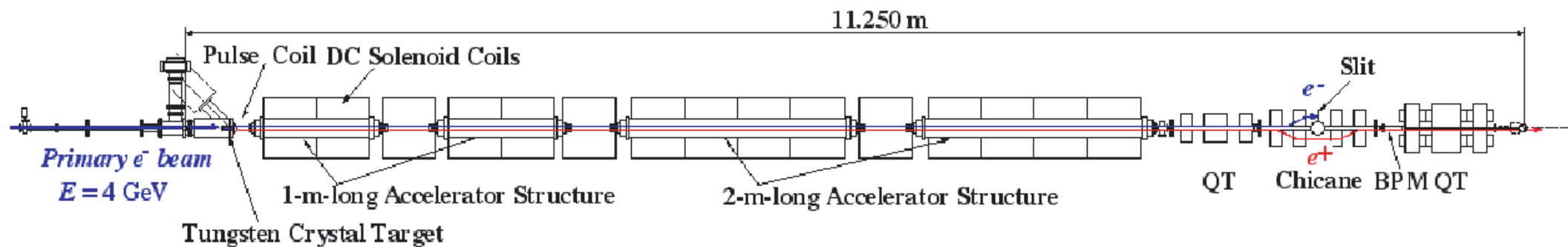


***NEW POSITRON SOURCE AT THE
KEKB INJECTOR LINAC BASED
ON ORIENTED TUNGSTEN
CRYSTAL CONVERTER***



KEKB Positron Source Layout

- Primary electron beam
- Electron beam
- Positron beam



Primary Electron Beam Parameters

- Energy – 4GeV
- Horizontal Angular Spread (RMS) – 0.2 mrad
- Vertical Angular Spread (RMS) – 0.1 mrad
- Horizontal Emittance – 660 mm mrad
- Vertical Emittance – 360 mm mrad
- Transverse Beam Size – 0.7 mm
- Bunch Duration – 10 ps
- Maximal beam rate – 50 Hz
- Bunch charge – 7.8 nC

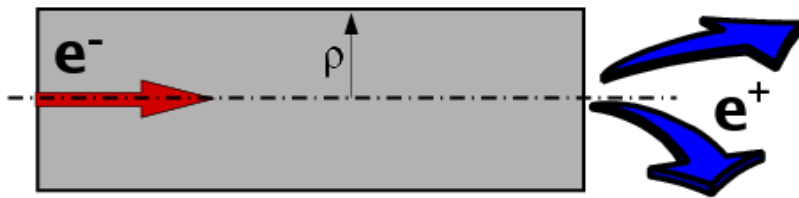
Positron production efficiencies for the first(second) bunch:

- Crystalline 10.5- mm-thick tungsten target – $0.23 \pm 0.02 (0.24 \pm 0.02)$
 - Amorphous 14-mm-thick tungsten target – $0.20 \pm 0.01 (0.20 \pm 0.01)$
-
-

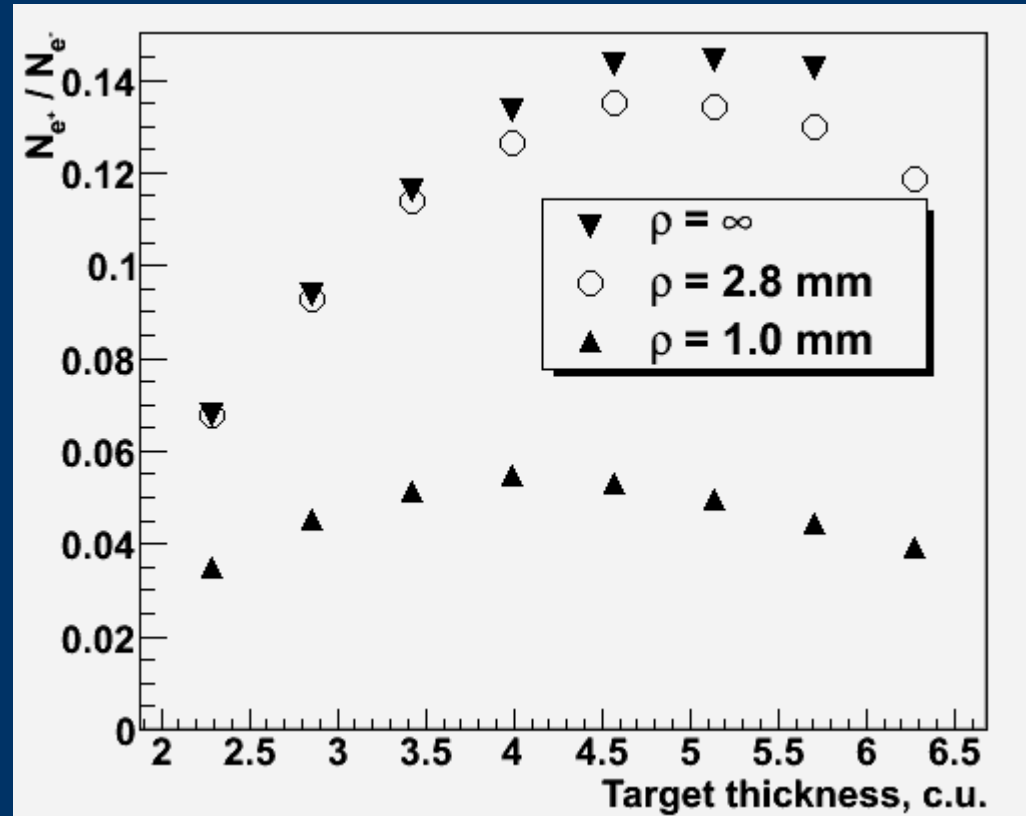
Acceptance condition:

$$8.6 \frac{\text{MeV}}{c} < p < 11.6 \frac{\text{MeV}}{c}, p_t < 2.4 \frac{\text{MeV}}{c}$$

Cylindrical tungsten target



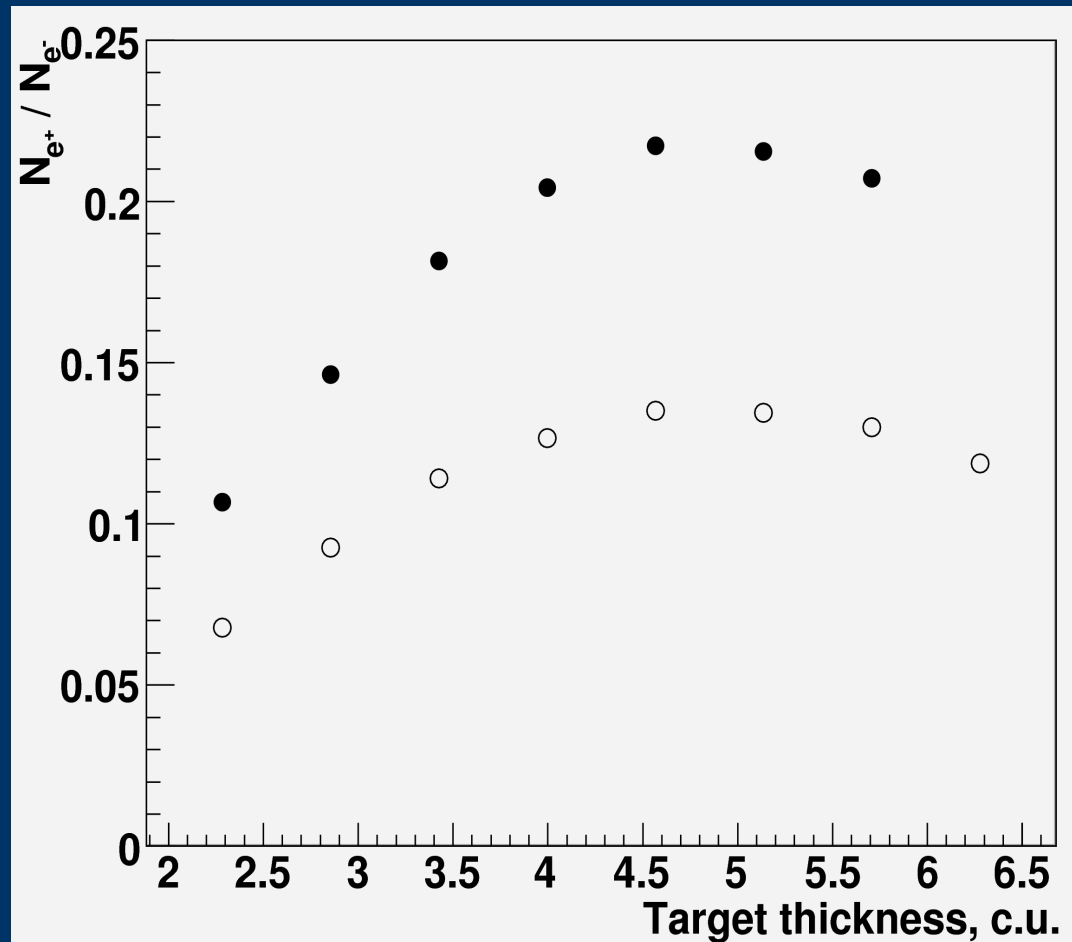
- Number captured positrons is depended on acceptance radius.
- For the given acceptance condition measured positron production efficiency essentially exceeds results of simulation...



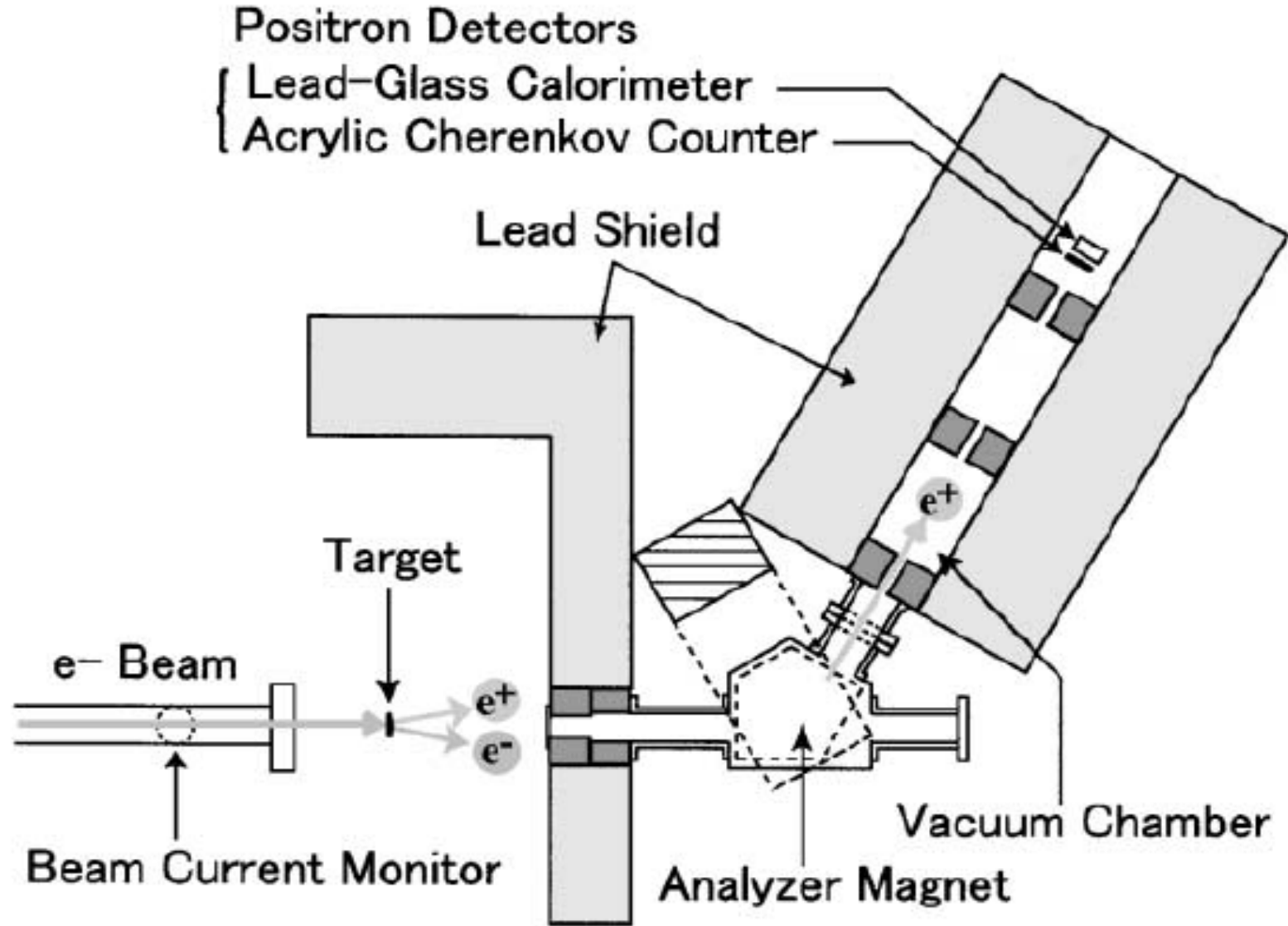
Acceptance condition:

Old : $8.6 \frac{\text{MeV}}{c} < p < 11.6 \frac{\text{MeV}}{c}, p_t < 2.4 \frac{\text{MeV}}{c}$
New: $7.8 \frac{\text{MeV}}{c} < p < 12.0 \frac{\text{MeV}}{c}, p_t < 2.8 \frac{\text{MeV}}{c}, \rho = 2.8 \text{ mm}$

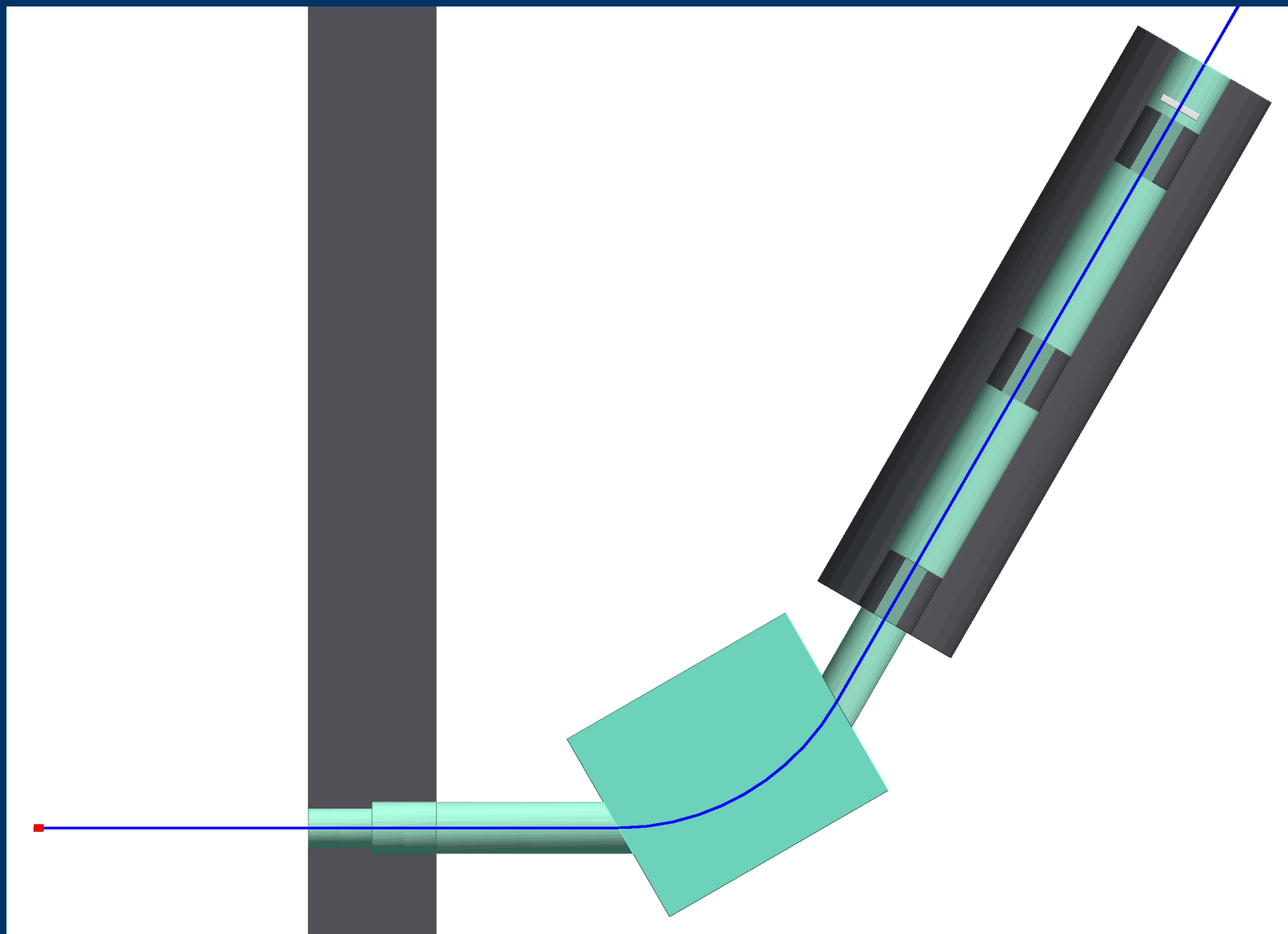
Accept. condition	Spatial spread σ , mm	Ang. spread σ' , mrad	Norm. emittance ϵ_n , mm·mrad
Old	0.866 ± 0.003	0.123 ± 0.003	1240
New	0.873 ± 0.004	0.145 ± 0.001	1520



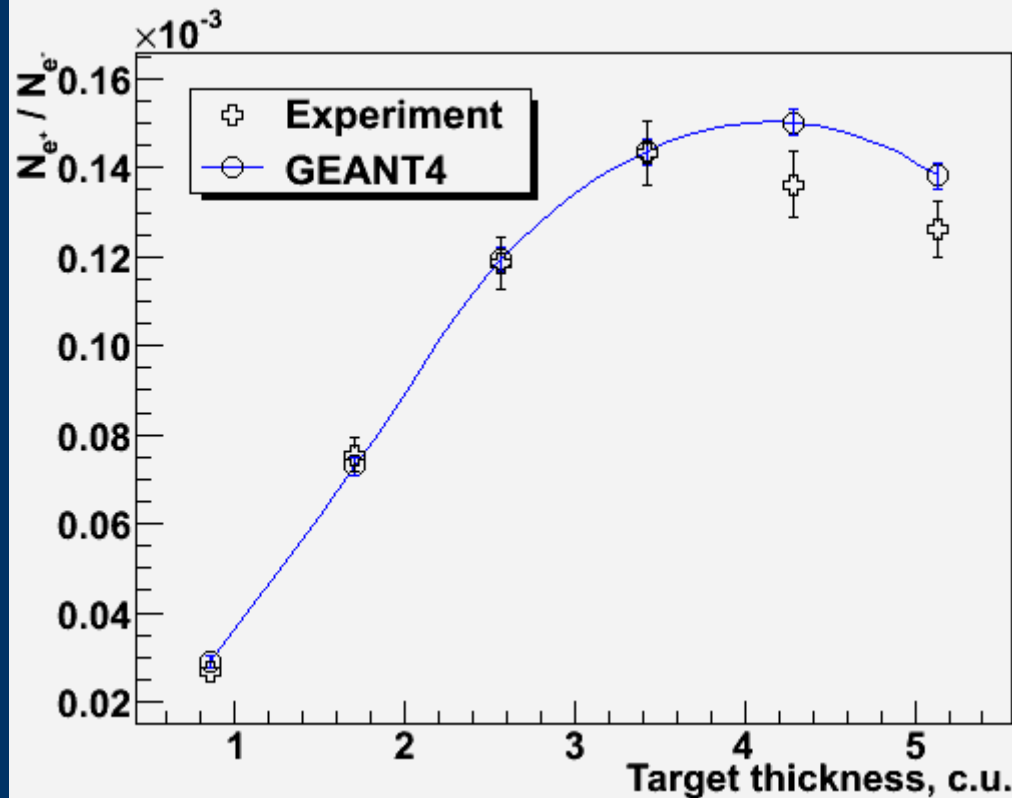
KEK experimental setup:



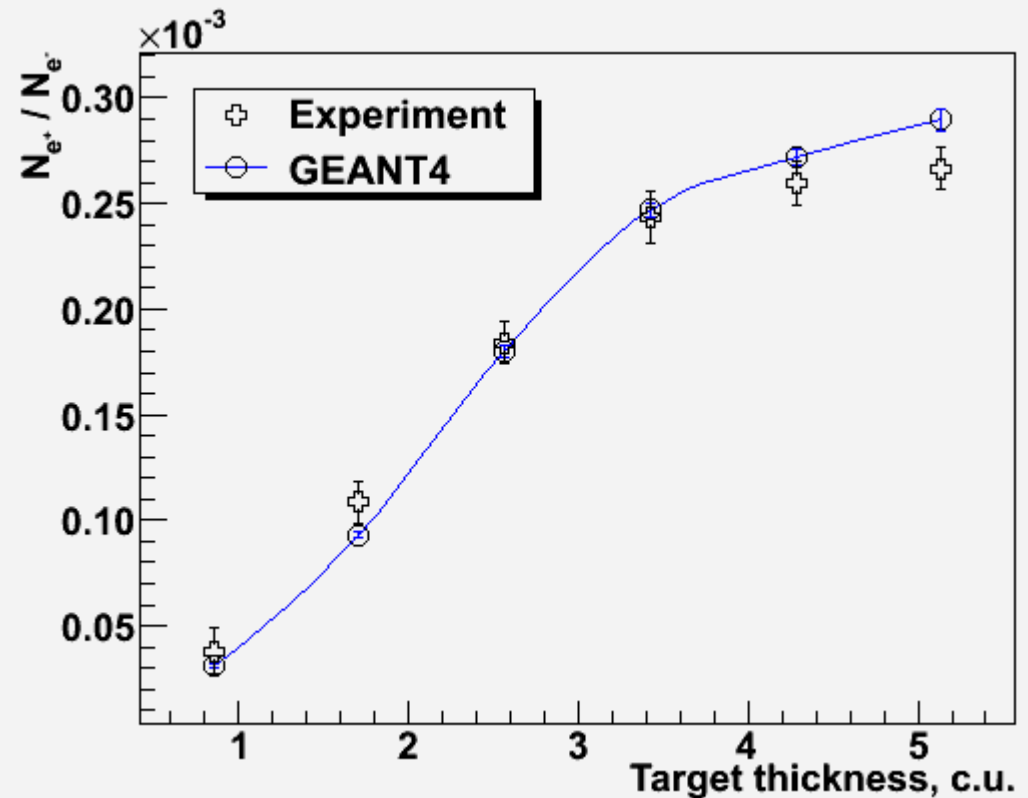
Geometry of the GEANT4 model



Positron yield from W_a targets

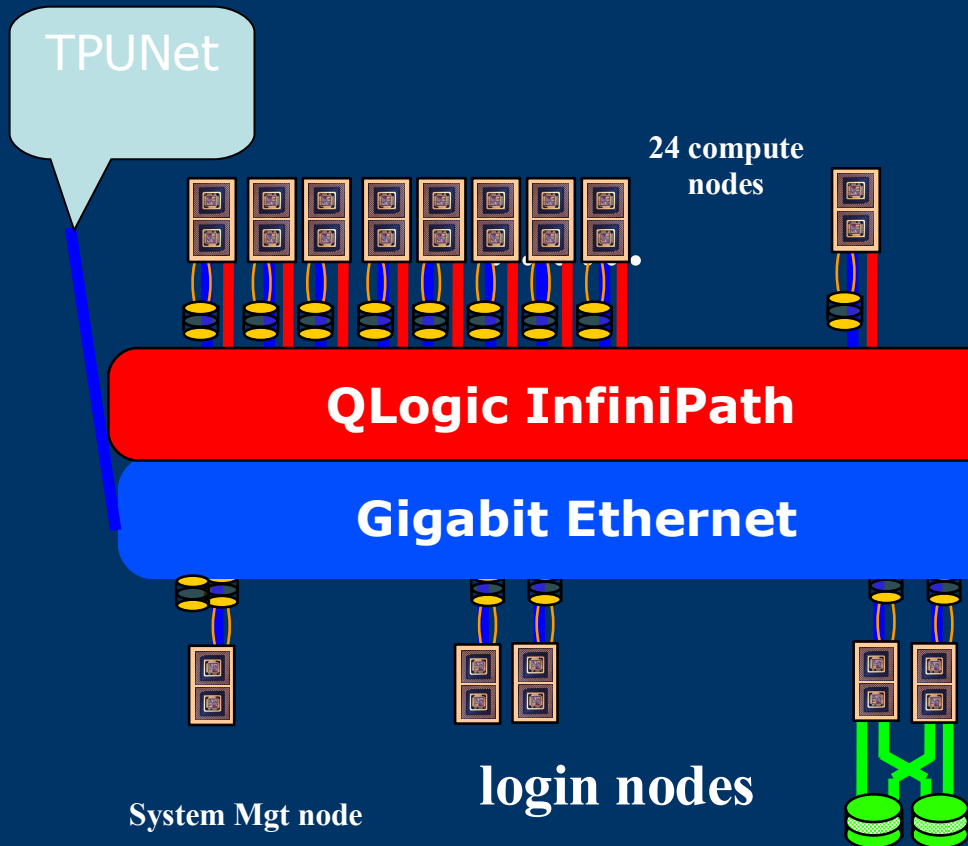


4 GeV beam



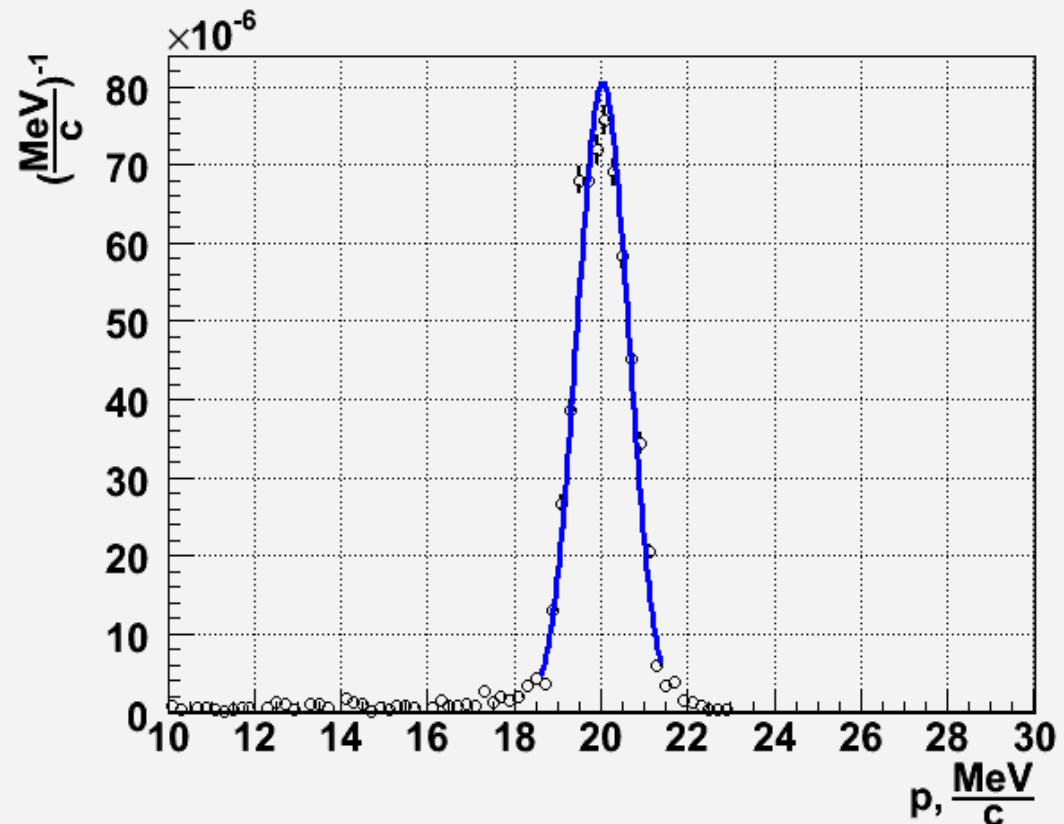
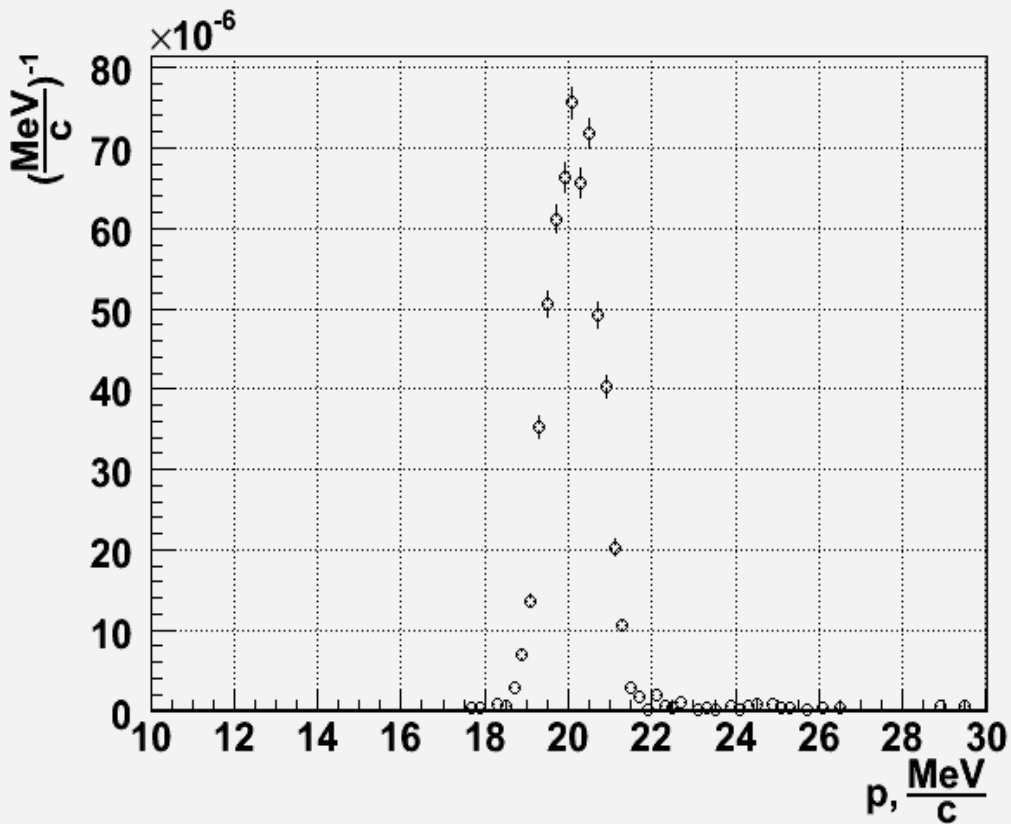
8 GeV beam

HPC Cluster SKIF-Polytech



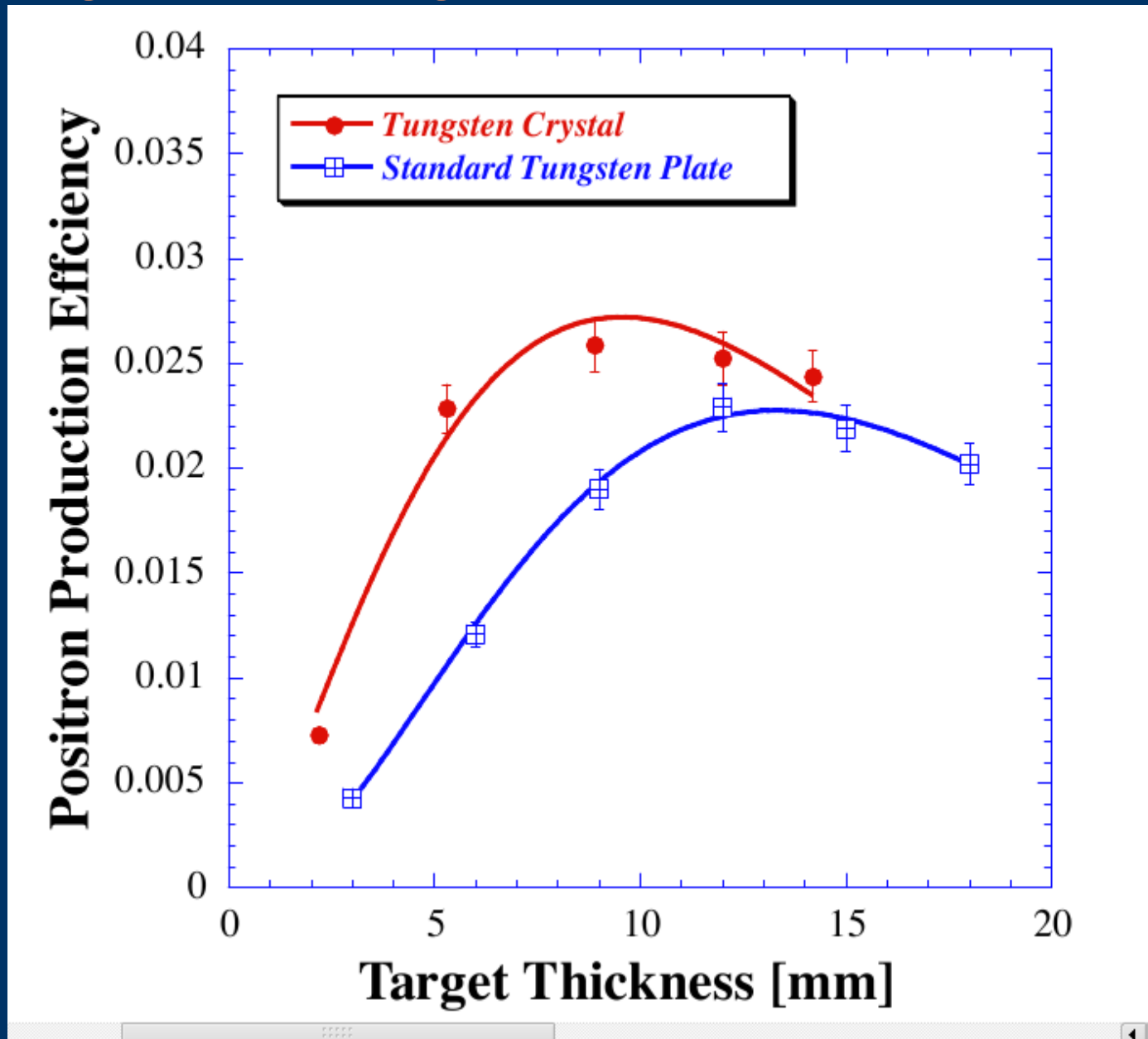
- 24 dual processor nodes
- Processors type : dual core Intel Xeon 5150, 2.667GHz
- MPI throughput: 800 Mb/c
- MPI latency : 2.5 usec.
- Peak performance: 1TFlop
- Network data storage system: 5TB.

e⁺ spectra beyond target and in counter , 4GeV beam, 9mm Wa

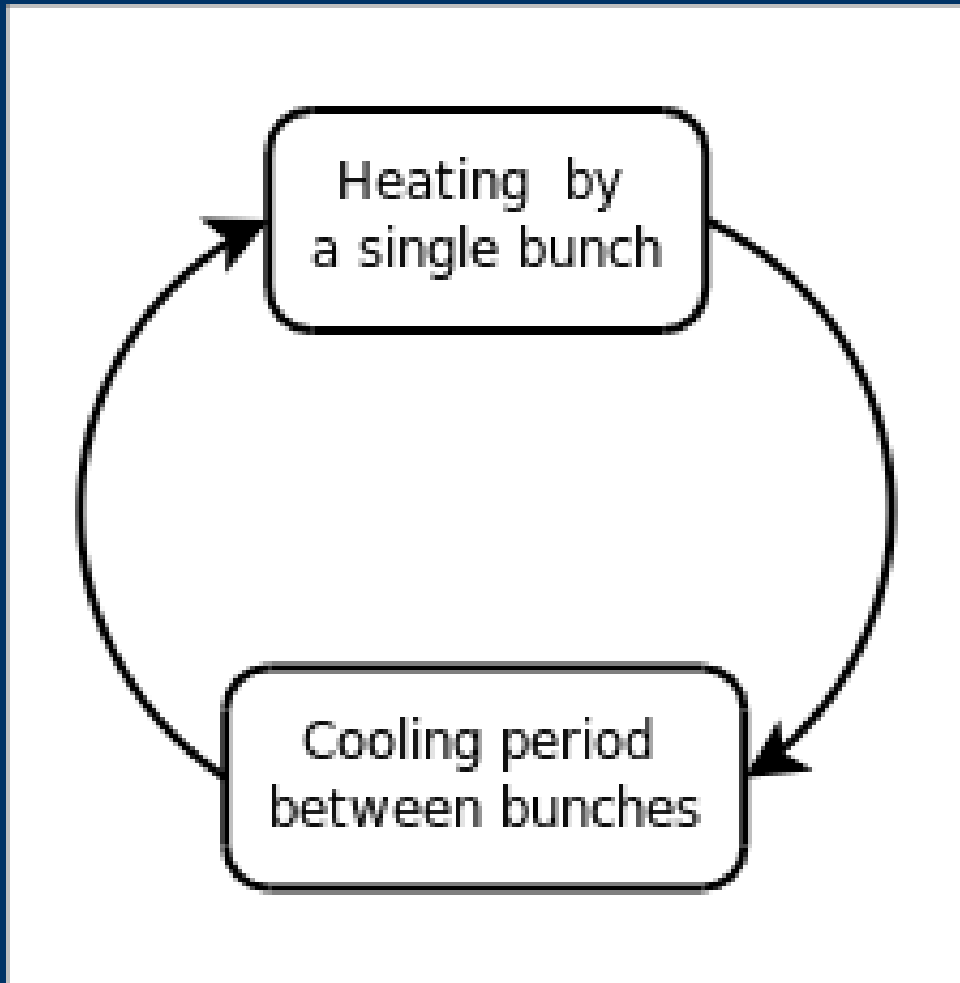


Calorimeter window : 18.6 – 21.4 MeV/c
Peak rms : 0.6 MeV/c

Positron-production efficiencies measured for the tungsten crystal as a function of the crystal thickness (The solid curve through the data are gamma-function fits of the data.)



Life cycle of target:



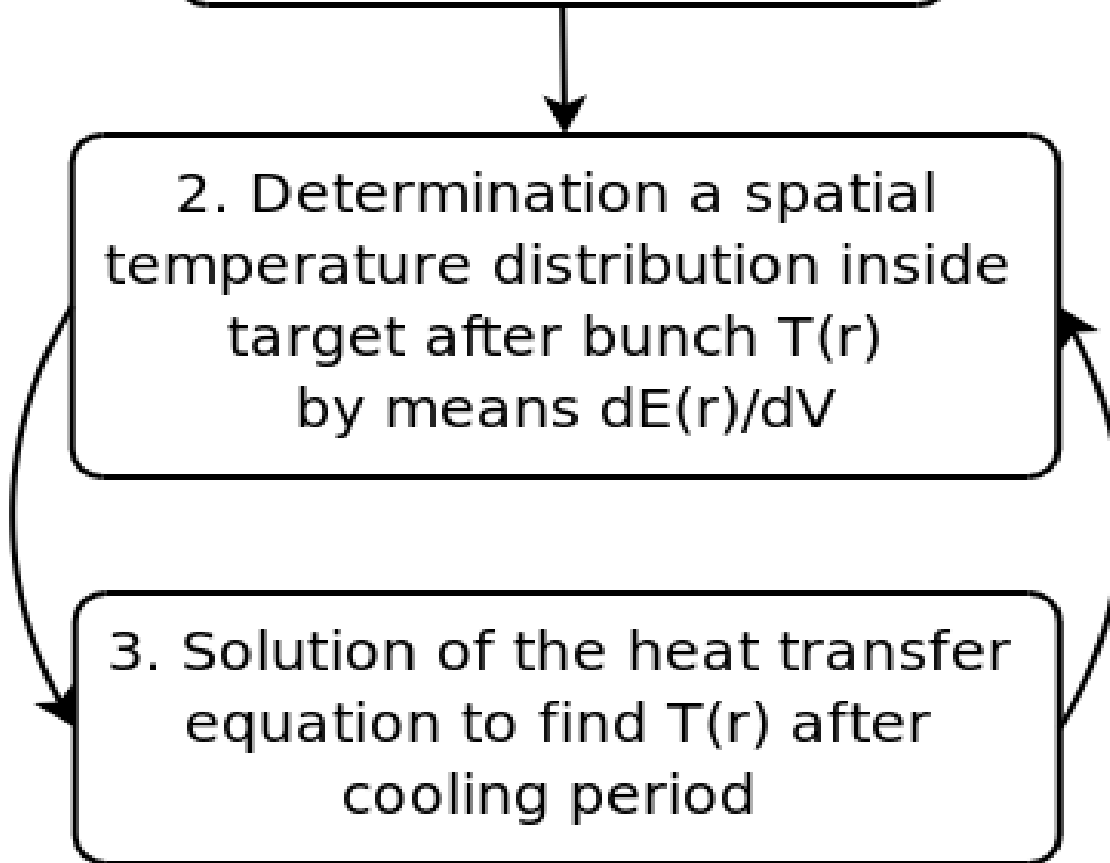
- In the model an energy deposition induced by single bunch considered as instant.
- Cooling period between bunches assumed to be $1/f$, where f – beam repetition rate.

Stages of simulation:

1. Calculation $dE(r)/dV$ - energy deposition induced by single bunch

2. Determination a spatial temperature distribution inside target after bunch $T(r)$ by means $dE(r)/dV$

3. Solution of the heat transfer equation to find $T(r)$ after cooling period



Calculation of energy deposition induced by beam bunch

- Math. model : Set of Boltzmann equations:

$$\begin{aligned} & \vec{\Omega} \nabla \Phi_i(\vec{r}, \vec{\Omega}, E) + \Sigma_i(\vec{r}, E) \Phi_i(\vec{r}, \vec{\Omega}, E) + \\ & \sum_j \int d\Omega' \int dE' \Sigma_{j,i}(\vec{r}, \vec{\Omega}' \rightarrow \vec{\Omega}, E' \rightarrow E) \Phi_j(\vec{r}, \vec{\Omega}', E') = \\ & S(\vec{r}, \vec{\Omega}, E), \\ & J = \int d\vec{r} \int dE \int d\vec{\Omega} \Phi(\vec{r}, \vec{\Omega}, E) D(\vec{r}, \vec{\Omega}, E) \end{aligned}$$

- Particles in effect : photons (photo, Compton, pair production), electrons, positrons (bremsstrahlung, ionization)
 - Solution method: statistical testing – Monte Carlo
 - Tools : GEANT4, CASCADE
-
-

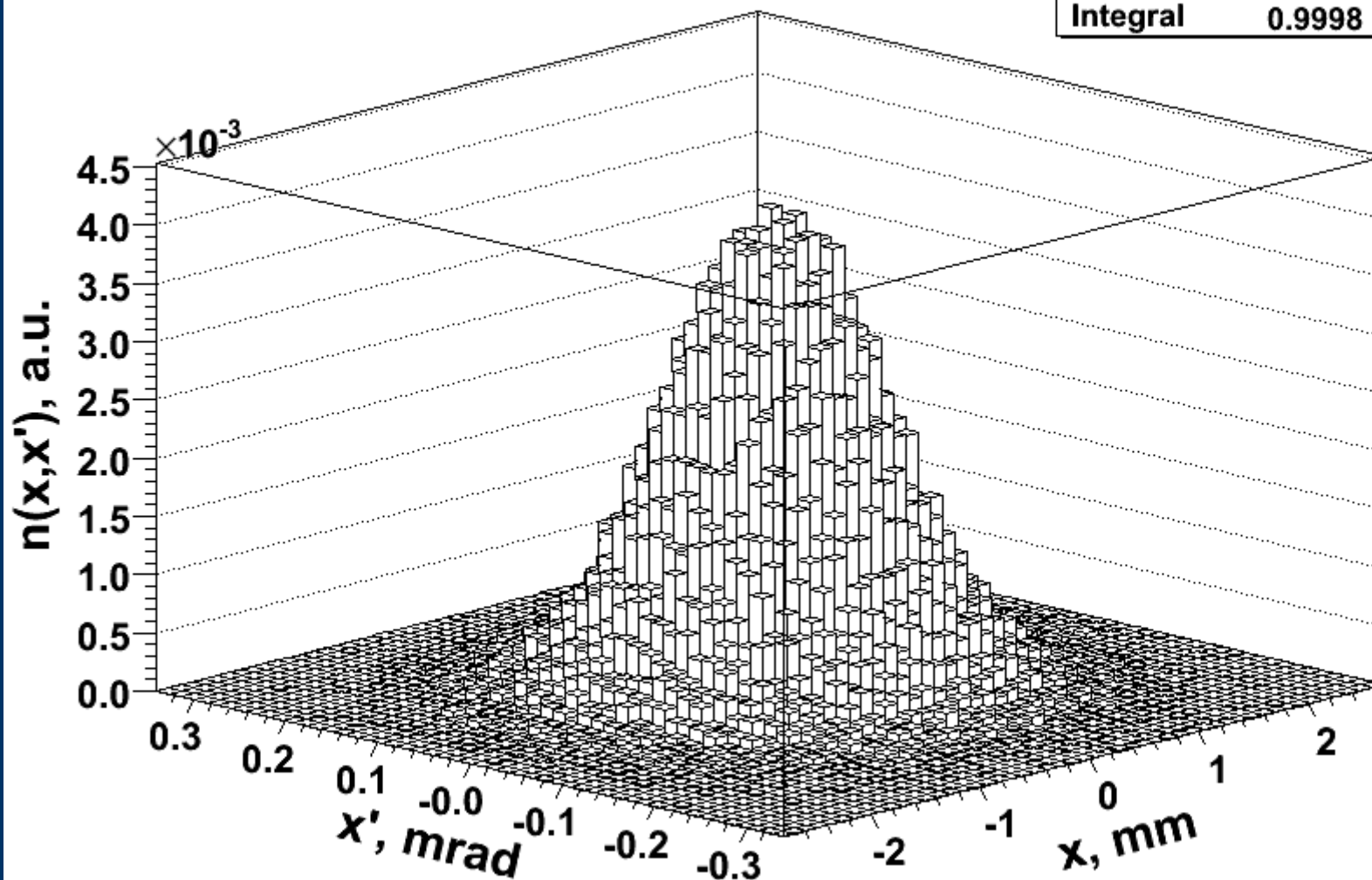
Beam model parameters:

- Beam energy – 4 GeV .
- Bunch charge – 7.8 nC .
- Gaussian model is used for spatial – angular distribution of electrons .

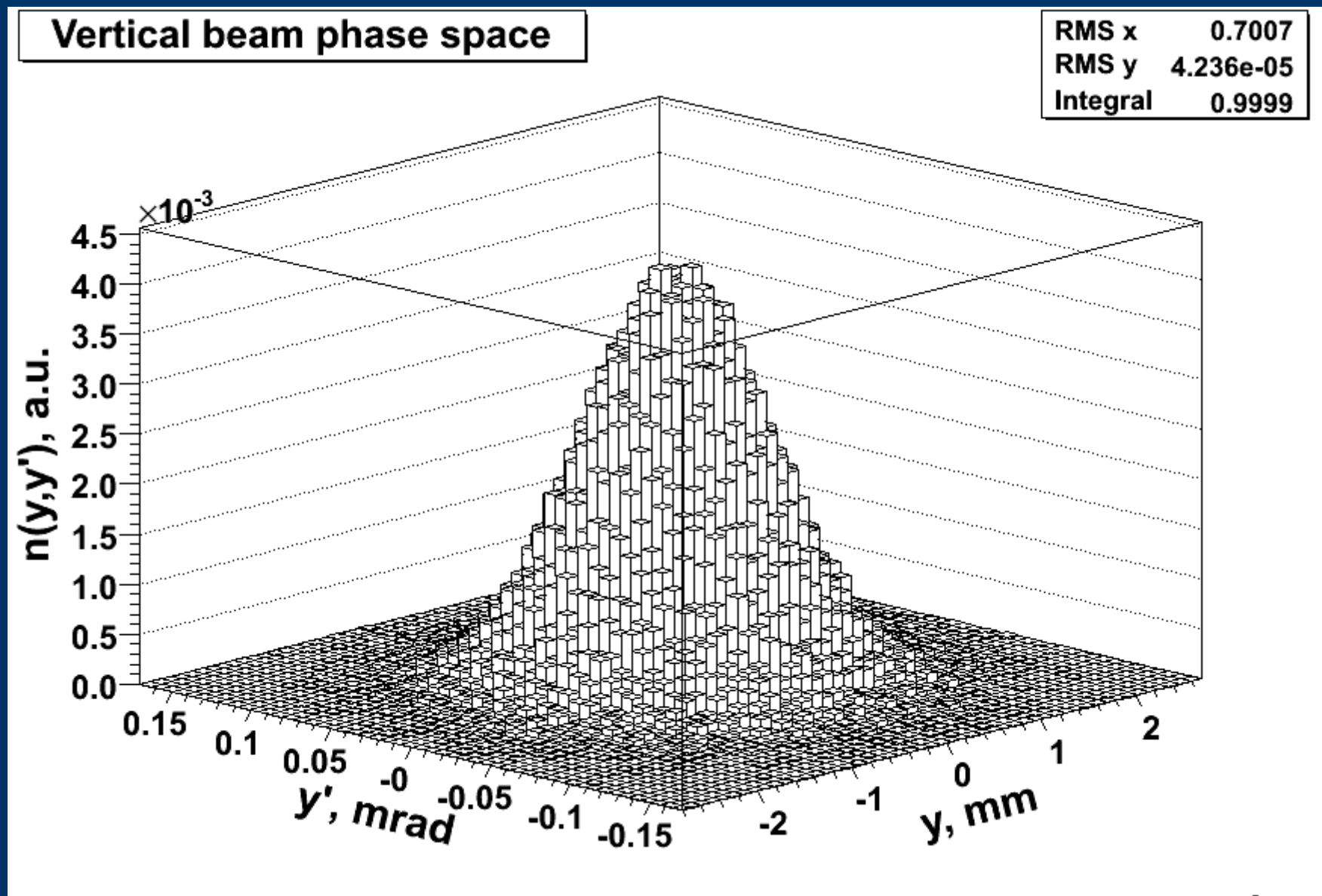
Beam model:

Horizontal beam phase space

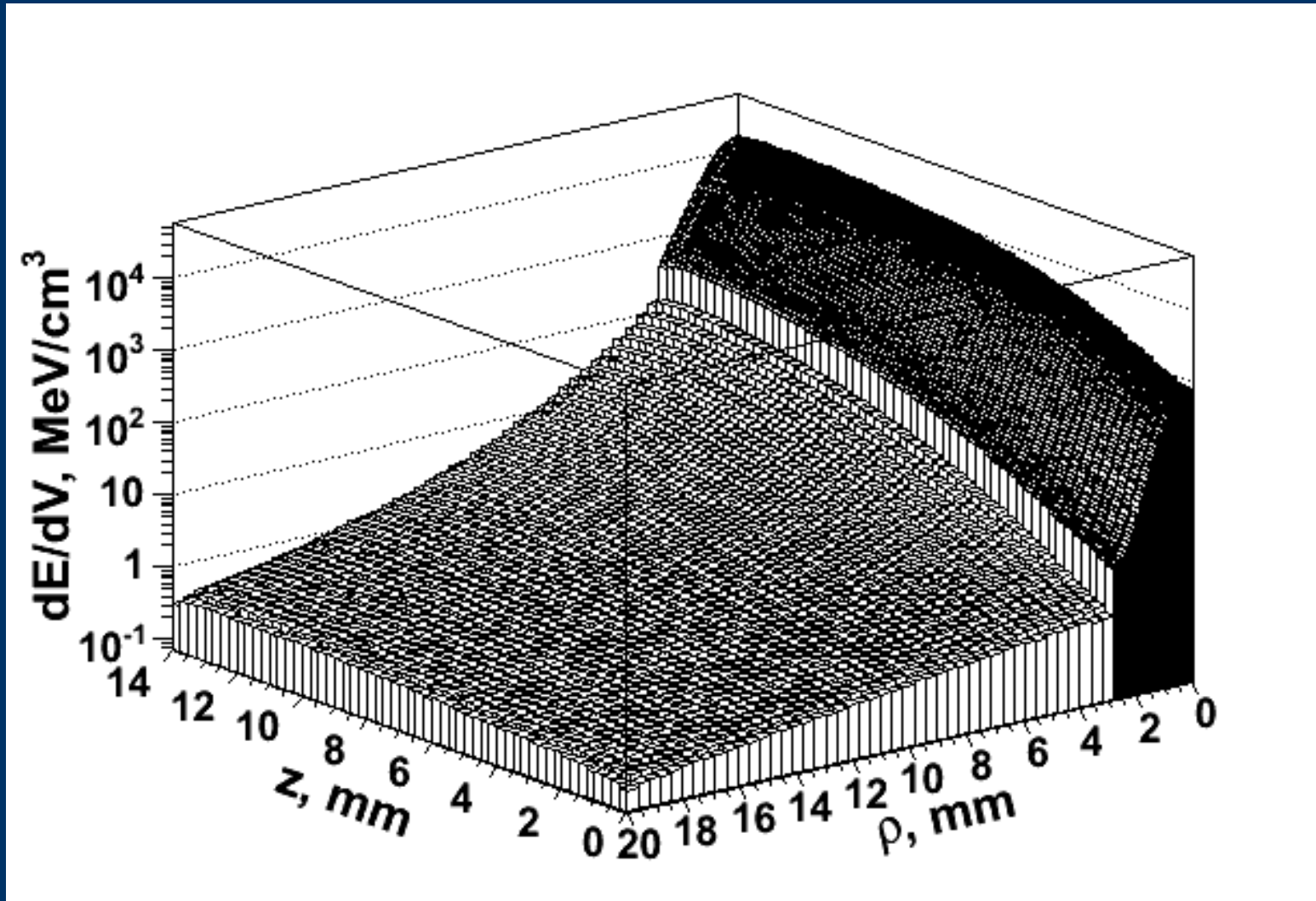
RMS x	0.6981
RMS y	8.522e-05
Integral	0.9998



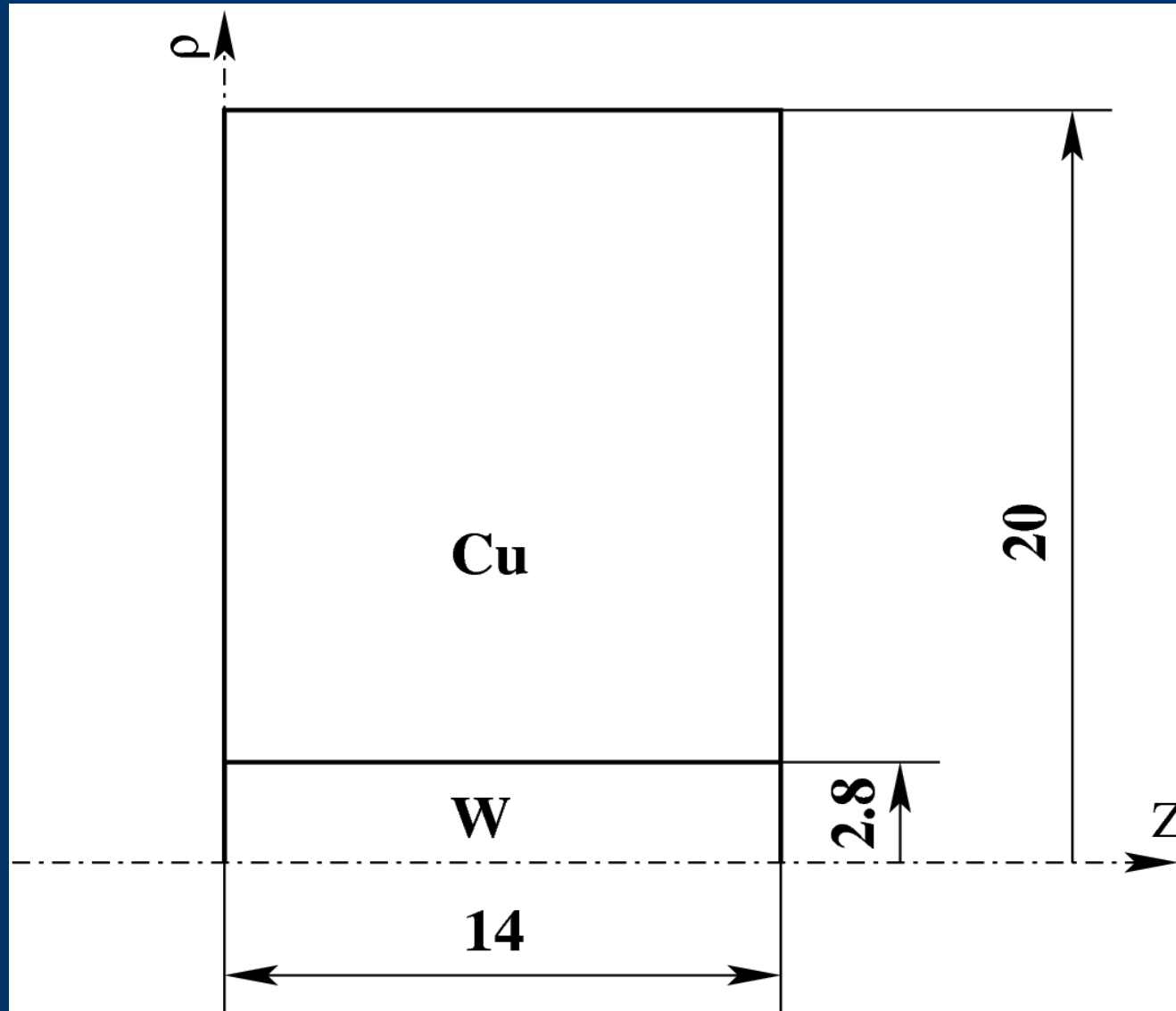
Beam model:



Energy deposition induced by single bunch (GEANT4) :



Geometry model for the heat transfer problem:



Determination a spatial temperature distribution after bunch:

- Math. Model:

$$\frac{d E(\vec{r})}{dV} = \rho \int_{T_0(\vec{r})}^{T(\vec{r})} du c(u)$$

where ρ - density, $c(u)$ - specific heat ,

$T_0(\vec{r}), T(\vec{r})$ - temperatures at \vec{r} before and after bunch, respectively.

- Method: Iterative procedure
-
-

Heat transfer between bunches

- Math. model:
$$c(T) \rho \frac{\partial T}{\partial t} = \text{div}(k \text{ grad } T)$$

- Boundary conditions : convective heat flux on upstream plane and side cylindrical surface of copper body:

$$k \frac{\partial T}{\partial n} + h(T - T_c) = 0, \quad T_c = 25^\circ \text{C}, \quad h = 0.93 \times 10^{-2} \text{ W/mm}^2 \text{ K}$$

- Initial condition: defined from solution of

$$\frac{dE(\vec{r})}{dV} = \rho \int_{T_0(\vec{r})}^{T(\vec{r})} du c(u)$$

with respect to the upper limit $T(\vec{r})$, $T_0(\vec{r}, t=0) = 25^\circ \text{C}$

- Solution method : Finite Volume Method (FVM)

Test example: Heat transfer in infinite tungsten cylinder.

- Initial condition: $T(\rho, t=0) = 100 \exp\left(-\frac{\rho^2}{2\sigma^2}\right)$, $\sigma = 0.7 \text{ mm}$

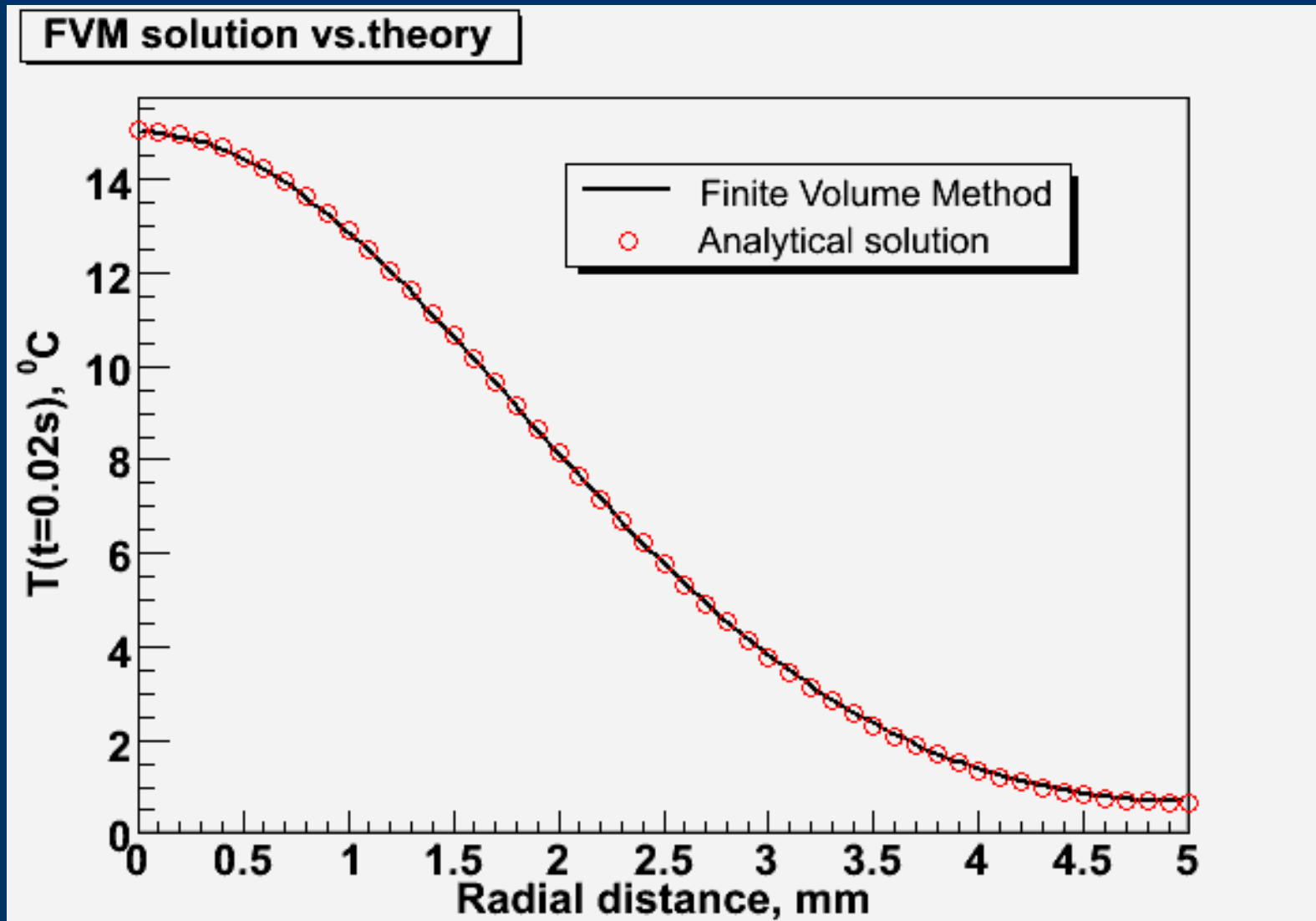
- Boundary condition: convective flux,

$$T_c = 0^\circ \text{C}, \quad h = 0.015 \text{ W/mm}^2 \text{K}$$

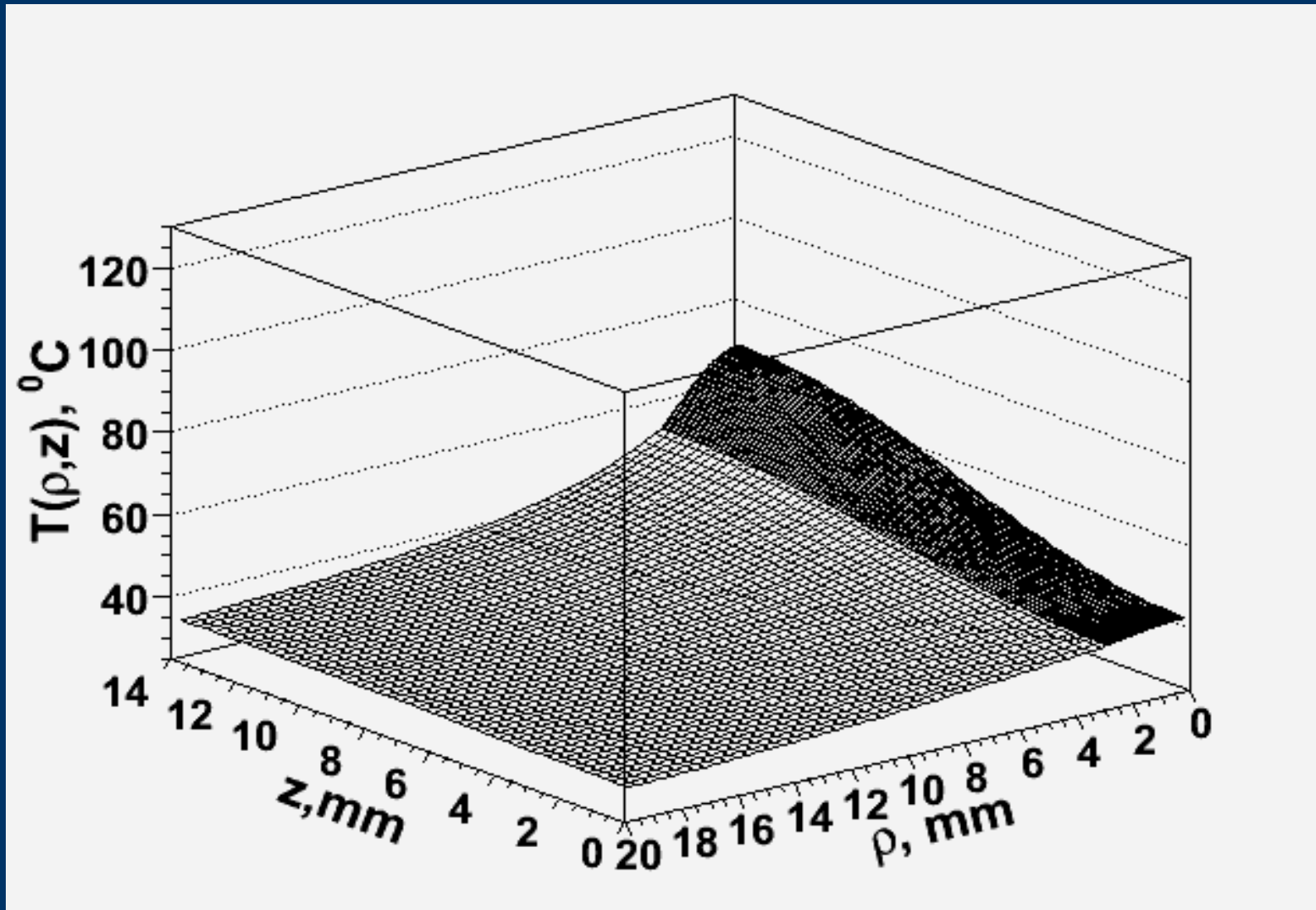
- Analytical solution:

$$T(\rho, t) = \frac{2}{\rho_0} \sum_{i=0}^{\infty} \exp(-\lambda_n^2 \alpha t) \frac{J_0(\lambda_n \rho)}{J_0^2(\lambda_n \rho_0) + J_1^2(\lambda_n \rho_0)}$$
$$\int_0^{\rho_0} \rho T(\rho, t=0) J_0(\lambda_n \rho) d\rho, \quad \lambda_n: \lambda \rho_0 \frac{J_1(\lambda \rho_0)}{J_0(\lambda \rho_0)} = \frac{h \rho_0}{k}$$

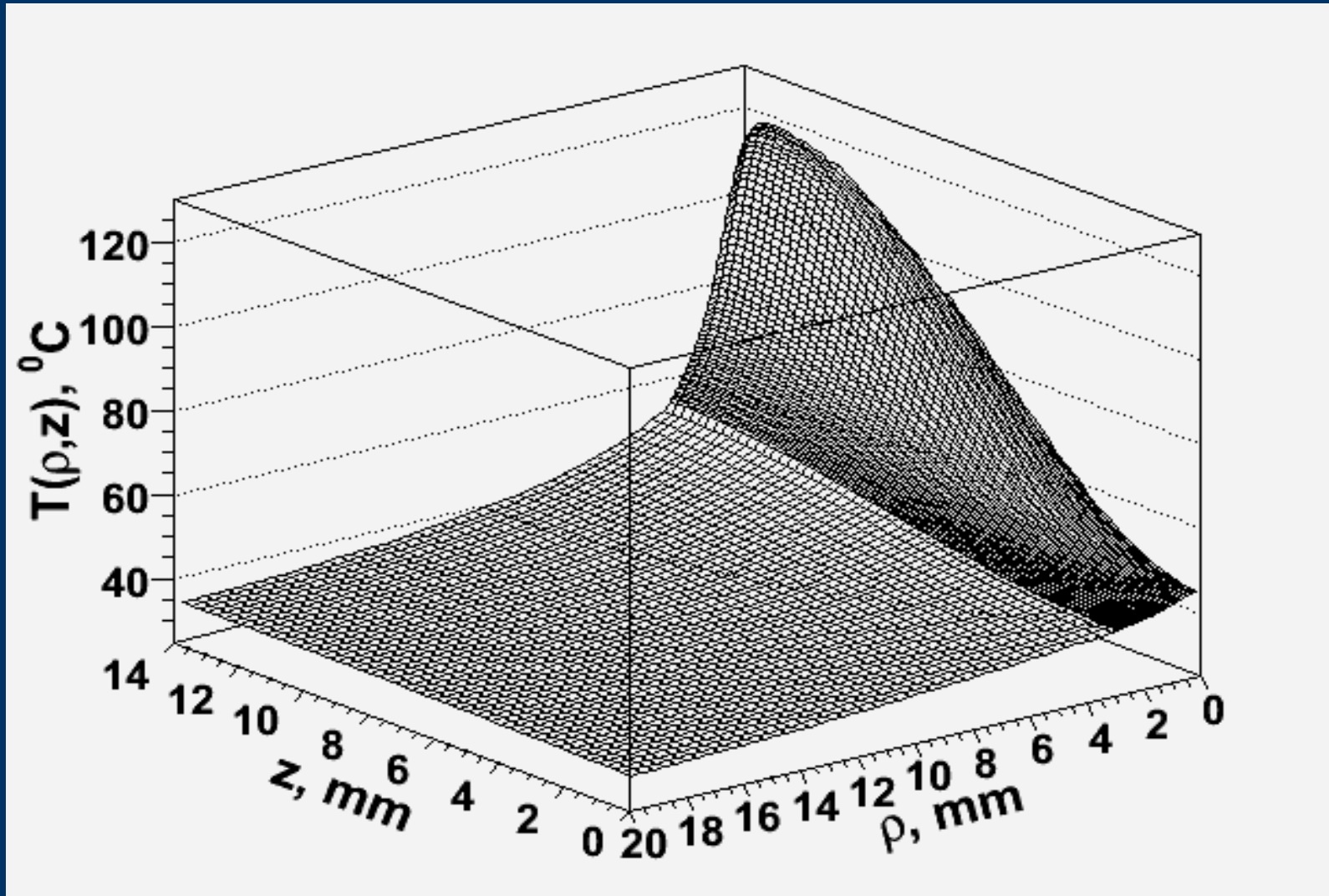
Test example: Heat transfer in infinite tungsten cylinder.



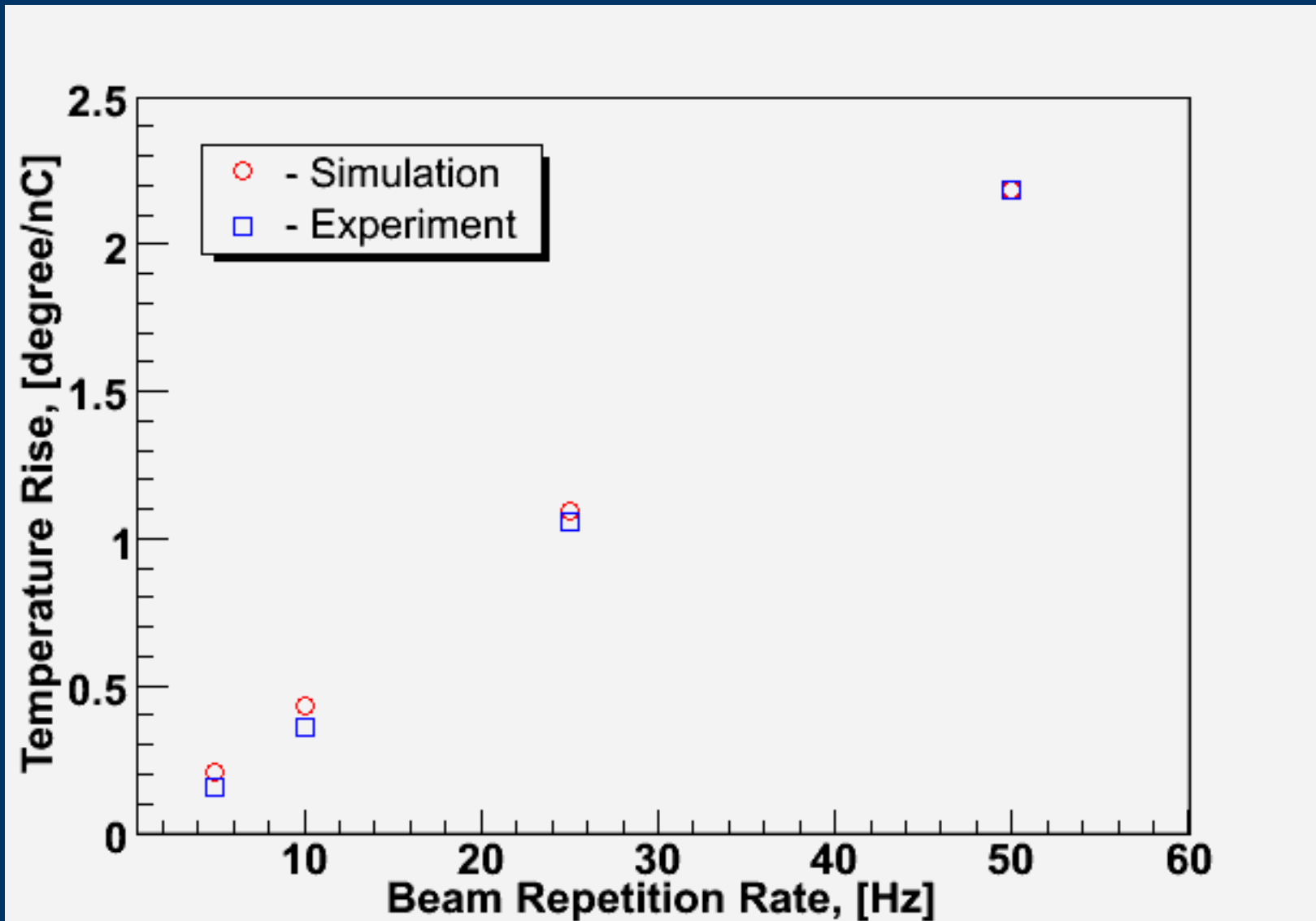
Steady state temperature distribution just before bunch for 14 mm amorphous target:



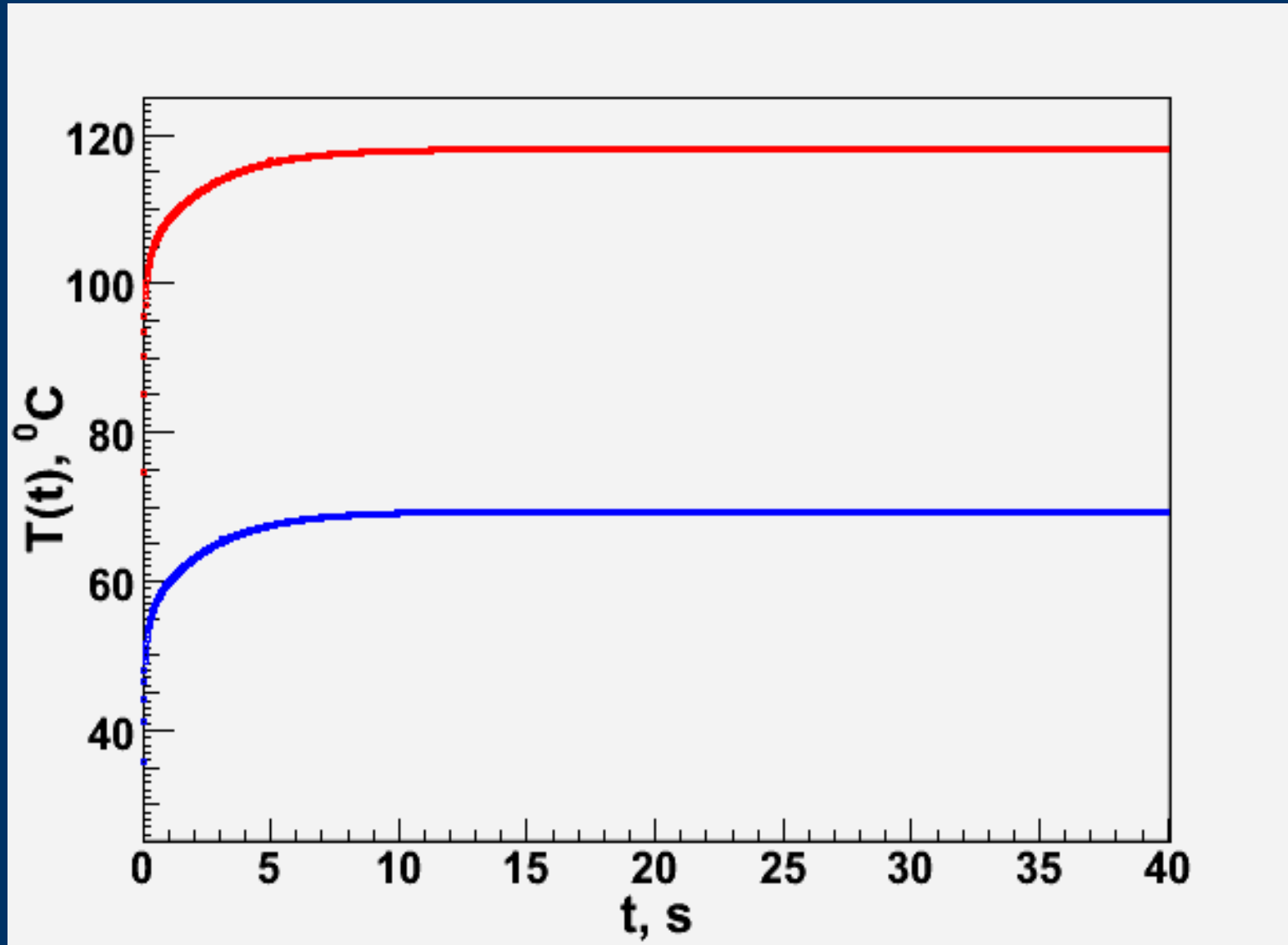
Steady state temperature distribution immediately after bunch:

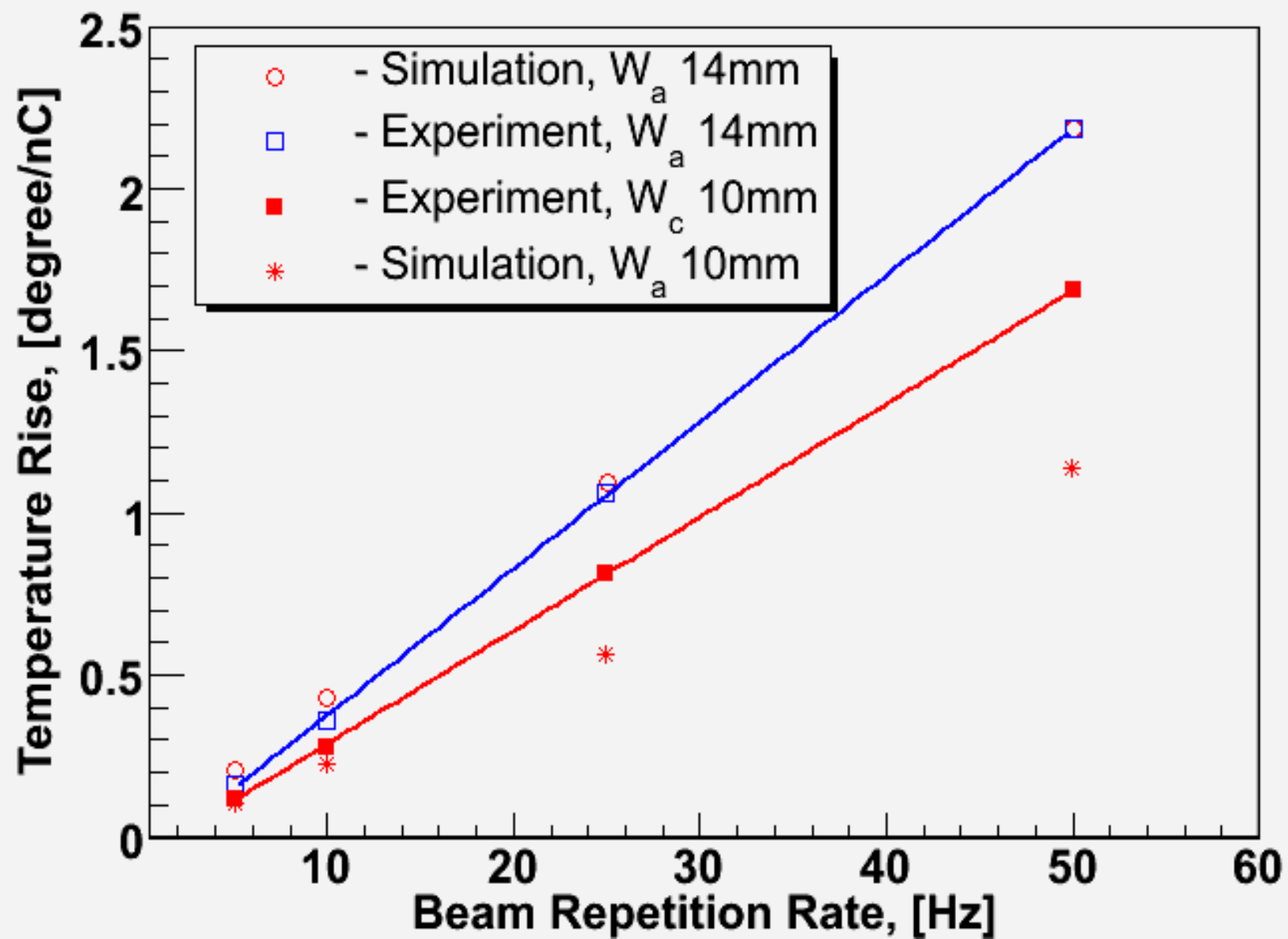


Temperature rise at downstream side of the 14 mm Wa target



***Max. temperatures before and after bunch
as function of irradiation time for the 14mm
Wa target***





Target model for simulation:

