beamstrahlung



Parameters of ILC BDS

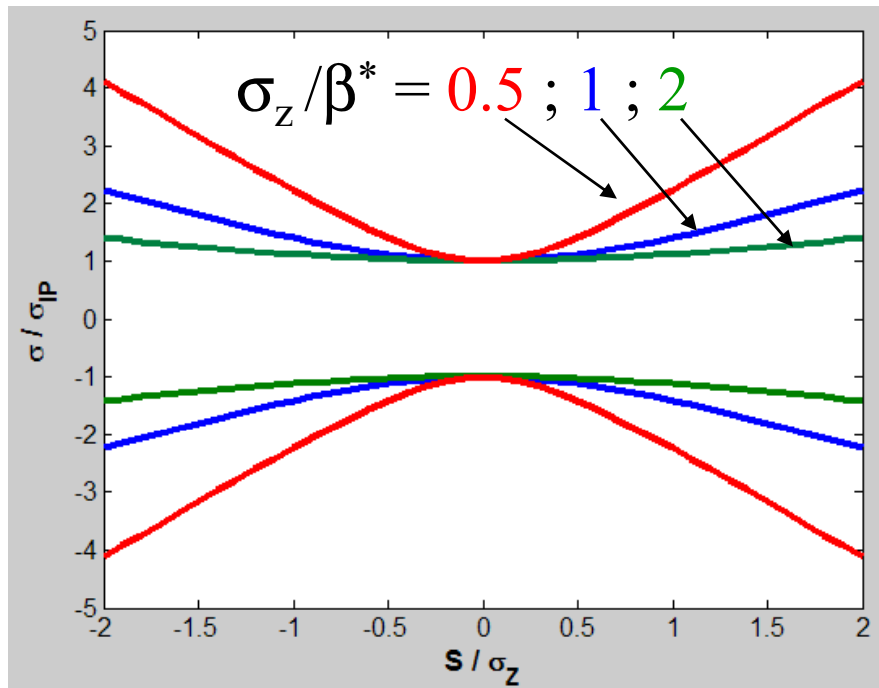
Length (linac exit to IP distance)/side	m	2226
Length of main (tune-up) extraction line	m	300 (467)
Max Energy/beam (with more magnets)	GeV	250 (500)
Distance from IP to first quad, L^*	m	3.5-(4.5)
Crossing angle at the IP	mrad	14
Nominal beam size at IP, σ^* , x/y	nm	655/5.7
Nominal beam divergence at IP, θ^* , x/y	μrad	31/14
Nominal beta-function at IP, β^* , x/y	mm	21/0.4
<u>Nominal bunch length, σ_z</u>	<u>μm</u>	<u>300</u>
<u>Nominal disruption parameters, x/y</u>		<u>0.162/18.5</u>
Nominal bunch population, N		2×10^{10}
Max beam power at main and tune-up dumps	MW	18
Preferred entrance train to train jitter	σ	< 0.5
Preferred entrance bunch to bunch jitter	σ	< 0.1
Typical nominal collimation depth, x/y		8-10/60
Vacuum pressure level, near/far from IP	nTorr	1/50

Hour-glass effect



Size at IP: $L^* (\epsilon/\beta)^{1/2}$

Beta at IP:
 $L^* (\epsilon/\beta)^{1/2} = (\epsilon \beta^*)^{1/2}$
 $\Rightarrow \beta^* = L^{*2}/\beta$

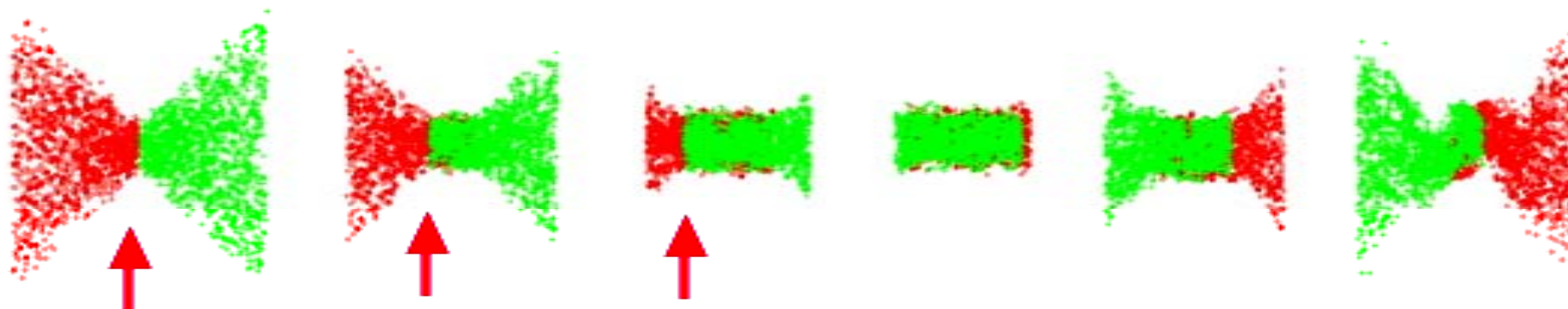


Behavior of beta-function
 along the final drift:

$$(\beta)^{1/2} = (\beta^* + S^2/\beta^*)^{1/2}$$

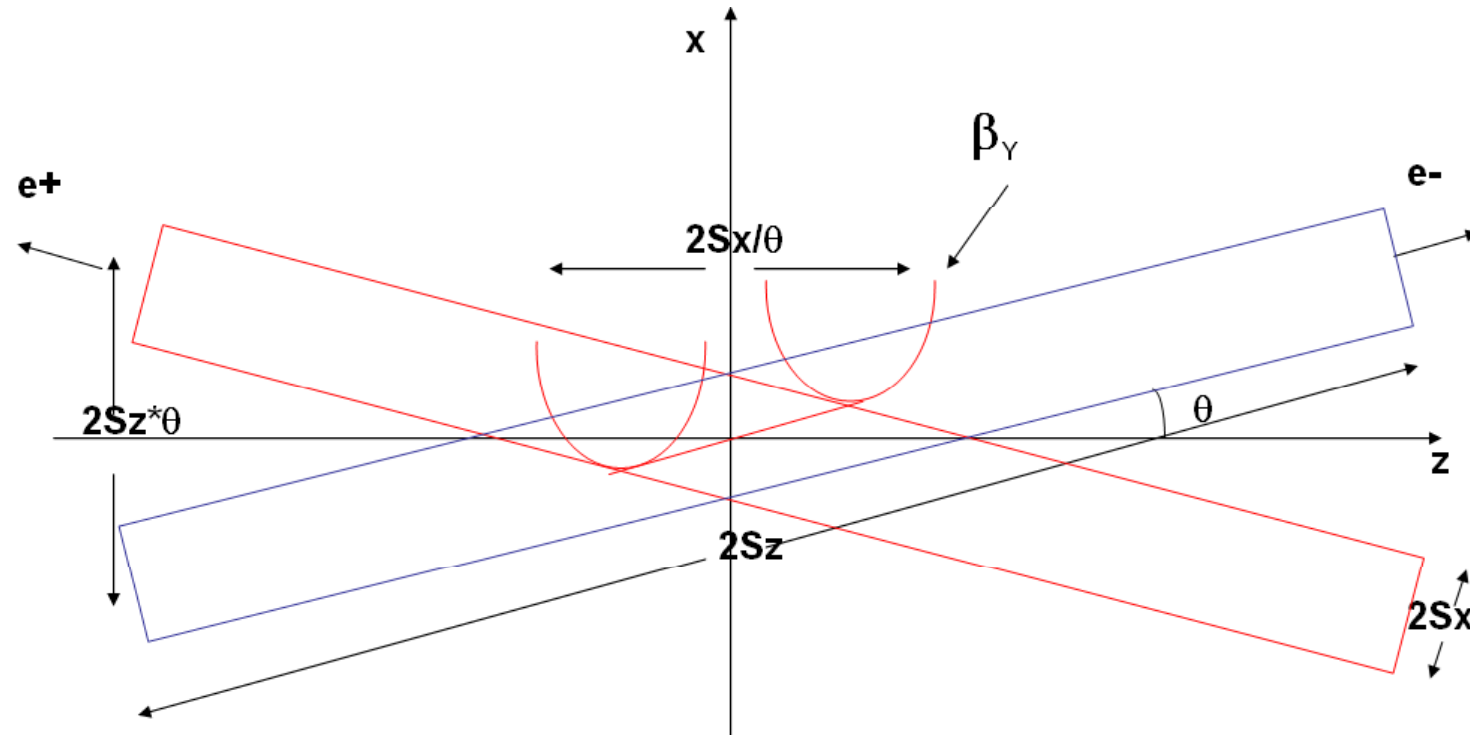
Reduction of β^* below σ_z does
 not give further decrease of
 effective beam size (usually)

Beam-beam: Travelling focus



- Suggested by V.Balakin – idea is to use beam-beam forces for additional focusing of the beam – allows some gain of luminosity or overcome somewhat the hour-glass effect
- Figure shows simulation of traveling focus. The arrows show the position of the focus point during collision
- So far not yet used experimentally

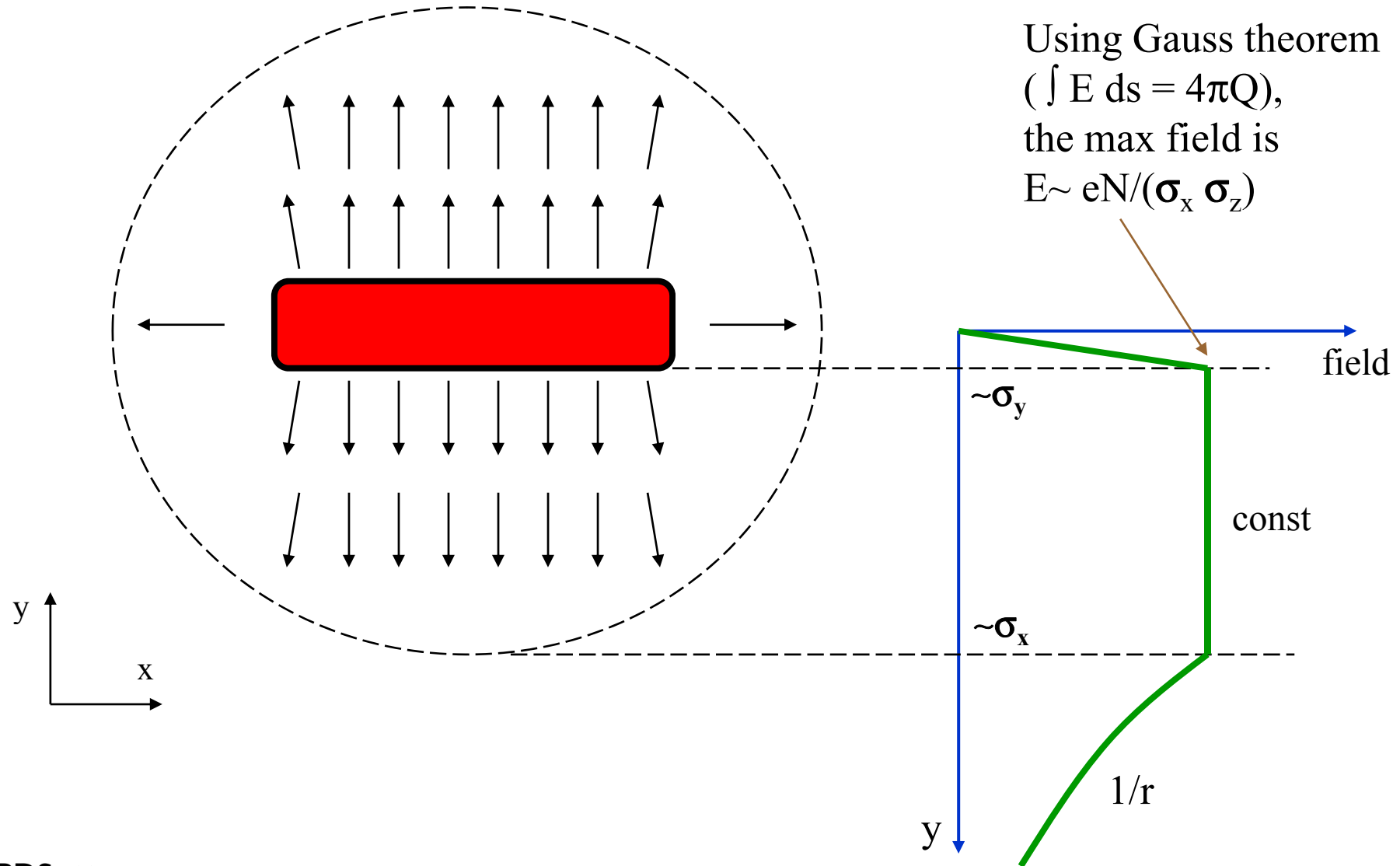
Beam-beam: Crabbed-waist



- Suggested by P.Raimondi for Super-B factory
- Vertical waist has to be a function of X . In this case coupling produced by beam-beam is eliminated
- Preparations for experimental verification are ongoing at DAFNE



Fields of flat bunch, qualitatively





Disruption parameter

- For Gaussian transverse beam distribution, and for particle near the axis, the beam kick results in the final particle angle:

$$\Delta x' = \frac{dx}{dz} = -\frac{2Nr_e}{\gamma\sigma_x(\sigma_x + \sigma_y)} \cdot x \quad \Delta y' = \frac{dy}{dz} = -\frac{2Nr_e}{\gamma\sigma_y(\sigma_x + \sigma_y)} \cdot y$$

- “Disruption parameter” – characterize focusing strength of the field of the bunch ($D_y \sim \sigma_z/f_{\text{beam}}$)

$$D_x = \frac{2Nr_e\sigma_z}{\gamma\sigma_x(\sigma_x + \sigma_y)} \quad D_y = \frac{2Nr_e\sigma_z}{\gamma\sigma_y(\sigma_x + \sigma_y)}$$

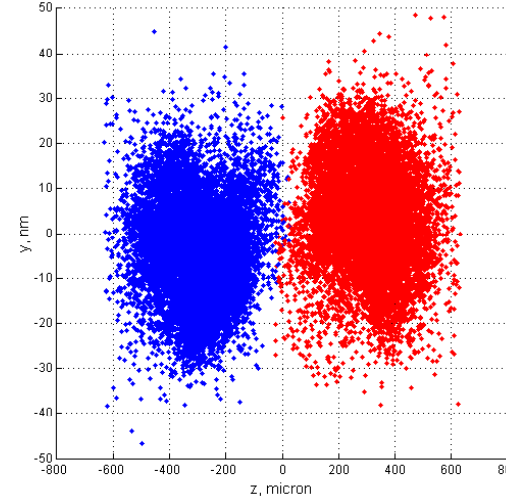
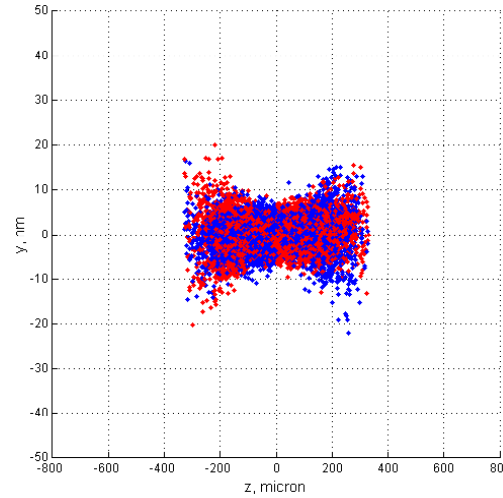
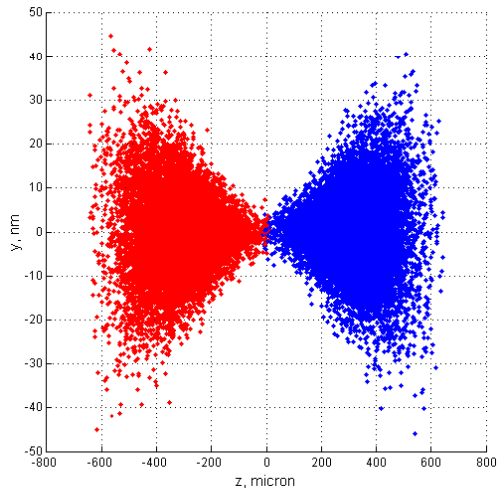
- $D \ll 1$ – bunch acts as a thin lens
- $D \gg 1$ – particle oscillate in the field of other bunch
 - If D is bigger than ~ 20 , instability may take place



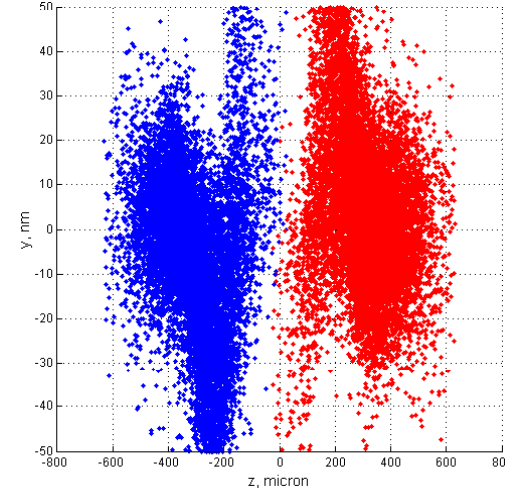
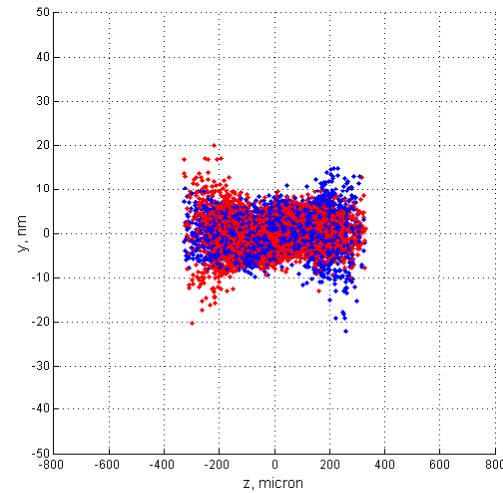
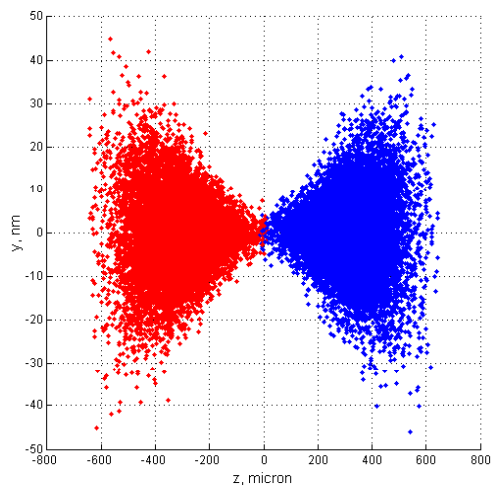
Beam-beam effects

H_D and instability

$$D_y = \frac{2r_e}{\gamma} \frac{N\sigma_z}{\sigma_x\sigma_y}$$



$D_y \sim 12$

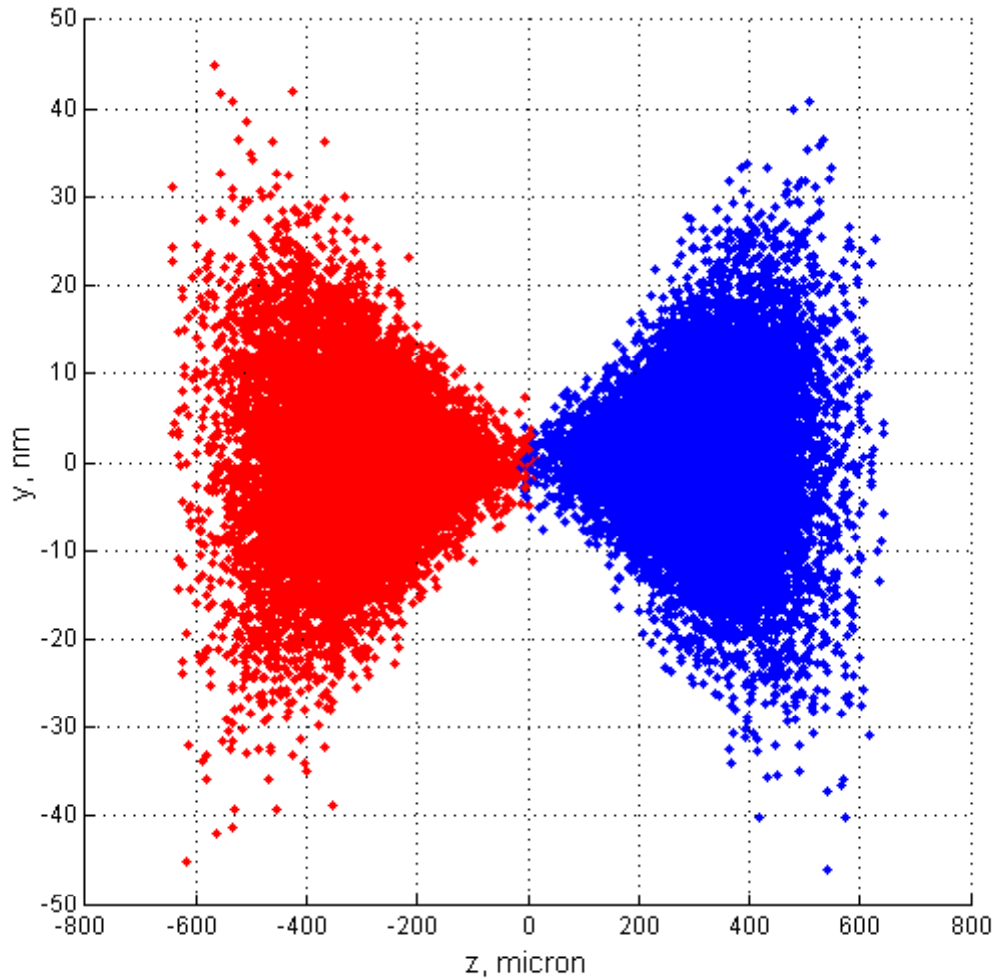


$N \times 2$
 $D_y \sim 24$



Beam-beam effects

H_D and instability



LC parameters
 $D_y \sim 12$

Luminosity
enhancement
 $H_D \sim 1.4$

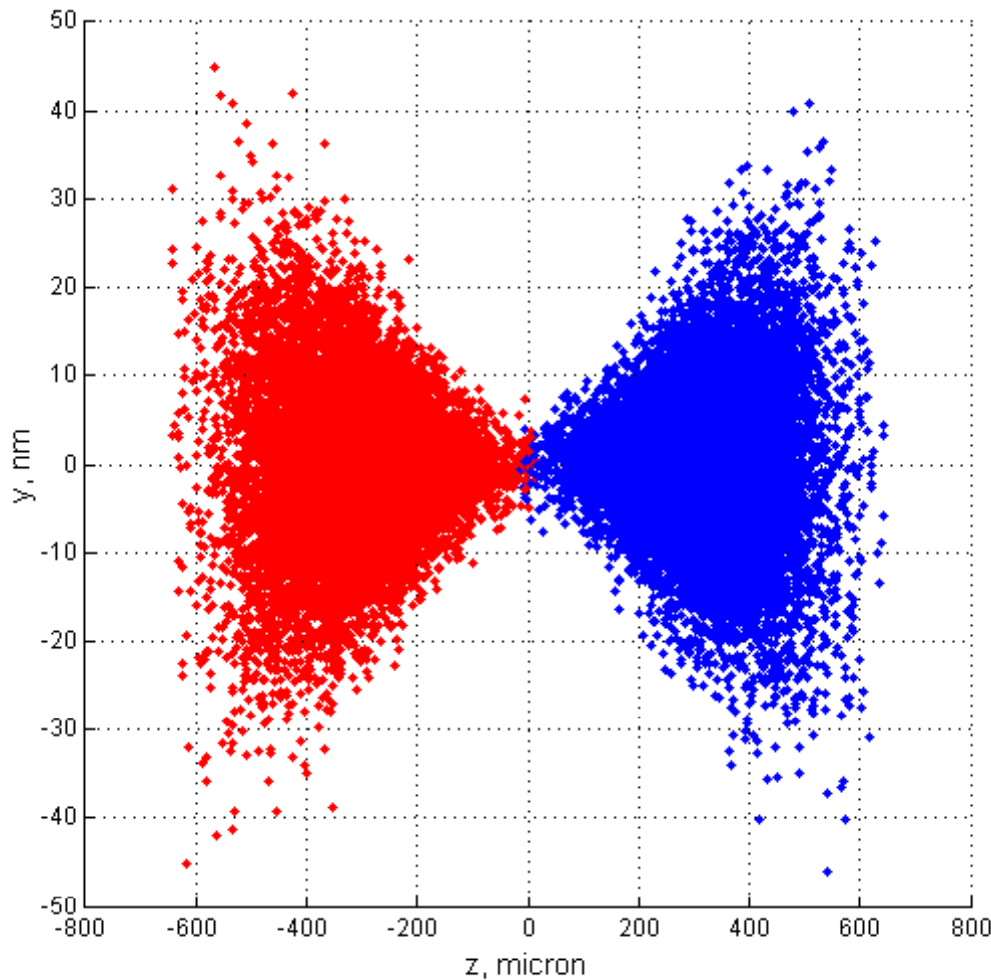
Not much of an
instability





Beam-beam effects

H_D and instability



$N \times 2$
 $D_y \sim 24$

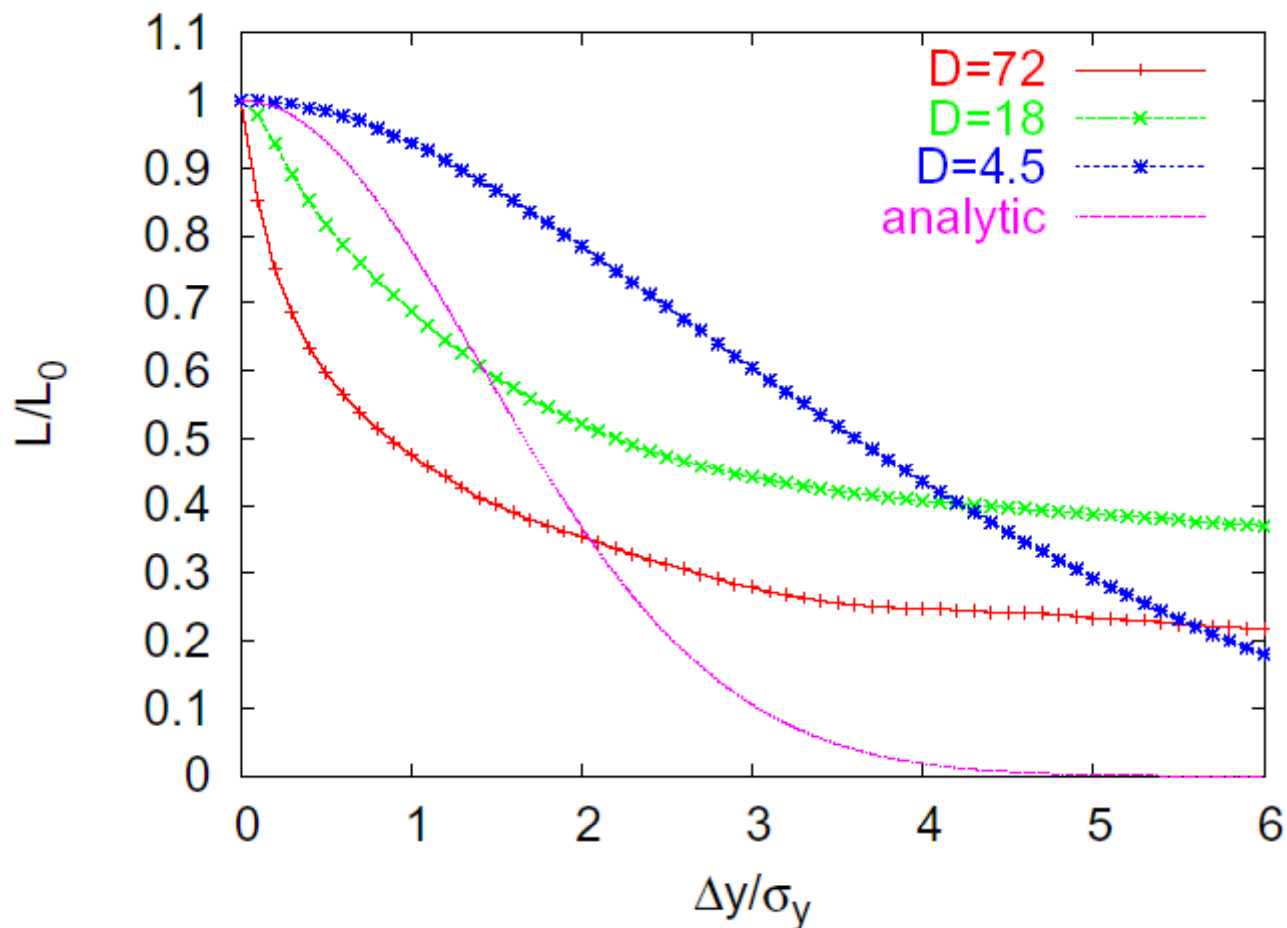
Beam-beam
instability is
clearly
pronounced

Luminosity
enhancement is
compromised by
higher
sensitivity to
initial offsets





Sensitivity to offset at IP



- Luminosity (normalized) versus offset at IP for different disruption parameters



Beamstrahlung

- Synchrotron radiation in field of opposite bunch
- Estimate R of curvature as $R \sim \sigma_z^2 / (D_y \sigma_y)$
- Using formulas derived earlier, estimate ω_c and find that $h\omega_c/E \sim \gamma N r_e^2 / (\alpha \sigma_x \sigma_z)$ and call it “Upsilon”

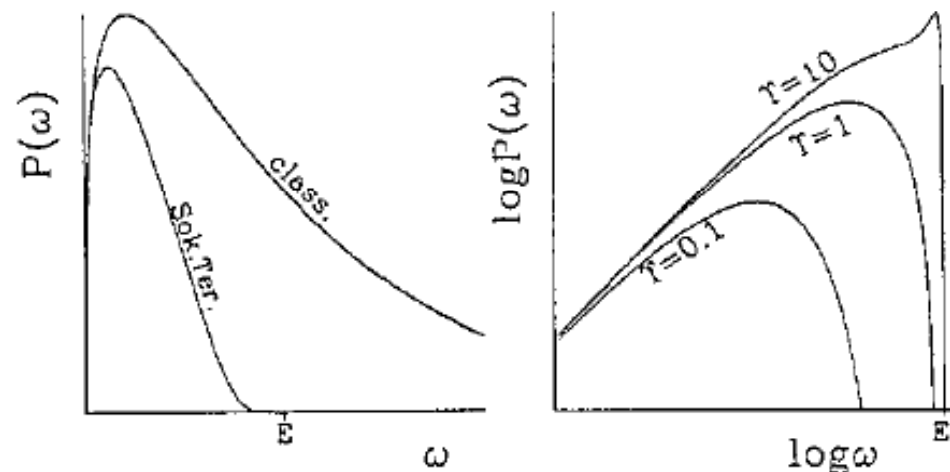
More accurate formula:
$$\Upsilon_{avg} \approx \frac{5}{6} \frac{N r_e^2 \gamma}{\alpha \sigma_z (\sigma_x + \sigma_y)}$$

- The energy loss also can be estimated from earlier derived formulas: $dE/E \sim \gamma r_e^3 N^2 / (\sigma_z \sigma_x^2)$
 - This estimation is very close to exact one
- Number of γ per electron estimated $n_{\gamma/e} \sim \alpha r_e N / \sigma_x$
 - which is usually around one γ per e



Classical and quantum regime

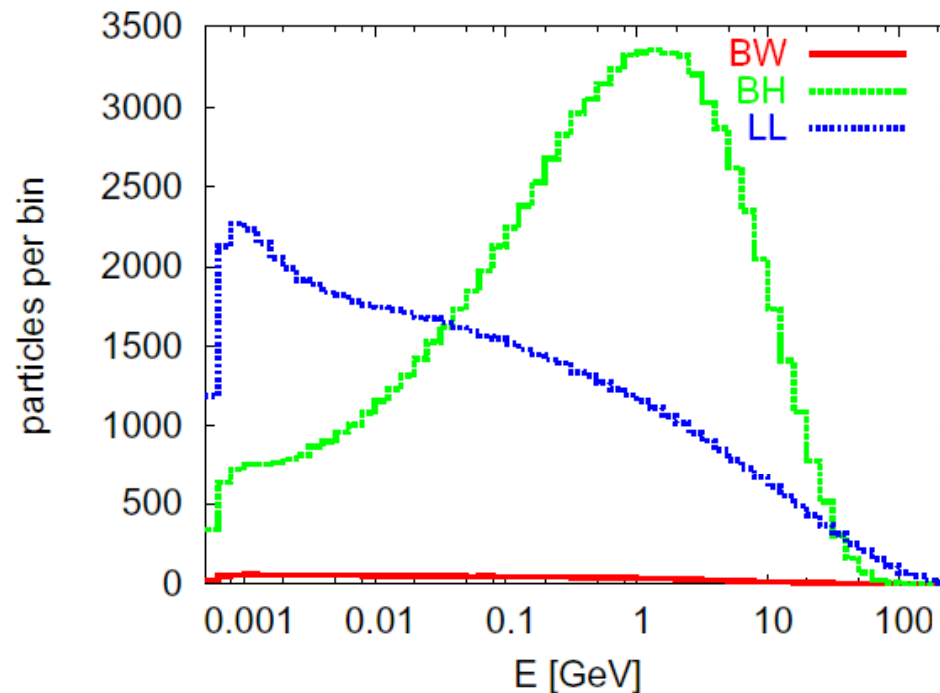
- The “upsilon” parameter, when it is $\ll 1$, has meaning of ratio of photon energy to beam energy
- When Upsilon become ~ 1 and larger, the classical regime of synchrotron radiation is not applicable, and quantum SR formulas of Sokolov-Ternov should be used.
- Spectrum of SR change ...



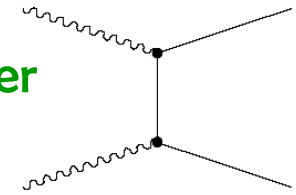


Incoherent* production of pairs

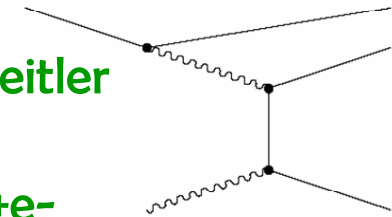
- Beamstrahlung photons, particles of beams or virtual photons interact, and create e^+e^- pairs



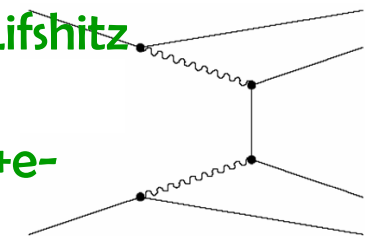
Breit-Wheeler
process
 $\gamma\gamma \rightarrow e^+e^-$



Bethe-Heitler
process
 $e\gamma \rightarrow ee^+e^-$



Landau-Lifshitz
process
 $ee \rightarrow eee^+e^-$



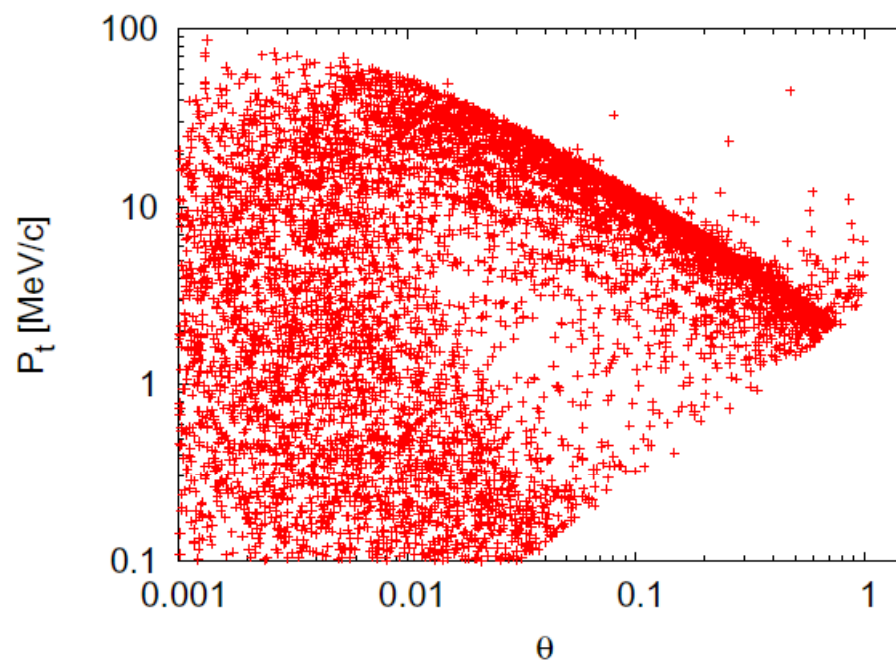
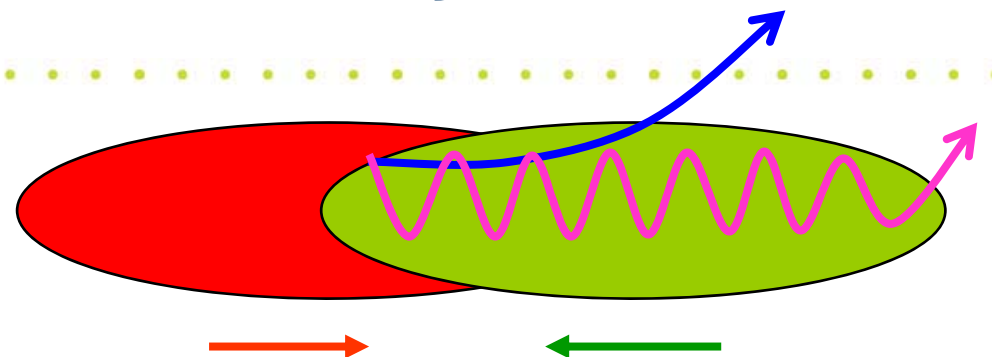
*) Coherent pairs are generated by photon in the field of opposite bunch. It is negligible for ILC parameters.

Deflection of pairs by beam

- Pairs are affected by the beam (focused or defocused)
- Deflection angle and P_t correlate
- Max angle estimated as (where ϵ is fractional energy):

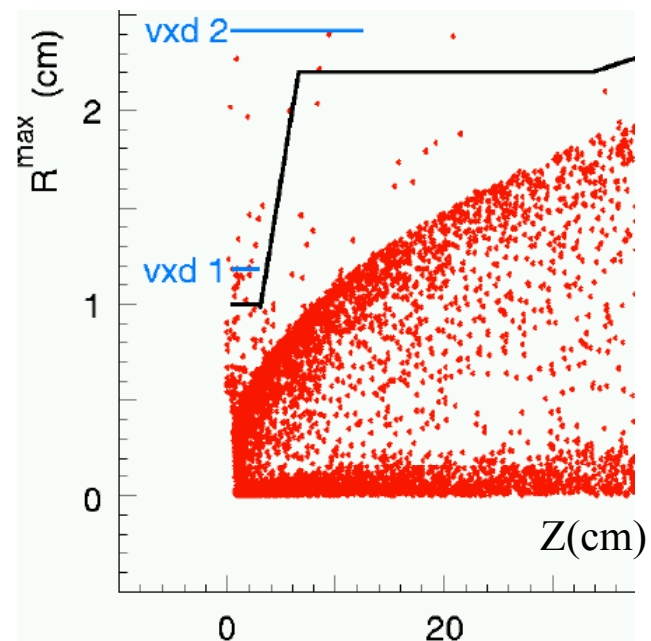
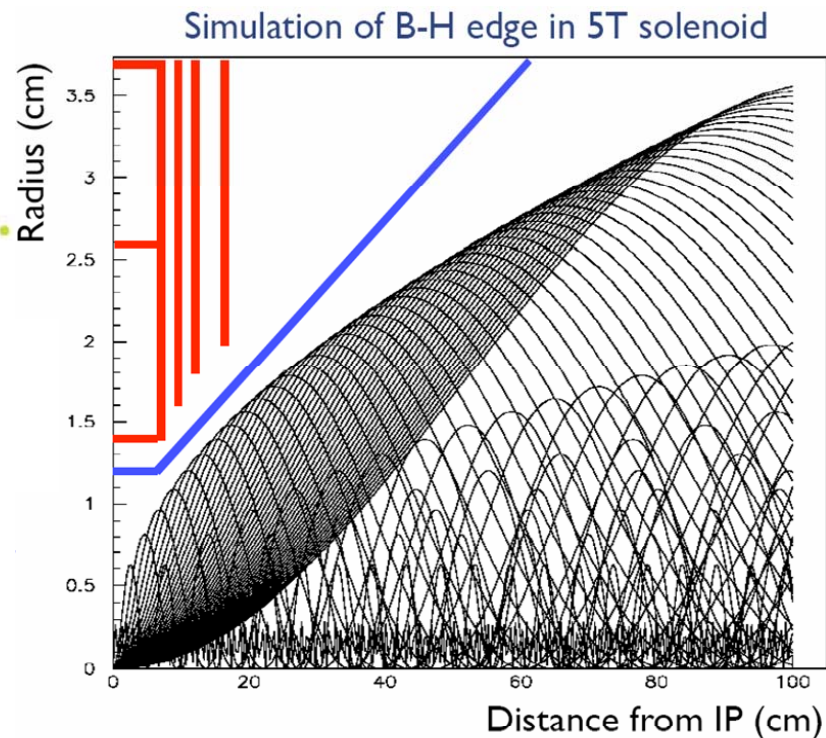
$$\theta_m = \sqrt{4 \frac{\ln\left(\frac{D}{\epsilon} + 1\right) D \sigma_x^2}{\sqrt{3} \epsilon \sigma_z^2}}$$

- Bethe-Heitler pairs have hard edge, Landau-Lifshitz pairs are outside



Deflection of pairs by detector solenoid

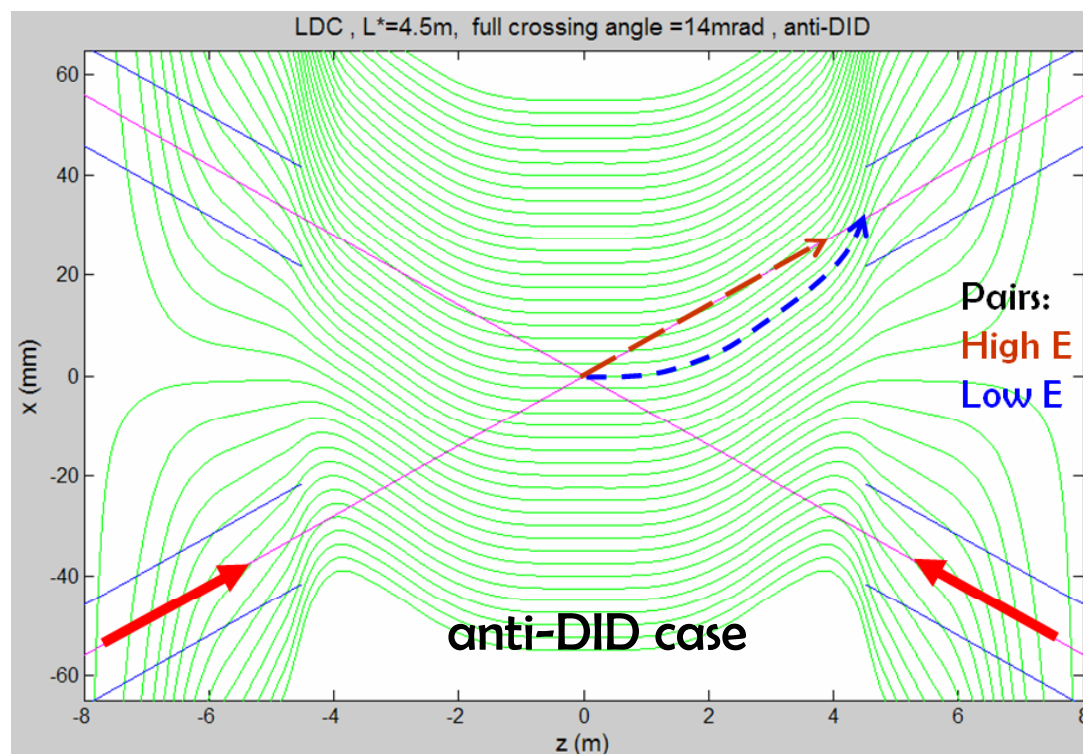
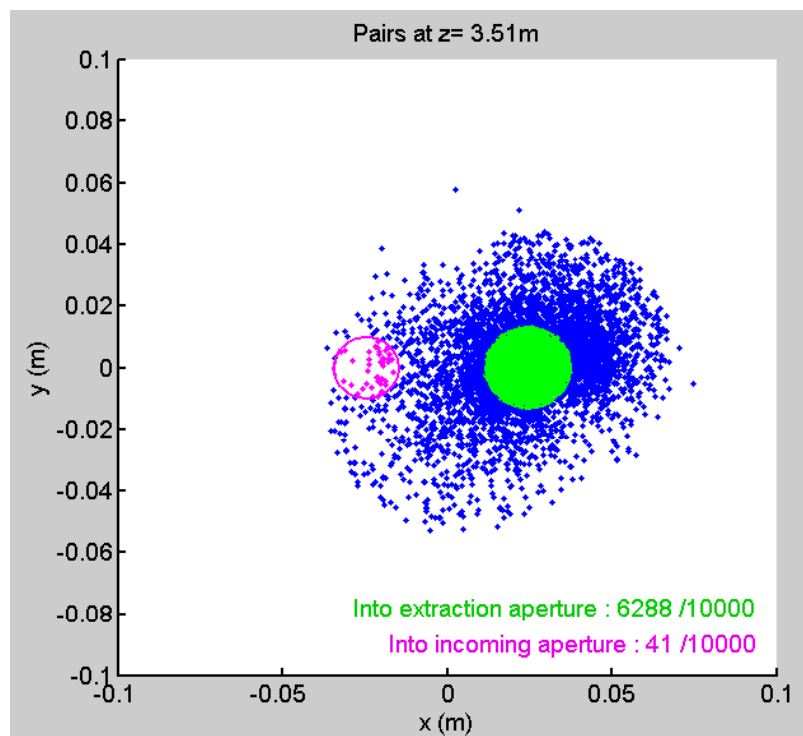
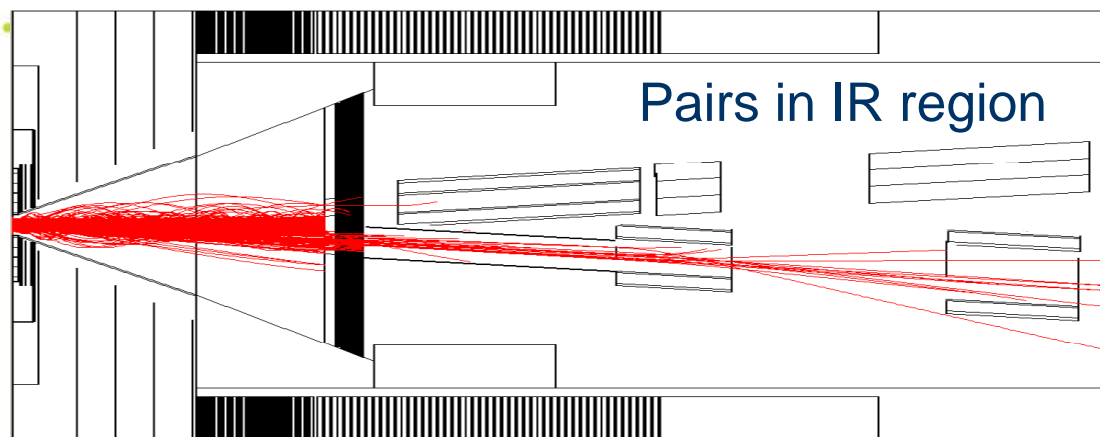
- Pairs are curled by the solenoid field of detector
- Geometry of vertex detector and vacuum chamber chosen in such a way that most of pairs (B-H) do not hit the apertures
- Only small number (L-L) of pairs would hit the VX apertures





Use of anti-DID to direct pairs

Anti-DID field can be used to direct most of pairs into extraction hole and thus improve somewhat the background conditions





Overview of beam-beam parameters (D_y , δ_E , Υ)

$$\text{Lumi} \sim H_D \frac{N^2}{\sigma_x \sigma_y}$$

- Luminosity per bunch crossing. H_D – luminosity enhancement

$$D_y \sim \frac{N \sigma_z}{\gamma \sigma_x \sigma_y}$$

- “Disruption” – characterize focusing strength of the field of the bunch ($D_y \sim \sigma_z / f_{\text{beam}}$)

$$\delta_E \sim \frac{N^2 \gamma}{\sigma_x^2 \sigma_z}$$

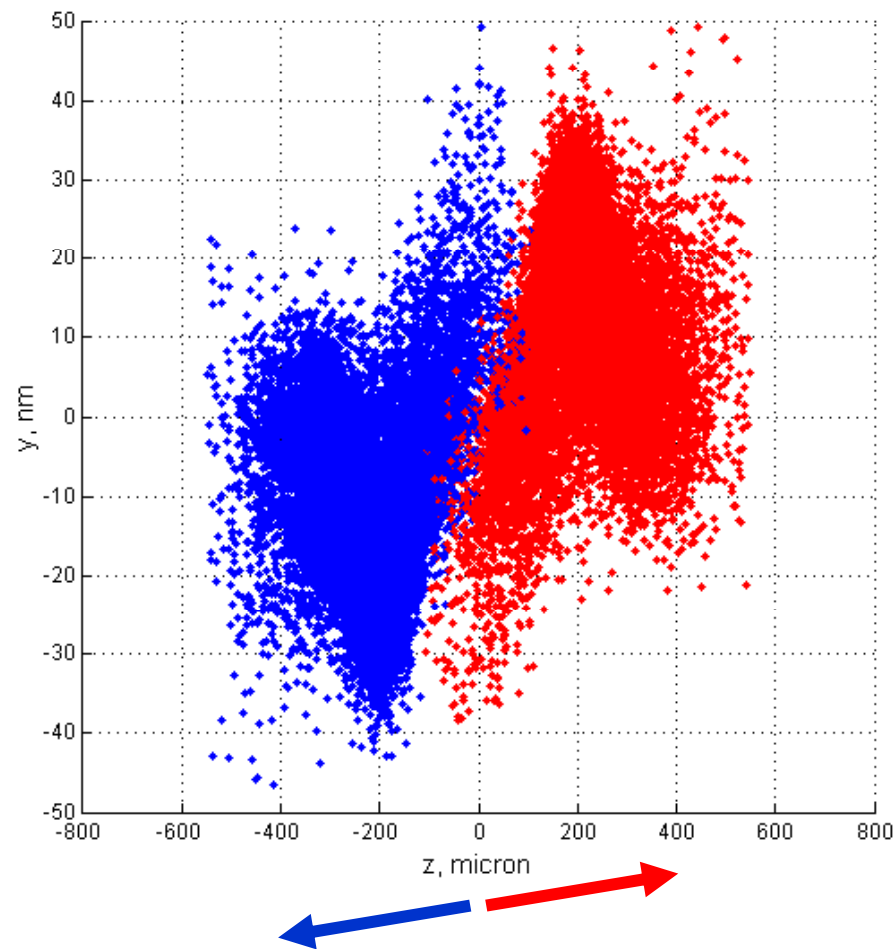
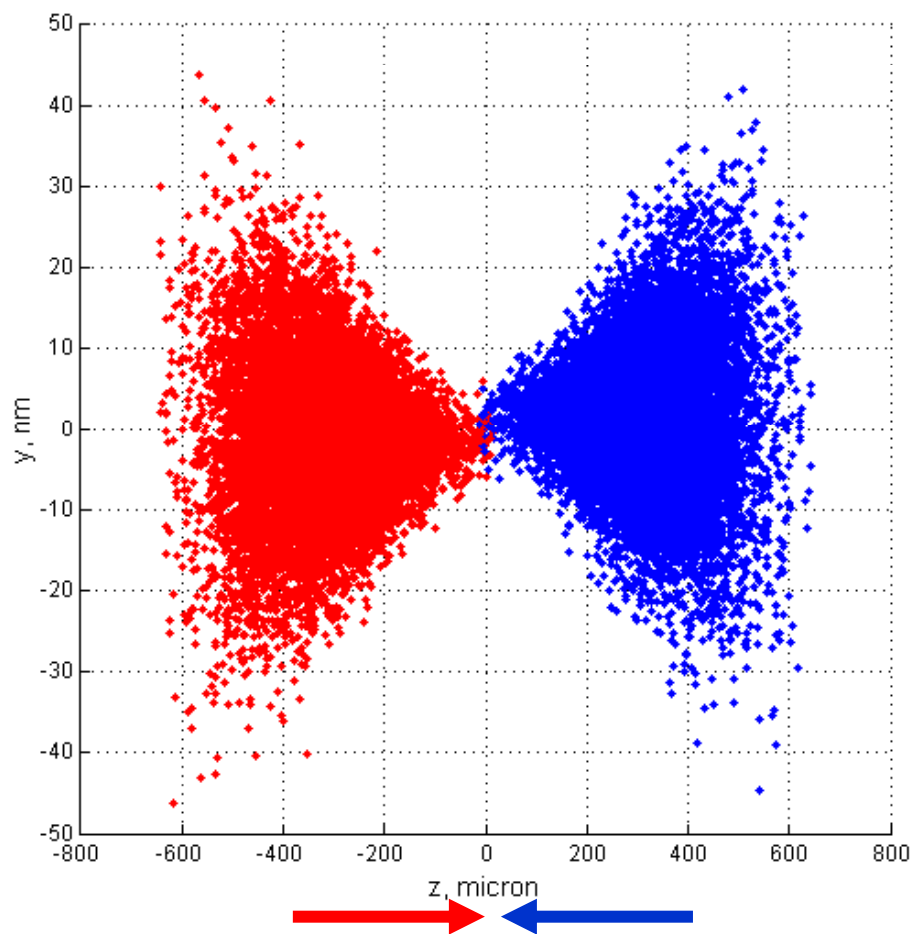
- Energy loss during beam-beam collision due to synchrotron radiation

$$\Upsilon \sim \frac{N \gamma}{\sigma_x \sigma_z}$$

- Ratio of critical photon energy to beam energy (classic or quantum regime)



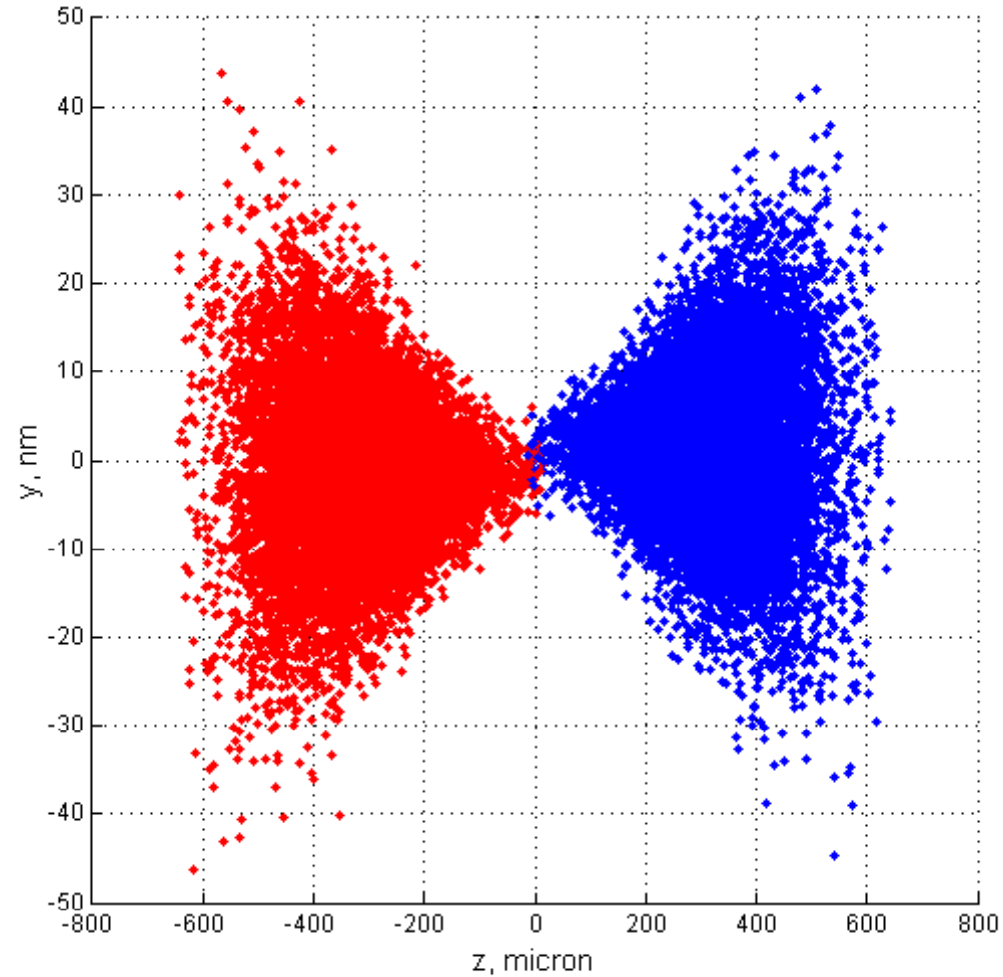
Beam-beam deflection



Sub nm offsets at IP cause large well detectable offsets (micron scale) of the beam a few meters downstream

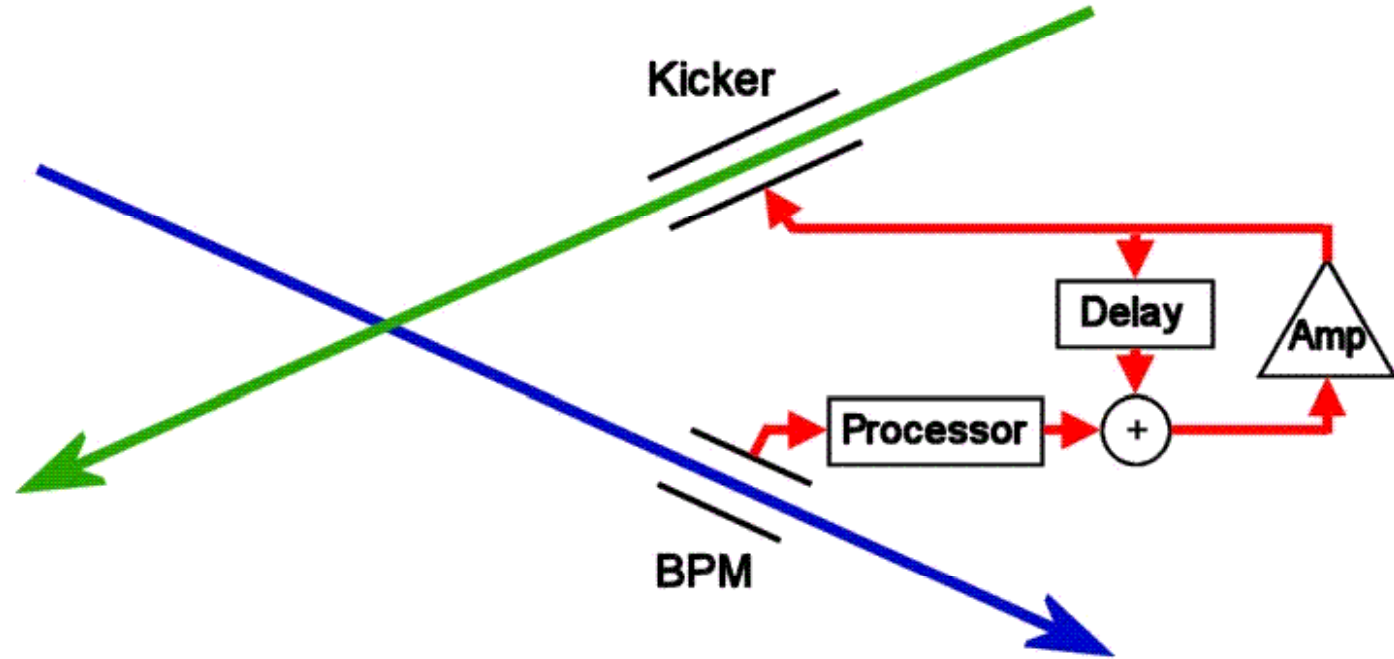


Beam-beam deflection allow to control collisions





Beam-Beam orbit feedback

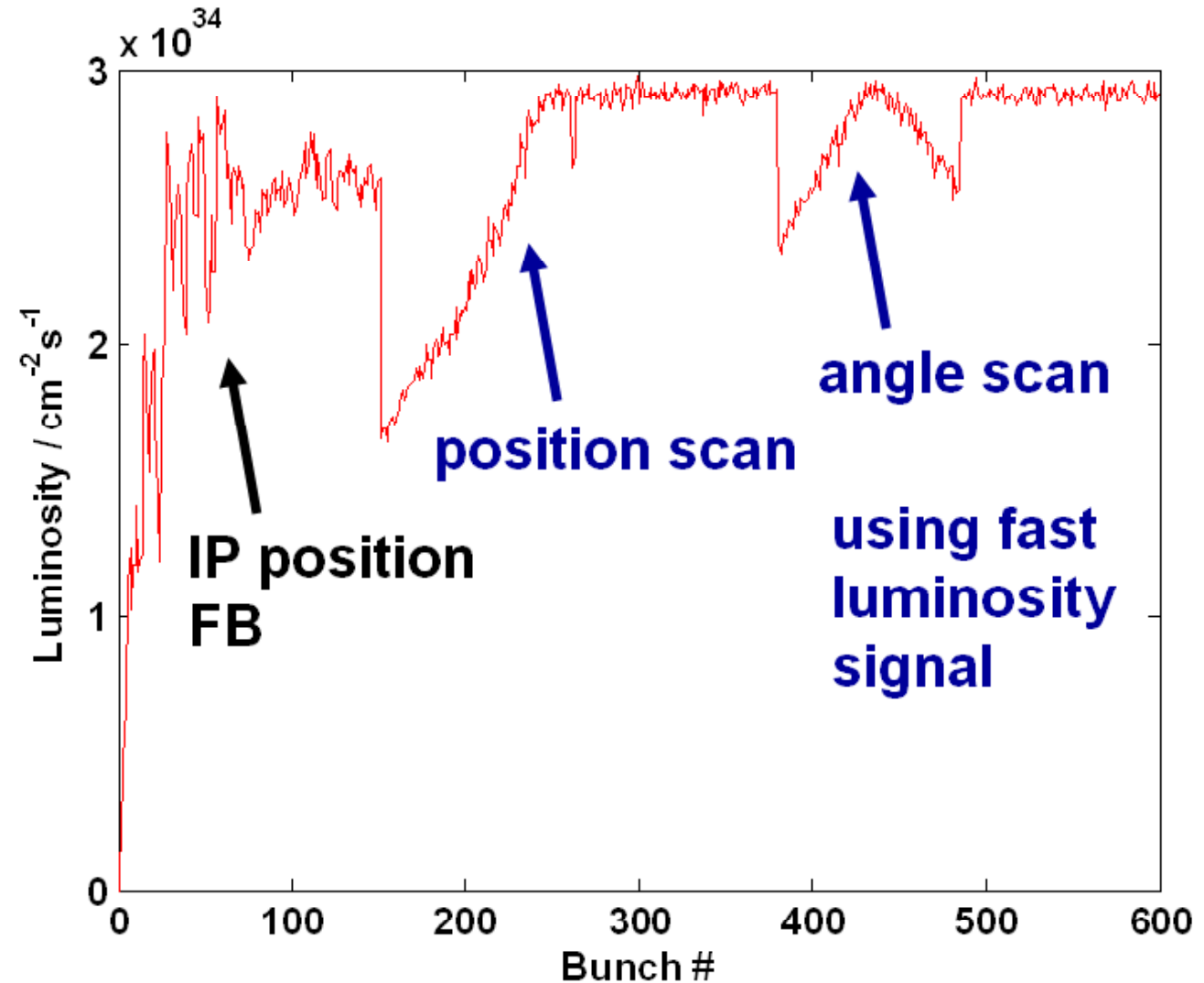


use strong beam-beam kick to keep beams colliding



ILC intratrain simulation

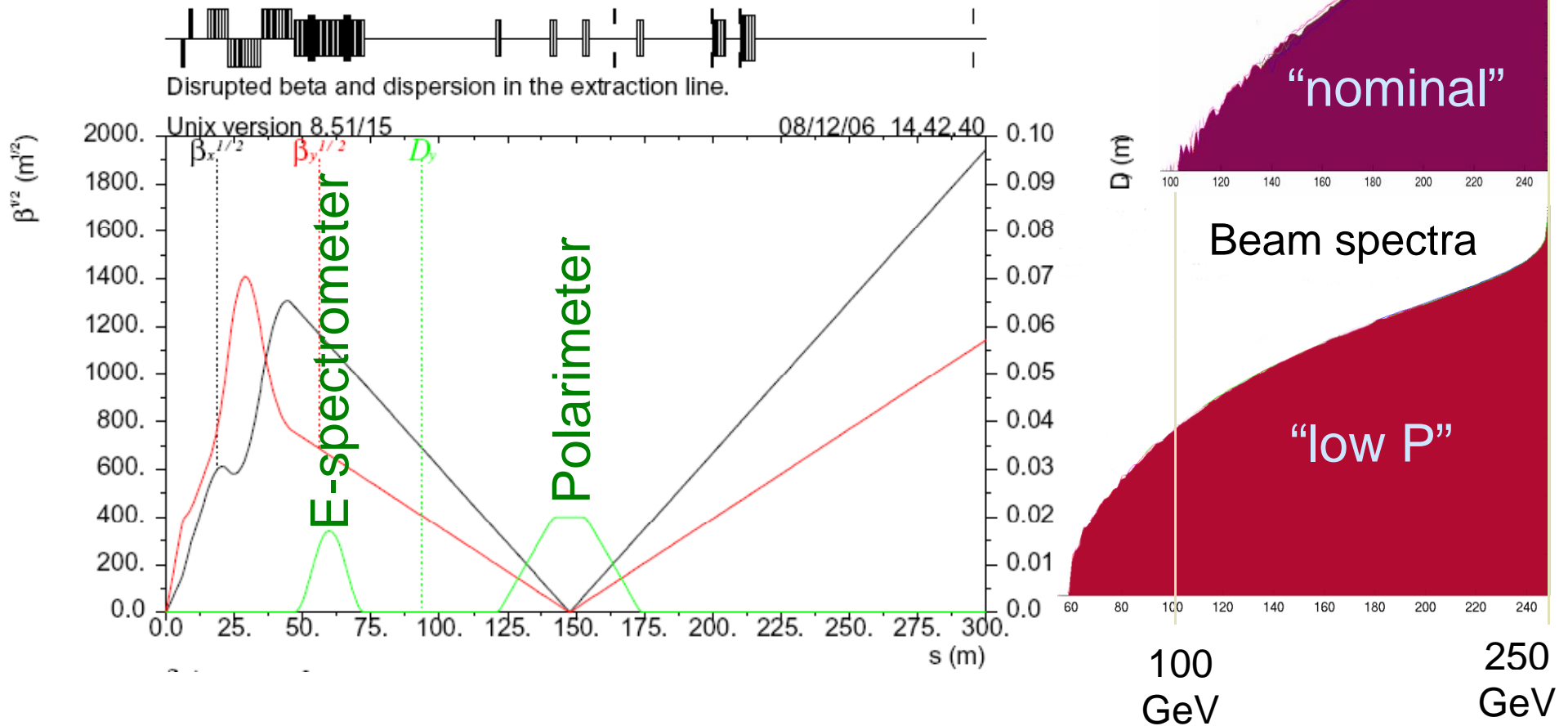
ILC intratrain feedback (IP position and angle optimization), simulated with realistic errors in the linac and “banana” bunches.



[Glen White]

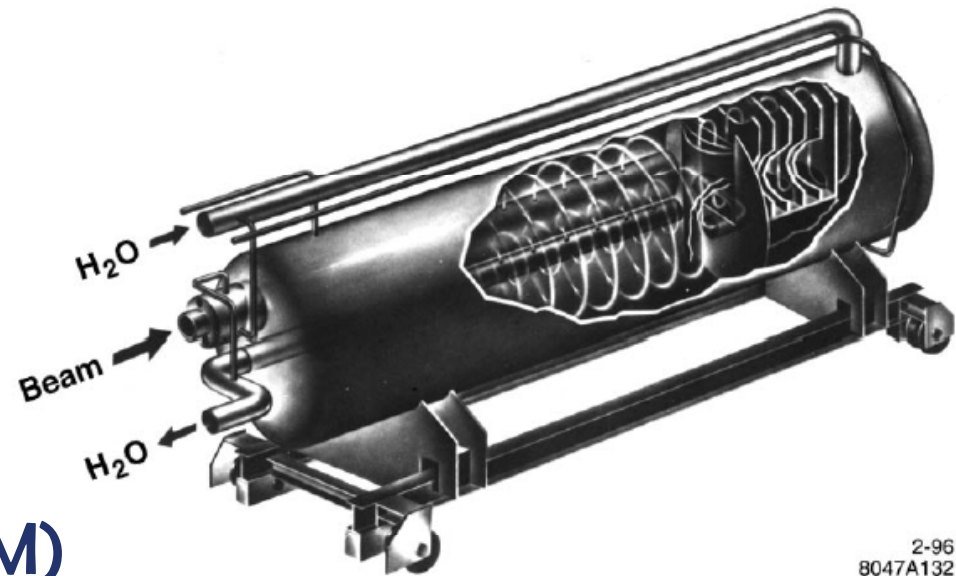


Optics for outgoing beam



Extraction optics need to handle the beam with ~60% energy spread, and provides energy and polarization diagnostics

ilc Beam dump



2-96
8047A132

- 17MW power (for 1TeV CM)
- Rastering of the beam on 30cm double window
- 6.5m water vessel; ~1m/s flow
- 10atm pressure to prevent boiling
- Three loop water system
- Catalytic H₂-O₂ recombiner
- Filters for 7Be
- Shielding 0.5m Fe & 1.5m concrete

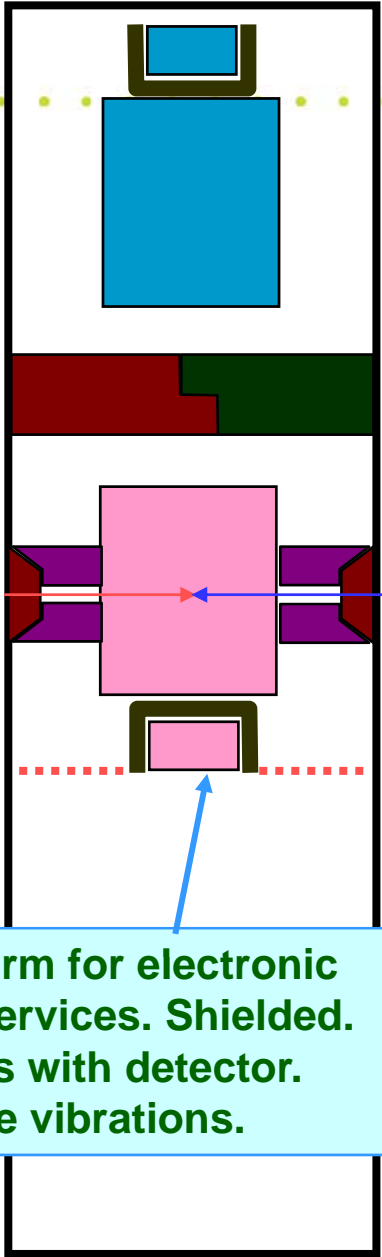
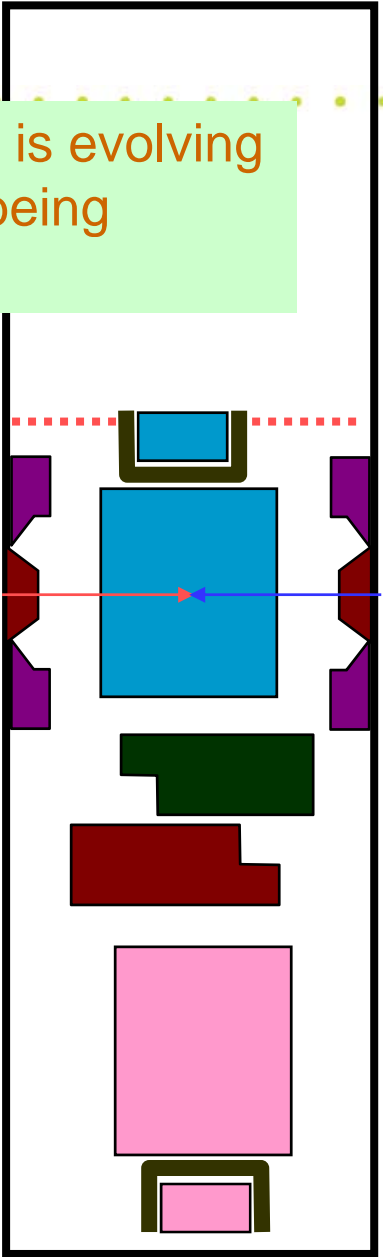
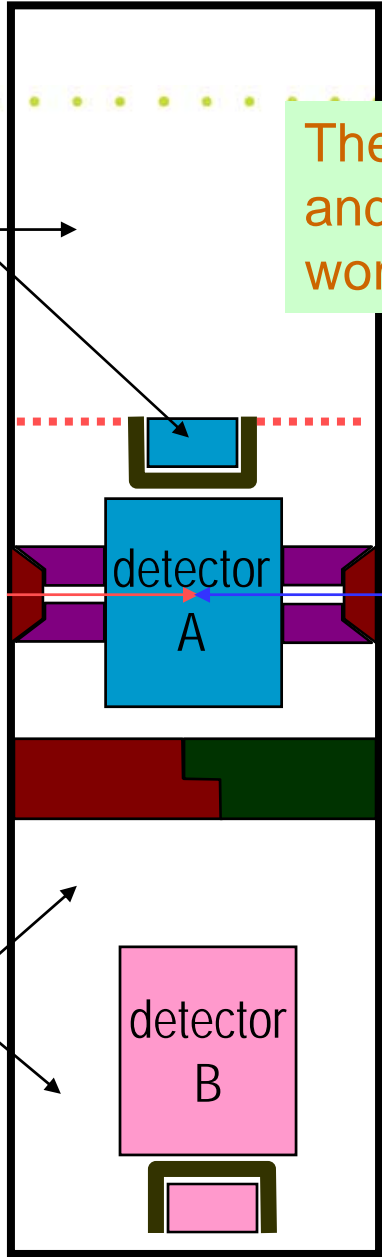


Concept of single IR with two detectors

may be accessible during run

The concept is evolving and details being worked out

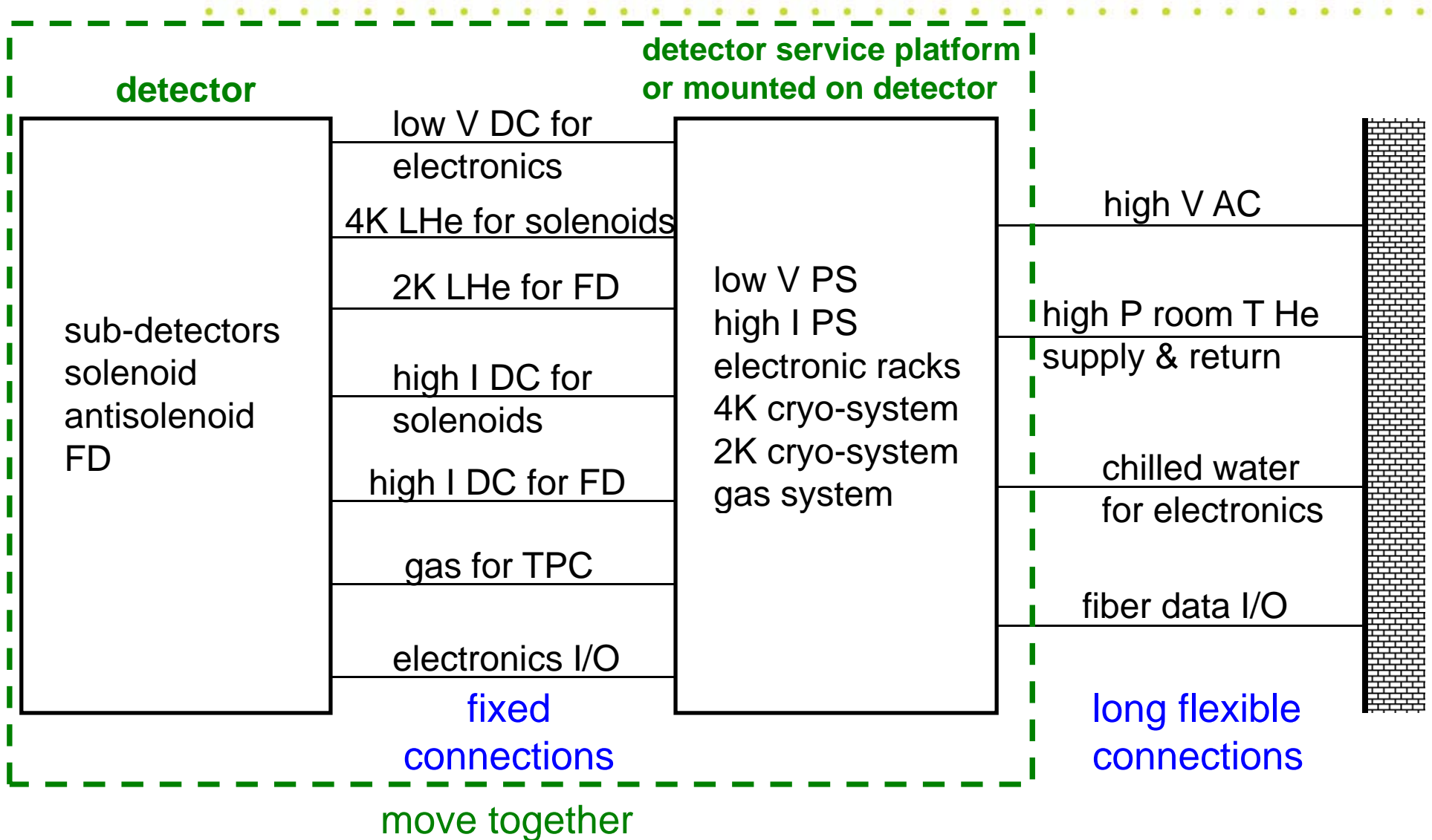
accessible during run



Platform for electronic and services. Shielded. Moves with detector. Isolate vibrations.

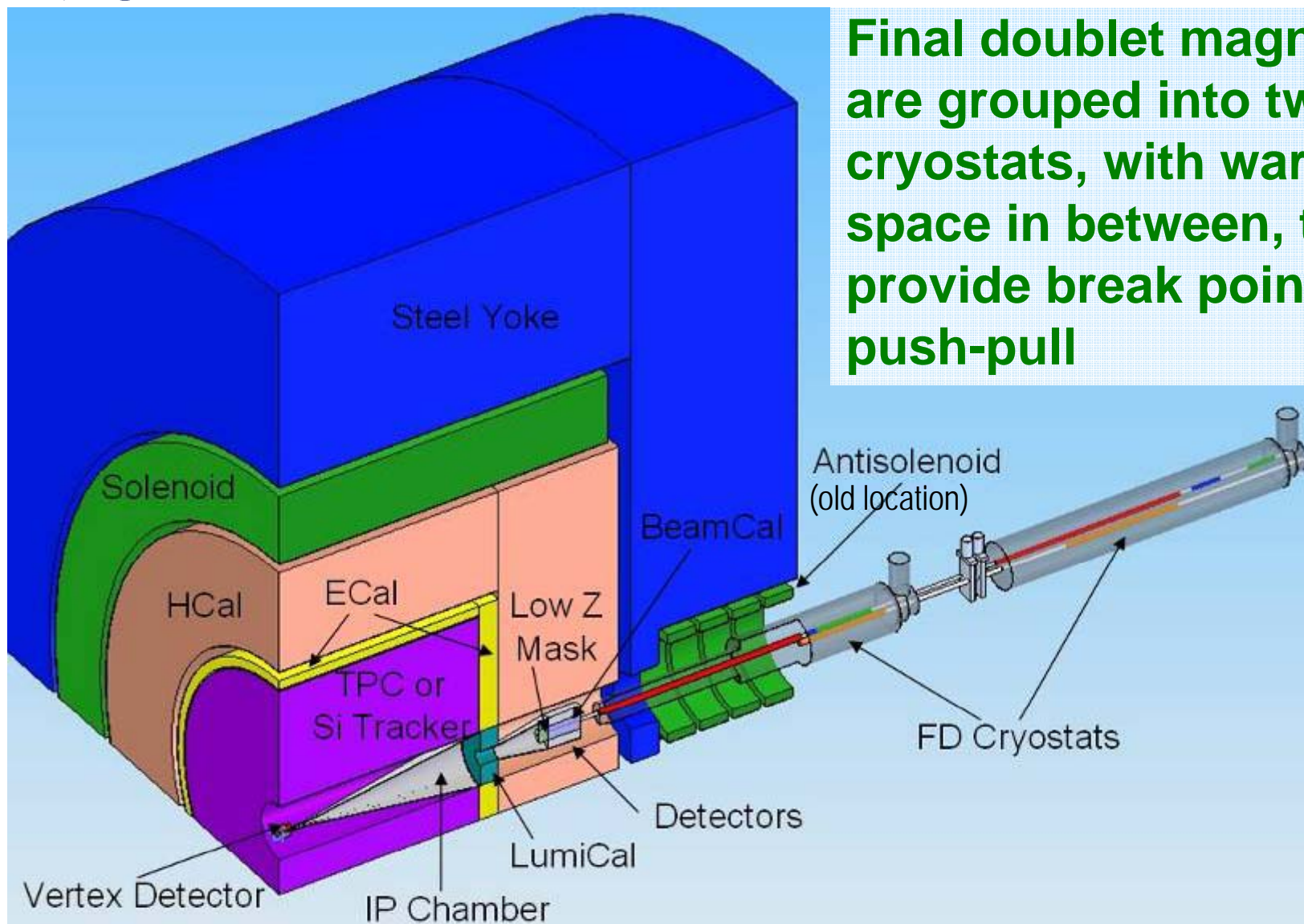


Concept of detector systems connections

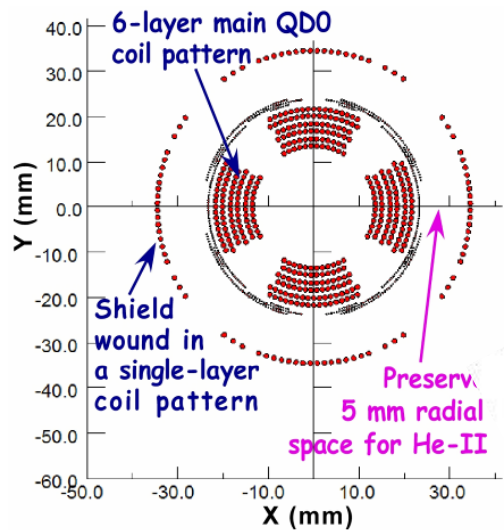




IR integration



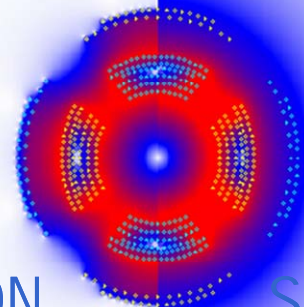
Final doublet magnets are grouped into two cryostats, with warm space in between, to provide break point for push-pull



Actively shielded QD0



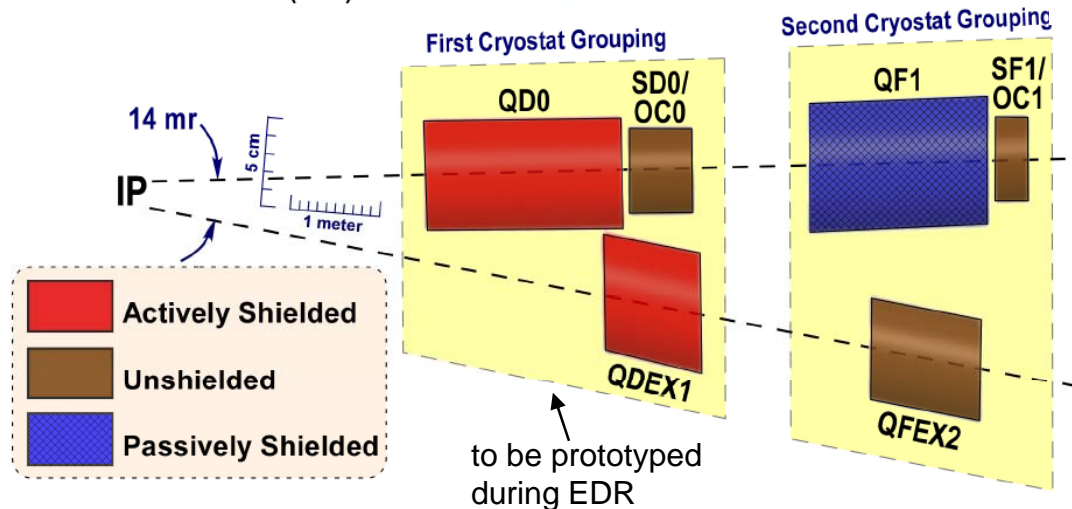
BNL



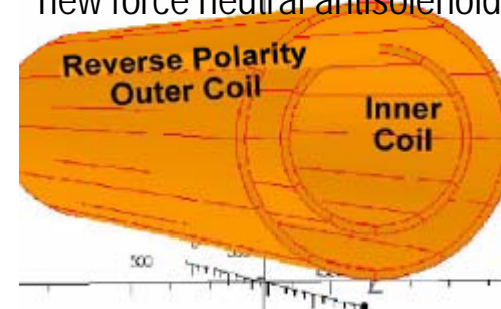
Shield ON

Shield OFF

Intensity of color represents value of magnetic field.



Two Coils; Different Radii
new force neutral antisolenoid



- Interaction region uses compact self-shielding SC magnets
- Independent adjustment of in- & out-going beamlines
- Force-neutral anti-solenoid for local coupling correction



IR magnets
prototypes at
BNL

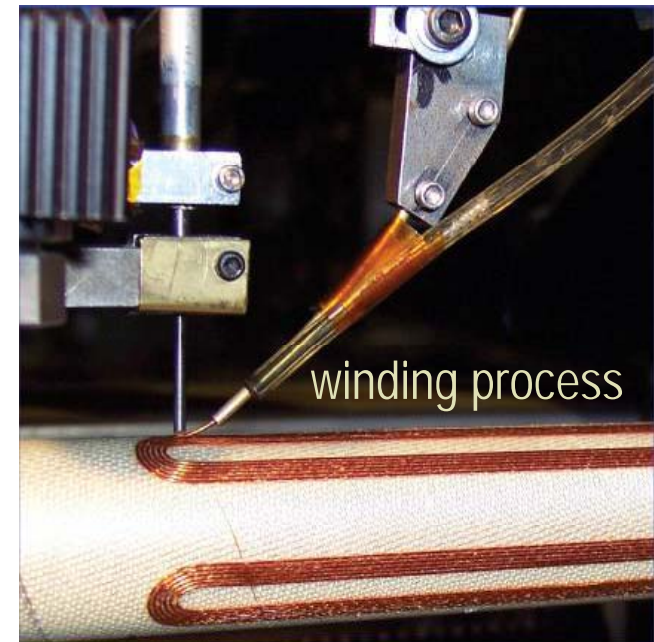
BNL prototype of self shielded quad



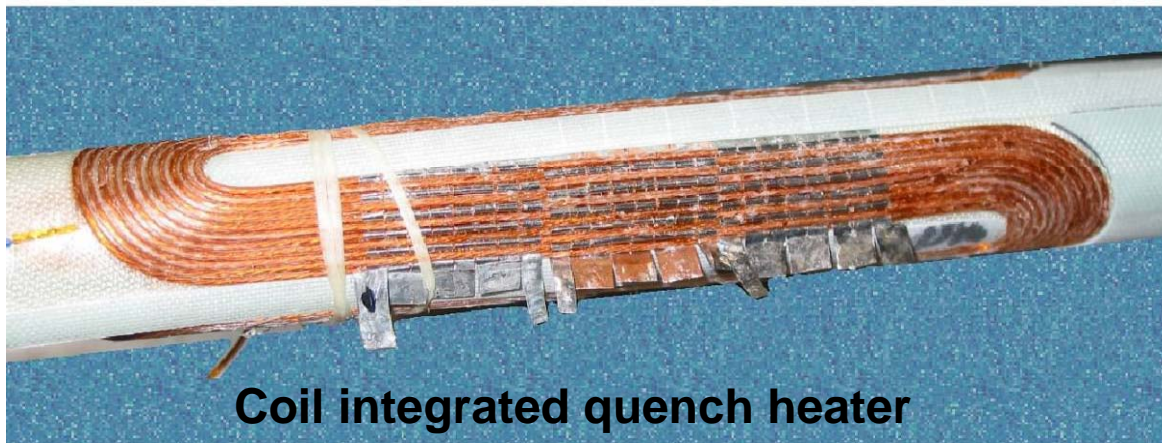
cancellation of the external field with a shield coil has been successfully demonstrated at BNL



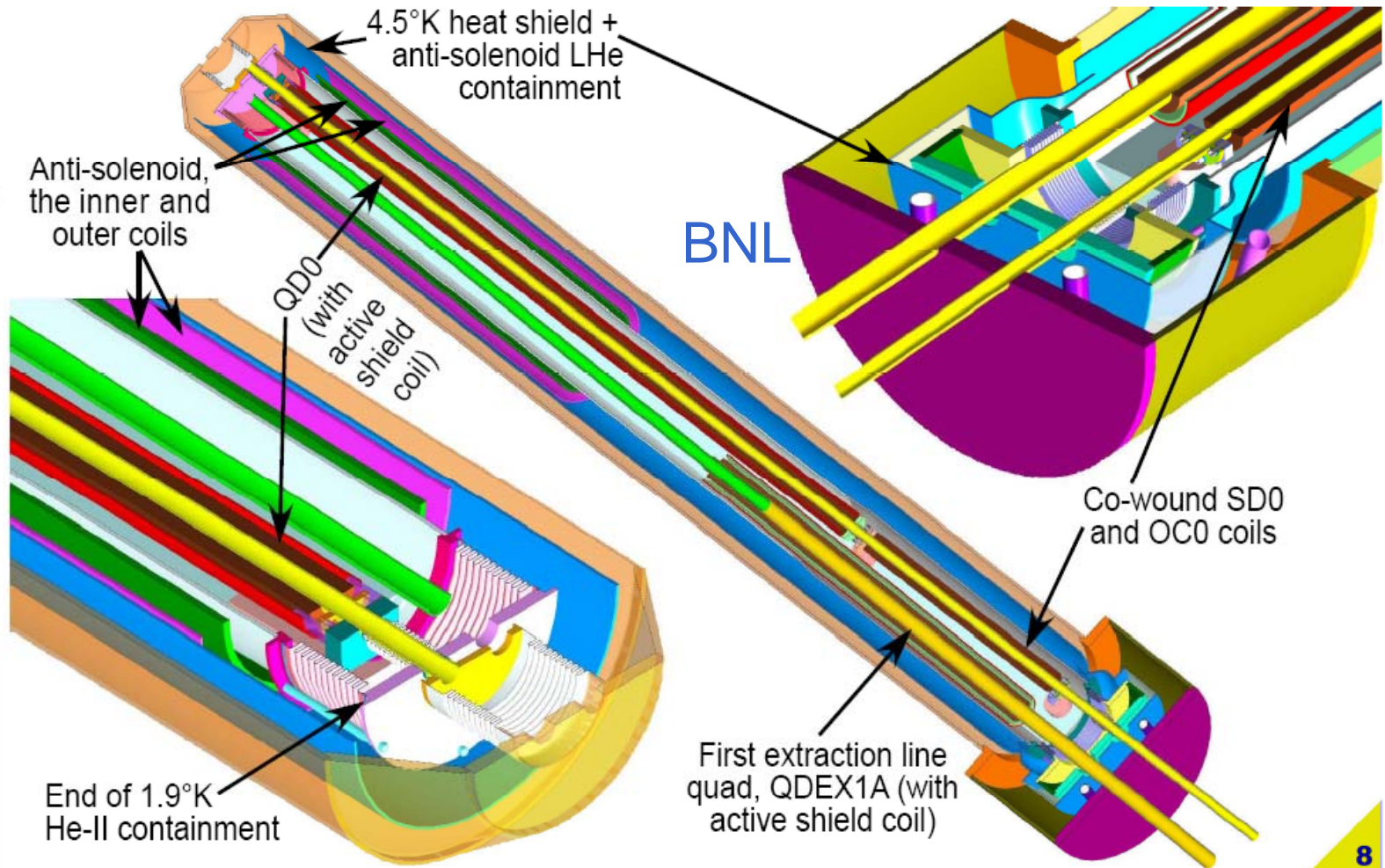
prototype of sextupole-octupole magnet



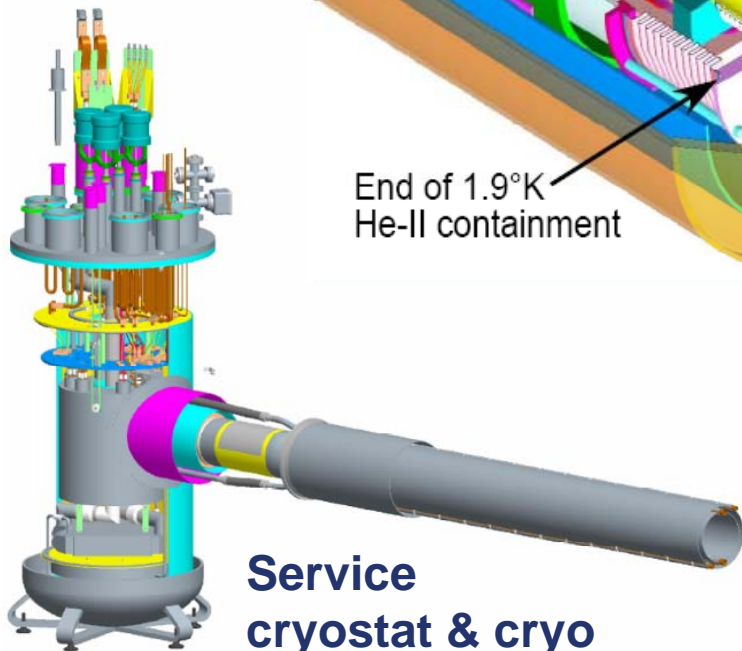
winding process



Coil integrated quench heater



8



- Detailed engineering design of IR magnets and their integration has started

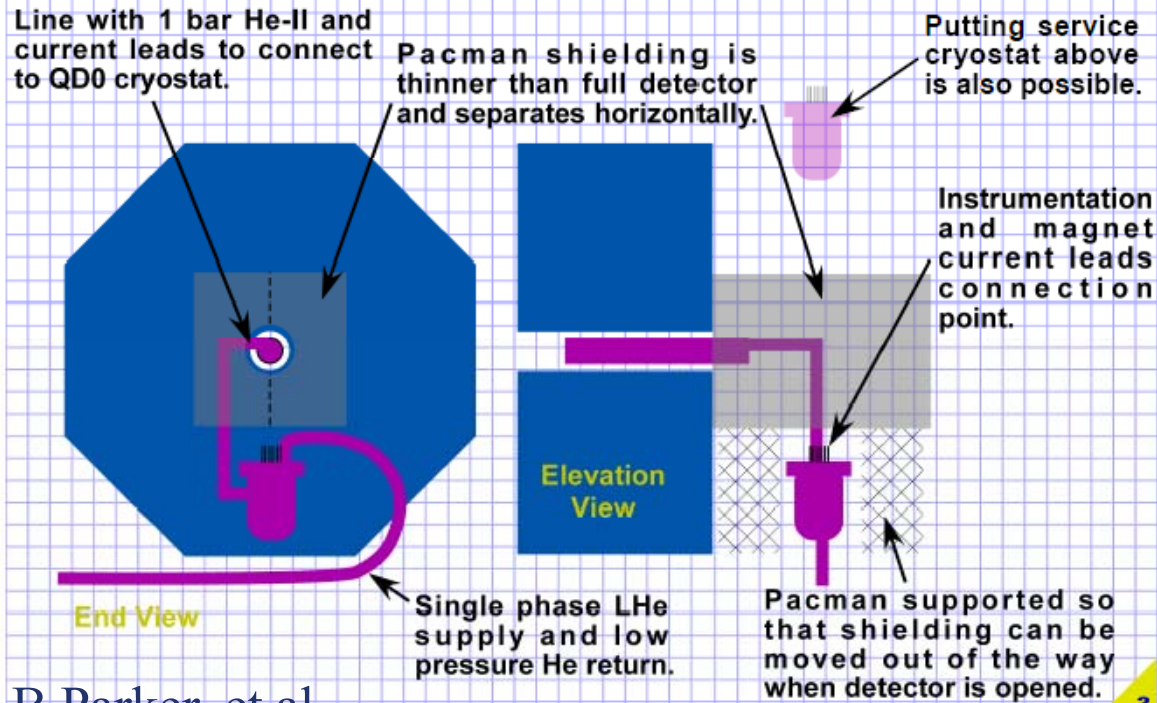


Present concept of cryo connection



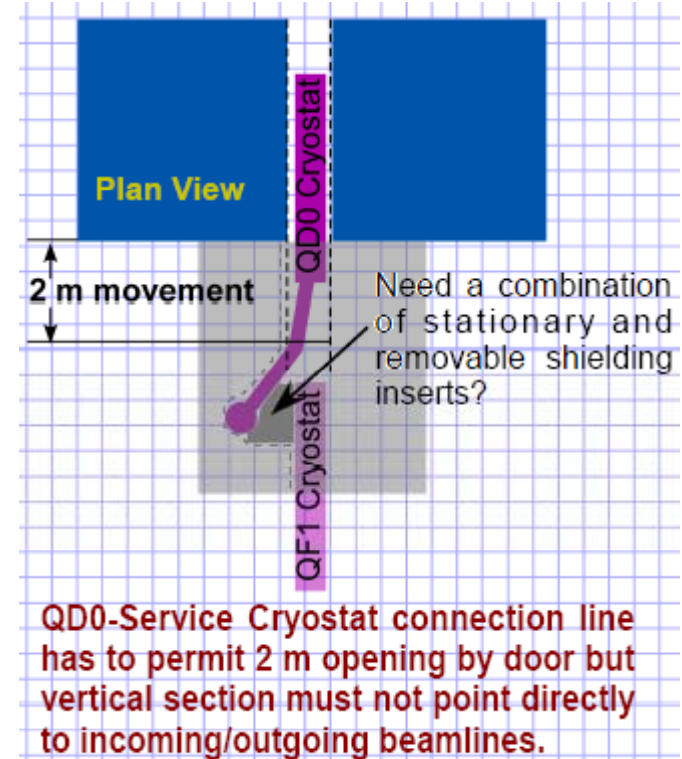
Vertical Layout for the Service Cryostat to QD0 Cryostat Transfer Line.

BROOKHAVEN
NATIONAL LABORATORY
Superconducting
Magnet Division

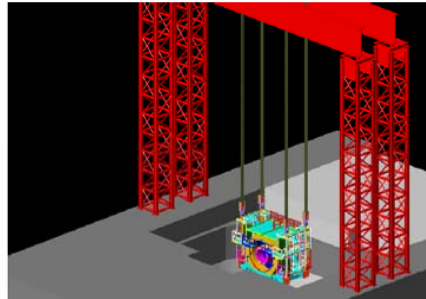
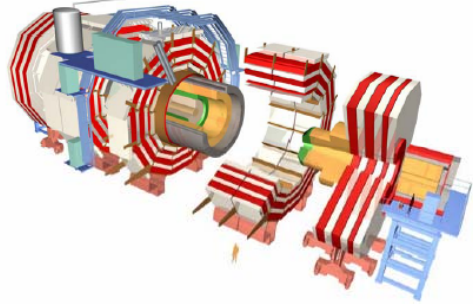


B.Parker, et al

3



ILC Detector assembly



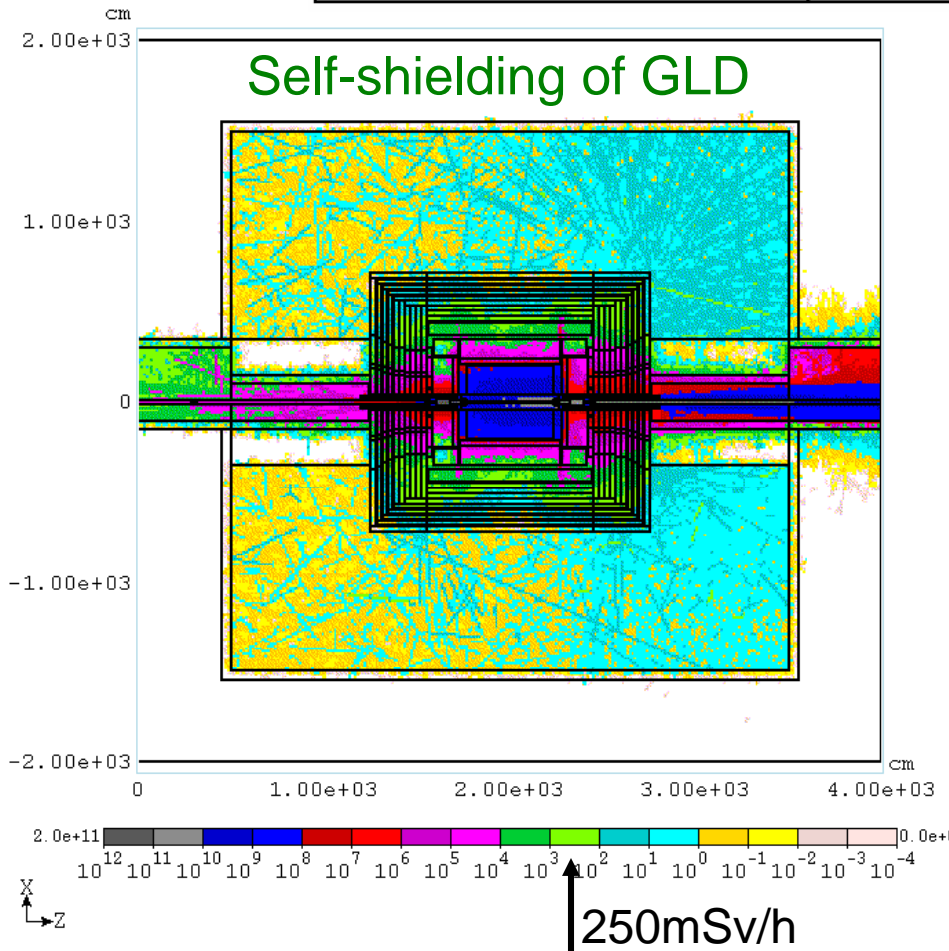
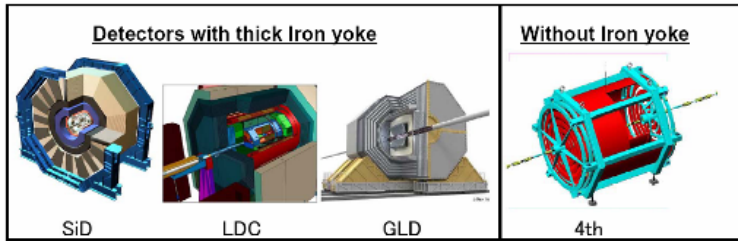
- CMS detector assembled on surface in parallel with underground work, lowered down with rented crane
- Adopted this method for ILC, to save 2-2.5 years that allows to fit into 7 years of construction



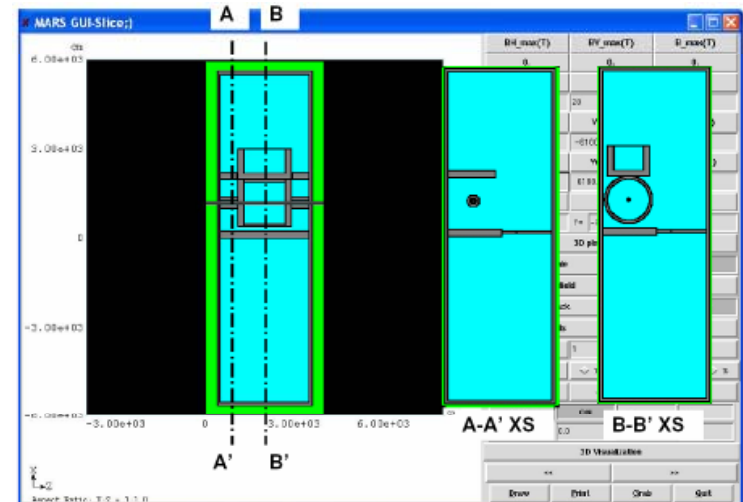
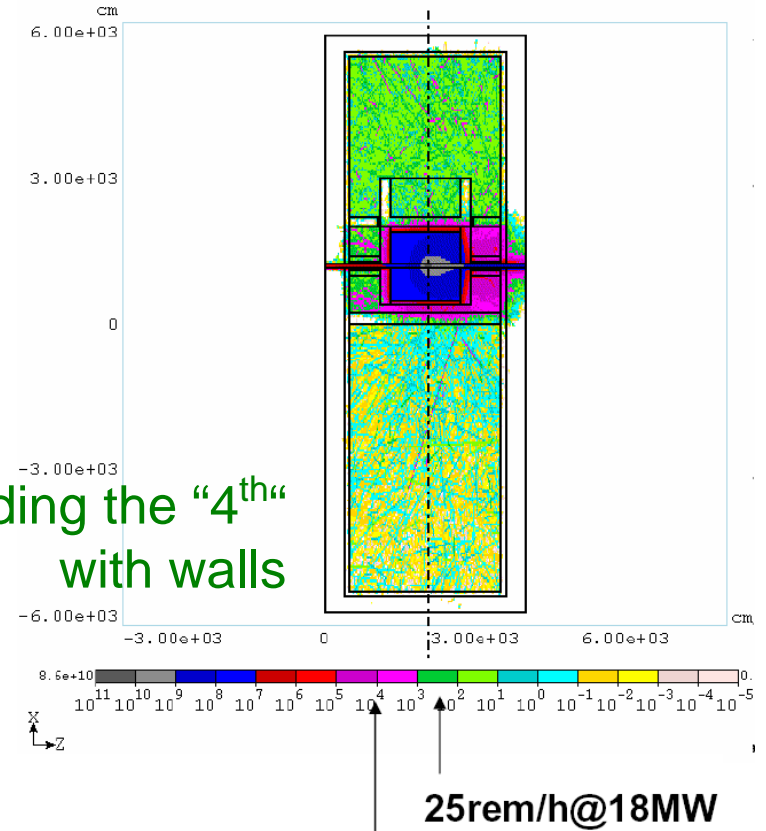
photos courtesy CERN colleagues



Shielding the IR hall



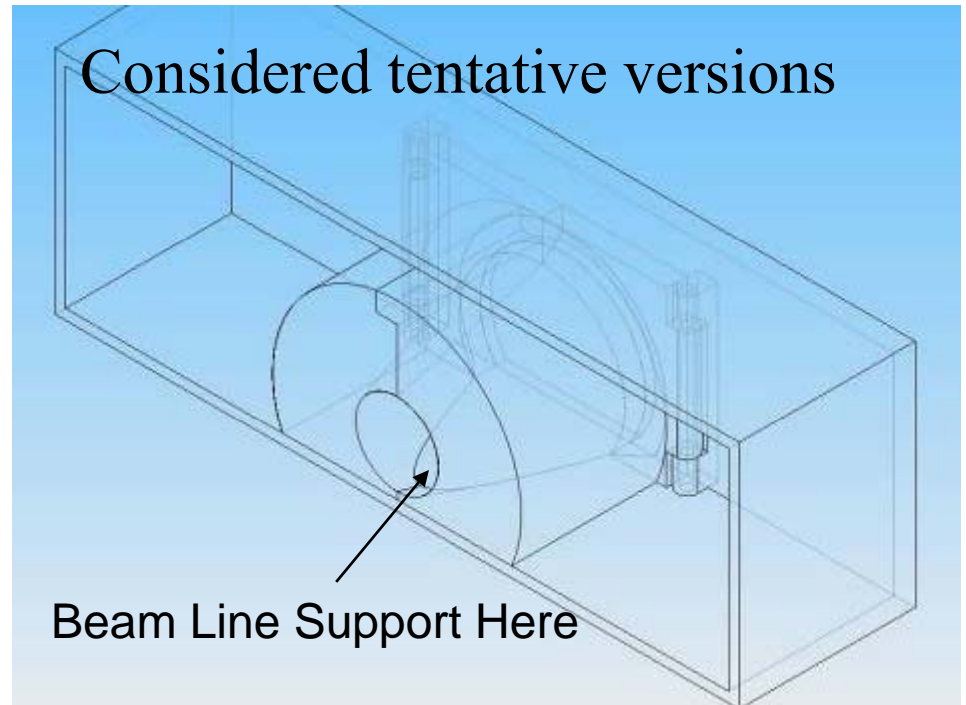
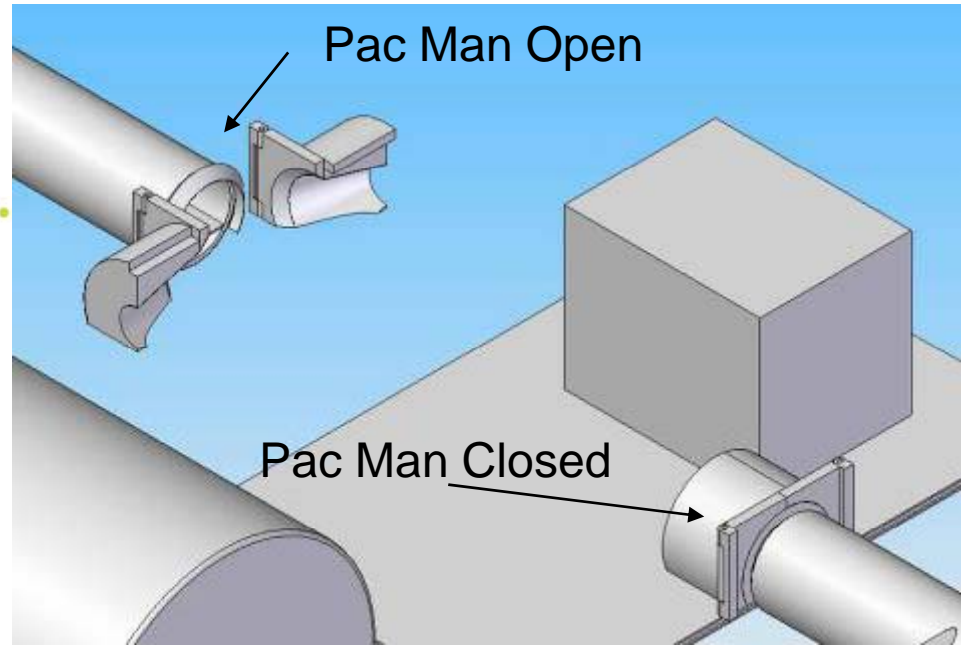
Shielding the "4th" with walls



Pacman design



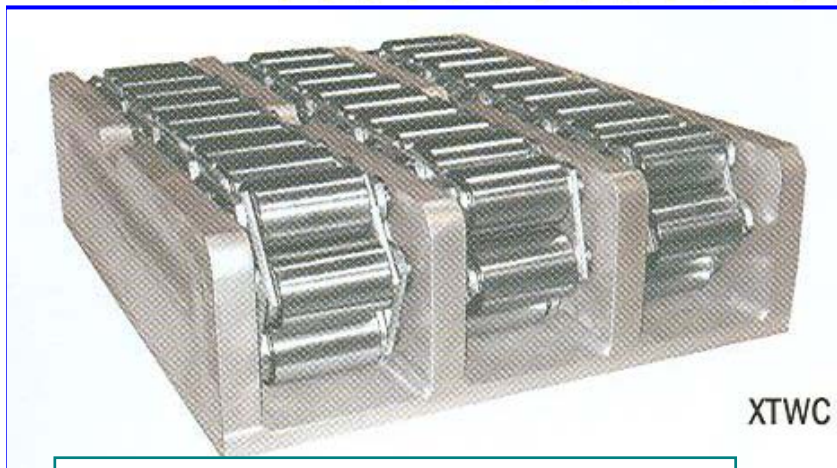
BDS: 96



John Amann



Moving the detector



XTWC

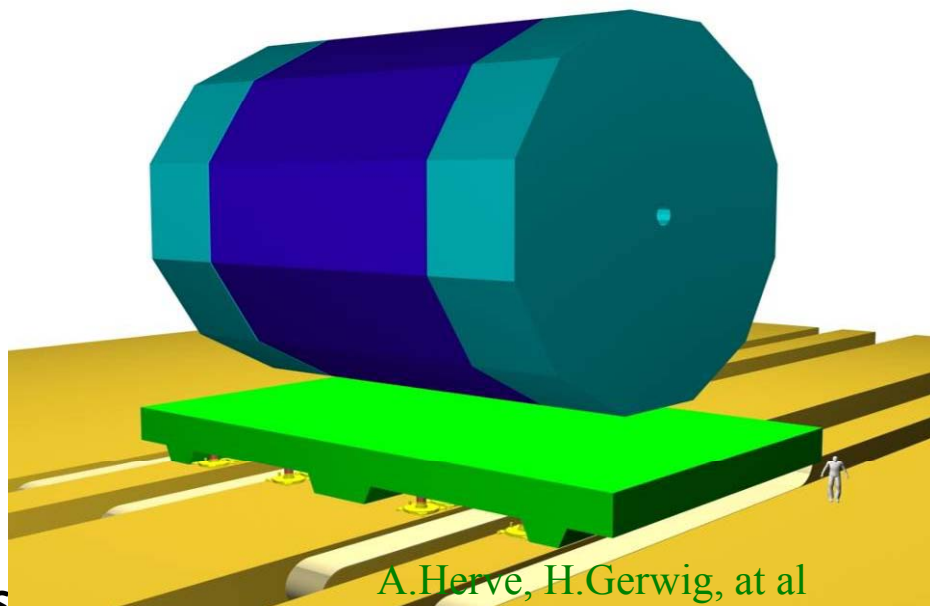
5000 ton Hilman roller module



Air-pads at CMS – move 2000k pieces

Is detector (compatible with on-surface assembly) rigid enough itself to avoid distortions during move?

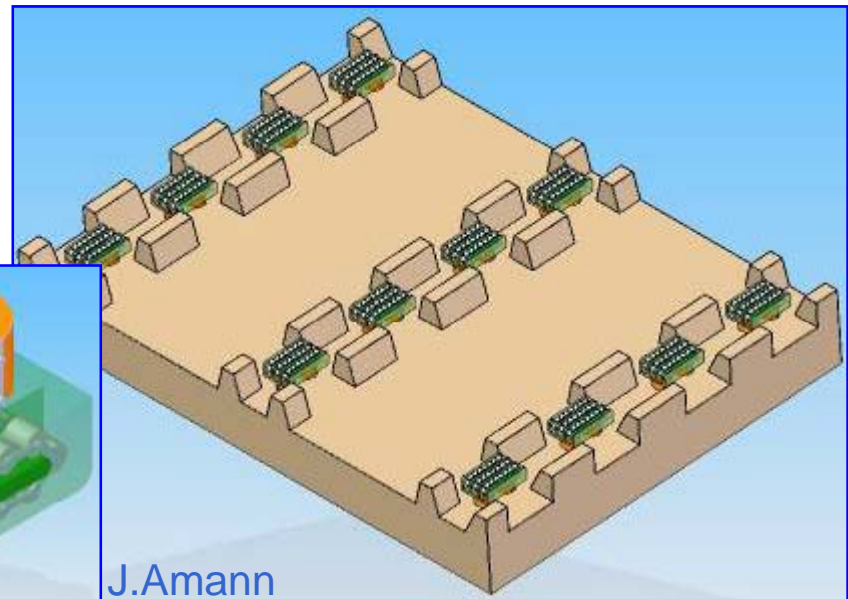
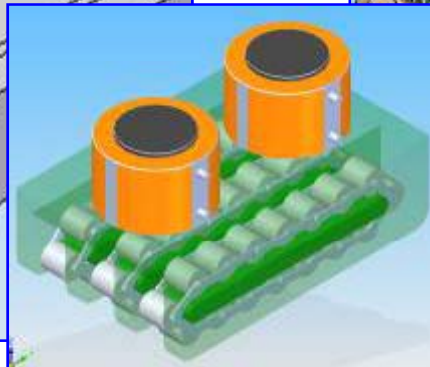
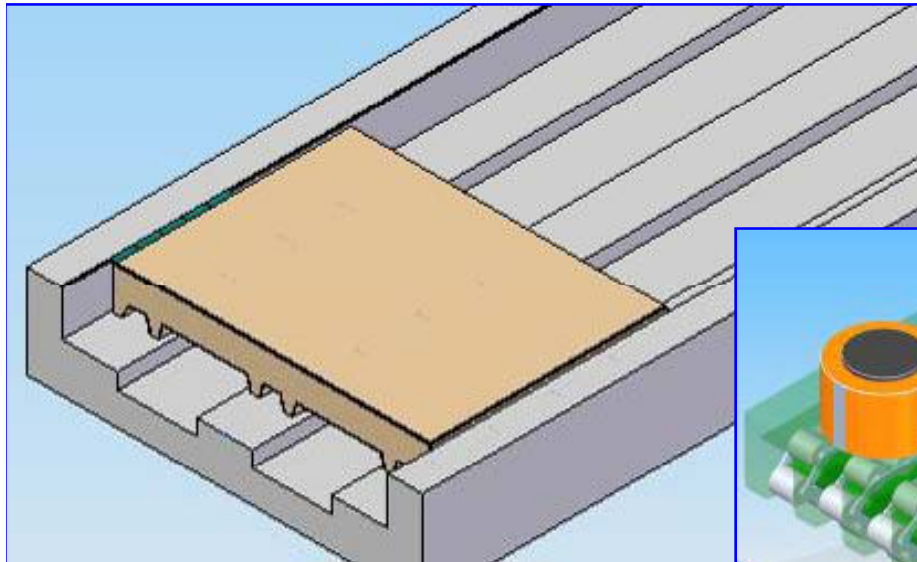
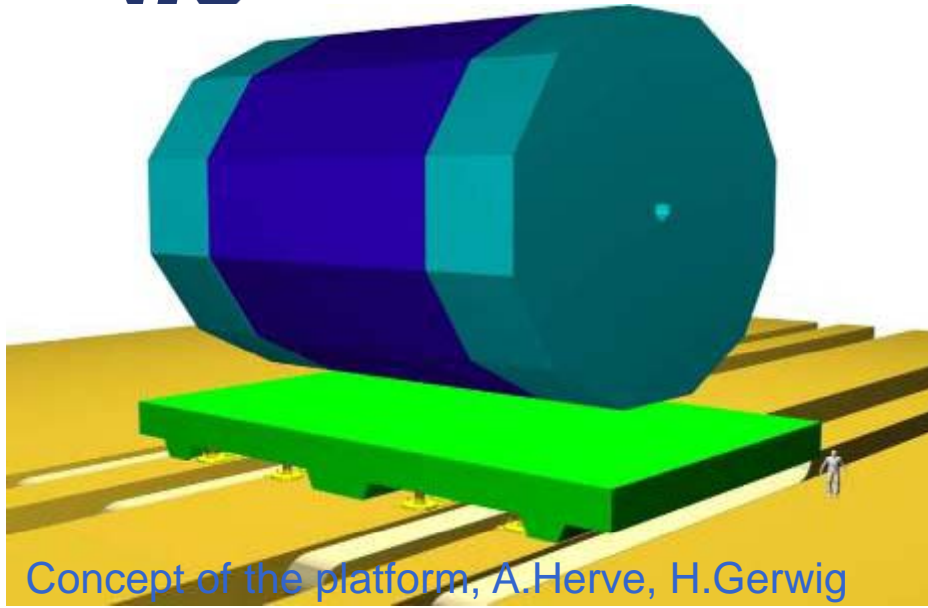
Concept of the platform to move ILC detector



A.Herve, H.Gerwig, et al

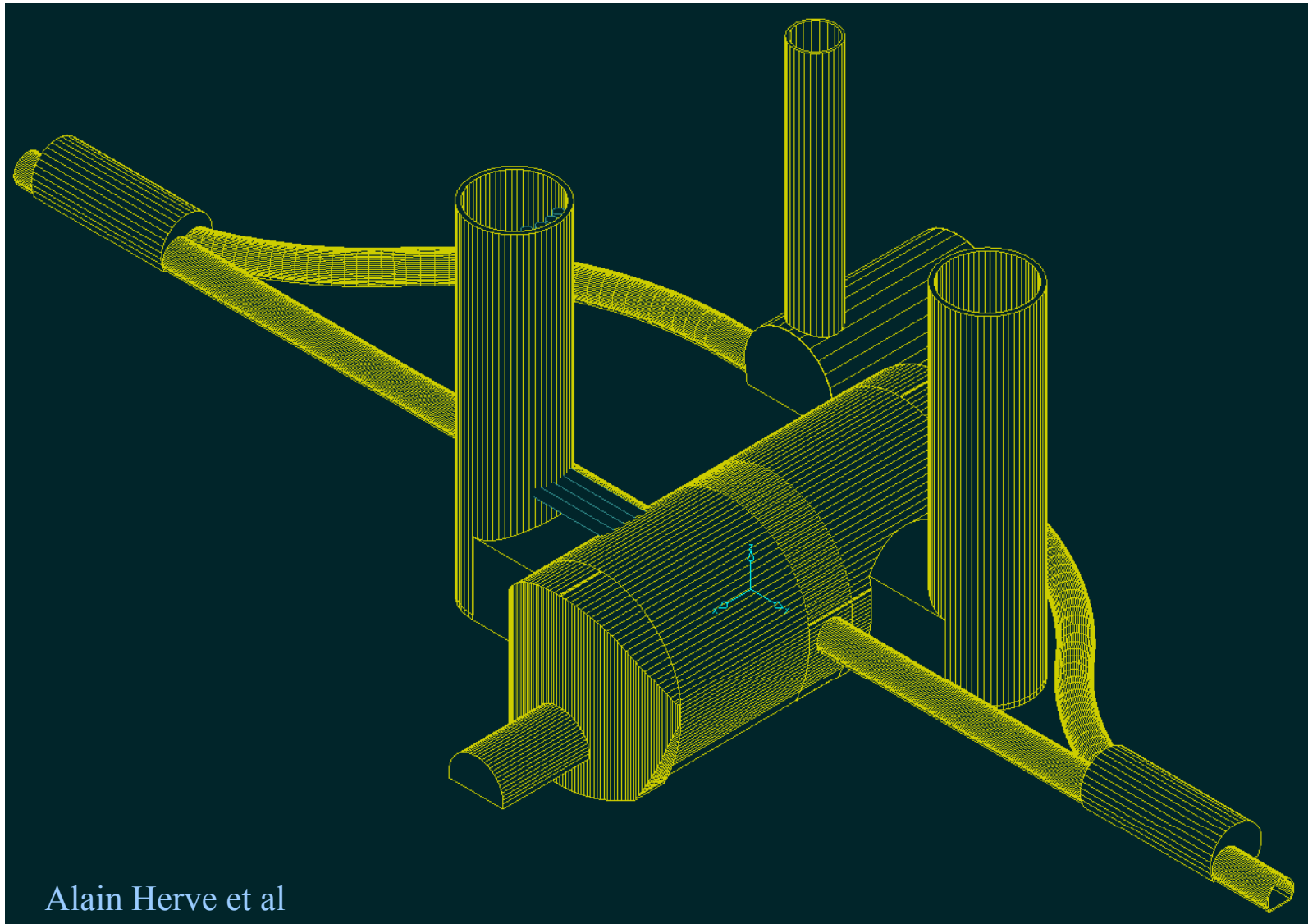


Moving the detector





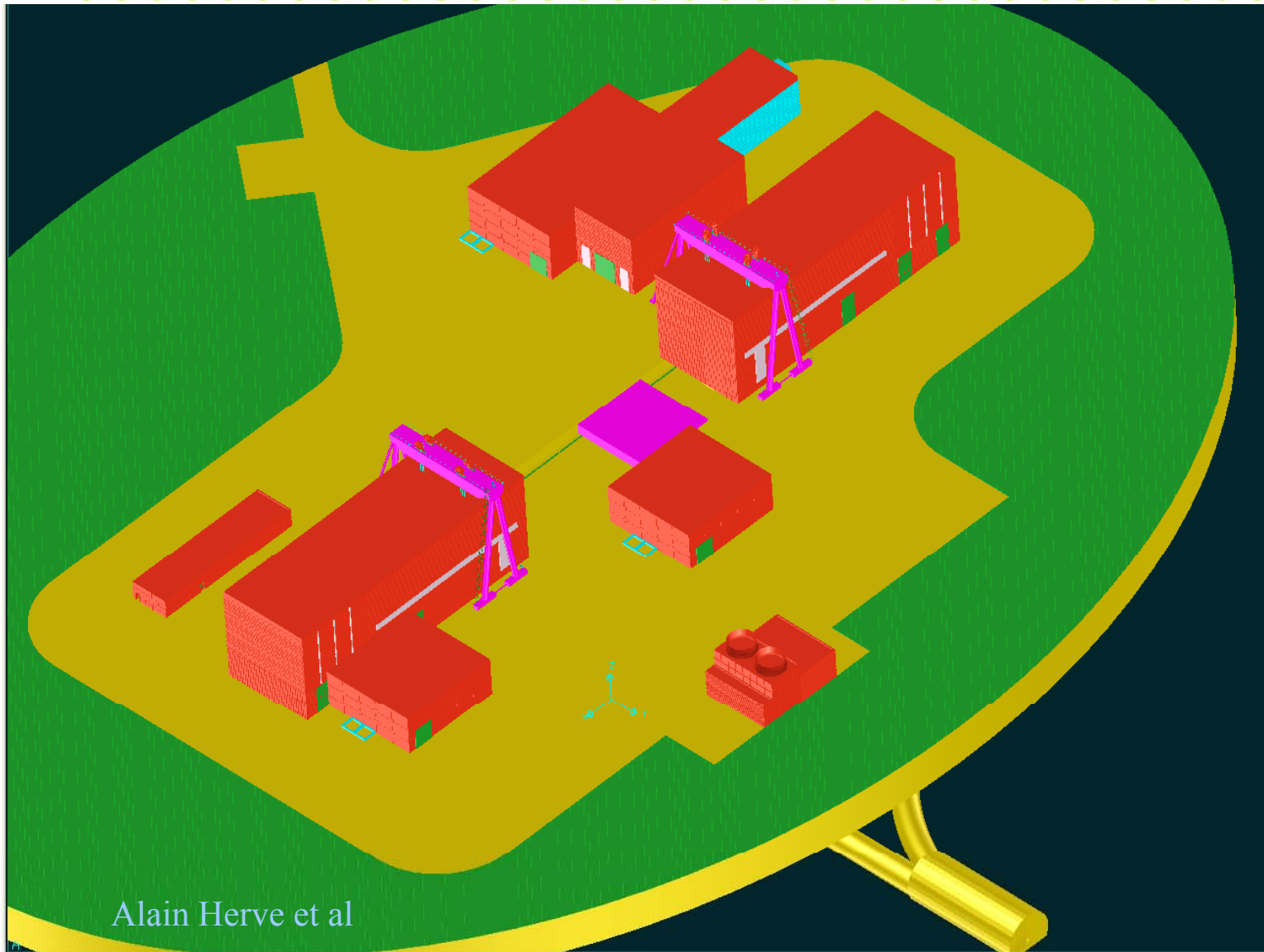
Configuration of IR tunnels and halls



Alain Herve et al



Configuration of surface buildings



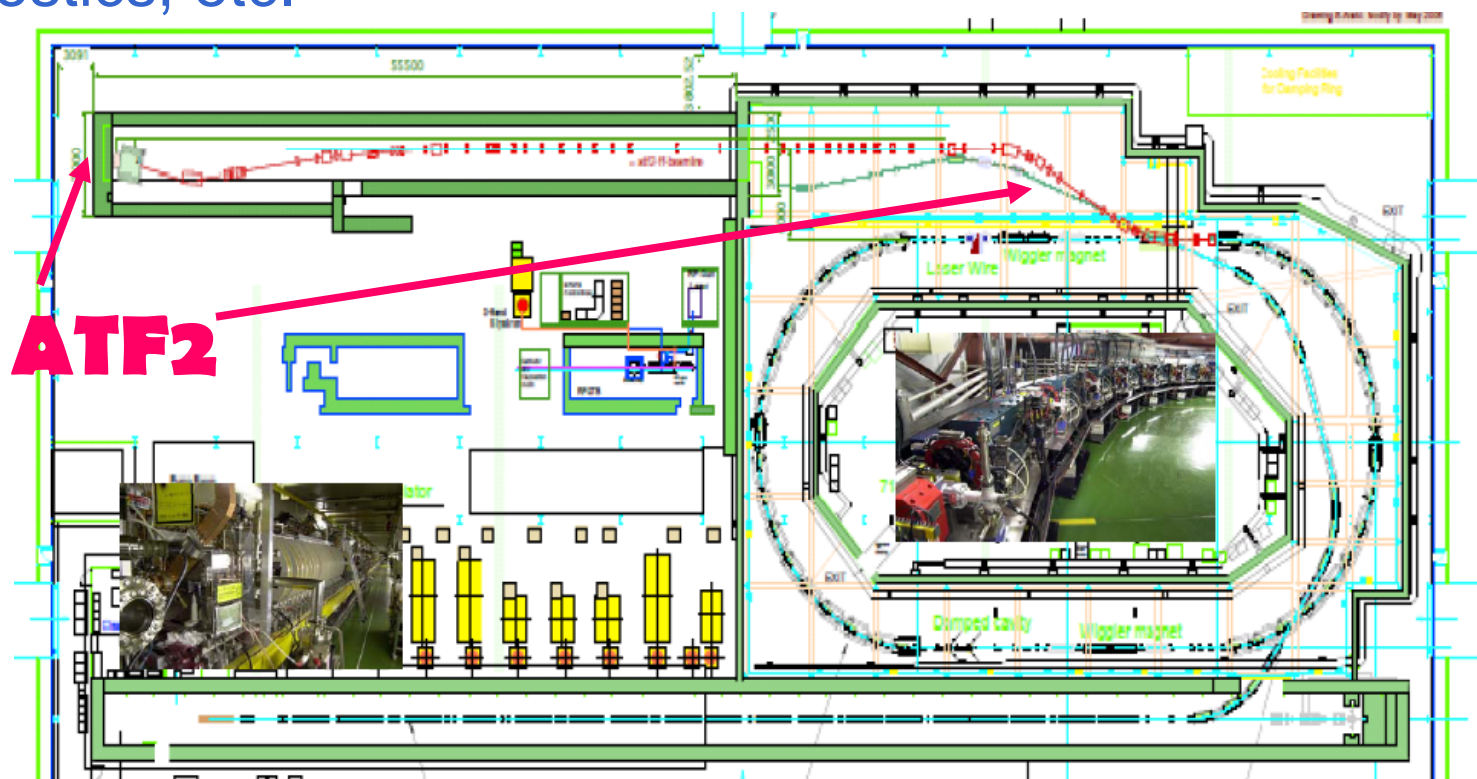
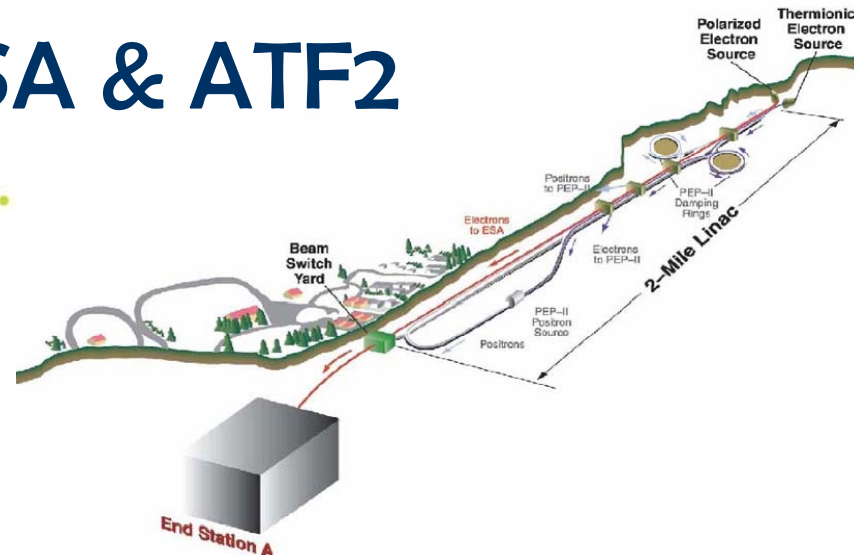
Alain Herve et al



Test facilities: ESA & ATF2

ESA: machine-detector tests; energy spectrometer; collimator wake-fields, etc.

ATF2: prototype FF, develop tuning, diagnostics, etc.

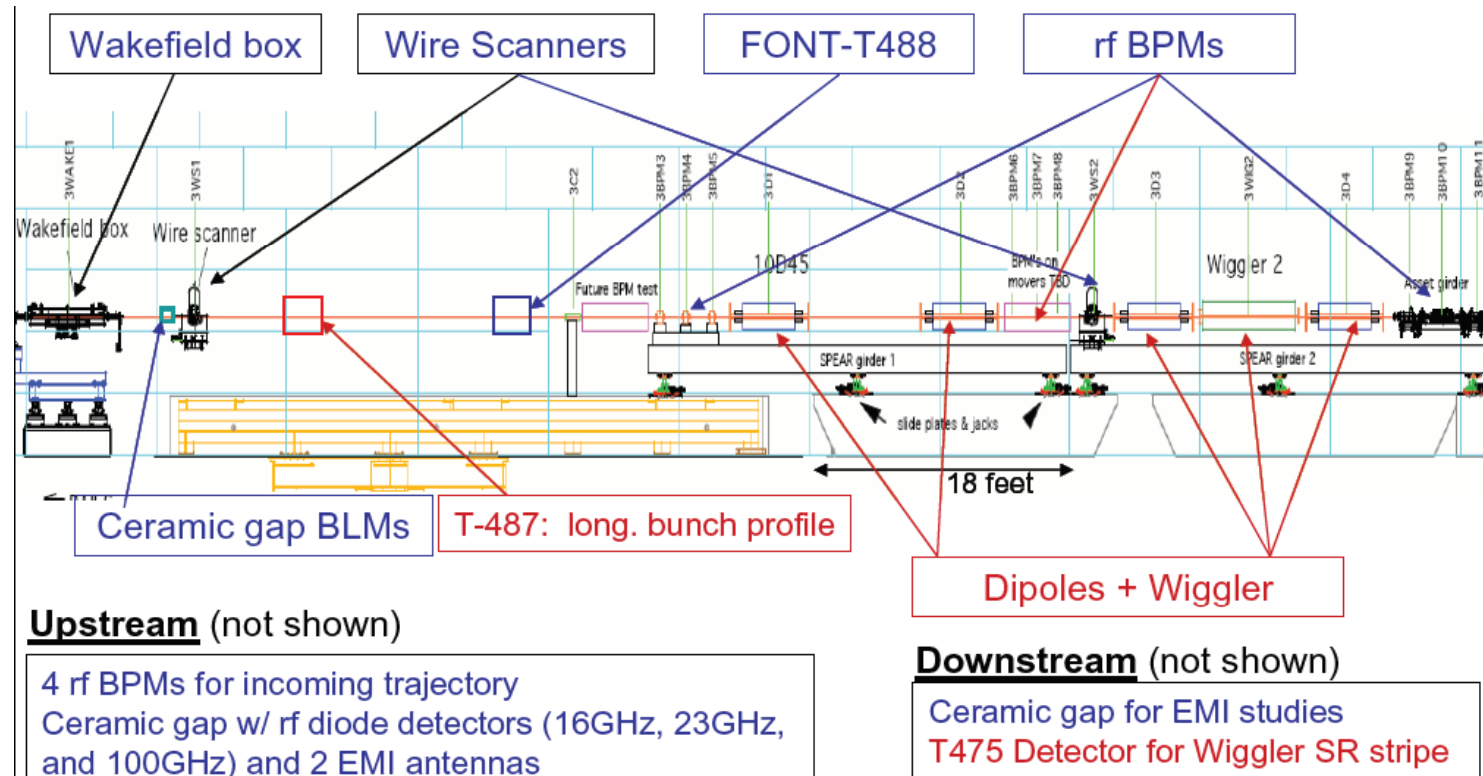
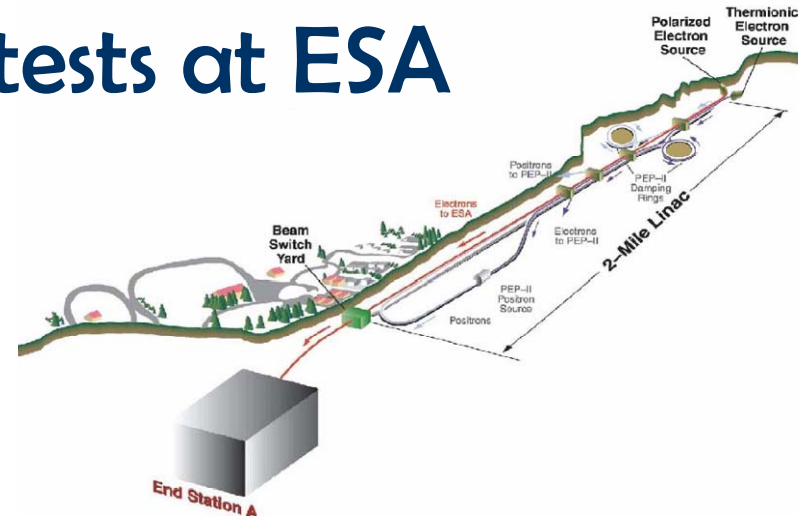




BDS beam tests at ESA

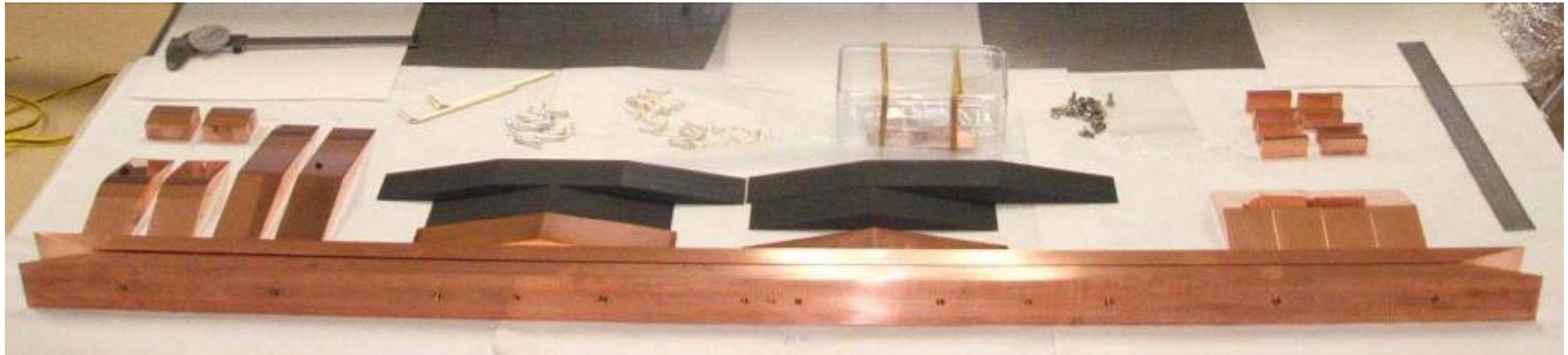
Study:

- BPM energy spectrometer
- Synch Stripe energy spectrometer
- Collimator design, wakefields
- IP BPMs/kickers—background studies
- EMI (electro-magnetic interference)
- Bunch length diagnostics

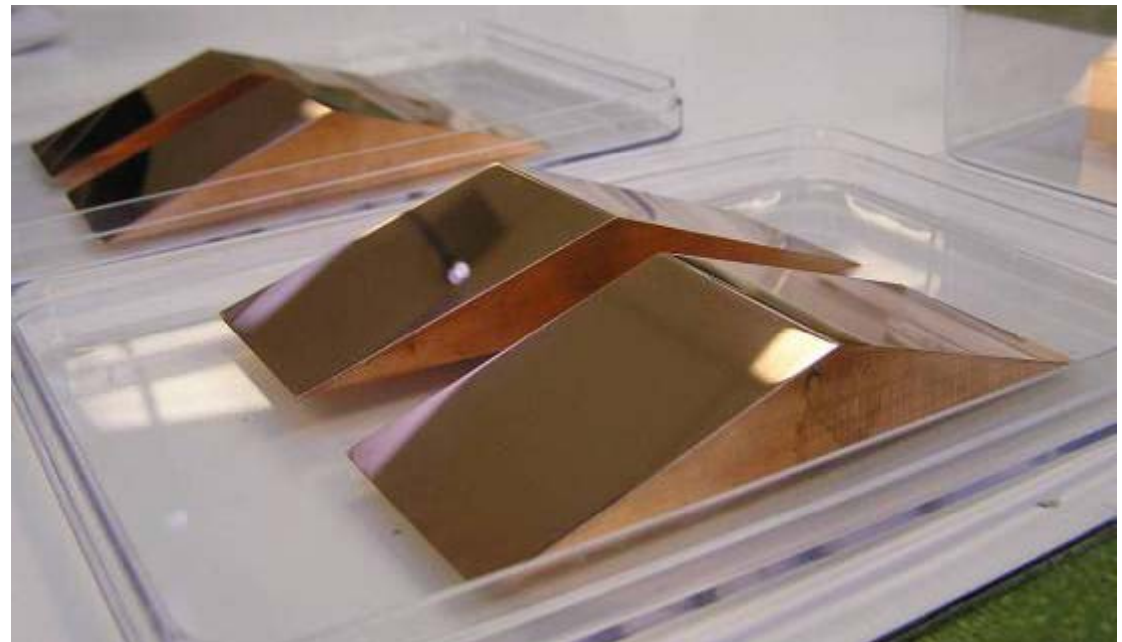




Collimator Wakefield study at ESA

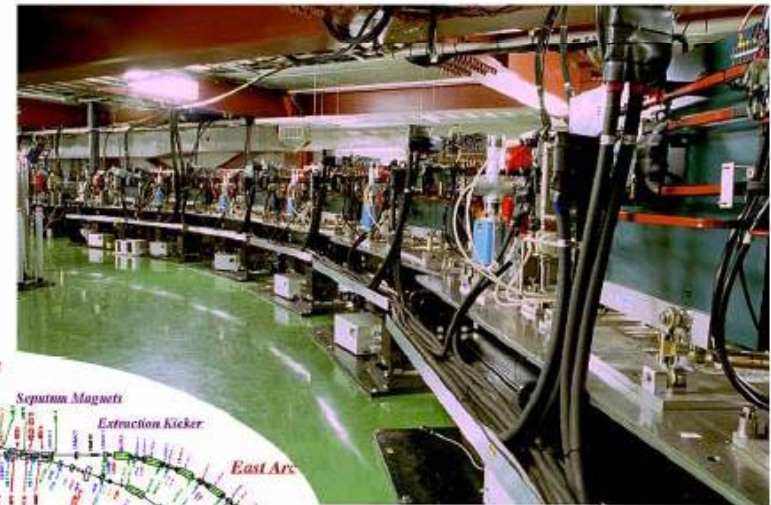


- Spoilers of different shape investigated at ESA (N.Watson et al)
- Theory, 3d modeling and measurements are so far within a factor of ~ 2 agreement



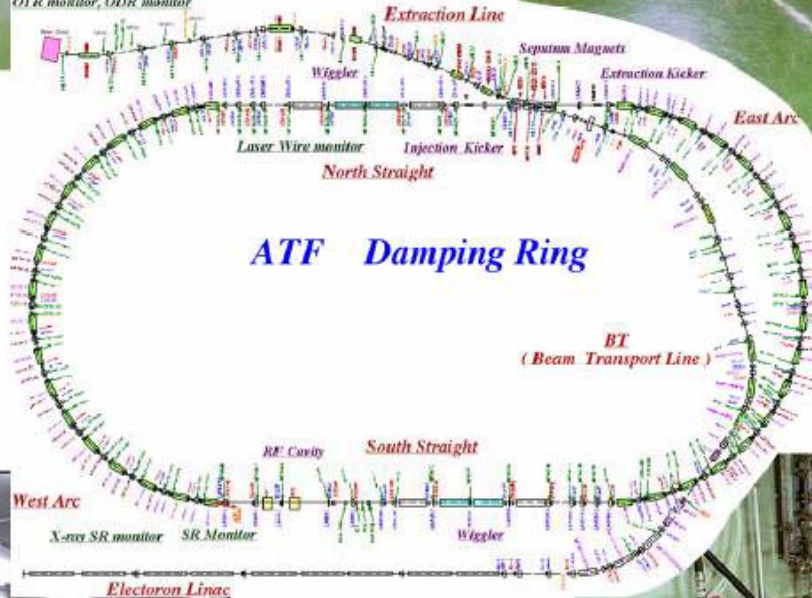


Extraction Line



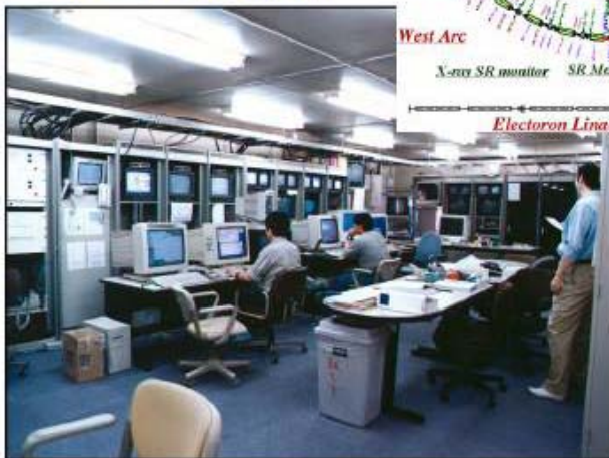
Damping Ring

ATF and ATF2



ATF Damping Ring

Linac

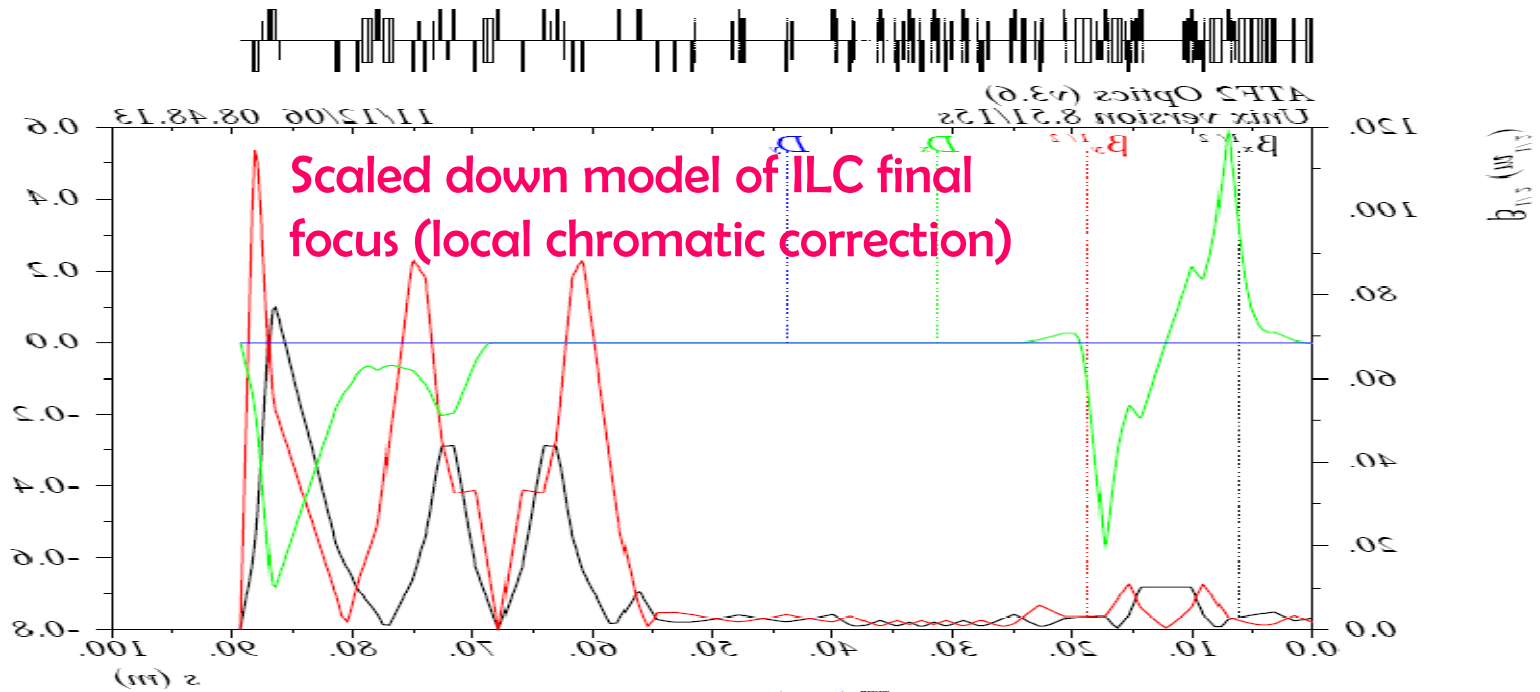


Control Room



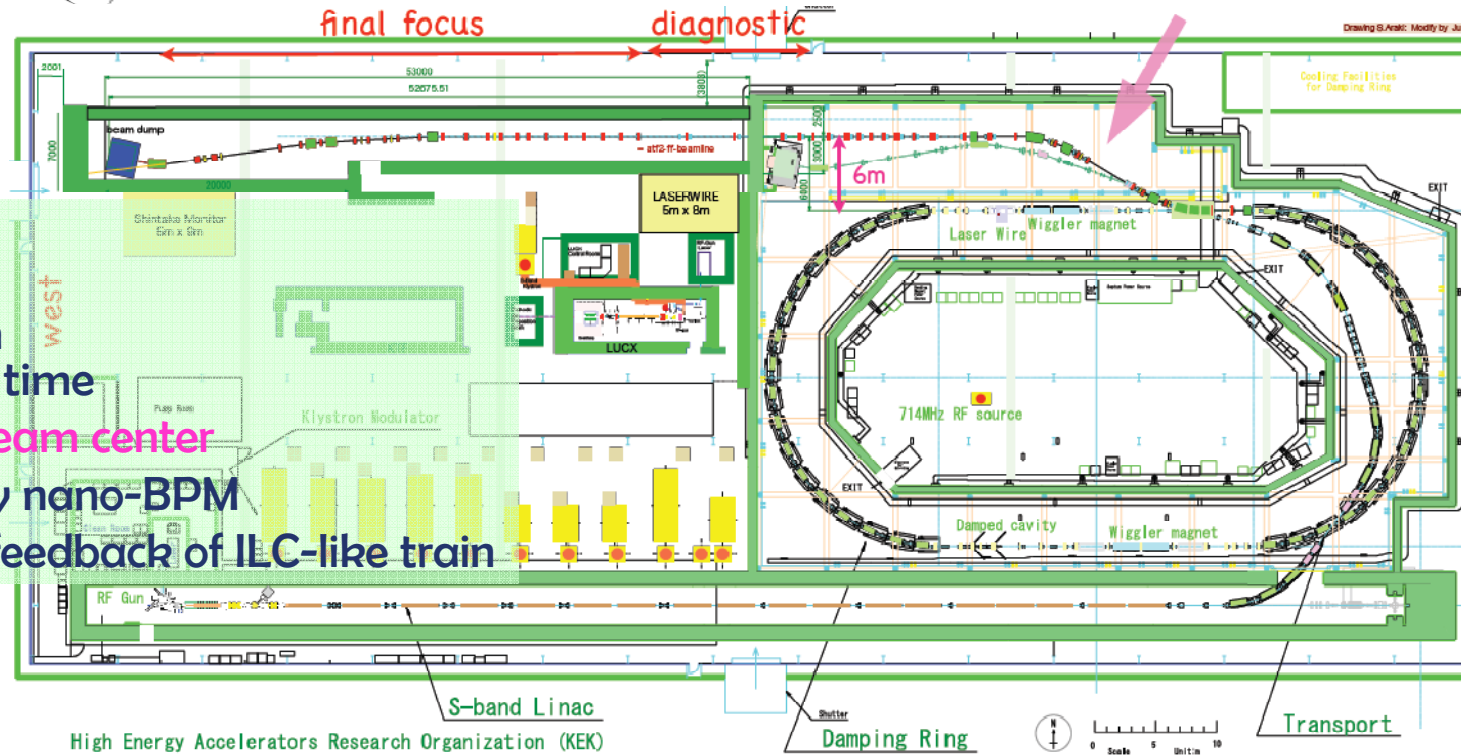


ATF2 – model of ILC BDS



ATF2 goals

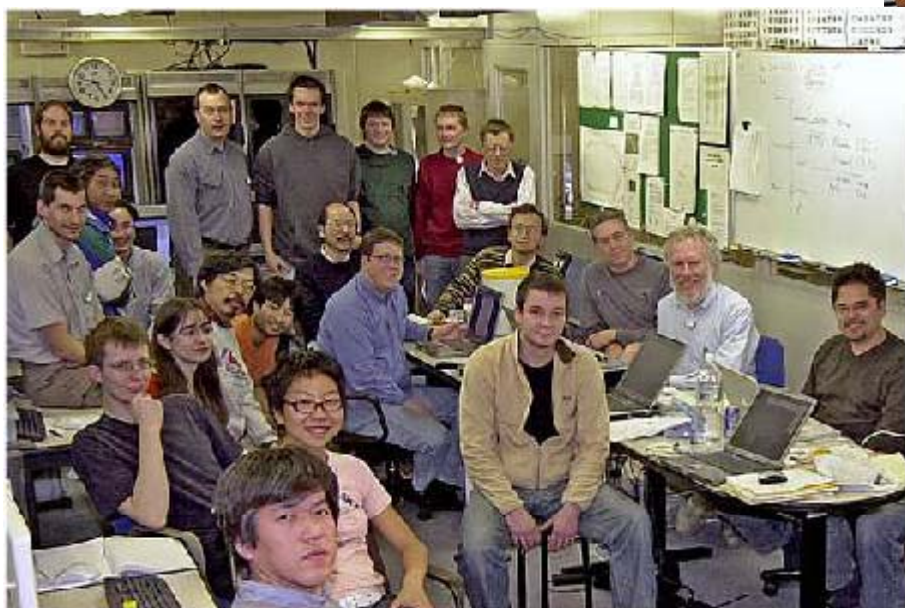
- (A) **Small beam size**
Obtain $\sigma_y \sim 35\text{nm}$
Maintain for long time
- (B) **Stabilization of beam center**
Down to $< 2\text{nm}$ by nano-BPM
Bunch-to-bunch feedback of ILC-like train





ATF collaboration & ATF2 facility

- ATF2 will prototype FF,
- help development tuning methods, instrumentation (laser wires, fast feedback, submicron resolution BPMs),
- help to learn achieving small size & stability reliably,
- potentially able to test stability of FD magnetic center.



- ATF2 is one of central elements of BDS EDR work, as it will address a large fraction of BDS technical cost risk.
- Constructed as ILC model, with in-kind contribution from partners and host country providing civil construction
- ATF2 commissioning will start in Autumn of 2008



ATF hall before ATF2 construction



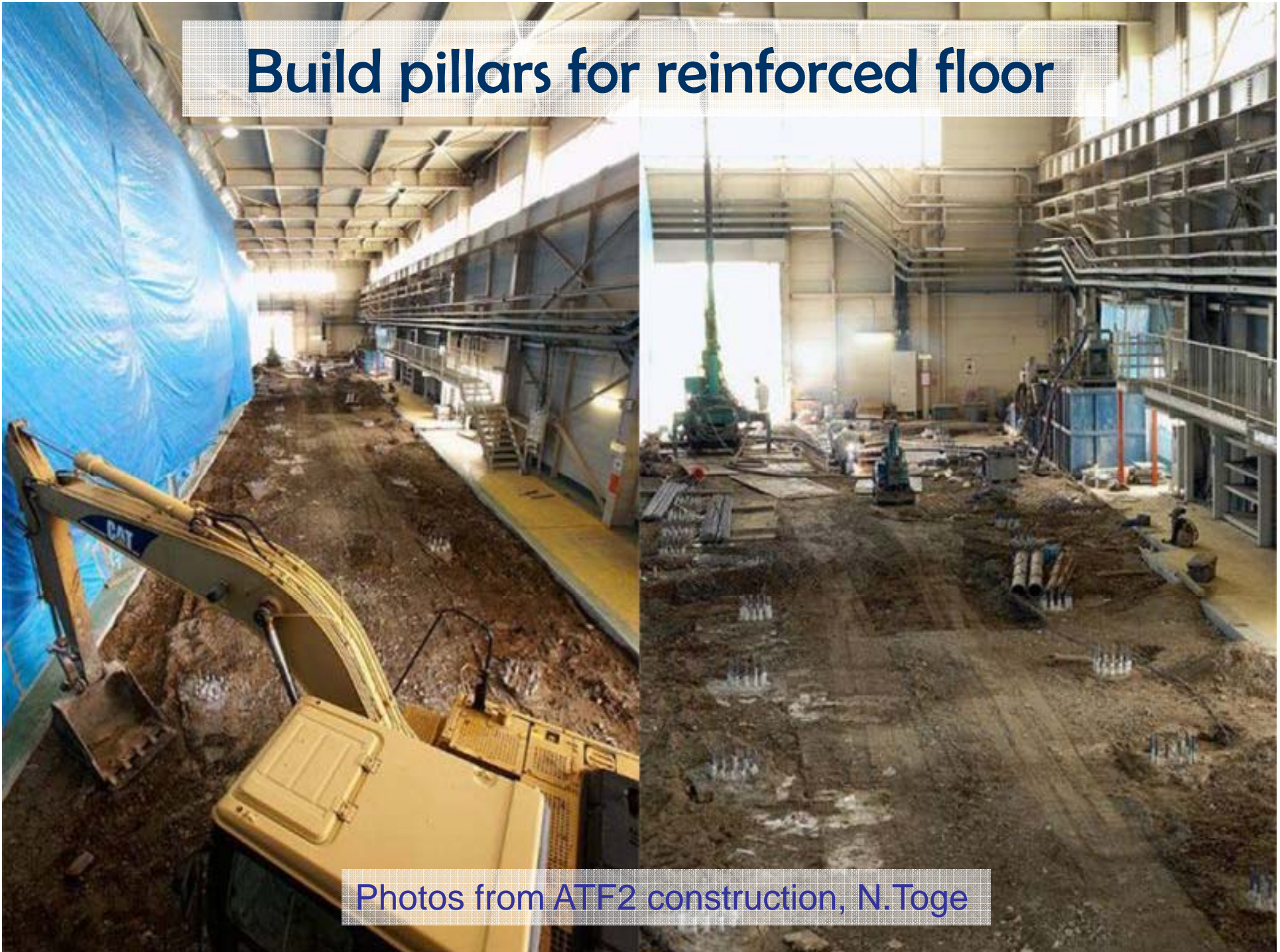


ATF hall emptied



Photos from ATF2 construction, N.Toge

Build pillars for reinforced floor



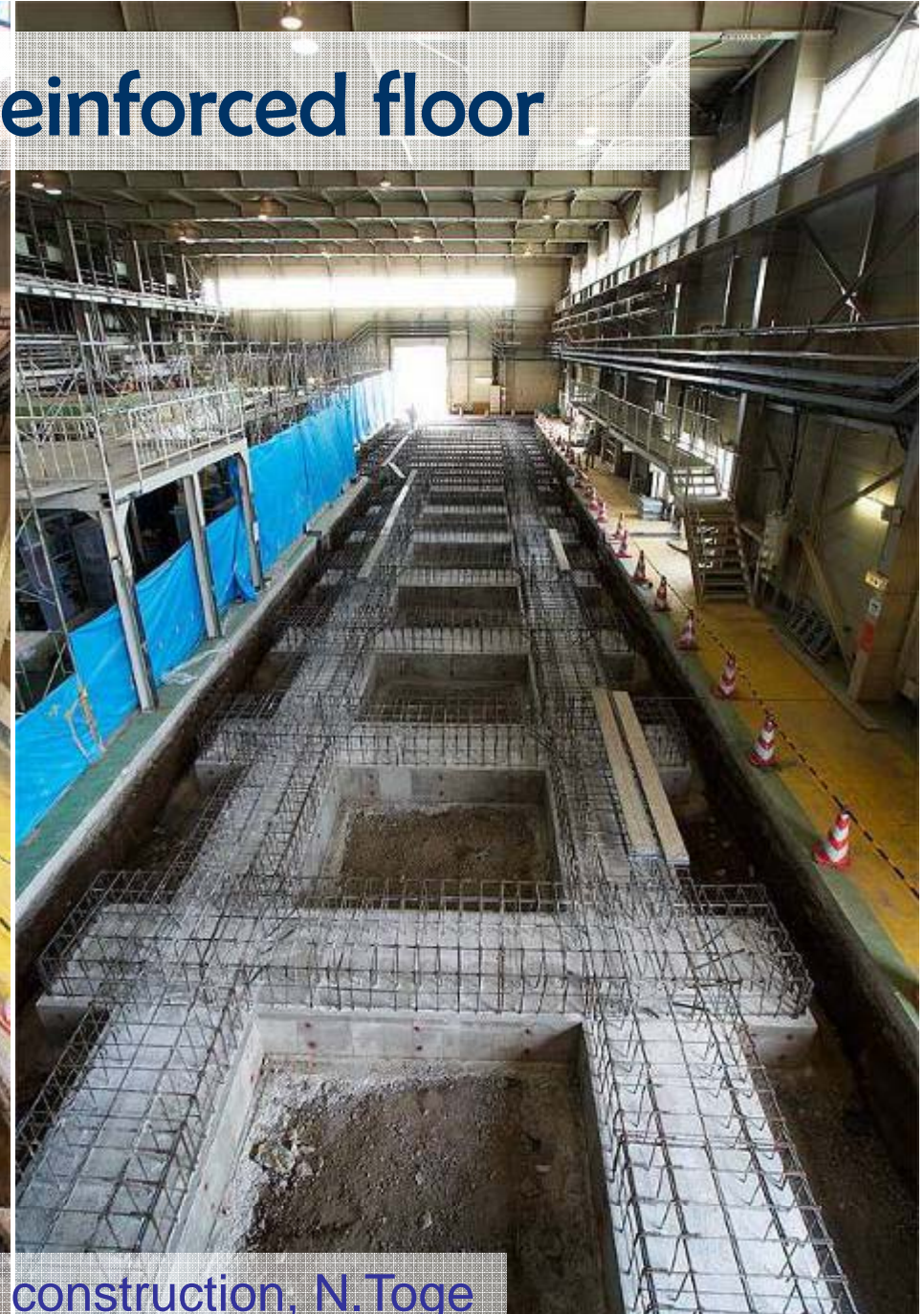
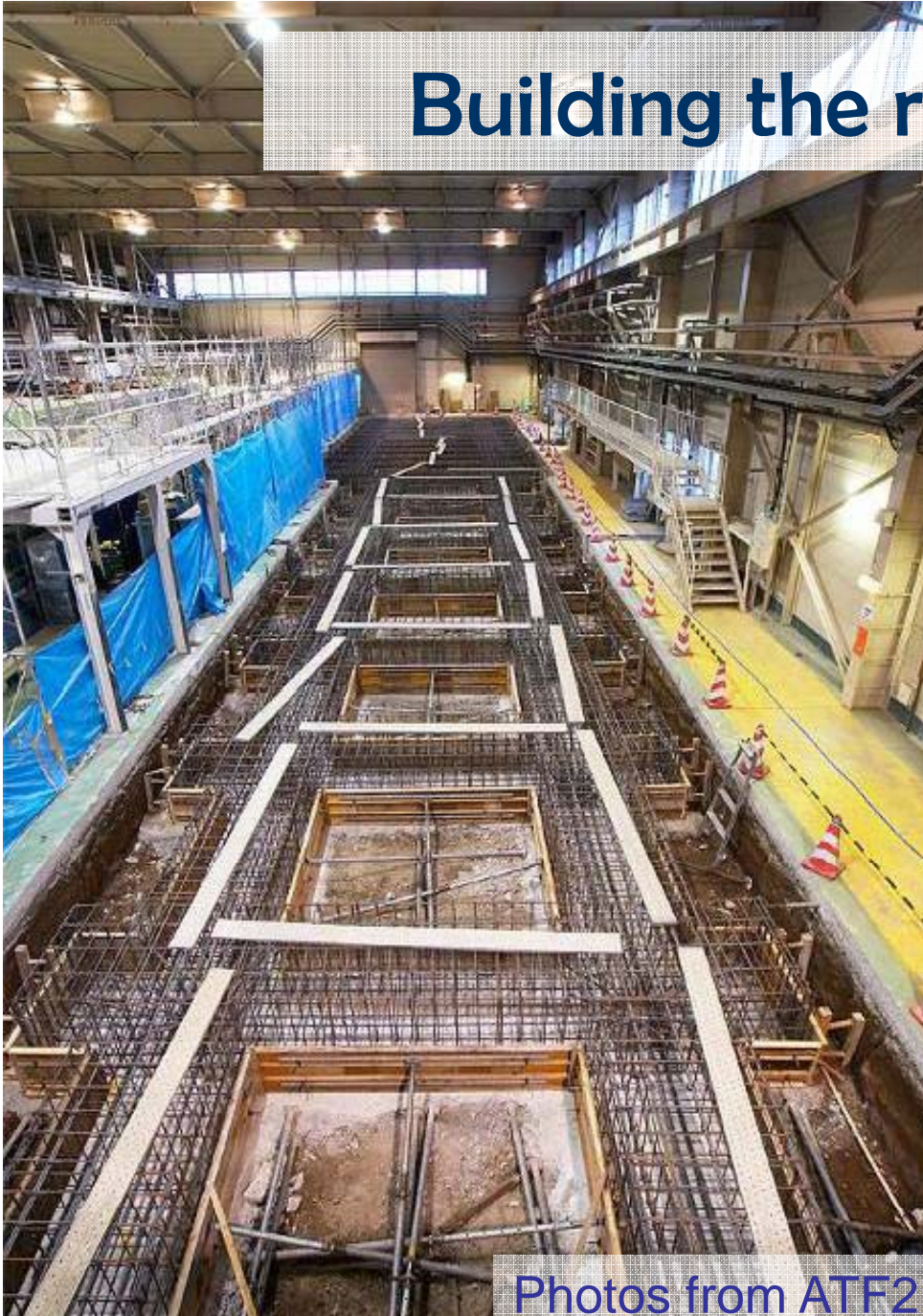
Photos from ATF2 construction, N. Toge

Build pillars for reinforced floor



Photos from ATF2 construction, N.Toge

Building the reinforced floor



Photos from ATF2 construction, N. Toge

Finishing the reinforced floor for ATF2



Photos from ATF2 construction, N.Toge



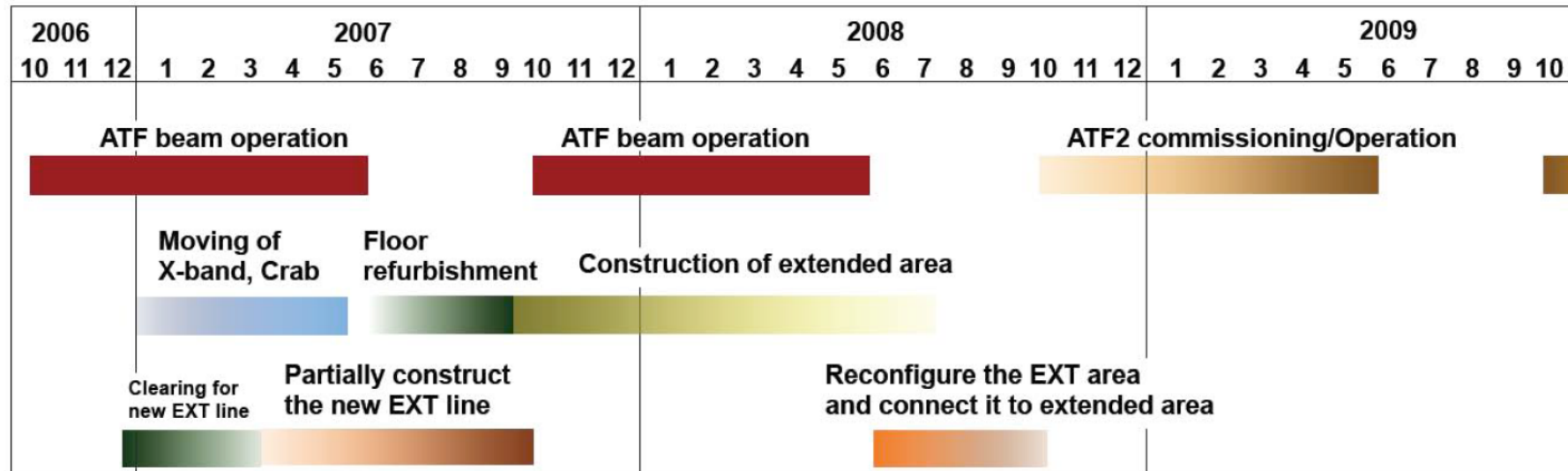
Finished reinforced floor for ATF2



Photos from ATF2 construction, N.Toge



ATF2 schedule

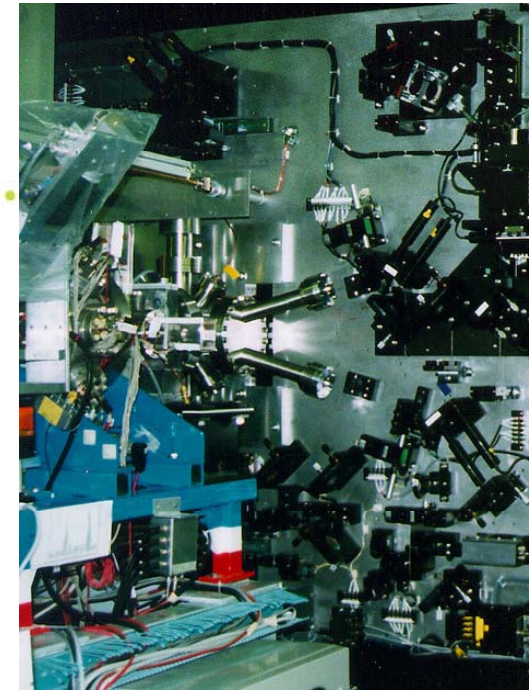


- **Construction of the extended shield area for final focus system can be done during the ATF beam operation.**
- Partial construction beside the current EXT line in shutdown week will release the work load for reconfiguration of the EXT line in summer of 2008.
- **ATF2 beam will come in October, 2008.**

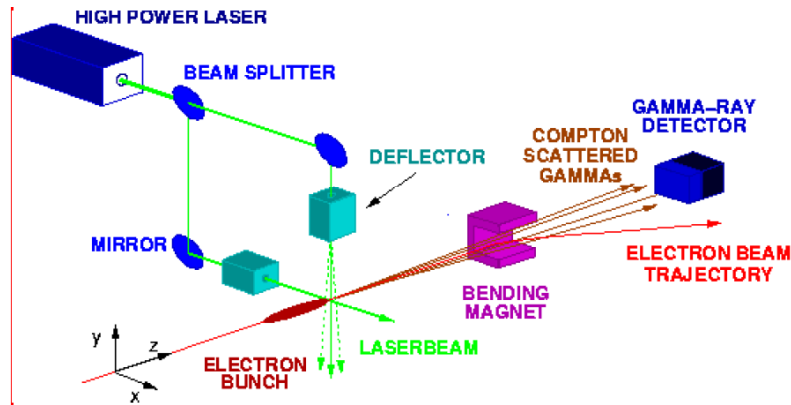


Advanced beam instrumentation at ATF2

- BSM to confirm 35nm beam size
- nano-BPM at IP to see the nm stability
- Laser-wire to tune the beam
- Cavity BPMs to measure the orbit
- Movers, active stabilization, alignment system
- Intratrain feedback, Kickers to produce ILC-like train

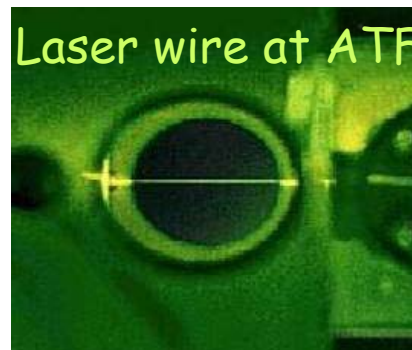
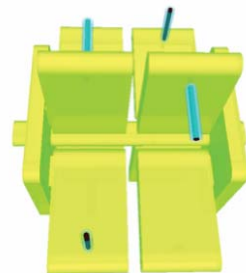


IP Beam-size monitor (BSM)
(Tokyo U./KEK, SLAC, UK)

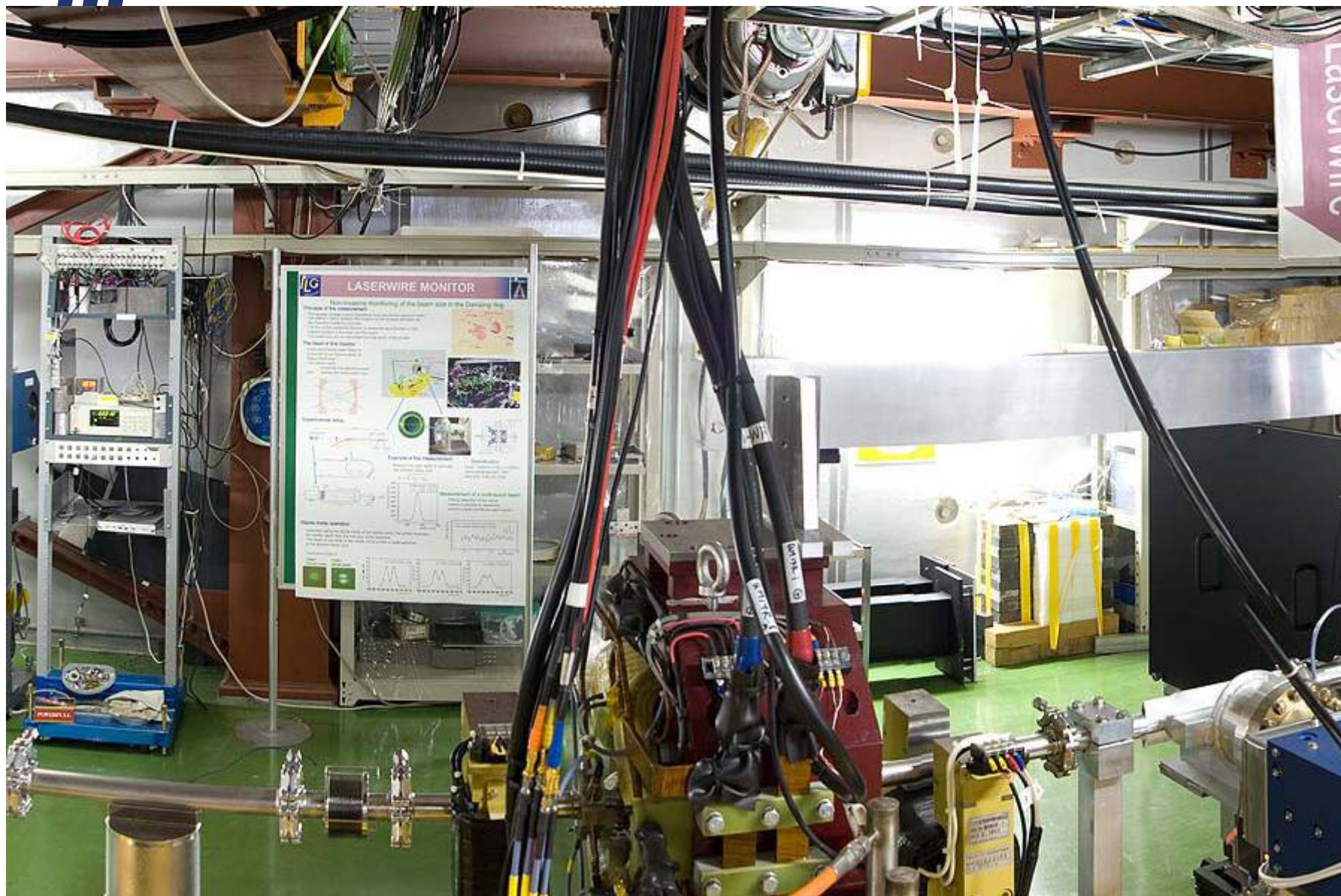


Laser-wire beam-size Monitor (UK group)

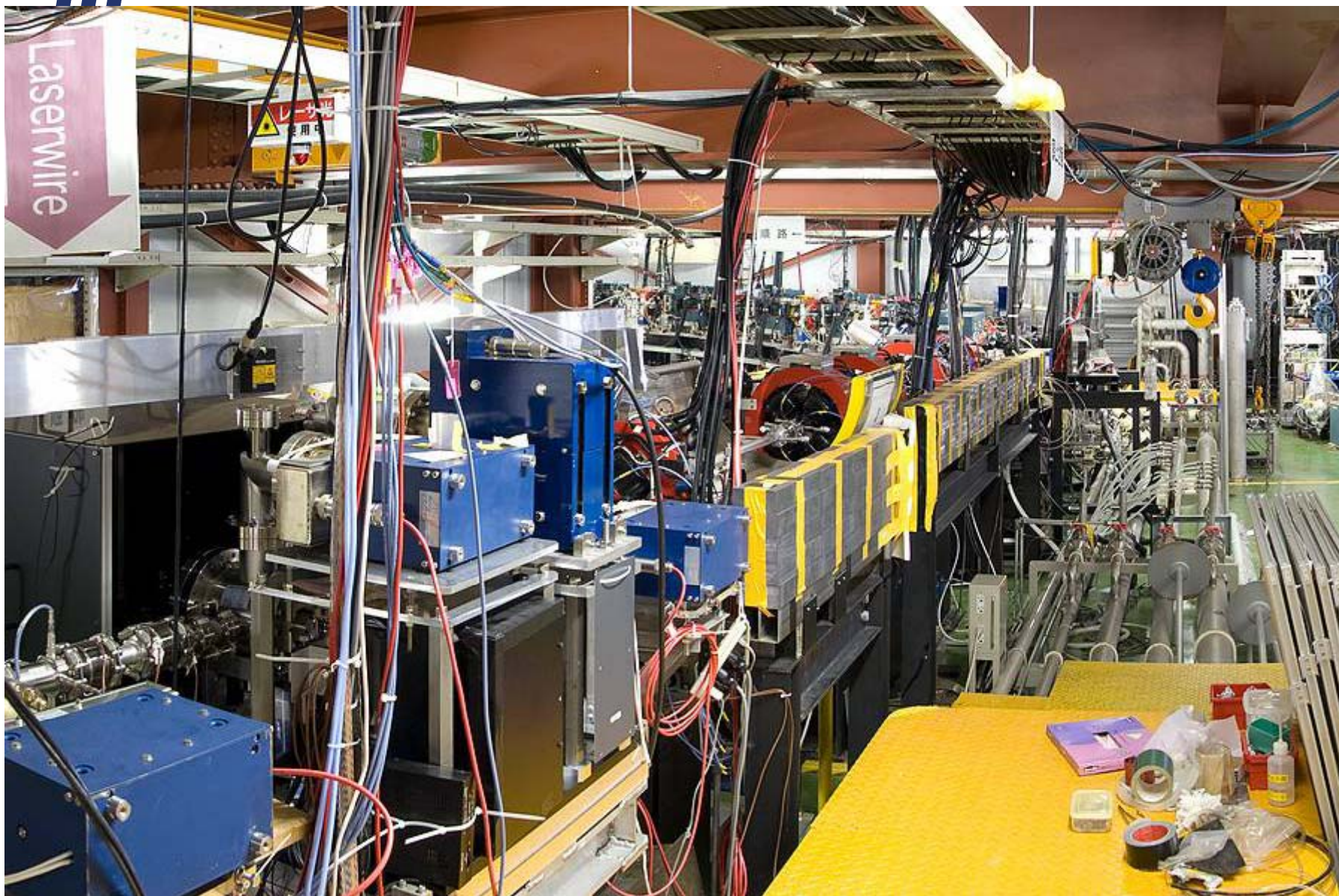
Cavity BPMs with 2nm resolution, for use at the IP (KEK)



Cavity BPMs, for use with Q magnets with 100nm resolution (PAL, SLAC, KEK)



Panoramic photo of ATF beamlines, N.Toge



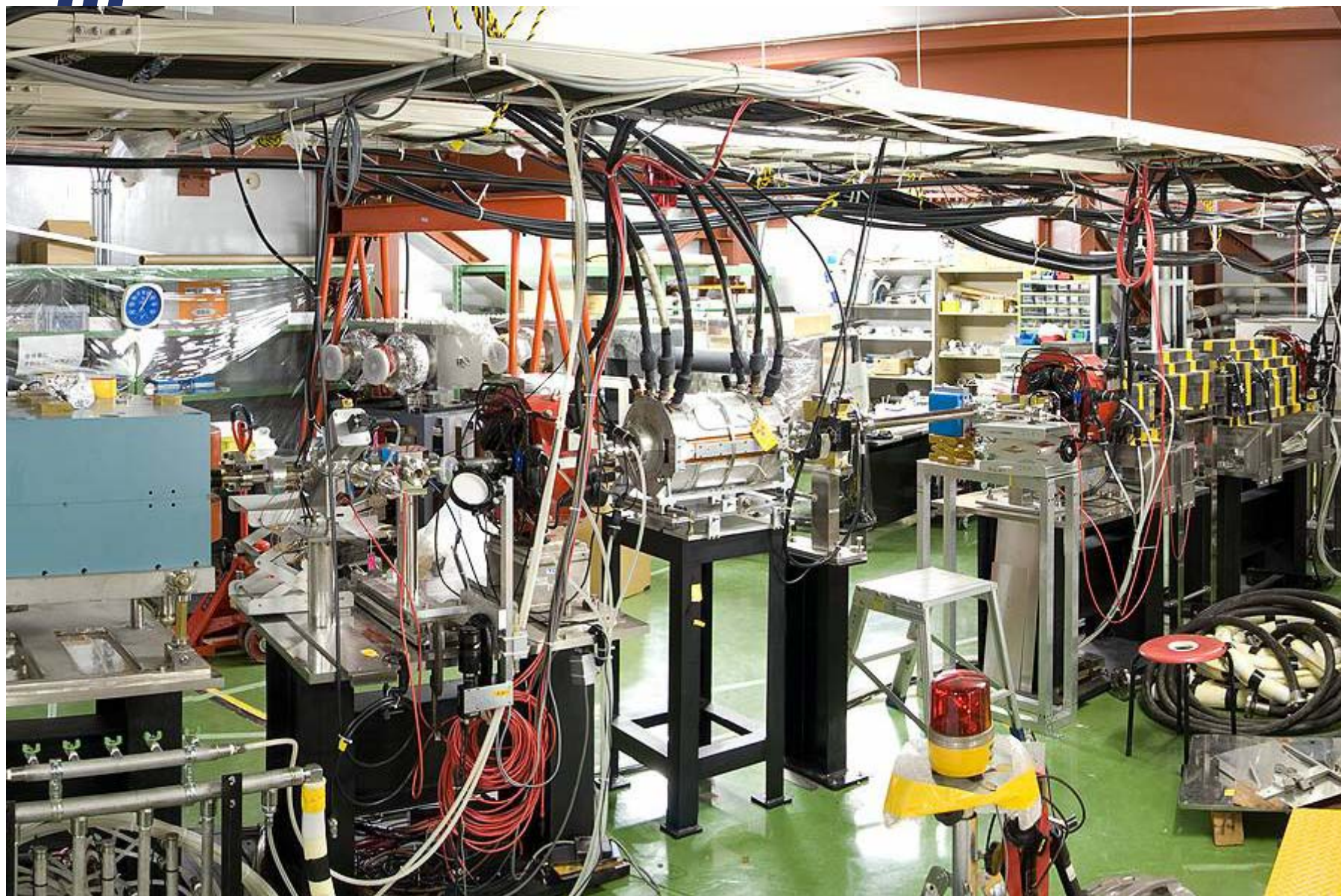
Panoramic photo of ATF beamlines, N.Toge



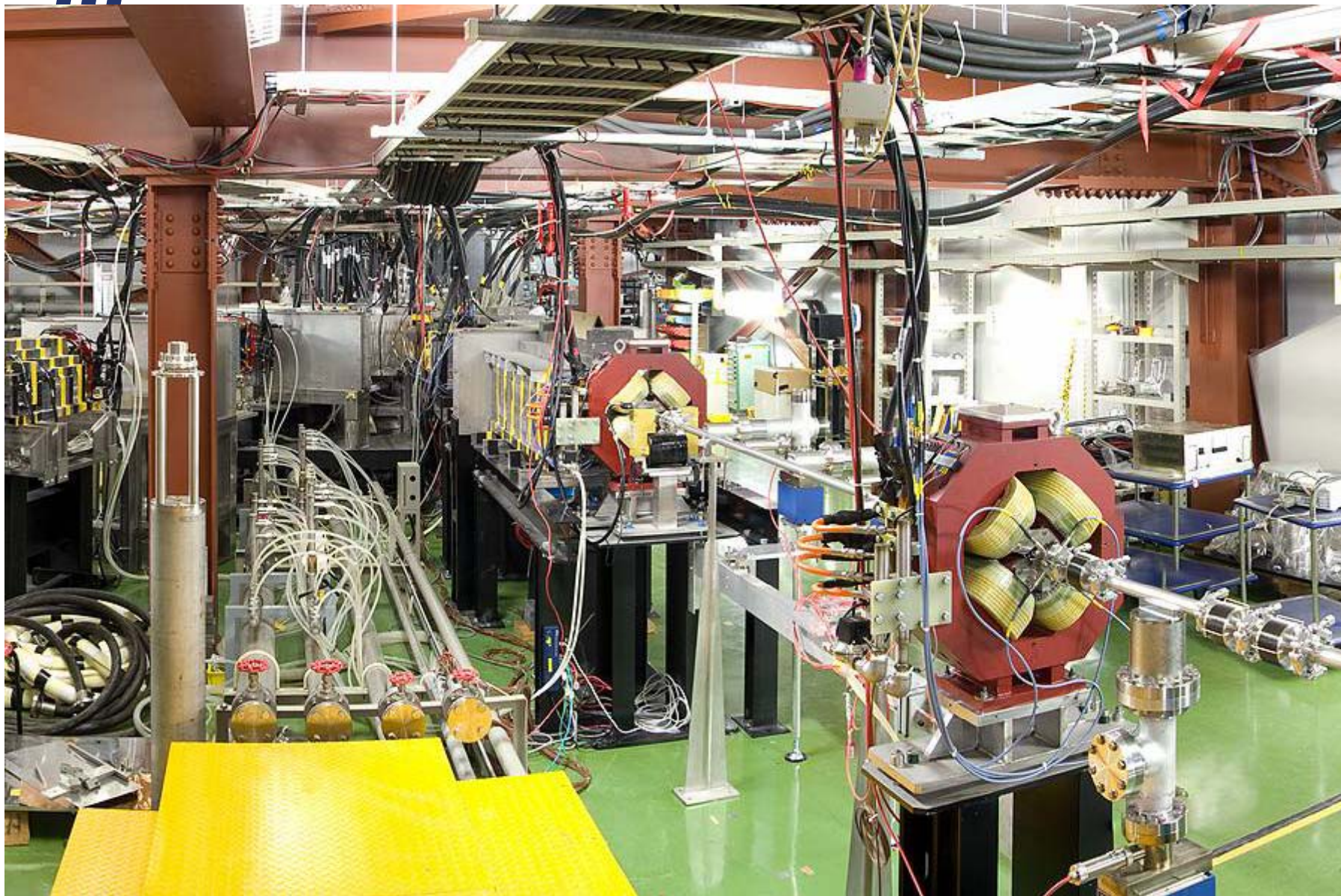
Panoramic photo of ATF beamlines, N.Toge



Panoramic photo of ATF beamlines, N.Toge



Panoramic photo of ATF beamlines, N.Toge



Panoramic photo of ATF beamlines, N.Toge

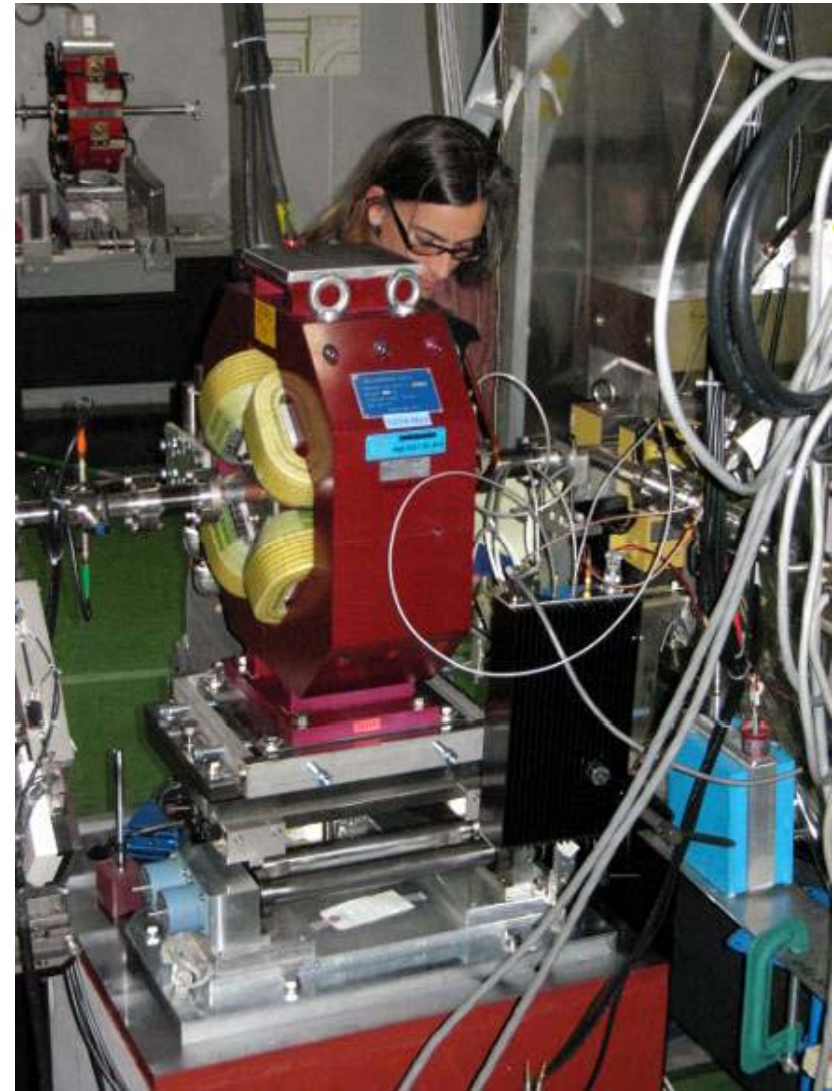


Panoramic photo of ATF beamlines, N.Toge

ilc ATF & ATF2



J.Nelson (at SLAC) and T.Smith (at KEK) during recent "remote participation" shift. Top monitors show ATF control system data. The shift focused on BBA, performed with new BPM electronics installed at ATF by Fermilab colleagues.



T.Smith is commissioning the cavity BPM electronics and the magnet mover system at ATF beamline



Parameter	Units	Value
Length (linac exit to IP distance)/side	m	2226
Length of main (tune-up) extraction line	m	300 (467)
Max Energy/beam (with more magnets)	GeV	250 (500)
Distance from IP to first quad, L*	m	3.5-(4.5)
Crossing angle at the IP	mrad	14
Nominal beam size at IP, σ^* , x/y	nm	639/5.7
Nominal beam divergence at IP, θ^* , x/y	μrad	32/14
Nominal beta-function at IP, β^* , x/y	mm	20/0.4
Nominal bunch length, σ_z	μm	300
Nominal disruption parameters, x/y		0.17/19.4
Nominal bunch population, N		2×10^{10}
Beam power in each beam	MW	10.8
Preferred entrance train to train jitter	σ_y	< 0.5
Preferred entrance bunch to bunch jitter	σ_y	< 0.1
Typical nominal collimation aperture, x/y		8–10/60
Vacuum pressure level, near/far from IP	nTorr	1/50



BEAM DELIVERY



Thanks to Bill Barletta for the picture



- Many thanks to colleagues whose slides, results or photos were used in this lecture, namely Tom Markiewicz, Nikolai Mokhov, Daniel Schulte, Mauro Pivi, Nobu Toge, Brett Parker, Nick Walker, Timergali Khabibouline, Kwok Ko, Cherrill Spencer, Lew Keller, Sayed Rokni, Alberto Fasso, Joe Frisch, Yuri Nosochkov, Mark Woodley, Takashi Maruyama, Eric Torrence, Karsten Busser, Graeme Burt, Glen White, Phil Burrows, Tochiaki Tauchi, Junji Urakawa, and many other

Thanks to you for attention!



Homework and exams

- Homework for tonight:
 - Several tasks and several multiple choice problems
- Final exam
 - Several multiple choice problems and questions