



Vacuum System for BDS

[Completeness of RDR]

Y. Suetsugu

J. Noonan and P. Michelato

- Design principle
- Basic design
- Cost estimation
- Issues to be discussed
- Summary



Design principle_1

- General remarks
 - **The vacuum system of RDR = The minimum design for cost estimation**
 - Cost per unit length
 - **No detailed design exists, that is, the layout of pumps and the diameter of pipes, for example, were determined from a general consideration.**
 - Not responding to each component
 - **Use standard UHV vacuum system**



Design principle_2

- Use standard UHV vacuum system_1
 - **Use standard materials:**
 - SS, Cu, Al-alloy, Cu-plated SS
 - Depend on SR power, impedance requirement
 - **Use standard pumps:**
 - Ion pumps, Ti-sublimation pumps, NEG (coating)
 - TMP (Turbo-molecular pump), scroll pump for rough pumping
 - Lumped pump system, basically



Design principle_3

- Use standard UHV vacuum system_2
 - **Use standard monitors:**
 - Vacuum gauge = BA gauge (Hot cathode type)
 - Mass Analyzer = Quadrupole Mass Spectrometer
 - **Use standard components:**
 - Conflat UHV flange
 - Manifolds compatible to Conflat flanges
 - Bellows chamber with RF shield inside
 - Gate valves with RF shield inside
 - Fire-retardant, radiation resistant cables
 - Etc.....



Basic design_1

- Requirement for pressure
(equivalent to N₂/CO):
 - **5×10⁻⁶ Pa (50 nTorr), basically.**
 - **1×10⁻⁷ Pa (1 nTorr) for some region at upstream side of IP**

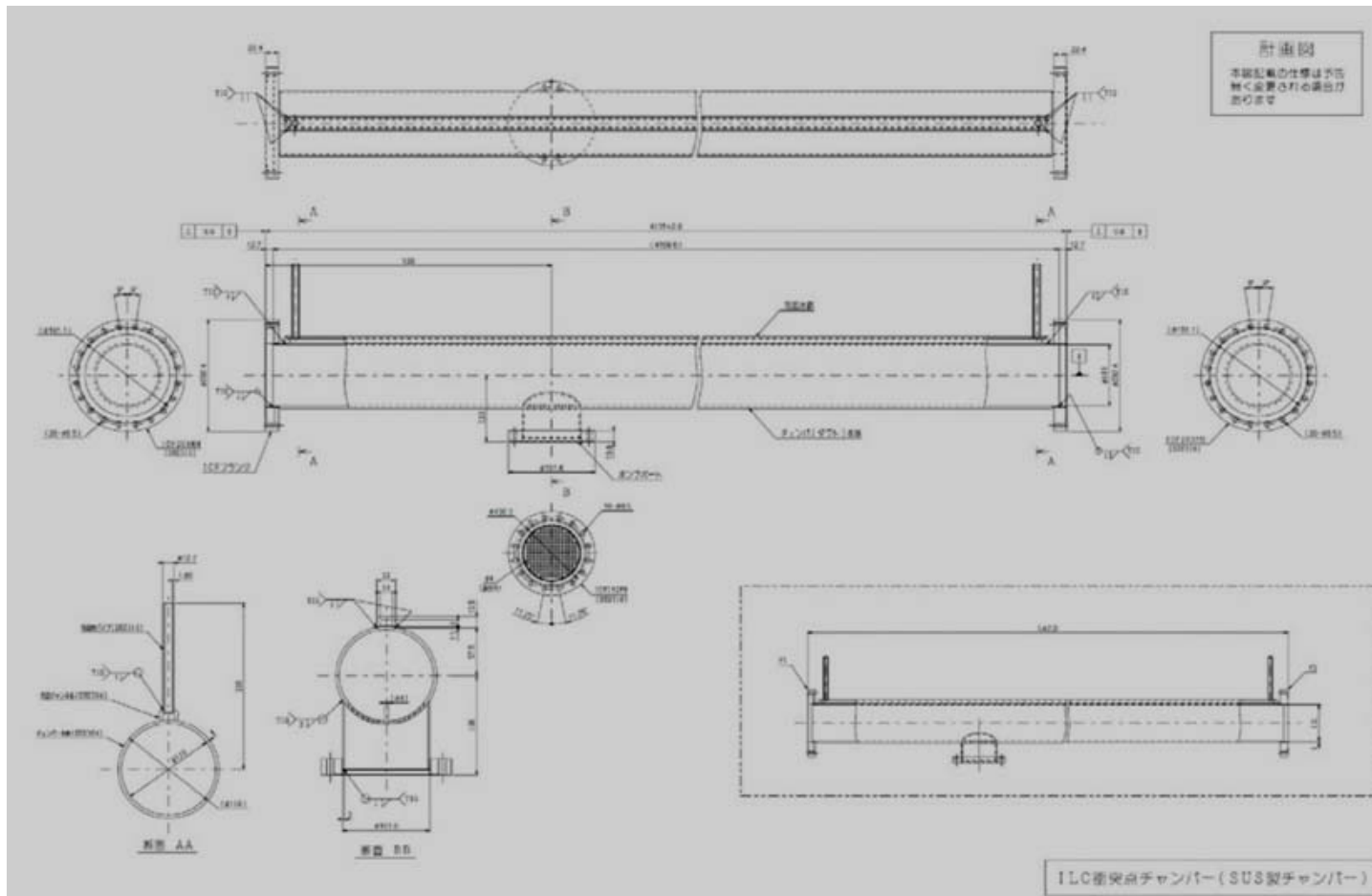


- Beam duct
 - **Duct material: Stain-less steel, basically**
Al-alloy or copper depending on SR power, and requirement from impedance
 - **No *in situ*. baking, basically**
 - **Each duct for an element is considered as a stand-alone one, that is, the flanges are at both sides of a duct.**
 - **The maximum length of a beam duct is 10 m.**
 - **The minimum length is 1 m.**
 - **One magnet has one beam duct**
 - **Circular cross section**
 - **Cooling channel at one side, if necessary**



Example_1

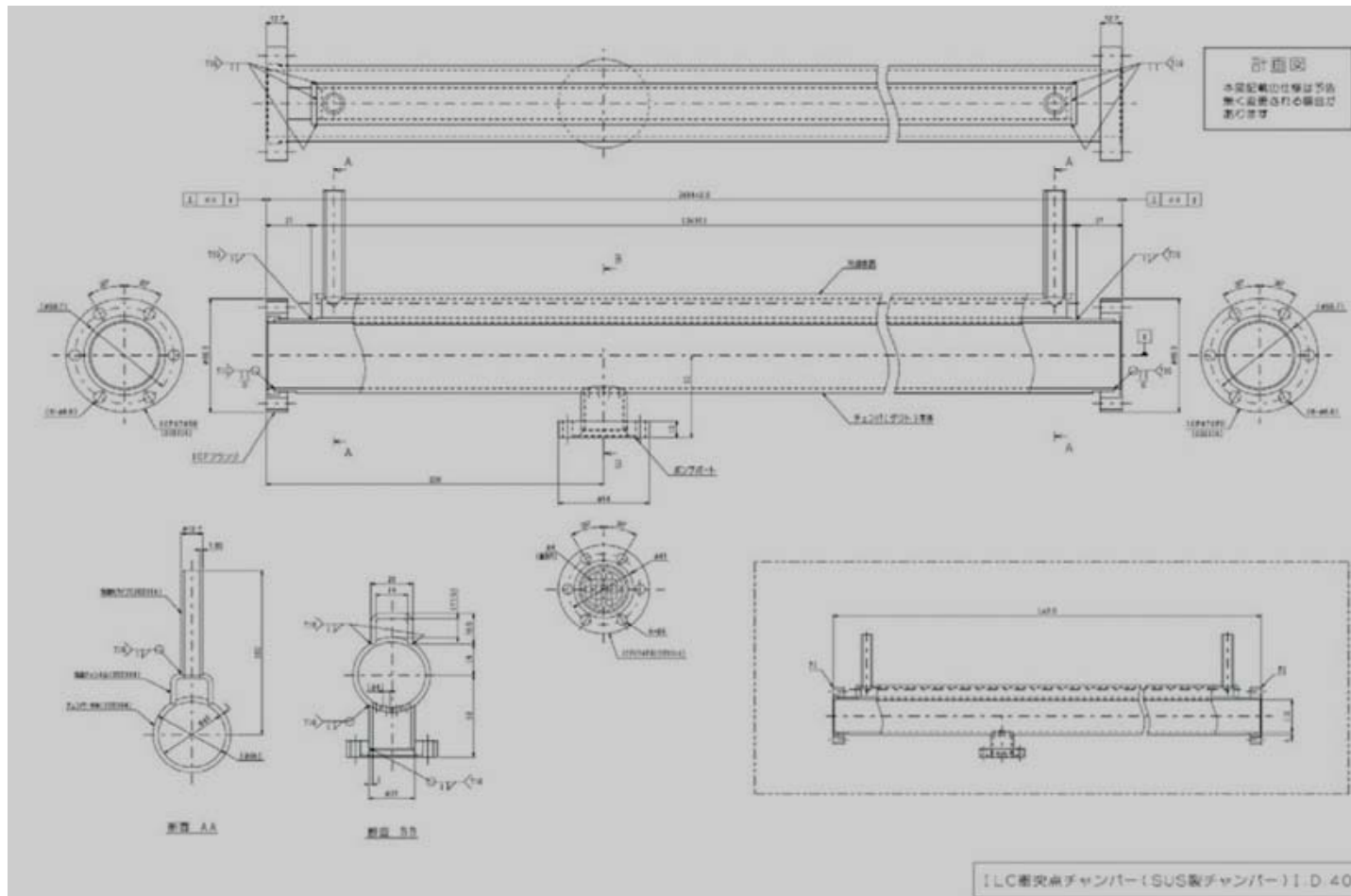
- Ex. SS_φ110mm duct





Example_2

- Ex. SS_φ40mm duct





Basic design_3

- Aperture
 - **Basically the apertures are the same to those of elements. The thickness of duct should follow the conditions as follows.**
 - [D : Diameter, t : thickness]**
 - $D < 20$ mm : $t = 1$ mm**
 - 20 mm $\leq D < 60$ mm : $t = 2$ mm**
 - 60 mm $\leq D < 100$ mm : $t = 3$ mm**
 - 100 mm $\leq D$: $t = 4$ mm**
- Gap between a duct and cores of a magnet should be larger than **1 mm**, to avoid interference.
- Beam pipes with a different aperture should be connected through a **taper** ($\sim 45^\circ$).



- Connection flange
 - Connection flange is ICF conflat type.
 - The diameter of the flange, D_f [mm], are:
 - [D_f : Flange diameter, D : duct diameter]
 - $D < 20$ mm : $D_f = 34$ mm (ICF 034)
 - $20 \leq D < 40$ mm : $D_f = 70$ mm (ICF 070)
 - $40 \leq D < 60$ mm : $D_f = 114$ mm (IFC 114)
 - Etc.....
 - Stainless-steel
 - Copper gasket
 - RF bridge between flange, if necessary.



- Surface treatment
 - Basically, the inner surface of the duct should be **cleaned by a detergent**.
 - The **acid cleaning** should etch the surface by about 1 micron to remove contaminated layer.
 - Following the **cleaning by pure water**, the duct should be dried by dry nitrogen.
 - Individual ducts will be baked, and leak checked as part of the vacuum system quality control.



- Accuracy of manufacturing
 - Total length = ± 2 mm for 10 m.
 - Tilt between the end flanges is 0.5 degree.
 - Displacement of the duct against the axis in the horizontal and vertical plane is ± 2 mm.
 - Slant of the end flanges against the axis of the duct is 1 degree.
 - Displacement of the center of end flanges against the axis of the duct is less than ± 0.5 mm.
 - Width of a gap inside should be less than 0.5 mm.
 - Inside step should be less than 0.5 mm.

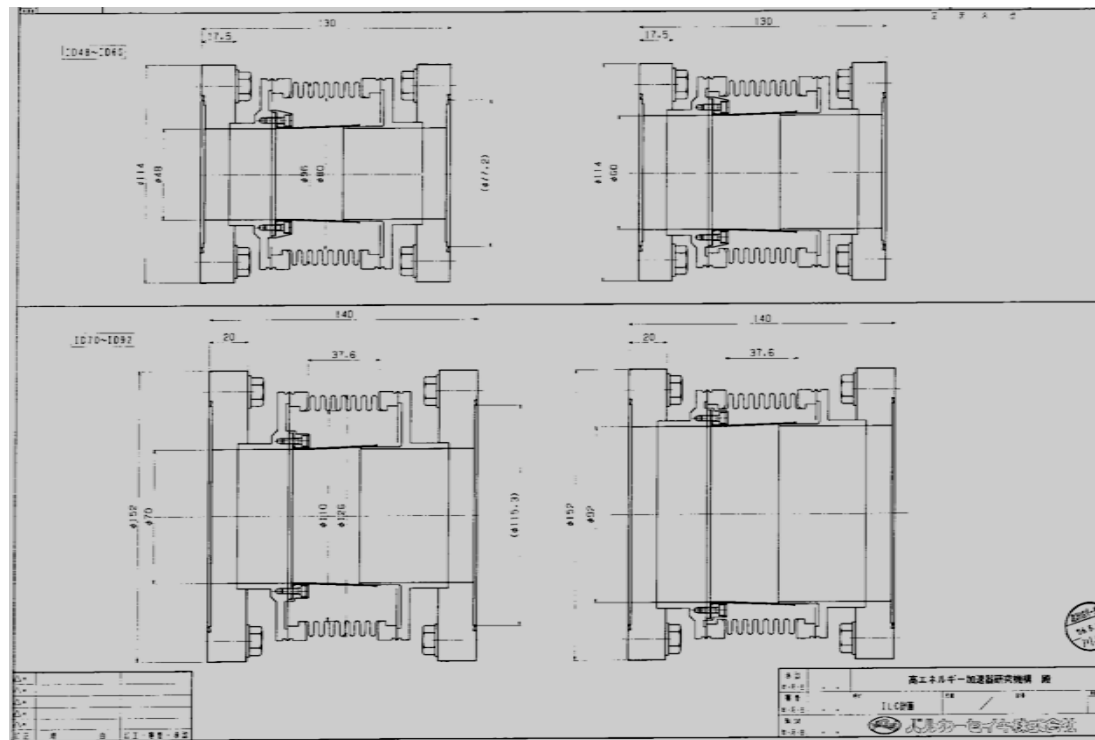


- Thermal gas desorption rate
 - Assumed to be $5 \times 10^{-8} \text{ Pa m}^3 \text{ s}^{-1} \text{ m}^{-2} \sim 5 \times 10^{-11} \text{ Torr l s}^{-1} \text{ cm}^{-2}$
 - Assumed thermal gas desorption rate was relatively large, because **no baking *in situ*** was basically assumed.
- Photo-desorption Rate
 - Assumed to be $1 \times 10^{-5} \text{ molecules photon}^{-1}$. Some extent of vacuum scrubbing is expected.
 - Photon density was assumed to be $1 \times 10^{17} \text{ photons s}^{-1} \text{ m}^{-1}$ for the copper region, and $1 \times 10^{15} \text{ photons s}^{-1} \text{ m}^{-1}$ for other regions.



Basic design_8

- Bellows chamber
 - With the same radius to adjacent beam pipes
 - With finger-type RF-shield





- Pumps

- Pumps: **Sputter ion pumps**

- Lumped pump scheme.

- Effective pumping speed, S [m^3s^{-1}], are:

[D : Diameter, S : Pumping speed]

$D < 20$ mm : $S = 0.02$ m^3s^{-1}

20 mm $\leq D < 40$ mm : $S = 0.04$ m^3s^{-1}

40 mm $\leq D < 60$ mm : $S = 0.06$ m^3s^{-1}

Etc.....

- Pumping speed includes the conductance of pumping slot. The actual pumping speed is the twice of the effective pumping speed.



- Rough pumping unit
 - **Oil-free system**
 - **A rough pumping unit consists of:**
 - A turbo-molecular pump ($S \sim 0.3 \text{ m}^3\text{s}^{-1}$)
 - A scroll pump ($S \sim 0.3 \text{ m}^3 \text{ min}^{-1}$)
 - A manifold (cross tube, for example),
 - A Pirani-gauge, a cold cathode gauge,
 - A leak valve, an electrical valve.
 - Controllers of pumps and gauges.
 - **Number of the rough pumping system is 20.**
 - **Removed during beam operation.**



- Gate valves
 - All metal valves
 - Each region (EFF1 and so on) has at least one gate valve.
 - Valves are located every 250 m at minimum
 - Apertures of gate valves are :
 - [D : Diameter, A : Aperture size]
 - $D < 60$ mm : $A = \text{ICF114}$
 - $60 \text{ mm} \leq D < 100$ mm : $A = \text{ICF152}$
 - $100 \text{ mm} \leq D < 150$ mm : $A = \text{ICF203}$
 - Etc.....



Basic design_12

- Gauge
 - Vacuum gauge: **BA (hot cathode), QMA**
 - The interval of gauge is **200 m.**
- L-Angle Valve
 - All-metal L-angle valve is located every **50 m.**
 - Rough pumping system is connected to the valve when the duct is evacuated from atmosphere.



Cost estimation_1

- General remarks
 - Basically, obtained from major vacuum manufactures.
 - Discussed among TS leaders to find reasonable numbers in all regions.
 - Based on TS leaders' experience so far.
 - For example, in Asia, KEK B-factory (~1996).
 - The present cost estimation, however, is not yet well optimized.
 - Diameter, lengths, etc.



Cost estimation_2

- Included terms
 - Beam ducts
 - Bellows chambers (with finger-type RF-shielding)
 - Pumps (and controllers, Rough pumping unit)
 - Vacuum gauges (and controllers)
 - Gate valves (and controllers, with RF-shielding)
 - Manifolds (6 ports for rough pumping unit and gauges)
 - Gaskets, bolts, Supports (in average number)
 - Control cables between components and controllers
 - Interlock box per one gate valve
 - Baking heaters and thermal insulators: Option
 - Preparation before installation, such as assembling, pre-baking of beam pipe, testing, etc.



Ex. of cost_1

- Beam duct (Base)
 - **Stain-less steel**
 - **Including:**
 - Detergent cleaning
 - Profit of company, Risk factor
 - Flanges, pumping ports
 - No cooling channel

1\$ = 120Yen
1\$ = 1.2 €

ϕ (Diameter)	US\$ /m
20 mm	200
100 mm	300
150 mm	350
200 mm	400



Ex. of cost_2

- Other Beam duct

1\$ = 120Yen
1\$ = 1.2 €

- **Including:**

- Design work by company,
- Profit of company, Risk factor
- Flange, pumping ports

Type	Factors from “Base”
Acid cleaning	X 1.2
Aluminum alloy	X 0.6
SS+Cu coating	X 2
Cu	X 2
With Cooling pipe	X 1.5



Cost estimation_3

- Not included terms
 - All R&D
 - Spares
 - Man power for Installation, such as transportation, setting, connection, alignment, leak-checking, (baking)
 - 4 km per year by 7 persons (1 specialist)
 - Power supply for baking: Option
 - Others (facilities)
 - Electric power, Cooling water system, Storage area of vacuum components before installation, and so on



Cost estimation_4

- Ambiguity in the present cost estimation
 - **Overall specifications and requirements are clear. But, the detailed specification are not yet given.**
 - Required pressure
 - Accuracy of manufacturing
 - Surface treatment
 - Gap between magnets, etc. ..
 - **Design is not yet fixed. The manufacturer counted a risk factor.**
 - Beam pipe radius, lengths
 - the structure of RF shielding at pumping port , etc. ..



Issues to be discussed_1

- Required pressure should be updated, at first.
- Detailed design responding to each component and region
 - **Aperture, lengths, etc. ..**
- Simplification of structure
 - **bellows chambers and gate valves**
- R&D
 - **Way to reduce gas desorption rate without baking**
 - Passivation, for example
 - **Quick connection flange**
- Optimization



Issues to be discussed_2

- Optimization_ Ex. Choice of duct material
 - **SS (stainless-steel), Al, or Cu.**
 - **In general, SS is cheaper and (may be) has higher reliability (for baking).**
 - **For ducts with a small radius the extrusion of Al pipe has an advantage in manufacturing.**
 - **SS pipe with Cu coating inside is also difficult to control the quality of the coating (and expensive).**
 - **Gas desorption rate of Al is comparative, if the surface is treated appropriately.**



Issues to be discussed_3

- Optimization_ Ex. Baking (in situ.) or not
 - Baking in situ. can much reduce the gas desorption rate, and can reduce the number of pumps.
 - Baking (up to 200 degrees), furthermore, make it possible to consider the NEG (Non Evaporable Getter) coating, which could improve the vacuum, especially for pipes with small radius.
 - Uniform baking along the beam pipe is difficult due to the firm fixing of the cavity BPM at present. The tuning of BPM will be required after baking.



Summary

- The design principle and the basic design of the vacuum system for BDS in RDR phase were summarized.
- The design is sufficient for the rough cost estimation, but primitive for the actual system.
- Detailed design and elaborative discussion should be required for ED phase.
 - **Design responding each component and region**
 - **Simplification of structures**
 - **Optimization of system**