

Advanced Beam Dynamicsc Workshop
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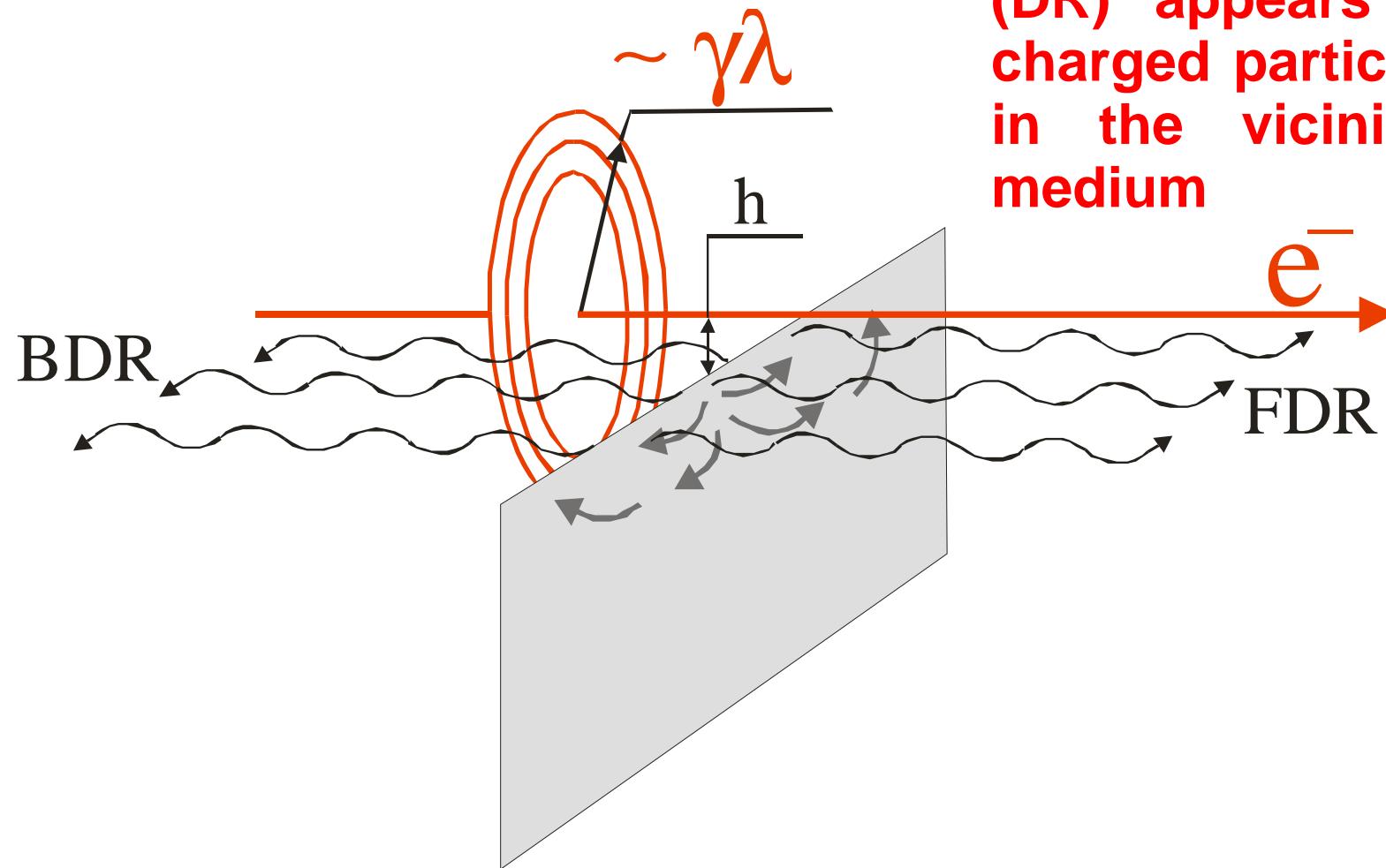
**SPATIAL RESOLUTION OF NON-
INVASIVE BEAM PROFILE
MONITORBASED ON OPTICAL
DIFFRACTION RADIATION**

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Diffraction radiation approach



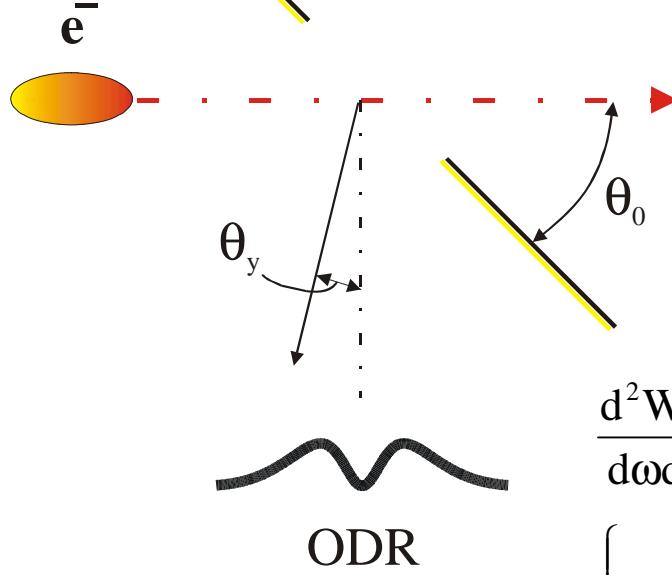
Diffraction radiation (DR) appears when a charged particle moves in the vicinity of a medium

Impact parameter, h , – the shortest distance between the target and the particle trajectory

$$h \leq \frac{\gamma\lambda}{2\pi}$$

λ - observation wavelength

Approach for the beam size measurements



Assume a Gaussian beam profile

$$G(\bar{a}_x, \sigma_y) = \frac{1}{\sqrt{2\pi}\sigma_y} \exp\left[-\frac{(\bar{a}_x - a_x)^2}{2\sigma_y^2}\right]$$

$$\frac{d^2 W_x^{\text{slit}}}{d\omega d\Omega} = \frac{\alpha |R_x|^2}{4\pi^2} \frac{\theta_x^2}{\gamma^{-2} + \theta_x^2} \frac{\exp\left(-\frac{2\pi a \sin \theta_0}{\lambda} \sqrt{\gamma^{-2} + \theta_x^2}\right)}{\gamma^{-2} + \theta_x^2 + \theta_y^2} \times$$

$$\left\{ \exp\left[\frac{8\pi^2 \sigma_y^2}{\lambda^2} (\gamma^{-2} + \theta_x^2)\right] \cosh\left[\frac{4\pi \bar{a}_x}{\lambda} \sqrt{\gamma^{-2} + \theta_x^2}\right] + \cos\left[\frac{2\pi a \sin \theta_0}{\lambda} \theta_y + 2\psi\right] \right\}$$

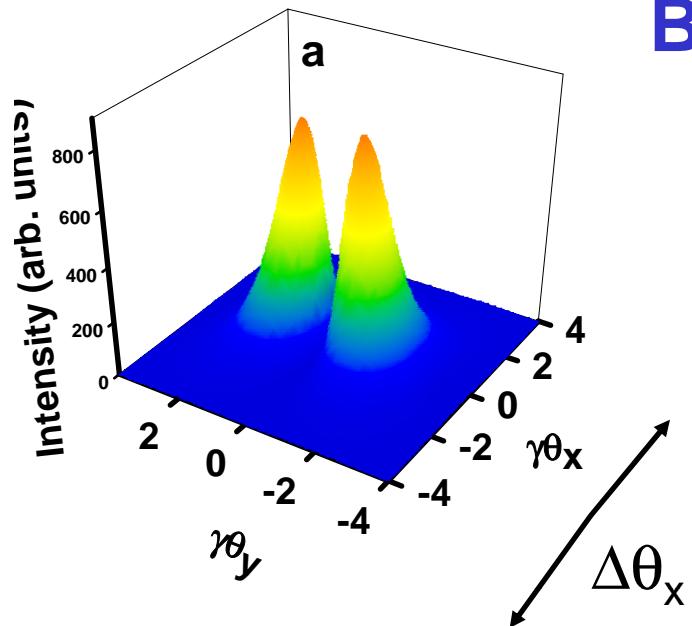
$$\frac{d^2 W_y^{\text{slit}}}{d\omega d\Omega} = \frac{\alpha |R_y|^2}{4\pi^2} \frac{\exp\left(-\frac{2\pi a \sin \theta_0}{\lambda} \sqrt{\gamma^{-2} + \theta_x^2}\right)}{\gamma^{-2} + \theta_x^2 + \theta_y^2} \times$$

$$\left\{ \exp\left[\frac{8\pi^2 \sigma_y^2}{\lambda^2} (\gamma^{-2} + \theta_x^2)\right] \cosh\left[\frac{4\pi \bar{a}_x}{\lambda} \sqrt{\gamma^{-2} + \theta_x^2}\right] - \cos\left[\frac{2\pi a \sin \theta_0}{\lambda} \theta_y + 2\psi\right] \right\}$$

$$\psi = \arctan\left(\frac{\theta_y}{\sqrt{\gamma^{-2} + \theta_x^2}}\right)$$

σ_y is the electron beam size and \bar{a}_x is its offset with respect to the slit center

Beam size effect

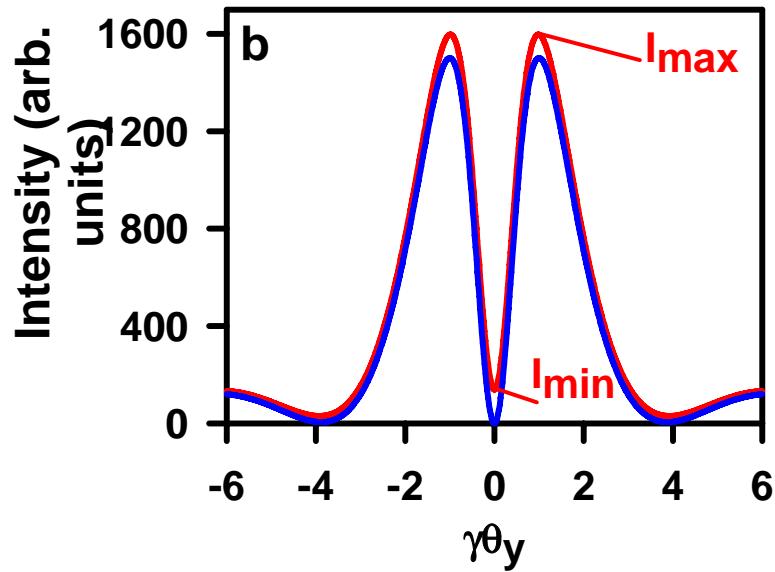


Projected vertical polarization component

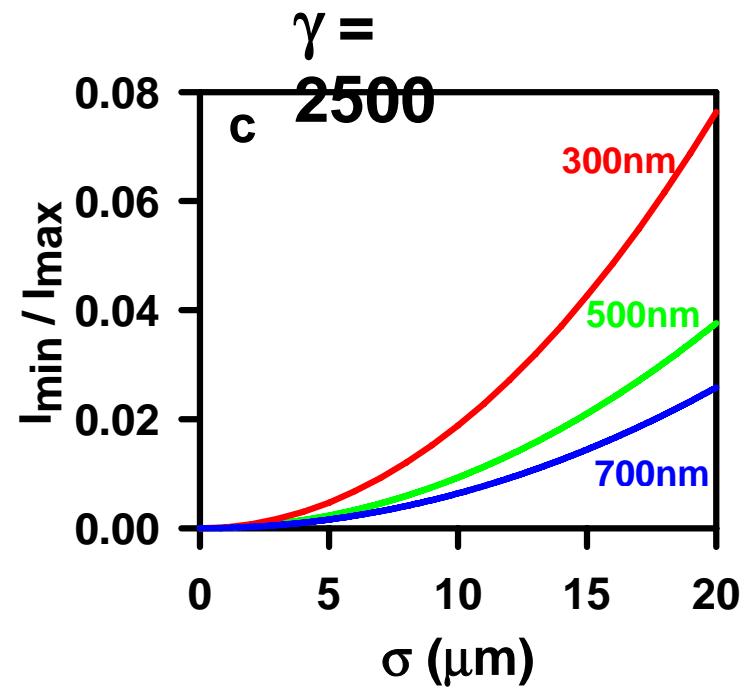
$$S(\theta_y, \sigma_y) = \int_{-\Delta\theta_x/2}^{\Delta\theta_x/2} \frac{d^2 W(\theta_x, \theta_y, \sigma_y)}{d\omega d\Omega} d\theta_x$$

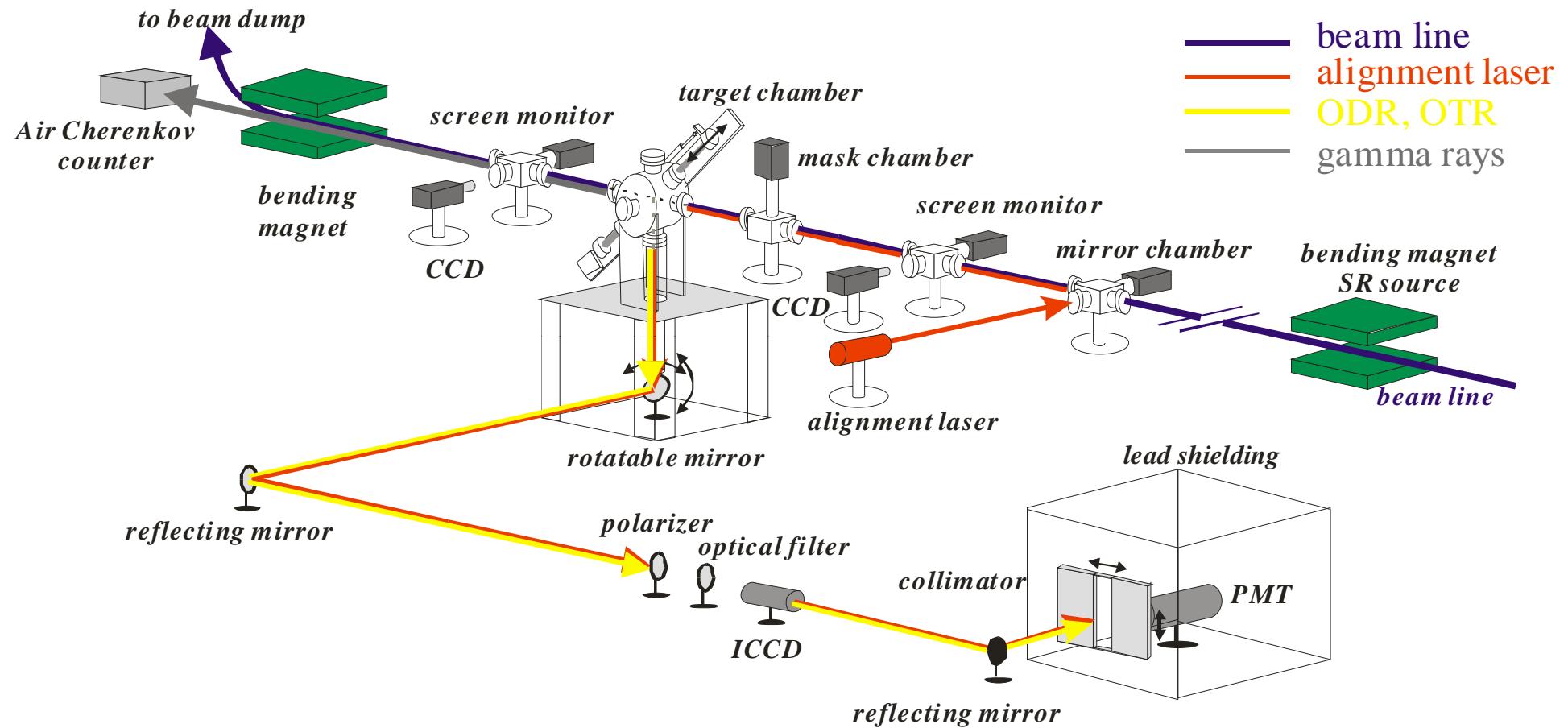
$\Delta\theta_x$ – x detector angular acceptance

Projection

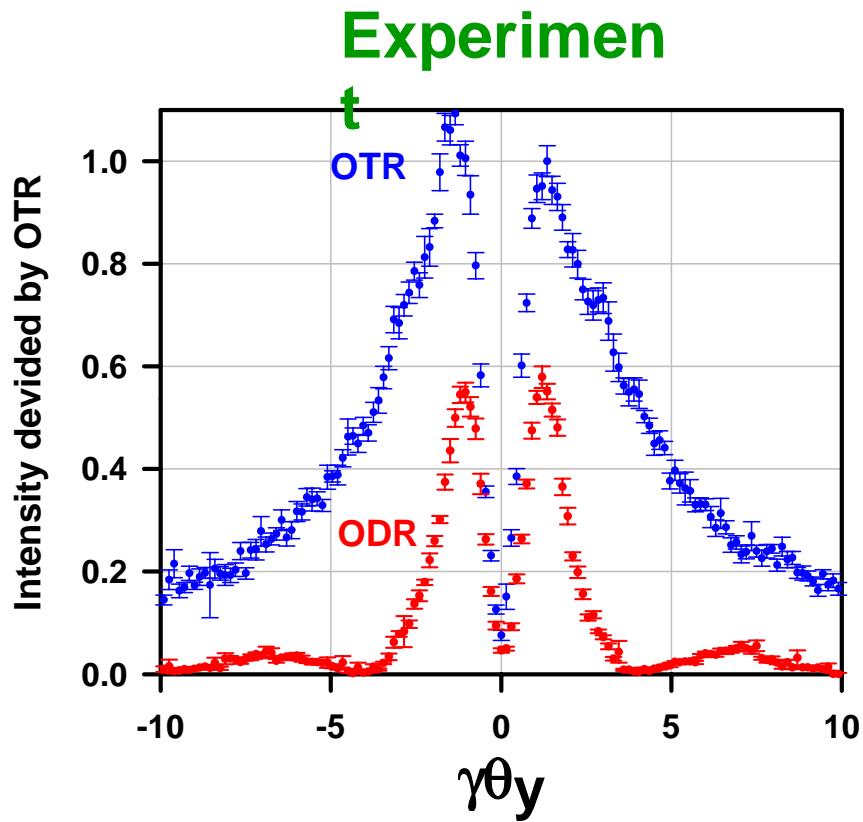


$\sigma_y=0$
 $\sigma_y=30\mu\text{m}$

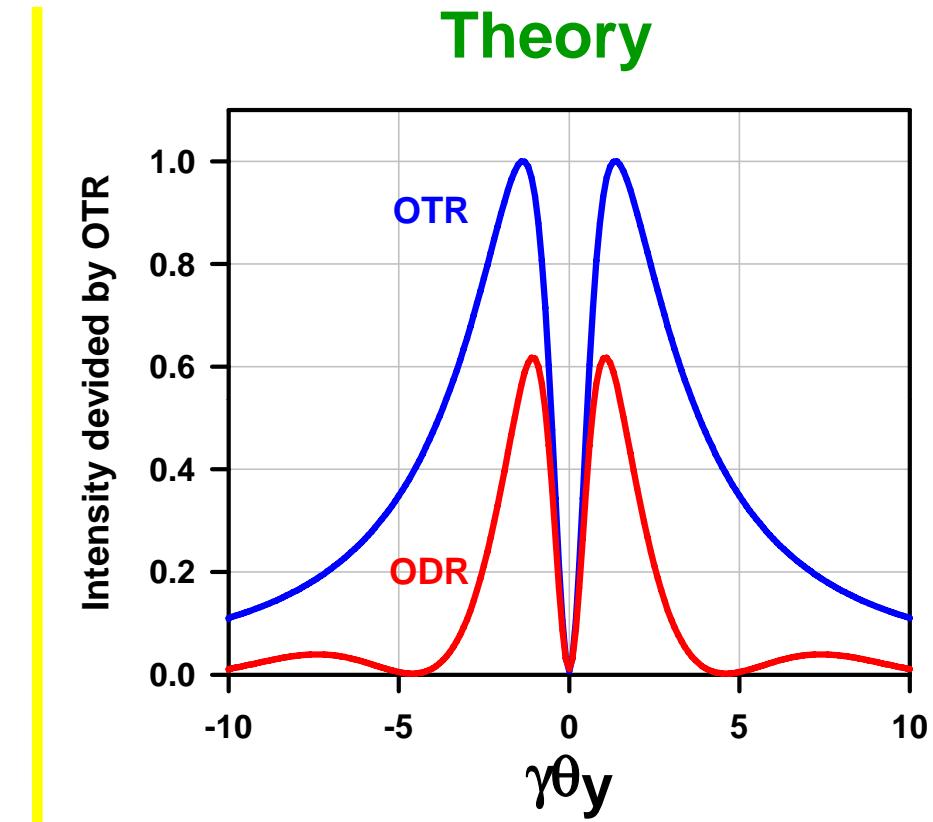




Measurements of the ODR projected vertical polarization component with PMT



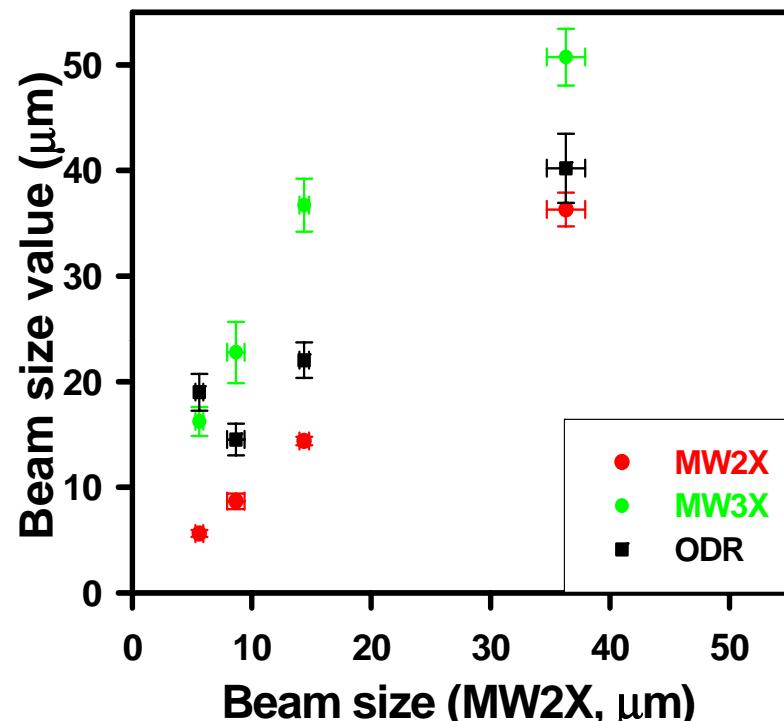
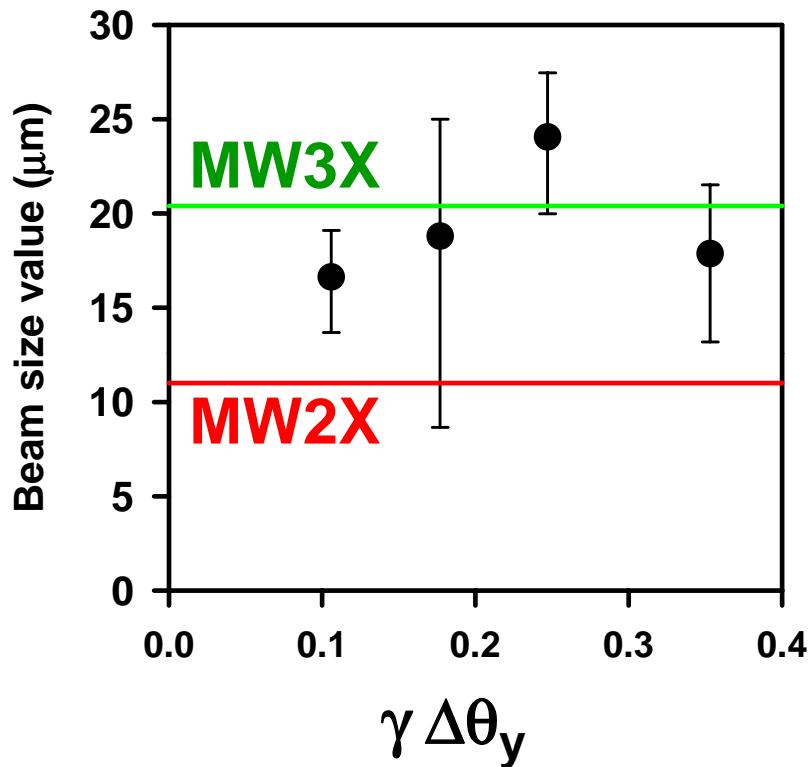
$$\frac{I_{ODR}^{\max}}{I_{OTR}^{\max}} = 58\%$$



$$\frac{I_{ODR}^{\max}}{I_{OTR}^{\max}} = 62\%$$

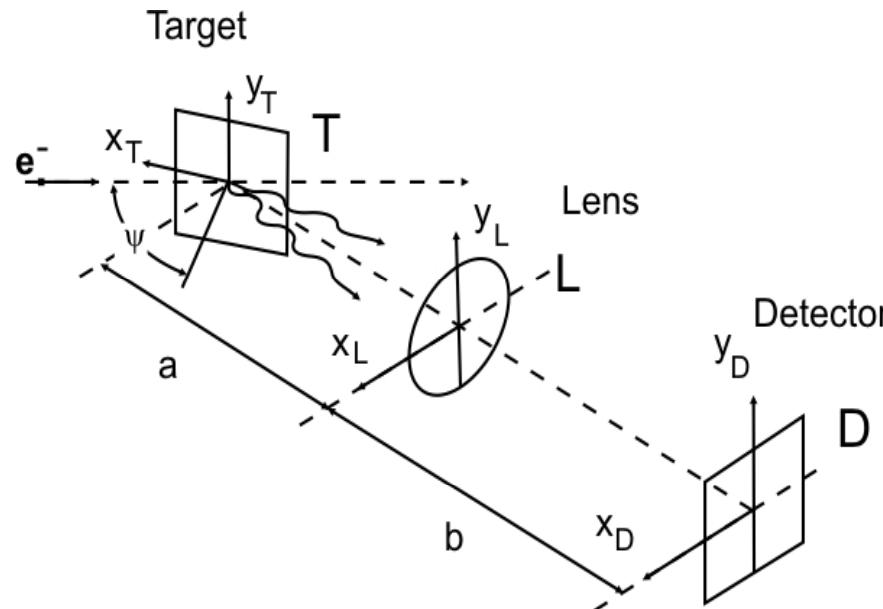
Optical filter $550 \pm 20\text{nm}$

Angular acceptance and beam size effect in ODR experiment

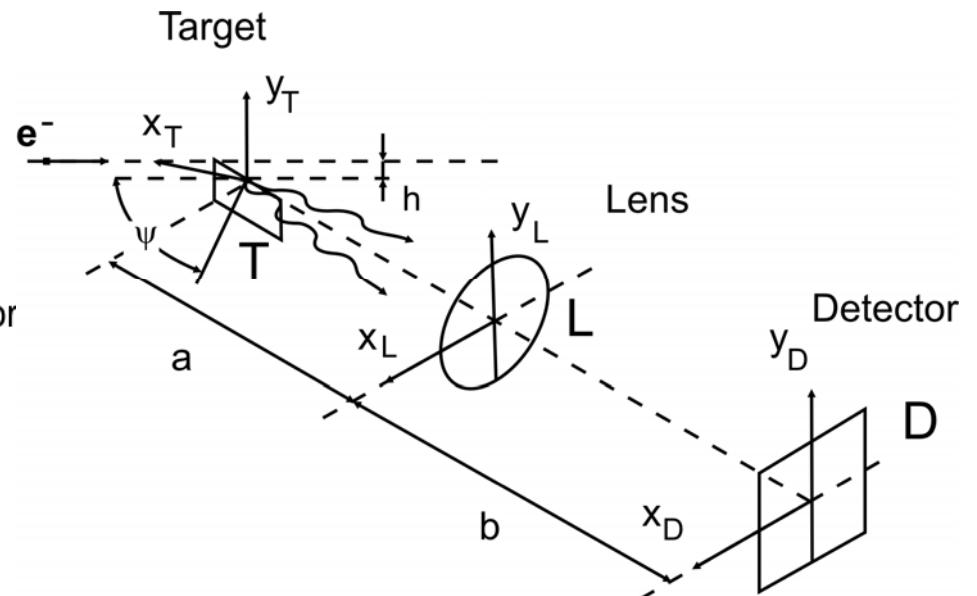


Optical transition radiation (OTR) beam size monitor

OTR monitor



ODR monitor



Pre-wave zone

$$a \leq \gamma^2 \lambda$$

Model

We shall introduce Cartesian coordinates on the target, lens and detector using T, L, D indices and use dimensionless variables

$$\begin{Bmatrix} x_T \\ y_T \end{Bmatrix} = \frac{2\pi}{\gamma\lambda} \begin{Bmatrix} X_T \\ Y_T \end{Bmatrix}, \quad \begin{Bmatrix} x_L \\ y_L \end{Bmatrix} = \frac{\gamma}{a} \begin{Bmatrix} X_L \\ Y_L \end{Bmatrix}, \quad \begin{Bmatrix} x_D \\ y_D \end{Bmatrix} = \frac{2\pi}{\gamma\lambda} \begin{Bmatrix} X_D \\ Y_D \end{Bmatrix}.$$

$$\begin{aligned} & \begin{Bmatrix} E_x^D(x_D, y_D) \\ E_y^D(x_D, y_D) \end{Bmatrix} = \text{const} \int dx_T dy_T \int dx_L dy_L \times \\ & \times \begin{Bmatrix} x_T \\ y_T \end{Bmatrix} \frac{K_1(\sqrt{x_T^2 + y_T^2})}{\sqrt{x_T^2 + y_T^2}} \exp[i(x_T x_L + y_T y_L)] \times \exp\left[i \frac{x_T^2 + y_T^2}{4\pi R}\right] \times \\ & \times \exp\left[-i\left(x_L \frac{x_D}{M} + y_L \frac{y_D}{M}\right)\right], \quad R = \frac{a}{\gamma^2 \lambda}, \quad M \text{ is magnification} \end{aligned}$$

For a rectangular lens with aperture $2x_m \times 2y_m$

$$-x_m \leq x_L \leq x_m , \quad -y_m \leq y_L \leq y_m$$

One may obtain

$$\begin{aligned} & \int_{-x_m}^{x_m} dx_L \int_{-y_m}^{y_m} dy_L \exp\left[-ix_L\left(x_T + \frac{x_D}{M}\right)\right] \exp\left[-iy_L\left(y_T + \frac{y_D}{M}\right)\right] = \\ & = 4 \frac{\sin\left[x_m\left(x_T + \frac{x_D}{M}\right)\right]}{x_T + \frac{x_D}{M}} \frac{\sin\left[y_m\left(y_T + \frac{y_D}{M}\right)\right]}{y_T + \frac{y_D}{M}} = \\ & = G_x(x_T, x_D, x_m)G(y_T, y_D, y_m). \end{aligned}$$

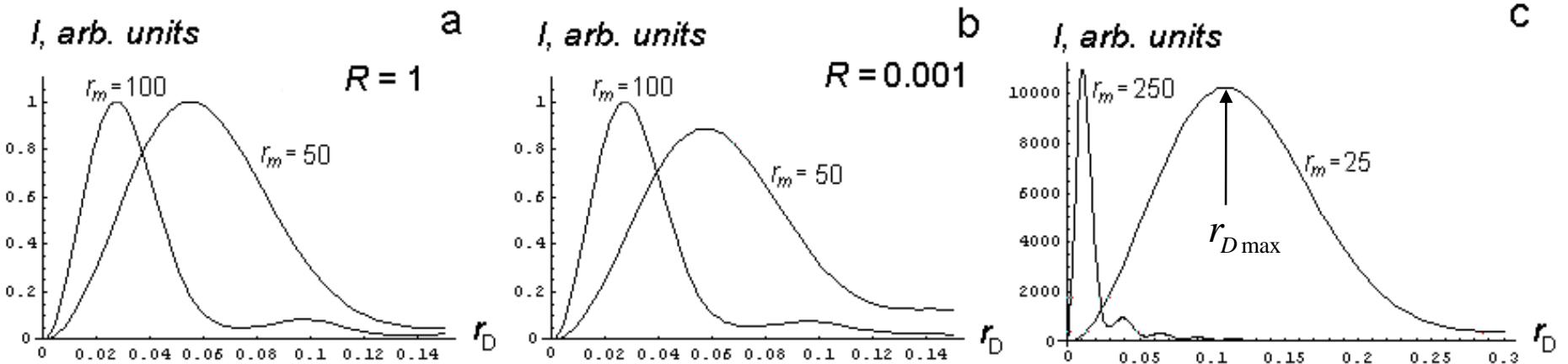
For M=1 fields on the detector surface may be written:

$$\begin{aligned} \begin{Bmatrix} E_x^D(x_D, y_D) \\ E_y^D(x_D, y_D) \end{Bmatrix} &= const \int dx_T dy_T \begin{Bmatrix} x_T \\ y_T \end{Bmatrix} \frac{K_1\left(\sqrt{x_T^2 + y_T^2}\right)}{\sqrt{x_T^2 + y_T^2}} \times \\ &\times \exp\left[i \frac{x_T^2 + y_T^2}{4\pi R}\right] G_x(x_T, x_D, x_m)G(y_T, y_D, y_m). \end{aligned}$$

Intensity on the detector surface

$$I = const \left(|E_x^D|^2 + |E_y^D|^2 \right)$$

OTR image from a single electron(point spread function, PSF)



a) Normalized shape of OTR source image on the detector plane for lens aperturer_m =100 (left curve) and r_m = 50 (right curve) in wave zone ($R = 1$);

b) OTR source image in «pre-wave zone» ($R = 0.001$) for the same conditions and with the same normalizing factors;

c) OTR source image at the fixed lens diameter for different distances between the target and the lens ($R = 0.01$, r_m = 250 - right curve; R = 0.1, r_m = 25 - left).

Spatial resolution of OTR monitor is defined by the distribution maximum position $r_{D \max}$

$$r_{D \max} \square \frac{3}{r_m} = \frac{3}{\gamma \theta_0}$$

Dimension variable:

$$\theta_0 = \frac{R_{L \max}}{a} - \text{lens acceptance}$$

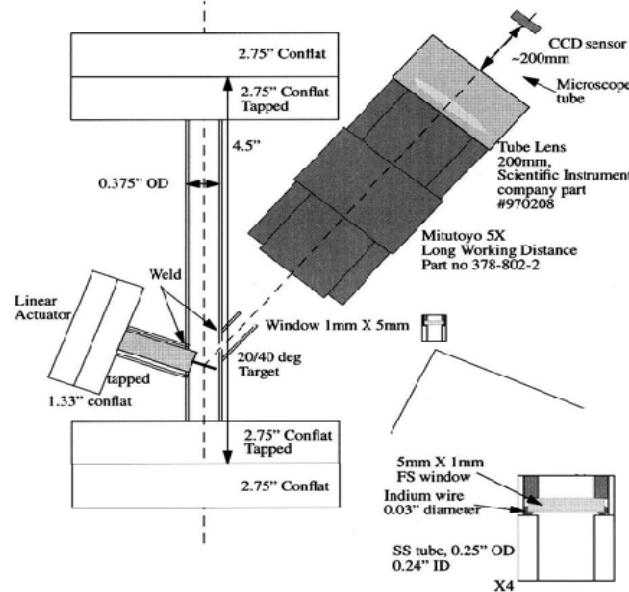
$$\sigma \approx \frac{\gamma \lambda r_{D \max}}{2\pi} \square \frac{1}{2} \frac{\lambda}{\theta_0}$$

- For optical diffraction radiation (ODR) there are 2 dimension parameters – wavelength and impact parameter h
- Which one is defined a spatial resolution?
- To obtain an intensity of ODR on detector surface one have to integrate ODR field on the target surface:

$$-x_{\max} \leq x_t \leq x_{\max} ,$$

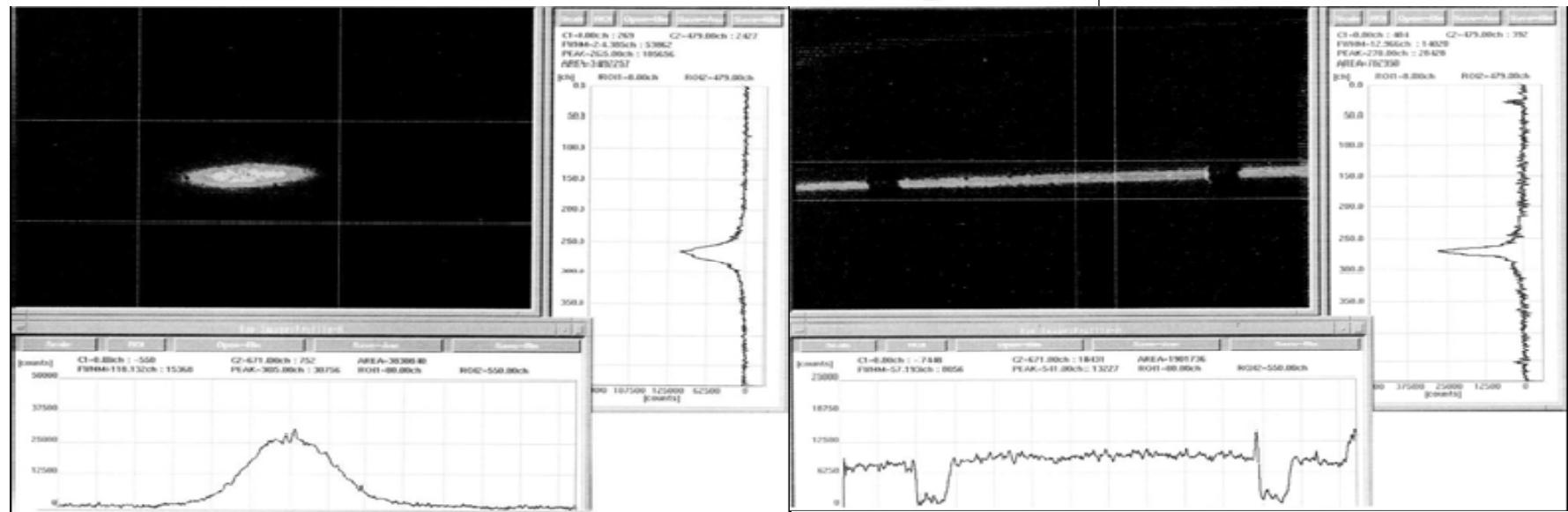
$$-h \leq y \leq y_{\max}$$

A Very High Resolution Optical Transition Radiation Beam Profile Monitor // Ross M. et al. SLAC-PUB-9280 July 2002



$$FWHM = 10\mu$$

$$FWHM = 5.8\mu$$

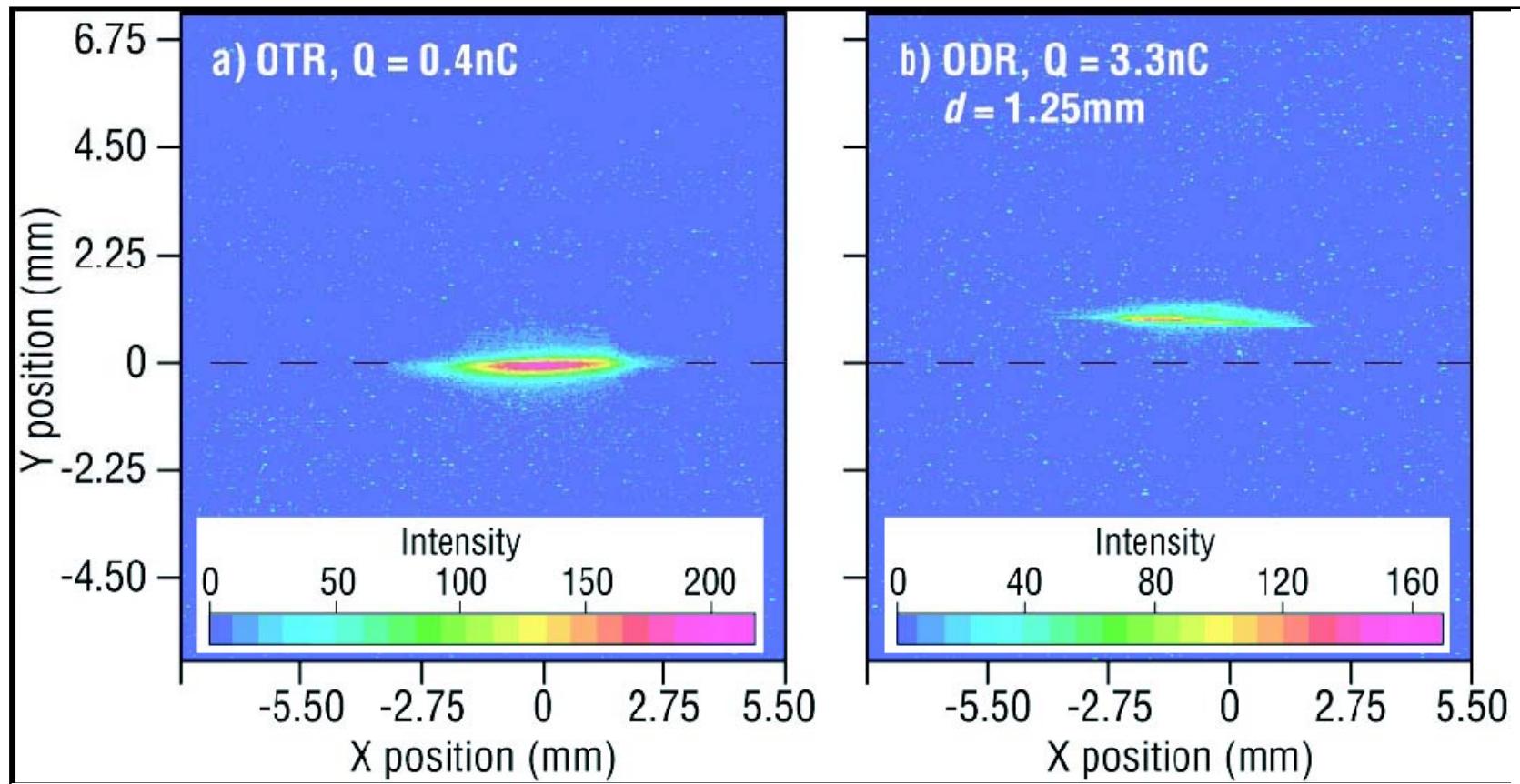


Near-field imaging of optical diffraction radiation generated by a 7-GeV electron beam

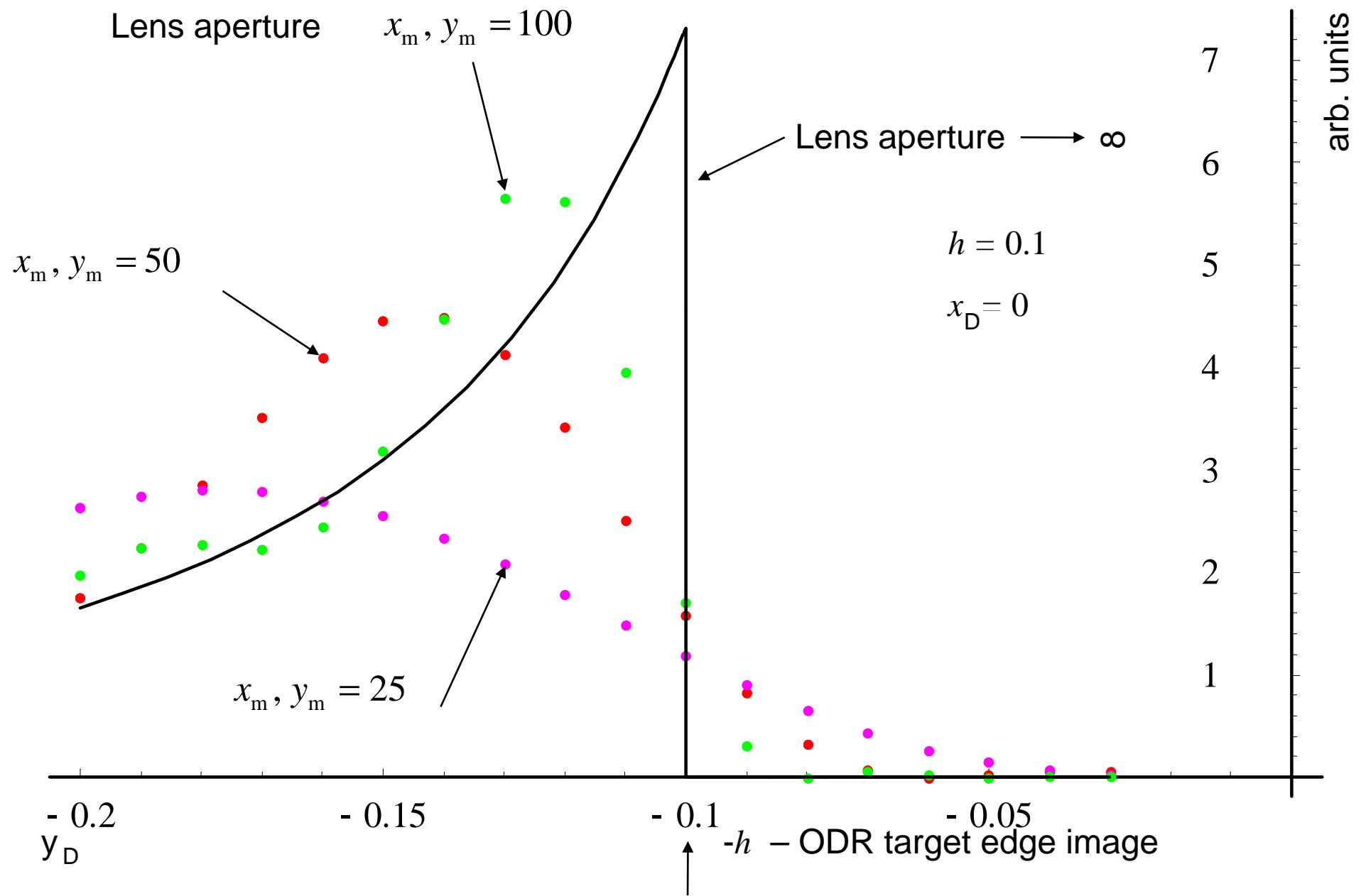
A. H. Lumpkin, W. J. Berg, N. S. Sereno, D.W. Rule,* and C.-Y. Yao

PHYSICAL REVIEW SPECIAL TOPICS - ACCELERATORS AND BEAMS 10,
022802 (2007)

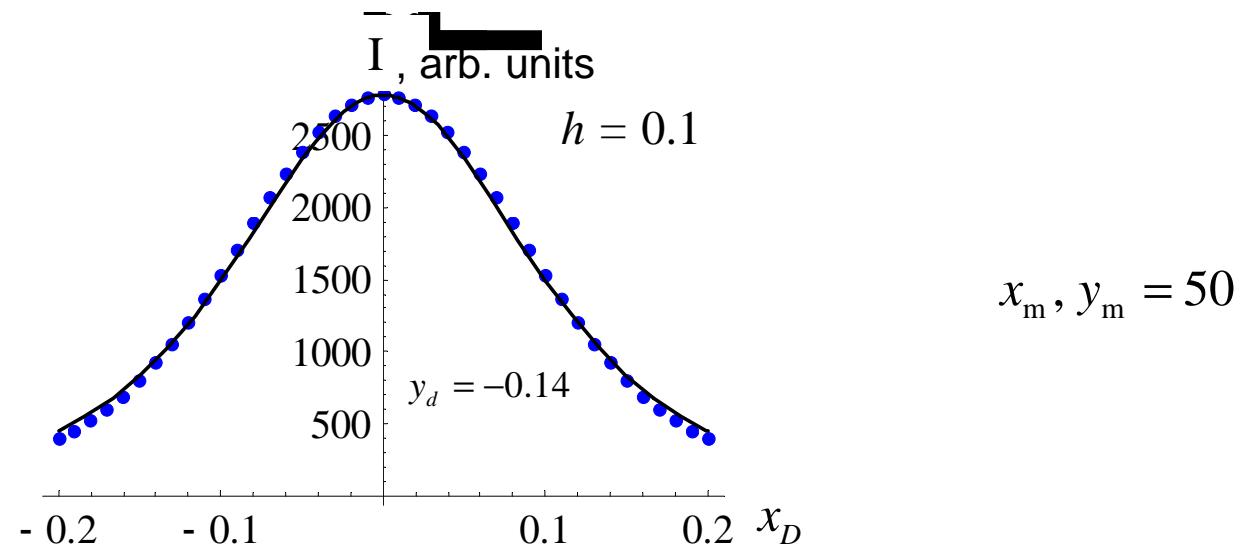
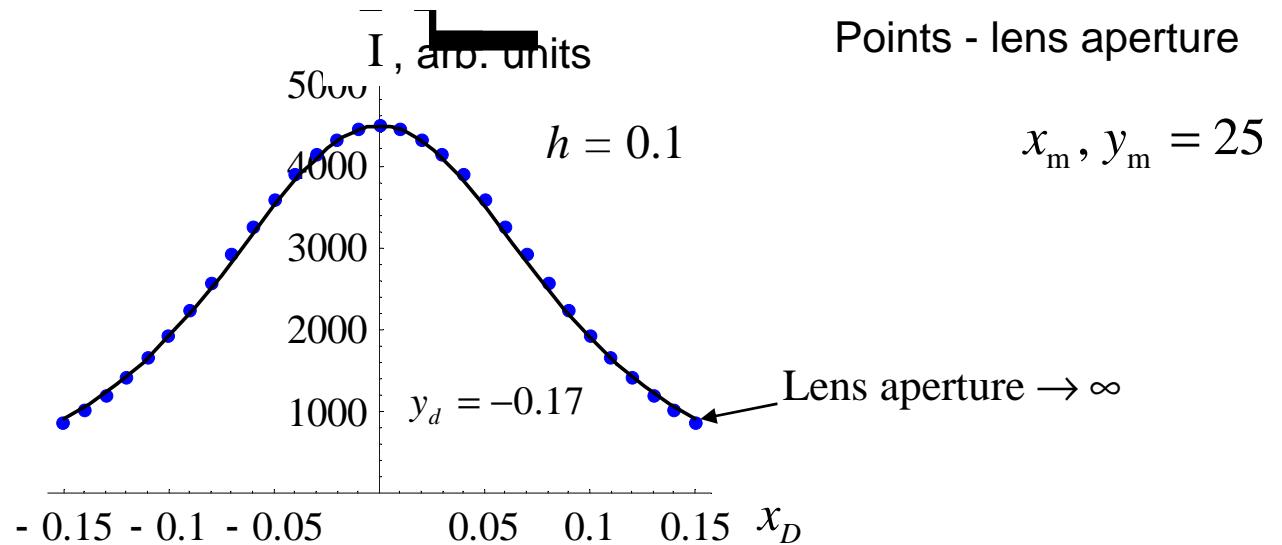
$$E = 7 \text{ GeV} \quad \lambda = 0.8 \mu\text{m} \quad h = 1.25 \text{ mm} \quad \sigma_x = 1375 \mu\text{m} \quad \sigma_y = 200 \mu\text{m}$$



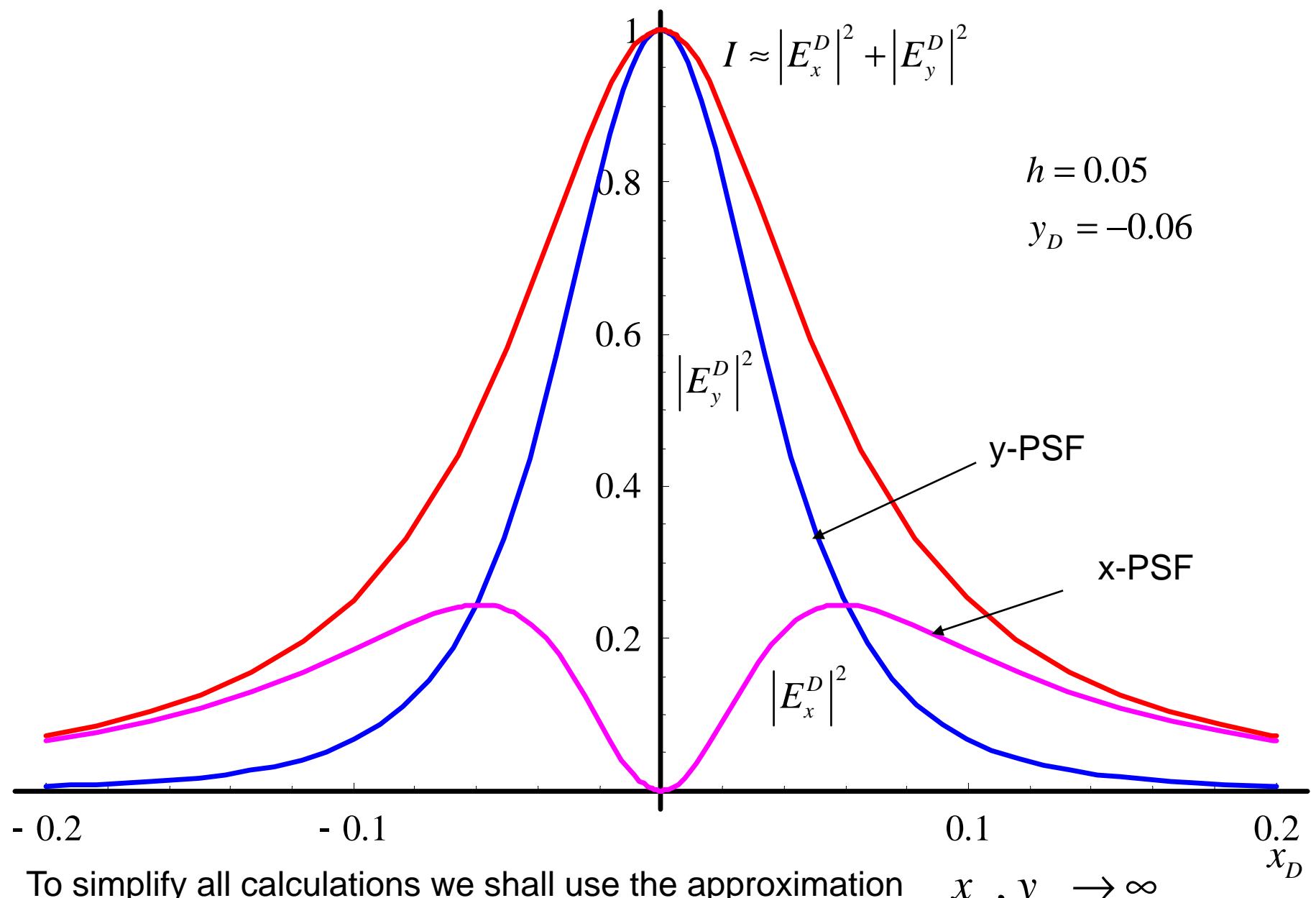
PSF for ODR case (perpendicular to target edge)



PSF for ODR case (parallel to target edge)

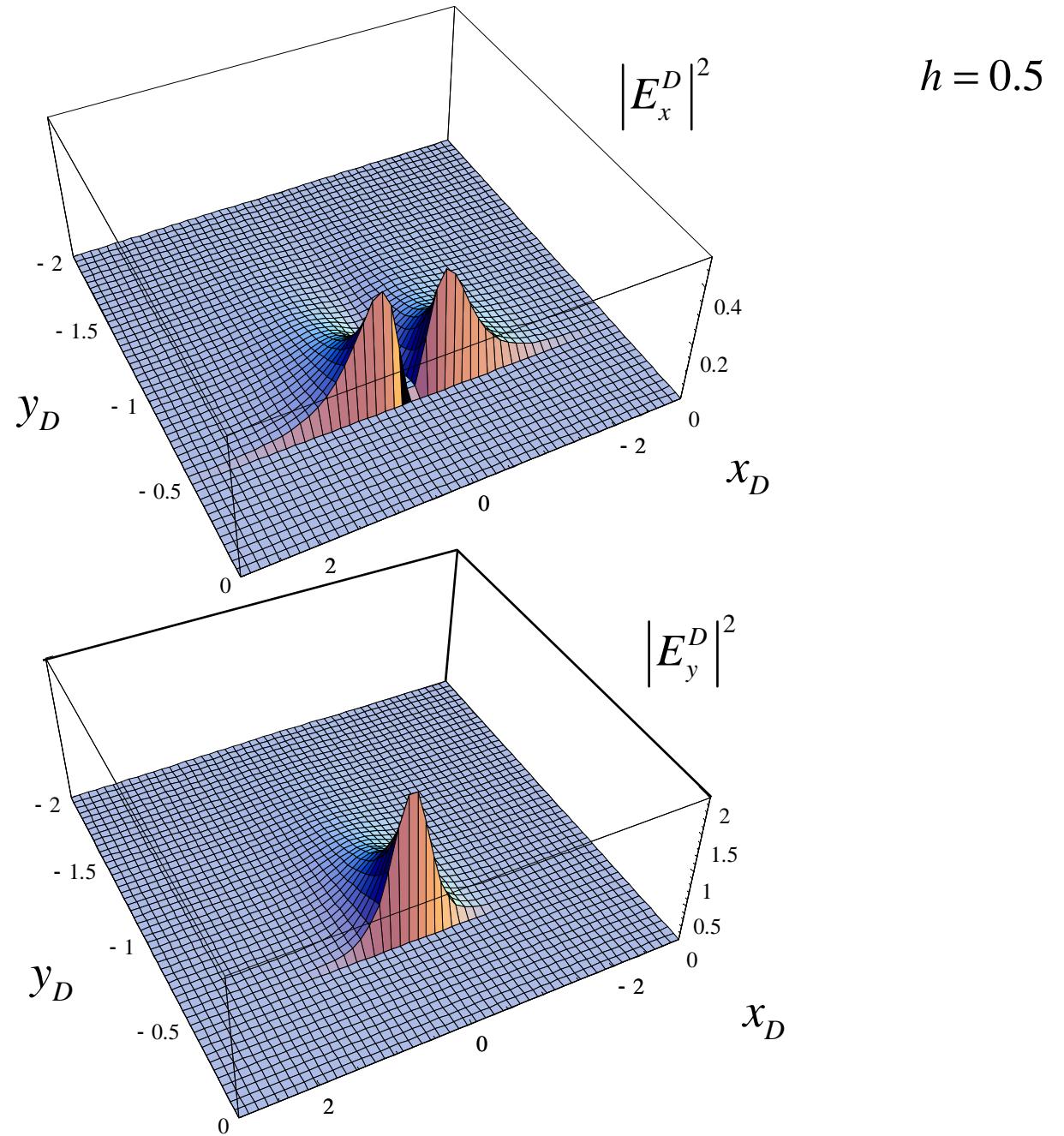


PSF for both ODR polarized components

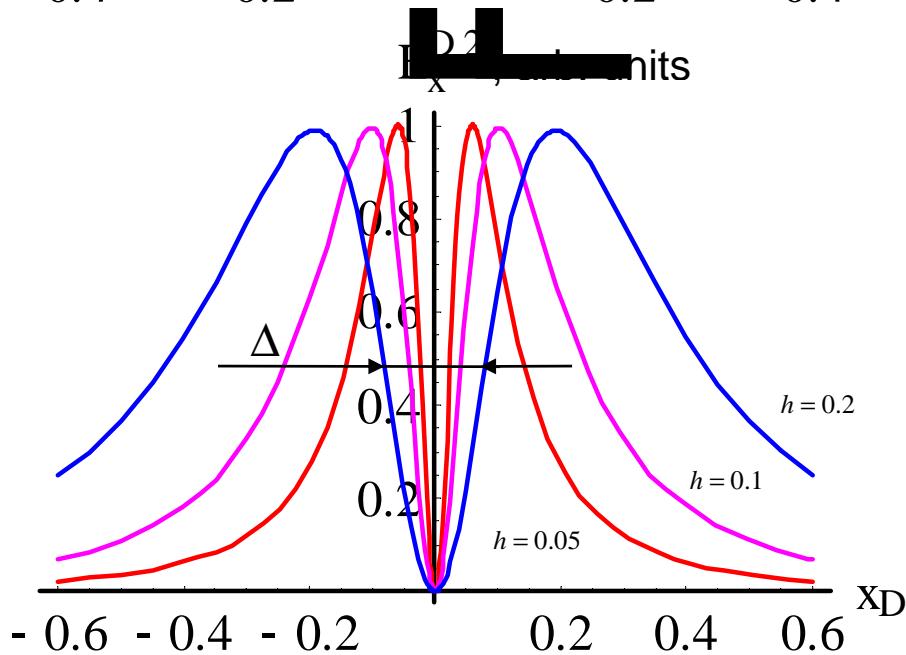
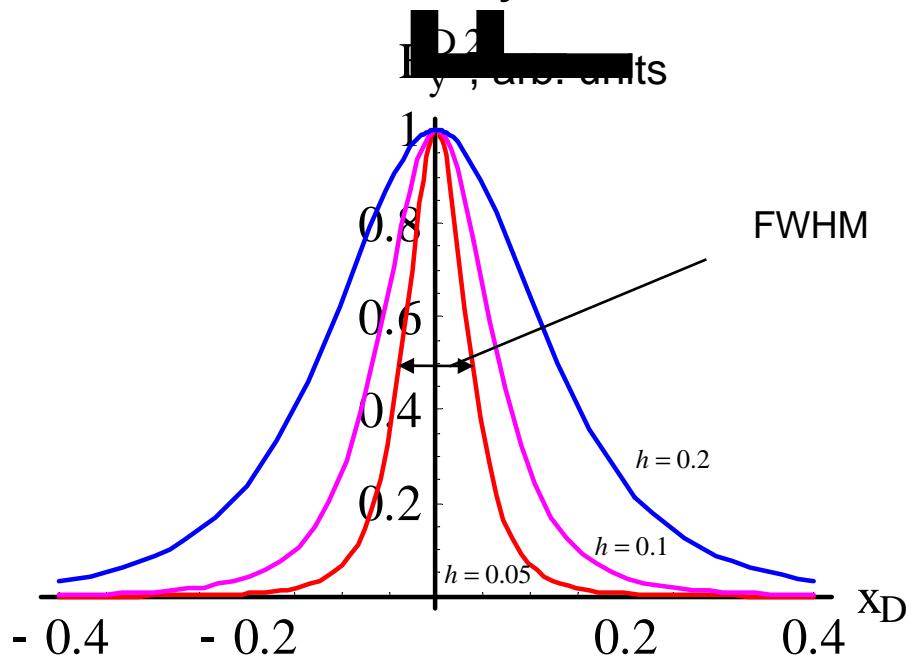


2D PSF for ODR case

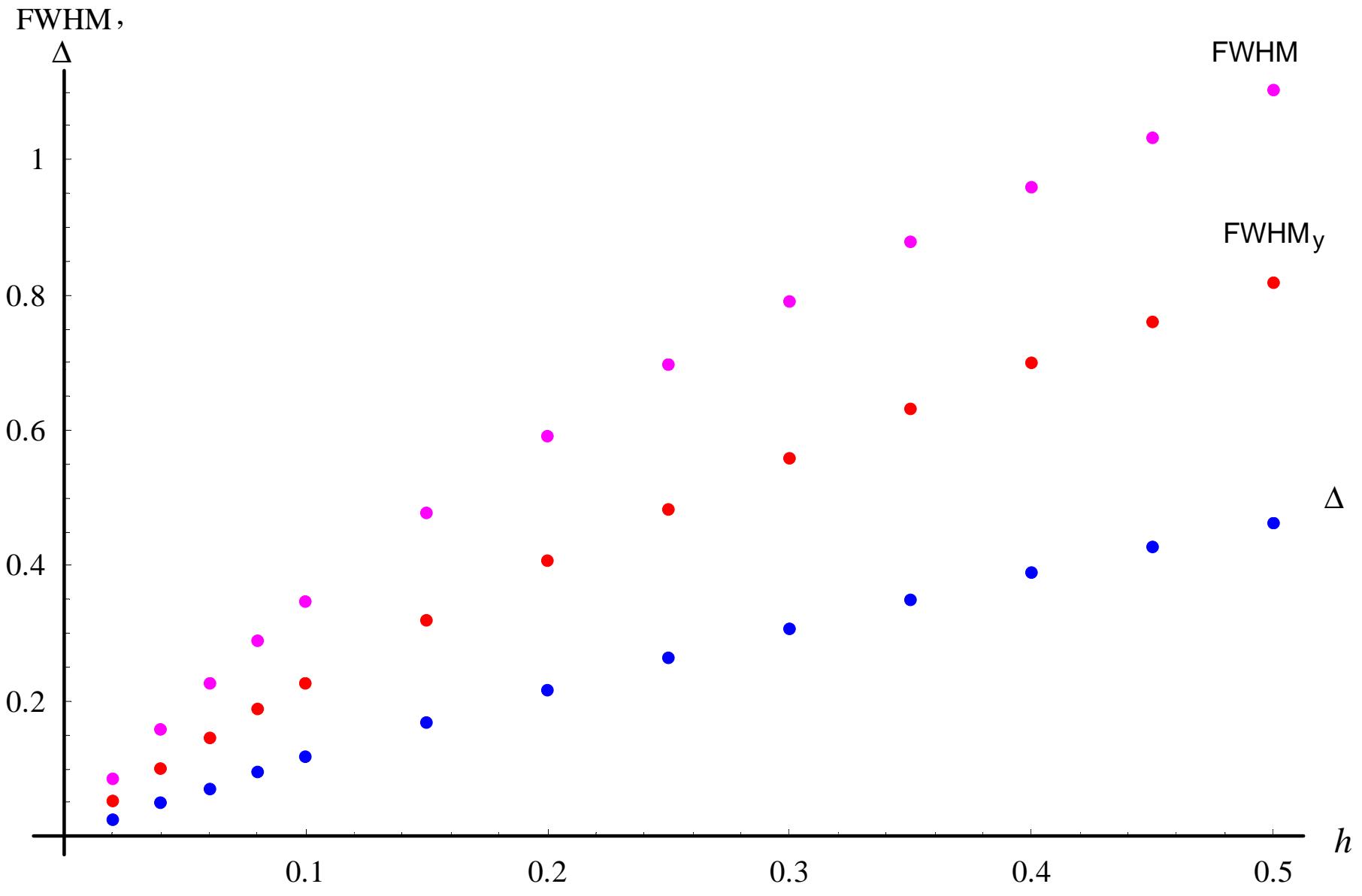
Significant broadening of deep (for $|E_x^D|^2$) and peak (for $|E_y^D|^2$) is observed with increasing of impact parameter h



Characteristics of y-PSF and x-PSF

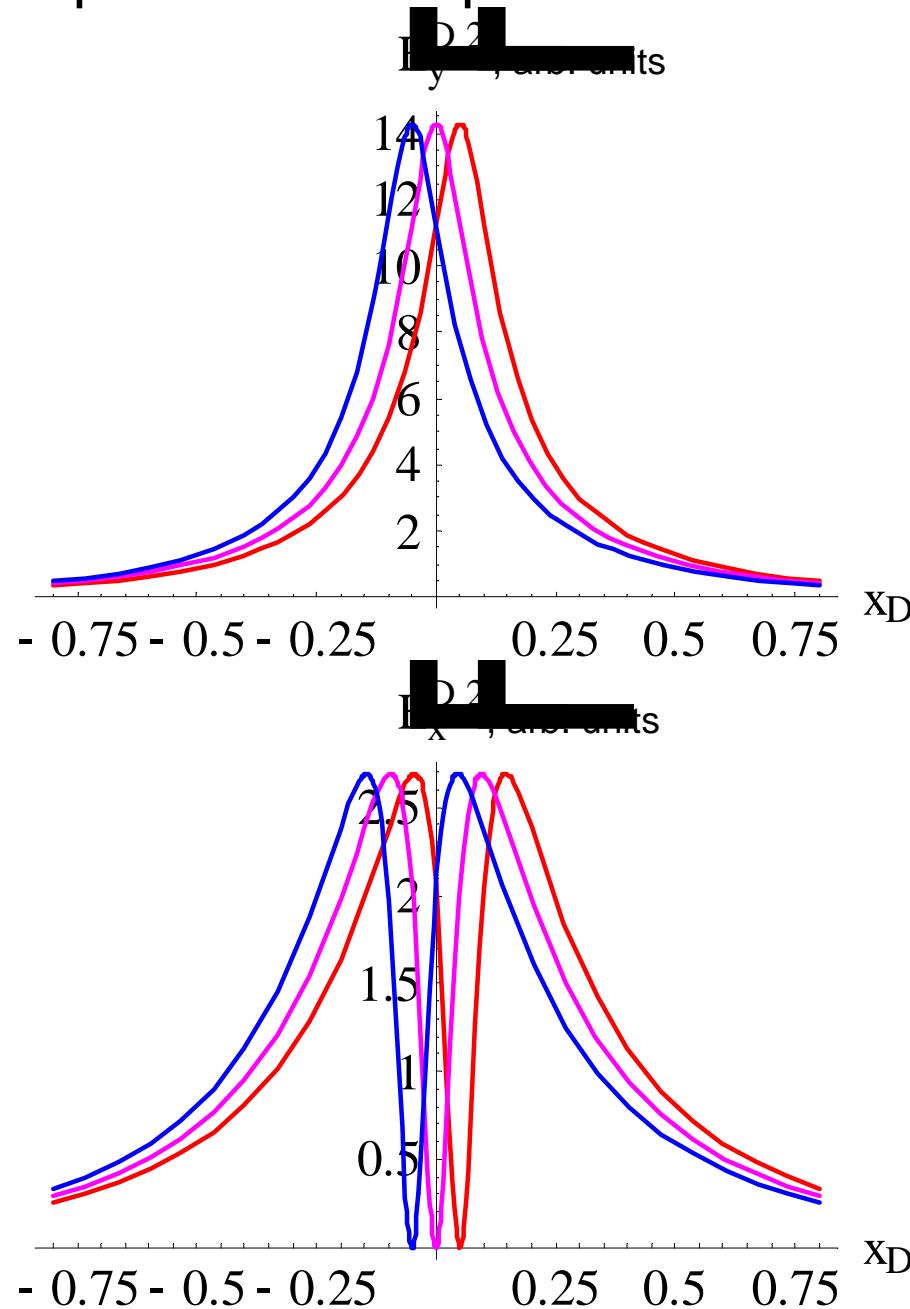


Dependence on impact parameter



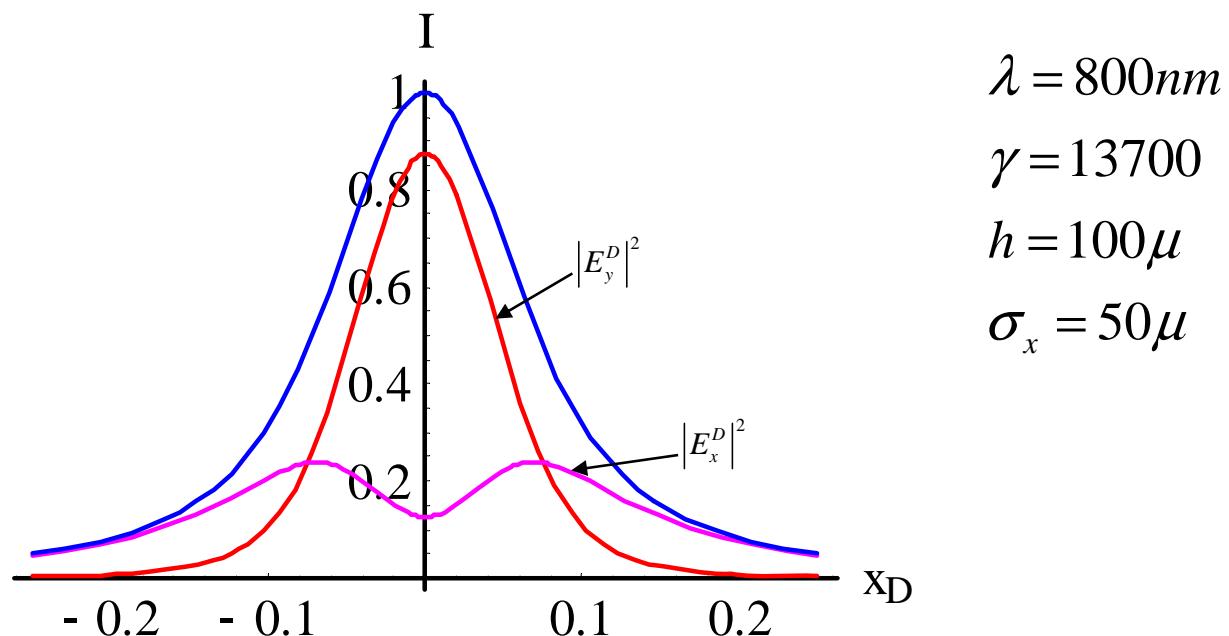
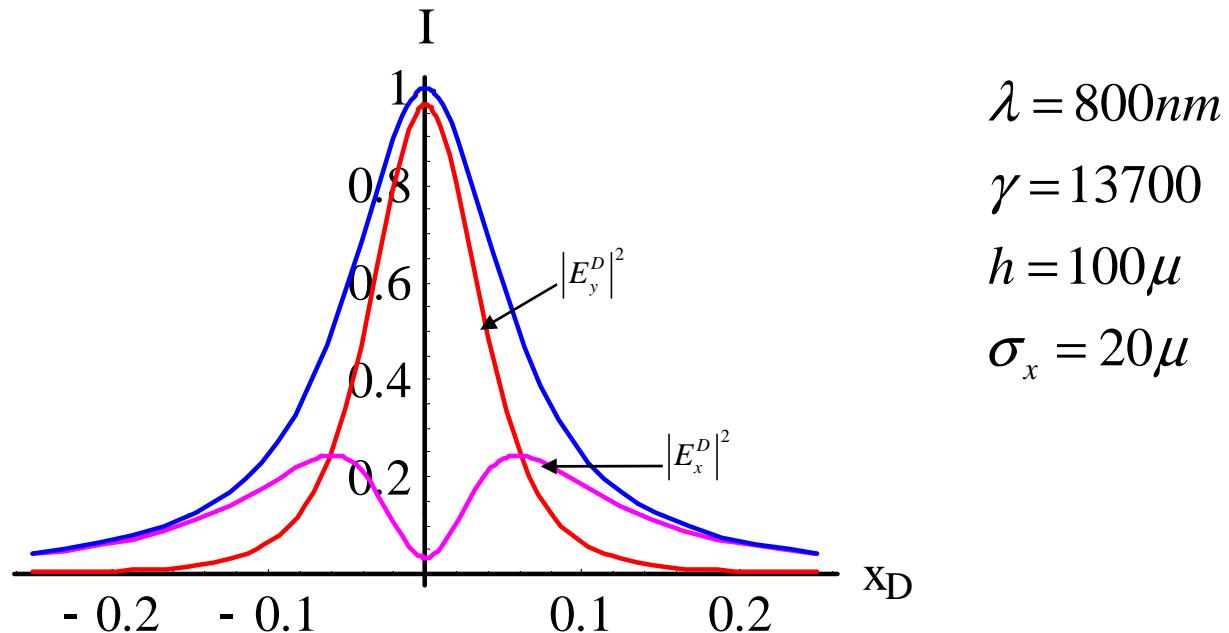
Almost linear dependence of FWHM and Δ on impact parameter

PSF dependence on particle offset



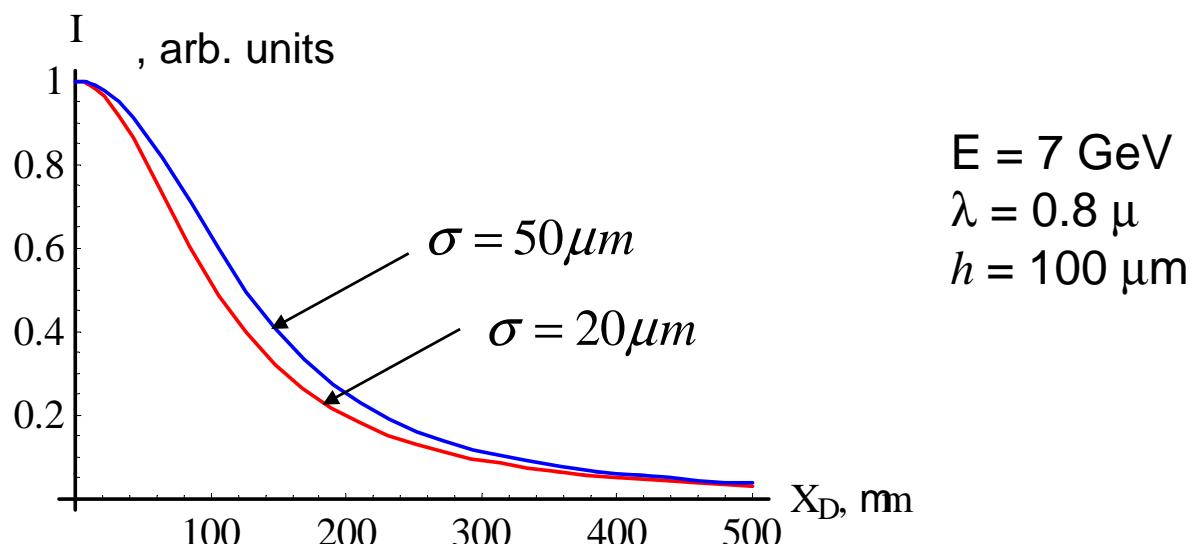
For small offset relative to optical axes distributions remain the same

“Smoothing” of PSF due to beam size



Dependence of smoothed PSF on beam size

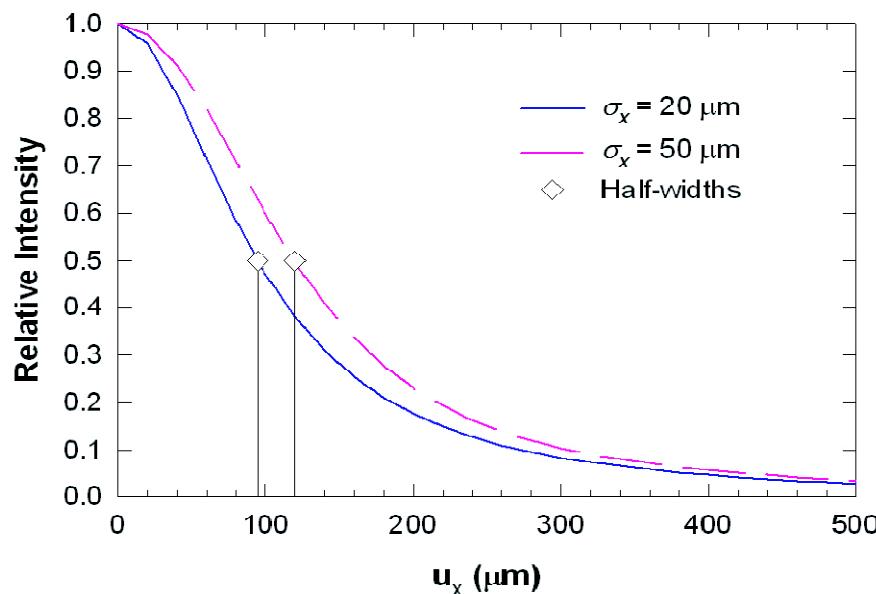
Developed model



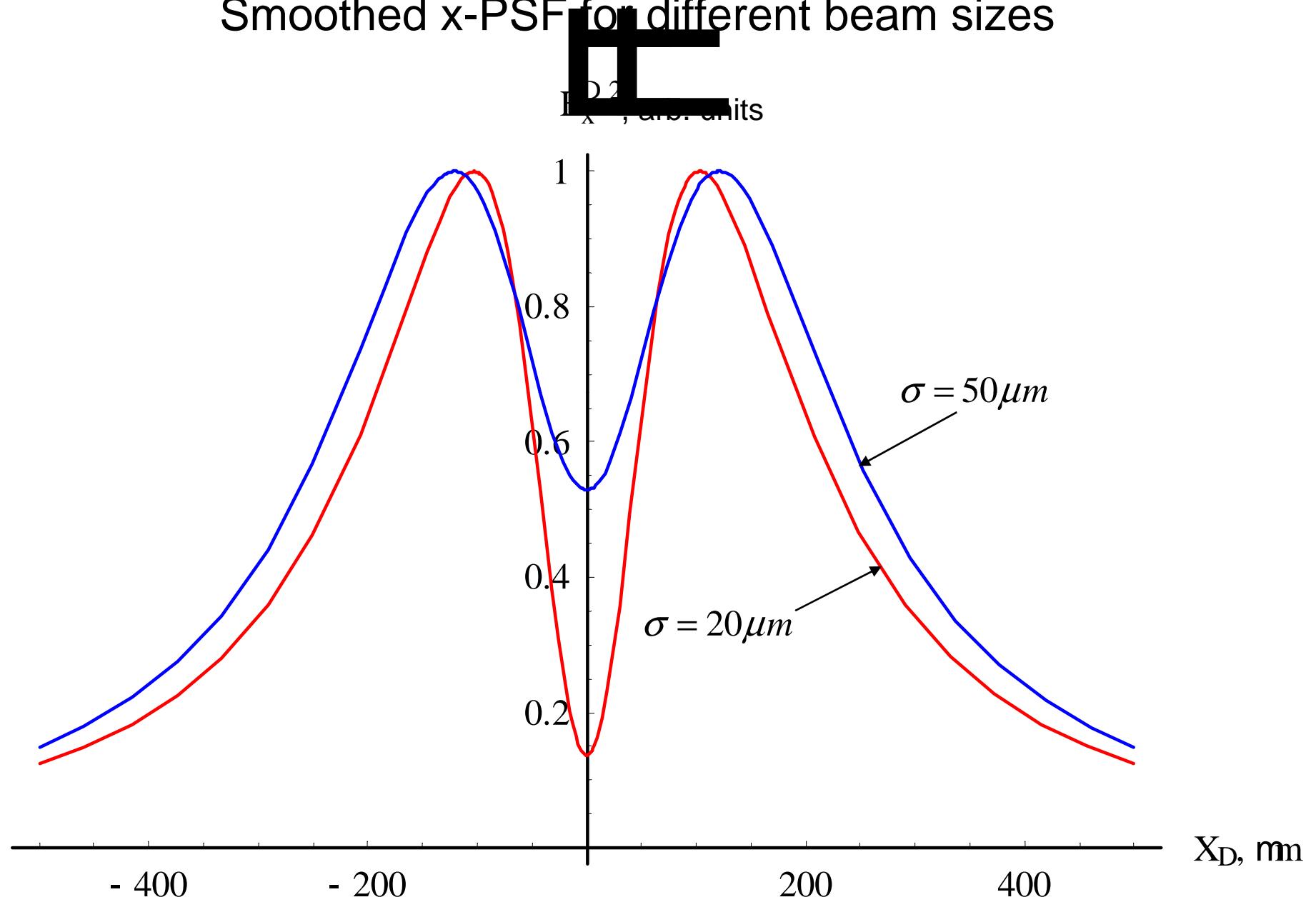
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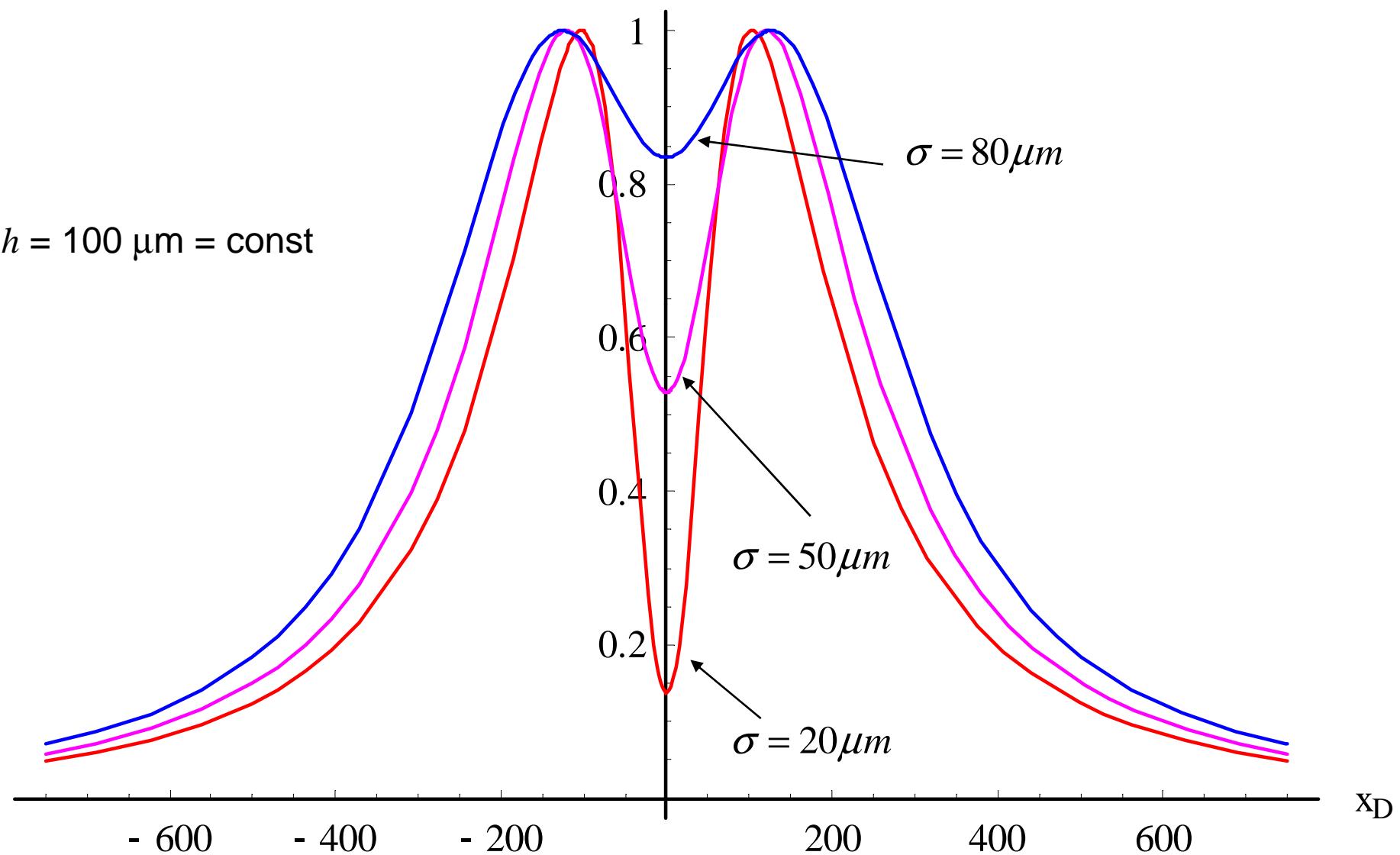
Smoothed x-PSF for different beam sizes



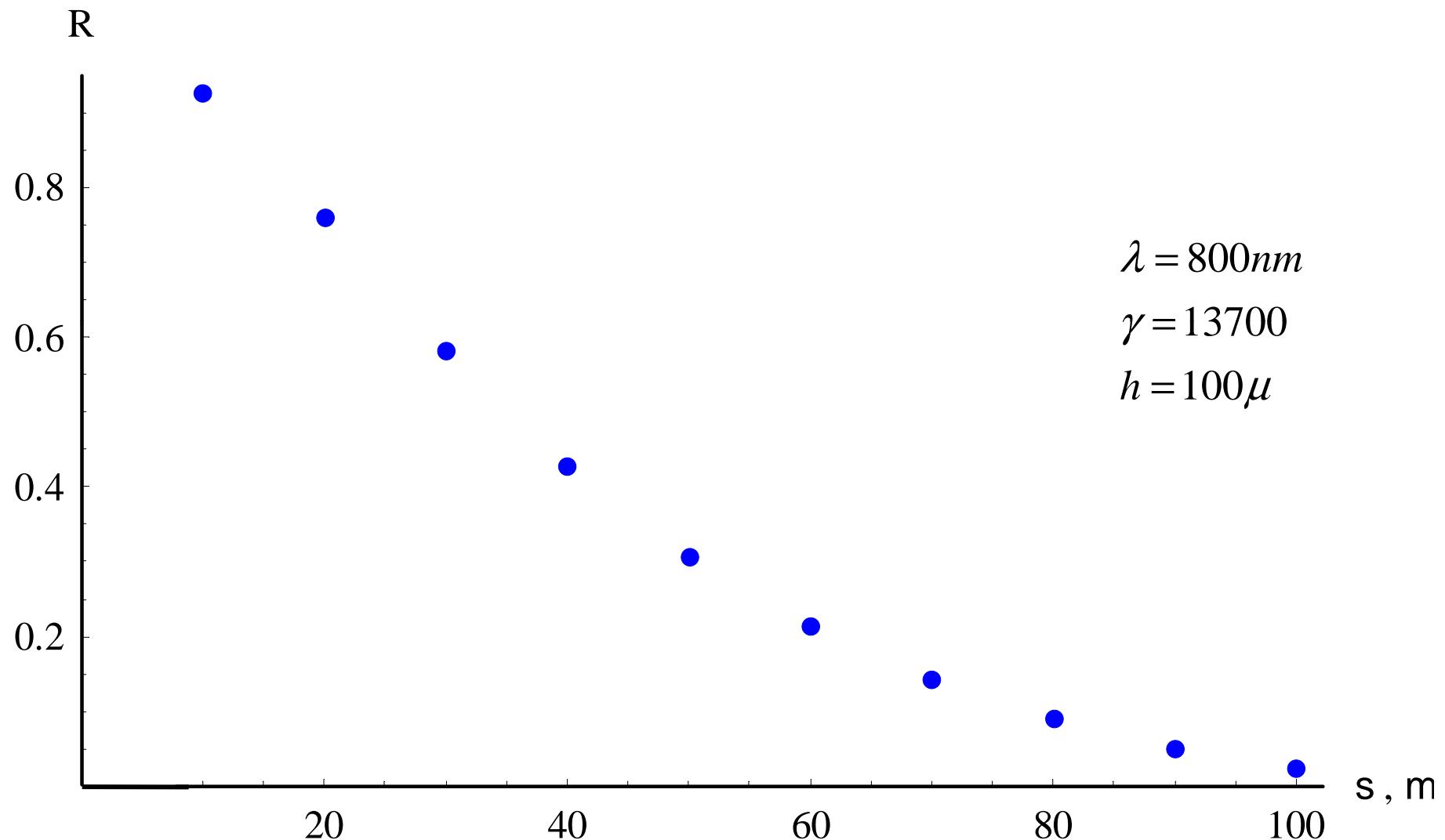
Smoothed off-axis intensity for different σ

$I_{x,y}$, abs. units

$h = 100 \mu m = \text{const}$

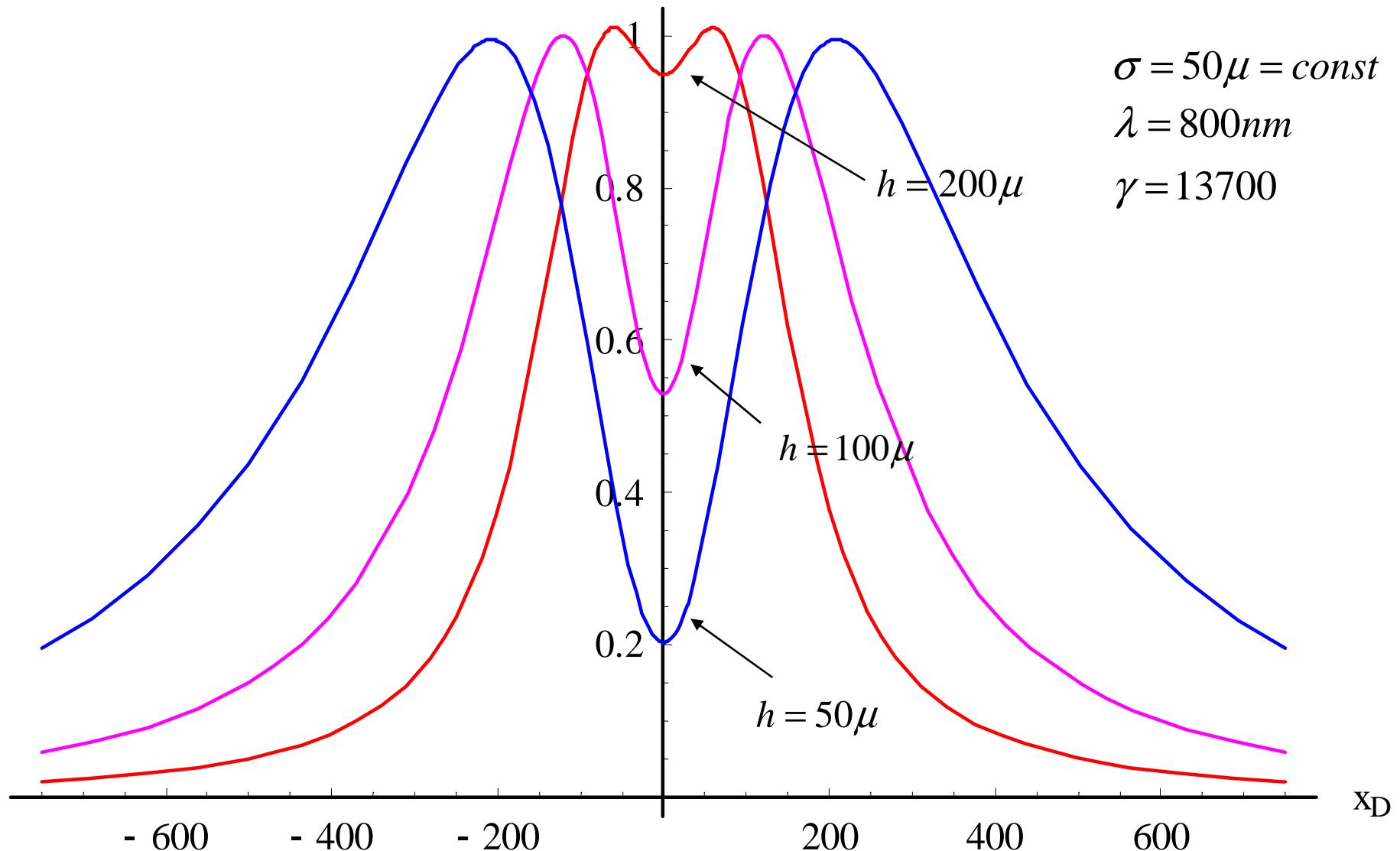


Ratio $R = \frac{I_{\max}^x - I_{\min}^x}{I_{\max}^x + I_{\min}^x}$ as a tool for beam size measurements

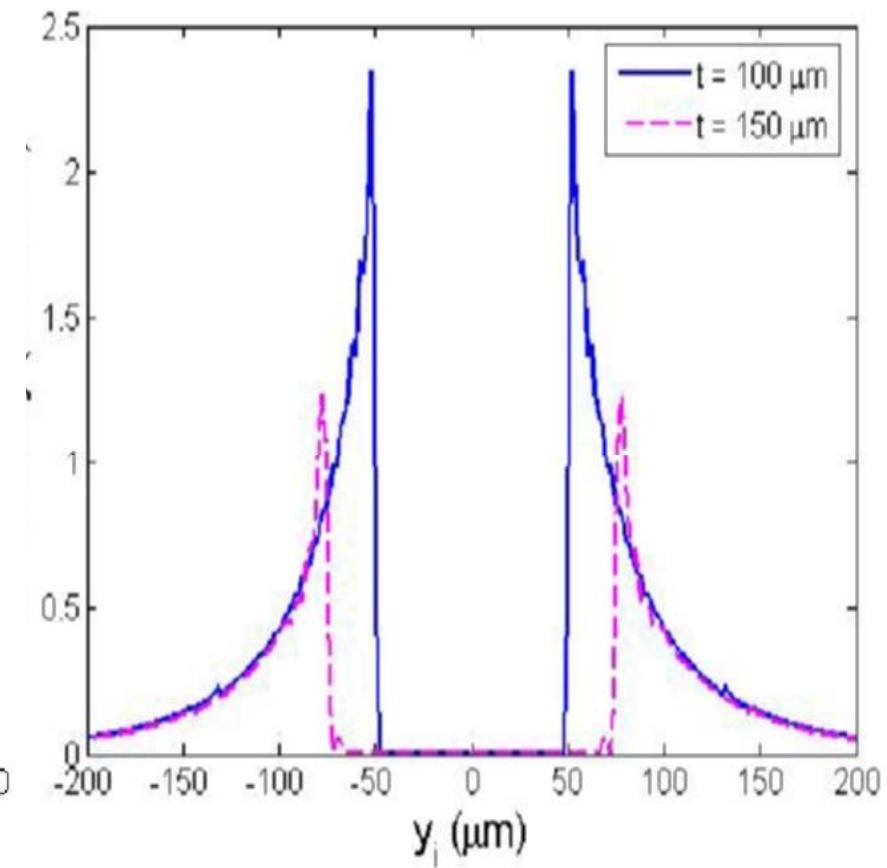
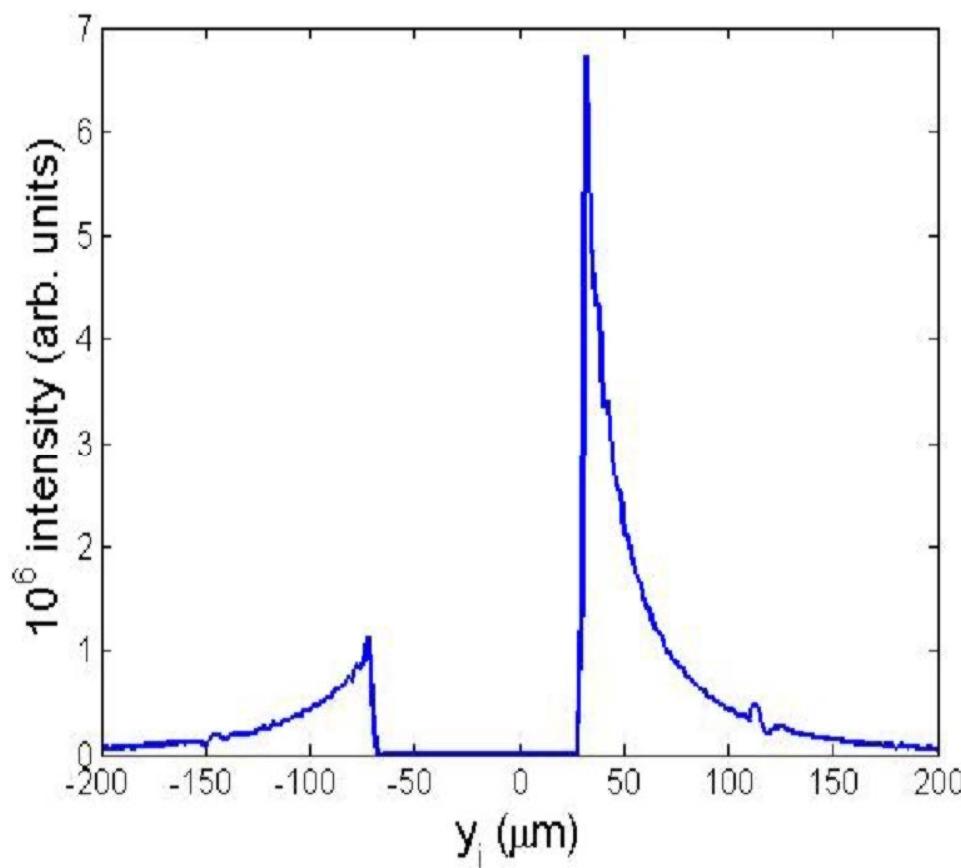


Dependence of x-component image on impact parameter

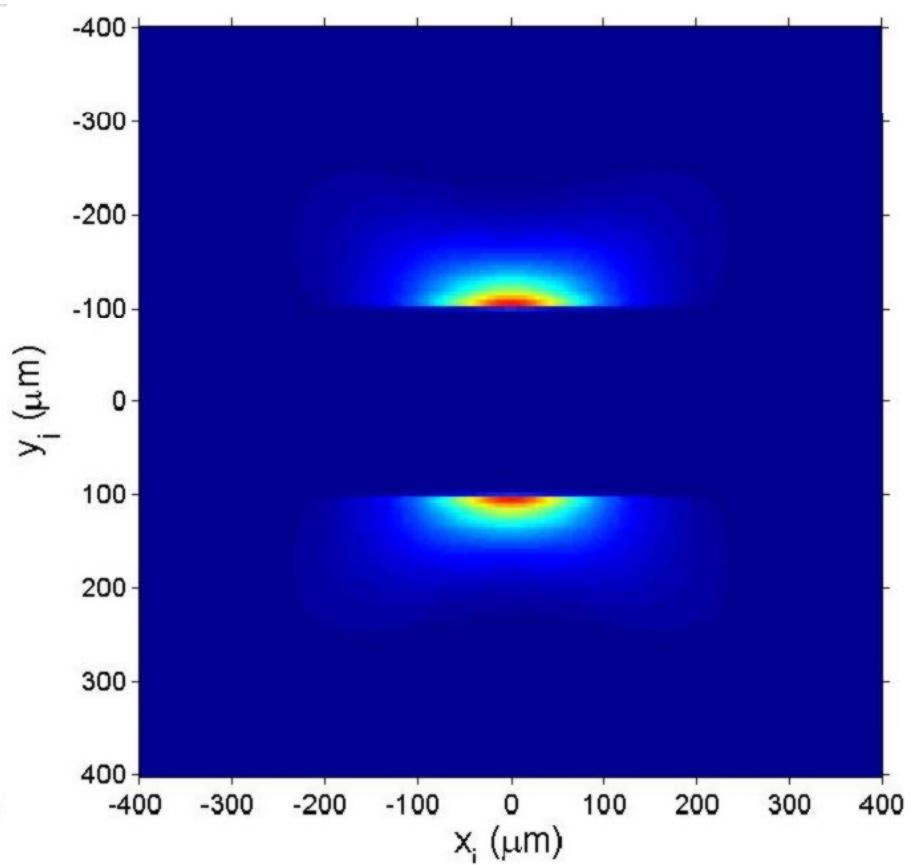
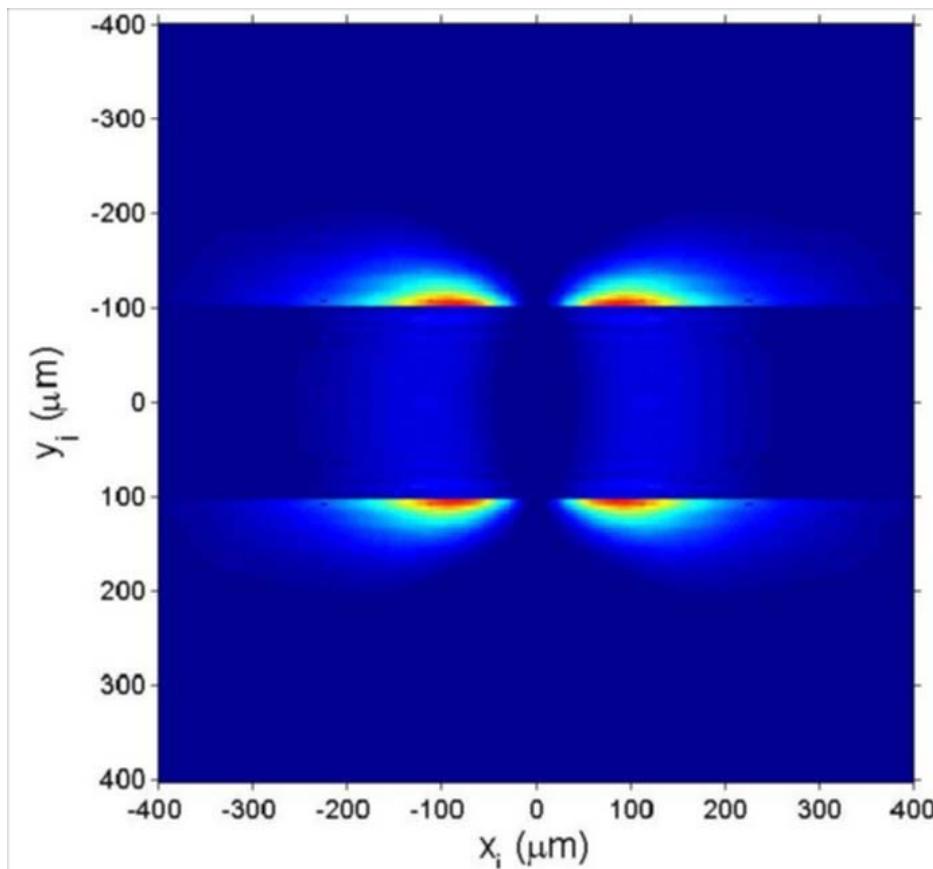
I_x^{D2} , units



ODR imaging of a slit



PSF – x, PSF-y for slit



Conclusion

- 1.The model developed allows to obtain 2D- and 1D-distributions of an ODR intensity on detector as well as distributions of both polarized components for beam with finite transversal sizes.
- 2.The ODR distribution from single electron (point spread function, PSF) is defined by impact parameter h only (if $h \gg \lambda$).
- 3.Polarized components of PSF may provide higher spatial sensitivity in contrast with total PSF.
- 4.The deep shape of polarized ODR x-component depends on a transverse beam size along target edge.
- 5.Measurements of deep "smoothing" allows to achieve a spatial resolution $\sigma_x \ll 0.2H$ (i.e. $\sigma_x \ll 10 \mu m$ for $H \ll 50 \mu m$)
- 6.For impact parameter $h \ll 0.1\gamma\lambda/2\pi$ there may be lost $\sim 60\%$ of a total ODR intensity measuring ODR X-component only.



Thanks for your
attention!

