RF And Wakefield Modeling For the ILC Main Linac

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Presented for the ML-KOM Meeting, 9-27-2007

Work supported by U.S. DOE ASCR, BES & HEP Divisions under contract DE-AC02-76SF00515





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Work supported by U.S. DOE ASCR, BES & HEP Divisions under contract DE-AC02-76SF00515





SLAC Parallel Codes under SciDAC1

- Electromagnetic codes in production mode:
 - Omega3P frequency domain eigensolver for mode and damping calculations
 - S3P frequency domain S-parameter computations
 - T3P time domain solver for transient effects and wakefield computations with beam excitation
 - Track3P particle tracking for dark current and multipacting simulations
 - V3D visualization of meshes, fields and particles





SLAC Parallel Codes under SciDAC2

Codes under development:

- Electromagnetics
 - Gun3P 3D electron trajectory code for beam formation and transport
 - Pic3P self-consistent particle-in-cell code for RF gun and klystron (LSBK) simulations
 - TEM3P integrated EM/thermal/mechanical analysis for cavity design
- Beam dynamics

Nimzovich – particle-in-cell strong-strong beambeam simulation





Applications To ILC R&D

- Accelerating Cavity (DESY, KEK, JLab)
 - Alternative design
 - HOM damping
 - Coupler asymmetry effects
- Cavity imperfection modeling
 - Effects On HOM damping
 - 3D Wakefields and beam dynamics
- Cryomodule and RF unit simulation
 - Trapped modes
 - Wakefidls, x-y coupling effects
- Cryomodule HOM heating
 - Beamline absorber
 - Heat load distribution in low temperature environment
- Integrated multi-physics tools for RF/Thermal/Mechanical analysis
- Input Coupler study
- L-Band Sheet Beam Klystron Gun and window modeling
- BDS Crab Crossing (FNAL/UK) Deflecting cavity
- Damping Ring (LBNL) Impedance calculations





Alternative Cavity Design – HOM Damping





A=30mm LL/Re-entrant Cell Comparison



L.J.

LL Cavity End-group Design

LL Shape

- >15% higher R/Q (1177 ohm/cavity)
- >12% lower Bpeak/Eacc ratio
- 20% lower cryogenic heating



- Most important modes are 0-mode in the 3rd band
- High R/Q in the 1st&2nd bands are up to 1/3 of the 3rd band
- Beam pipe tapers down to 30-mm, 3rd band damped locally by HOM couplers
- Damping criteria: 3rd band mode Qext<10⁵ (?)







LL Cavity End-group



Effective damping achieved by optimizing: •End-group geometry to increase fields in coupler region •Loop shape and orientation to enhance coupling •Optimized azimuthal coupler orientation for x-y mode polarization





Multipacting in HOM Coupler





MP trajectories at 15-MV/m.



Initial optimized design: multipacting in the gap between the flat surface and outer cylinder at field levels starting from 10-MV/m and up.





larger gap

round surfaces

Re-optimized loop: with round surfaces and a larger gap.

- No multipacting up to 50MV/m.
- Qext for the 3rd band mode is 3.4x10⁴





Cavity Imperfection

- HOM damping
- X-Y coupling
- Effects on beam emittance





TESLA Cavity Measurement Data





The actual cell shape differ from the ideal design due to fabrication errors





Dipole mode frequencies shift and Qext scatter.







- Determine shape deformation from measured cavity data, inverse and forward methods
- Important to understand effect on Qext and x-y coupling of beam dynamics
- Actual deformation? geometry measurement data will be very helpful





Cylindrical Symmetric Deformation (200micro on top/607micro on disk)

- cause frequency shift



 $f\pi$ -f8 π /9=772KHz within meas. Range. 1st/2nd dipole band mode freq. shift roughly fit measurement data.

8-cavity measurement v.s. simulation/fitting



Need add randomness to imperfection parameters to model "realistic cavities"





Cell elliptical deformation (dr=250micro)

- cause mode Mode x-y coupling& Qext scattering







Coupler RF and SW Kicks

- Found to be important issues
- Studies being carried out
- See for details
 - Igor Zagorodnov and Martin Dohlus talk, ILC Workshop, DESY, 31 May, 2007
 - Z. Li cavity KOM talk, Sept. 20, 2007





TTFIII Coupler – Multipacting Analysis



Multipacting Simulation – Track3P

- 3D parallel high-order finite-element particle tracking code for dark current and multipacting simulations (developed under SciDAC)
- Track3P
 - traces particles in resonant modes, steady state or transient fields
 - accommodates several emission models: thermal, field and secondary
- MP simulation procedure
 - Launch electrons on specified surfaces with different RF phase, energy and emission angle
 - Record impact position, energy and RF phase; generate secondary electrons based on SEY according to impact energy
 - Determine "resonant" trajectories by consecutive impact phase and position
 - Calculate MP order (#RF cycles/impact) and MP type (#impacts /MP cycle)
- Track3P benchmarked extensively
 - Rise time effects on dark current for an X-band 30-cell structure
 - Prediction of MP barriers in the KEK ICHIRO cavity





Mulitpacting in Coax of TTFIII Coupler



More simulations being carried out to understand measurement details.





Modeling ILC Cryomodule & RF Unit



Physics Goal: Calculate wakefield effects in the 3-cryomodule RF unit with realistic 3D dimensions and misalignments

- Trapped mode and damping
- Cavity imperfection effects on HOM damping
- Wakefield effect on beam dynamics
- Effectiveness of beam line aborsorber





ILC 8-Cavity Module



A dipole mode in 8-cavity cryomodule at 3rd band

First ever calculation of a 8 cavity cryomodule

- ~ 20 M DOFs
- ~ 1 hour per mode on 1024 CPUs for the cryomodule

To model a 3-module RF unit would require

- >200 M DOFs
- Advances in algorithm and solvers
- Petascale computing resources





- TDR 8-Cavity Module 3rd Band Modes From Omega3P Calculation (R. Lee)
- **╶**≈<u>\\\\\\</u>

Calculated on NERSC Seaborg: 1500 CPUs, over one hour per mode



Kick Factor Of One Set Of 3rd Band Modes in the 8-Cavity TDR Module



- Modes above cutoff frequency are coupled through out 8 cavities
- Modes are generally x/y-tilted & twisted due to 3D end-group geometry
- Both tilted and twisted modes cause x-y coupling







One polarization mode is well damped.

INVESTIGATION OF A HIGH-Q DIPOLE MODE AT THE TESLA CAVITIES

N. Baboi^{*}, M. Dohlus, DESY, Hamburg, Germany C. Magne, A. Mosnier, O. Napoly, CEA, Saclay, France H.-W. Glock, Uni Rostock, Germany

At TTF several experiments have been made in order to study the HOMs. By modulating the beam current [2], several high impedance modes have been found to have a very high Q [3]. Specially a mode around 2.585 GHz, the last of the 3rd dipole band, having an estimated impedance $R/Q = 15 \ \Omega/cm^2$, was found to be badly damped in 2 cavities of the first module. Nevertheless, the other polarization of the same mode is better damped. It was found that this mode is badly damped in one of the cavities of the 2rd and 3rd modules as well. The results are summarized in Table. 1.

Table 1. Results of HOM investigations for the last mode of the 3^{rd} dipole passband (R/Q = $15 \Omega/cm^2$)

Cavity nr./module	Freq. [GHz]	Q
#3 (S10) / 1	2.5845	1.1·10 ⁶
#6 (S11) / 1	2.5862	8.6·10 ⁴
#5 (A15) / 2	2.5845	4.2·10 ⁵
#7 (S28) / 3	2.5906	6.5·10 ⁵



Recent Advances in Solver and Meshing - Improving Modeling Efficiency

Linear Solver

Simulation capabilities limited by memory available even on DOE flagship supercomputers – develop methods for reducing memory usage

Method	Memory (GB)	Runtime (s)
MUMPS	155.3	293.3
MUMPS + single precision factorization	82.3	450.1

<u>Meshing</u>

- Invalid quadratic tets generated on curved surface
- Collaborated with RPI on a mesh correction tool
- Runtime of corrected model faster by 30% (T3P)



Invalid tets (yellow)







Beamline Absorber Study Using T3P



 $Kloss = \frac{1}{Q} \int_{0}^{+\infty} W_z(s)q(s)ds$

Calculate the total energy stored in the cavity

 $Energy(t) = \int (\frac{1}{2}\varepsilon E(t)^2 + \frac{1}{2}\mu H(t)^2)dv$

Calculate the energy absorption in the beam line absorber.

 $Energy(t) = \int \int \sigma E^2(t) \, dv \, dt$

Calculate the power heating on the NC beam pipe

 $Energy = \int \frac{1}{2\pi} Rs(\omega) H_t^2(\omega) d\omega ds$

Calculate power propagating in beam pipe

Energy $(t) = \int \int \vec{E}(t) \times \vec{H}(t) \cdot \vec{n} \, ds \, dt$

Eg.1: single cavity with beamline absorber (*εr=15, absorber conductivity=0.6*) bunch: *σz=10mm Q=3.2nc, beam on axis*





Eg.2: single cavity with beamline absorber (*εr=15, absorber conductivity=0.6*) bunch: *σz=5mm Q=3.2nc, beam on axis*



Ez(f) in the cavity

Results for Single cavity with beamline absorber

One bunch Q=3.2nc, bunch length=0.01m Loss factor (V/pc)=3.566V/pc	Lossy dielectric conductivity σ=0.6 Within 40ns
Total Energy Generated by Beam (J)	3.65e-5
Total Energy Left in cavity (J)	3.27e-5
(Total Energy due to fundament mode (J))	<u>(2.06e-5)</u>
Total Energy into beam pipe (J)	2.10e-6
Total Energy Loss in the absorber (J)	2.68e-6
Total Energy Loss on the NC beampipe wall (J)	1.24e-8

One bunch Q=3.2nc, bunch length=0.005m Loss factor (V/pc)=5.14V/pc	Lossy dielectric conductivity σ =0.6 Within 70ns
Total Energy Generated by Beam (J)	5.26e-5
Total Energy Left in cavity (J)	3.97e-5
(Total Energy due to fundament mode (J))	<u>(2.12e-5)</u>
Total Energy into beam pipe (J)	9.164e-6
Total Energy Loss in the absorber (J)	6.586e-6 J
Total Energy Loss on the NC beampipe wall (J)	

Next steps:

- Short bunches big challenges in memory and computation time
- Frequency dependent lossy material
- Multi-cavity cascading effects
- HOM power leakage through HOM couplers 3D simulation

Multi-physics Analysis for Accelerator Components

- Virtual prototyping through computing
 - RF design
 - RF heating
 - Thermal radiation
 - Lorentz force detuning
 - Mechanical stress
 - Optimization
- Large-scale parallel computing enables:
 - Large system optimization
 - Accurate and reliable multi-physics analysis
 - Fast turn around time
- TEM3P integrated parallel multi-physics tools
- -> Analyze RF/Thermal/Mechanical effects in ILC cavity and module





TEM3P: Multi-Physics Analysis



- Finite element based with highorder basis functions
 - Natural choice: FEM originated from structural analysis!
- Use the same software infrastructure as Omega3P
 - Reuse solvers framework
 - Mesh data structures and format
- Parallel





TEM3P for LCLS RF Gun – Benchmark Example



Benchmark TEM3P against ANSYS







RF Gun EM Thermal/Mechanical Analysis



Mesh for Thermal/Mechanical analysis Mesh: 0.6 million nodes. Materials: Copper + Stainless steel Thermal analysis: 7 cooling channels

Magnetic field on the cavity inner surface generates RF heat load





Thermal/Mechanical Analysis Benchmarked With ANSYS







Multi-physics Analysis for SRF Cavities and Cryomodules

- Thermal behaviors are highly nonlinear
 - To implement nonlinear temperature dependent materials
- Meshing thin shell geometry
 - Anisotropic high-order mesh will reduce significant amount of computing
 - Working with RPI/ITAPS









L-Band Sheet Beam Klystron



LBSK gun –

- Simulated using GUN3P, a parallel, 3D, finite-element (up to 4th order) electron trajectory code
- Parallel computation allows high resolution simulation with fast turnaround time



LSBK Window Modeling



Trapped modes



• MP analysis







Summary

- A suite of parallel codes in electromagnetics and beam dynamics was developed for accelerator design, optimization and analysis
- Have applied these codes to the ILC cavity design, cavity imperfection analysis, multi-cavity wakefield calculations, RF heating calculation, etc.
- Integrate RF/Thermal/Mechanical capability is being developed for multi-physics analysis.
- Through the SciDAC support and collaborations, advances in applied math and computer science are being made towards Petascale computing of large accelerator systems such as the ILC RF unit, etc



