

# Measurement & Calculation of the Lorentz Detuning for the transient response of the resonant cavity

- ❖ Introduction
- ❖ “Two modes” model
- ❖ Method of the calculation for the transient response
- ❖ Case of Flat-top
- ❖ Comparison between experiment and calculation
- ❖ Piezo Compensation Strategy
- ❖ Next Measurement Plan
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# Introduction

The shape of the resonant cavity is generally deformed by the Lorentz force.



The frequency of the cavity is changed according to the square of the field strength.



The cavity is detuned, and the field may not be constant during the flat-top of the pulse.



It is necessary to compensate or lower the detuning by the Lorentz force.

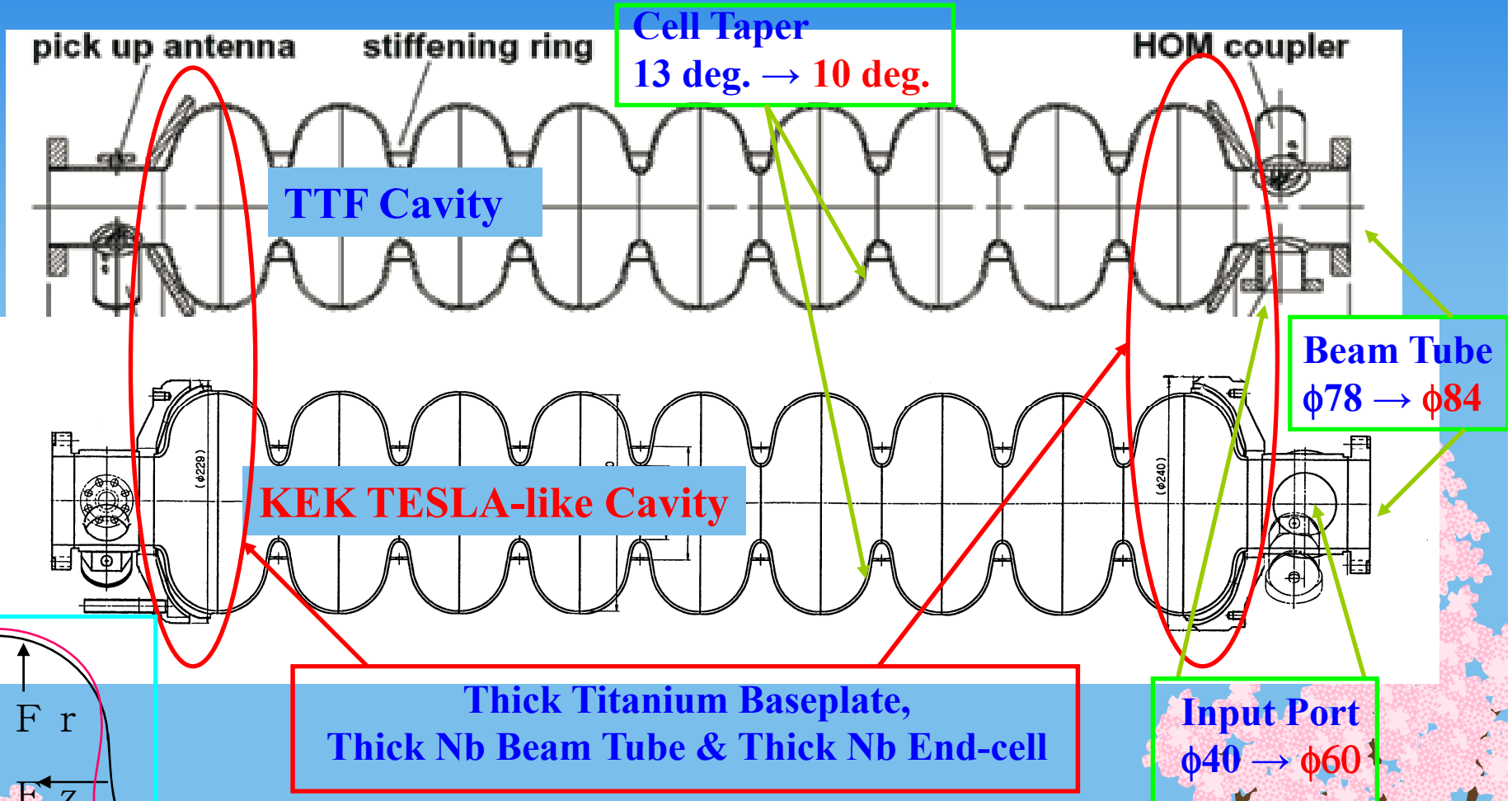


The methods to do it are following...

- (1) Using Piezo
- (2) Putting the initial offset to the cavity frequency
- (3) Increasing the mechanical strength of the cavity support

STF B.L. cavity is mechanically stronger than TESLA's one!

# Improvement in the KEK TESLA-like Cavities



**KEK TESLA-like Cavity**

**Thick Titanium Baseplate,  
Thick Nb Beam Tube & Thick Nb End-cell**

**KEK TESLA-like Cavity**

**TTF Cavity**

**80 kN/mm  
-480 Hz**

**13 kN/mm  
-1050 Hz**

**(31.5 MV/m)**

**Stiffness of Cavity  
Fixing Support  
Lorentz Detuning**

# Mechanical Oscillation (Two Modes Model)

Very roughly speaking, the fast mode is mainly contributed to the Lorentz Detuning before 500 $\mu$ sec and the slow mode after 500  $\mu$ sec.

Oscillation Amplitude ( $X_k$ )

Offset Compensation

Fast mode

Slow mode

Stationary Amplitude

Piezo Compensation

$E_{acc}$

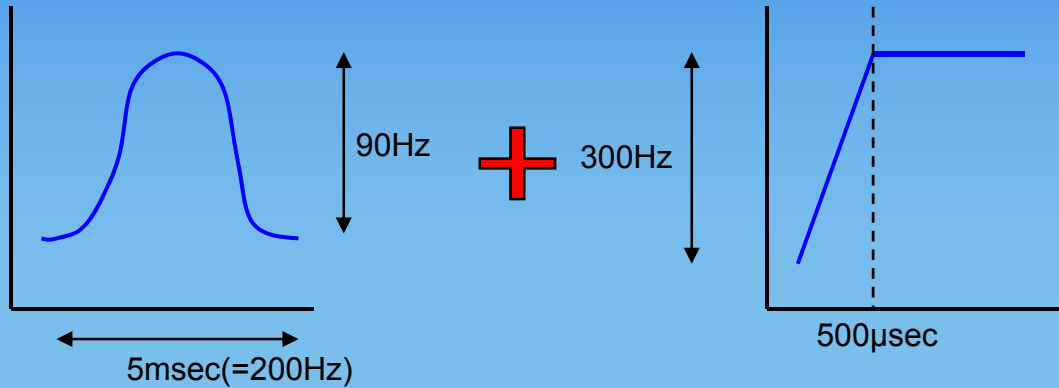
1.5 msec.

Time

The behavior of the filling is considered not to be different between on resonance and the slight detuning.

# Two Modes Model

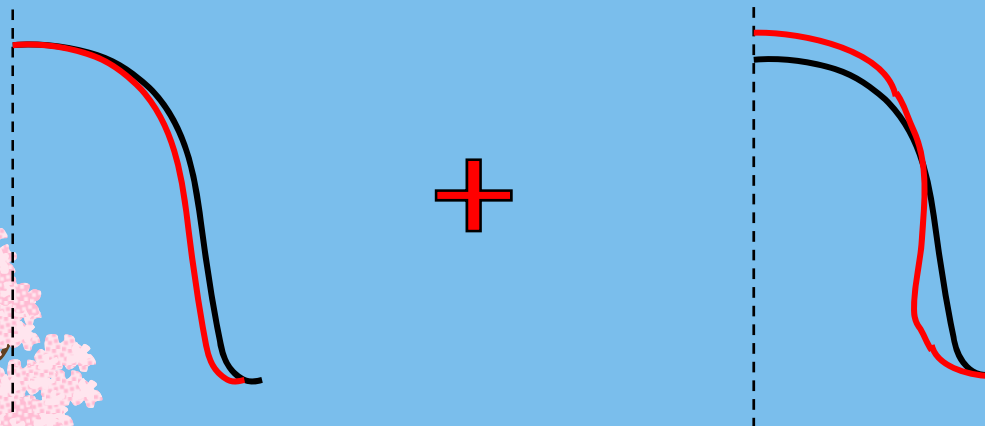
In this model, the Lorentz detuning is generated by two modes. One is the “slow mode” and the other is “fast”.



slow mode  
(sine)

fast mode  
(linear)

In the simulation



From the mechanical calculation

Actually, so many modes exist in 9-cell cavity!  
But, these modes are mainly effective.

# Cavity Voltage Equation

From J. Slater

$$\frac{d^2}{dt^2} V(t) + \left(1 + j \frac{Q_L}{Q_o}\right) \frac{\omega_o}{Q_L} \frac{d}{dt} V(t) + \omega_o^2 V(t) = U(t)$$

$$\tilde{V} = \tilde{V}_d + (\tilde{V}_o - \tilde{V}_d) \exp\left(-\frac{t}{T_F}\right) \exp\left(j \frac{\tan \psi}{T_F} t\right)$$

Equi-angular Spiral

If the factor in each term is constant in time, this equation can be solved analytically.

But, if not so...

# Method of the calculation for the transient response

Within the very short period ( $\Delta t$ ), the following equation is filled and solved analytically.

$$\begin{aligned} \tilde{V}_n &= \tilde{V}_{g,n} + \left( \tilde{V}_{n-1} - \tilde{V}_{g,n} \right) \exp\left(-\frac{\Delta t}{T_F}\right) \exp\left(j \tan \psi_{n-1} \frac{\Delta t}{T_F}\right) \\ &= \tilde{V}_{n-1} \exp\left(-\frac{\Delta t}{T_F}\right) \exp\left(j \tan \psi_{n-1} \frac{\Delta t}{T_F}\right) \\ &\quad + \tilde{V}_{g,n} \left( 1 - \exp\left(-\frac{\Delta t}{T_F}\right) \exp\left(j \tan \psi_{n-1} \frac{\Delta t}{T_F}\right) \right) \\ \tilde{V}_{g,n} &\propto \cos \psi_{n-1} \exp(j \psi_{n-1}) \end{aligned}$$

1  $\mu$  sec

Generally normalized by 1

# Expressions and values for the calculation

## Used expressions

$$\begin{aligned}\tilde{V}_n &= \tilde{V}_{g,n} + (\tilde{V}_{n-1} - \tilde{V}_{g,n}) \exp\left(-\frac{\Delta t}{T_F}\right) \exp\left(j \tan \psi_{n-1} \frac{\Delta t}{T_F}\right) \\ &= \tilde{V}_{n-1} \exp\left(-\frac{\Delta t}{T_F}\right) \exp\left(j \tan \psi_{n-1} \frac{\Delta t}{T_F}\right) \\ &\quad + \tilde{V}_{g,n} \left(1 - \exp\left(-\frac{\Delta t}{T_F}\right) \exp\left(j \tan \psi_{n-1} \frac{\Delta t}{T_F}\right)\right) \\ \tilde{V}_{g,n} &\propto \cos \psi_{n-1} \exp(j \psi_{n-1})\end{aligned}$$

## Used numerical values

filling time :  $T_f = 2Q_L / \omega_0$

$$\tan \Psi = -2Q_L \Delta f / f_0$$

$f_0 = 1300.25 \text{ MHz}$

$Q_L = 1.15 \times 10^6$  (from horizontal test for STF B.L. #3

cavity)

$\Delta t = 1 \mu \text{ sec}$  (sufficiently short)

$\Delta f = \text{sine} + \text{linear}$  ( $t < 500 \mu \text{ sec}$ )

$\Delta f = \text{sine}$  ( $t > 500 \mu \text{ sec}$ )

After 500  $\mu \text{ sec}$ , the fast mode disappears, because the damping is very fast.



# Example of the calculation for the transient response

Input data (frequency)

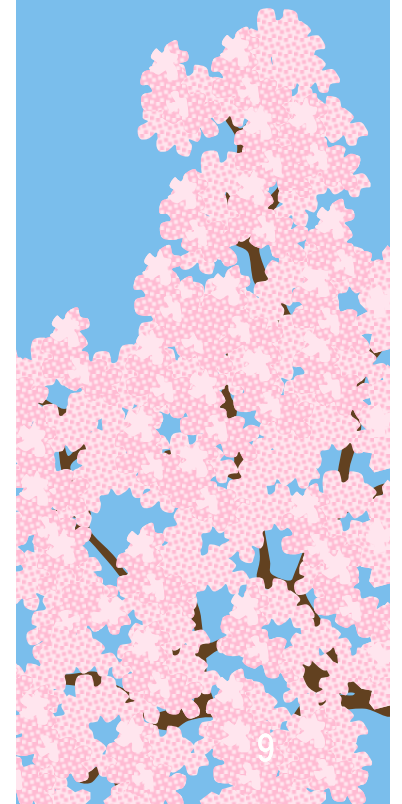
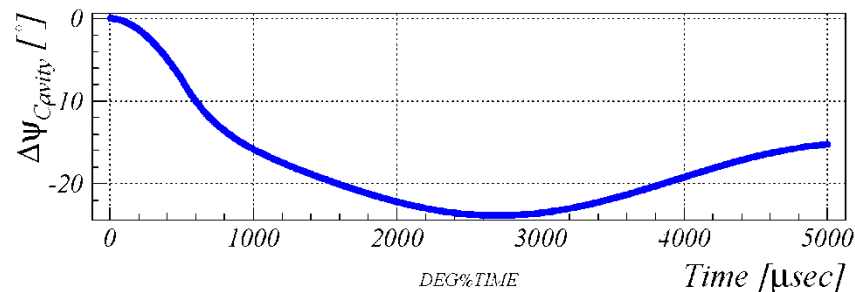
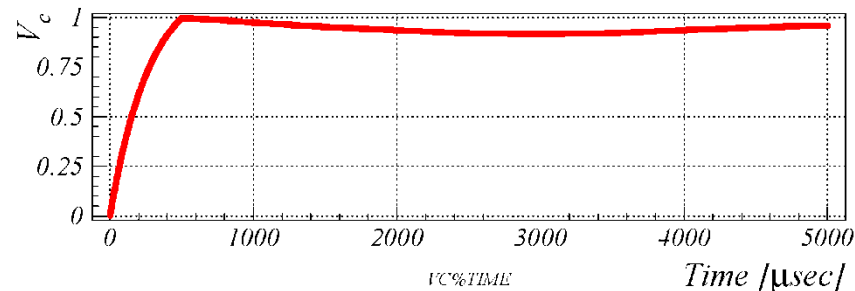
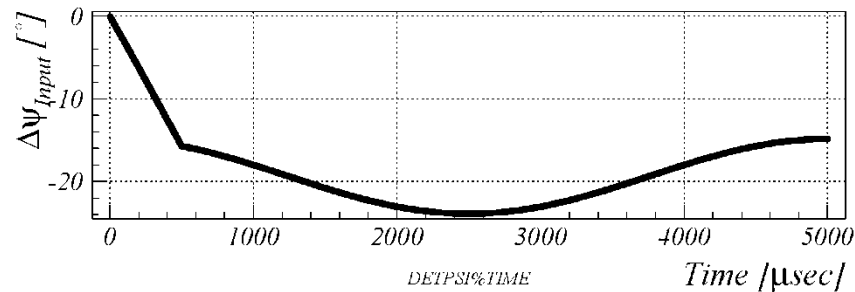
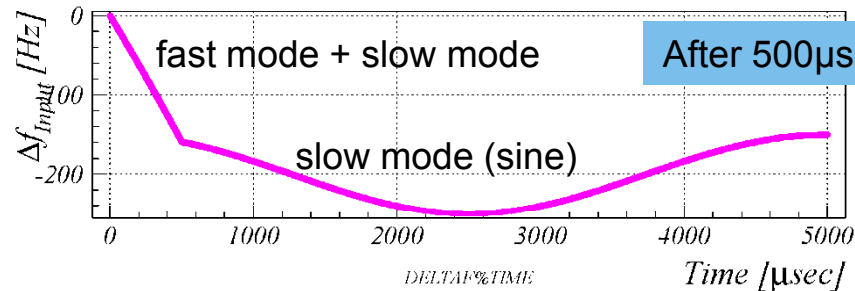
$$\tan \Psi = -2Q_L \Delta f / f_0$$

Input data (degree)

Output data ( $V_C$ )

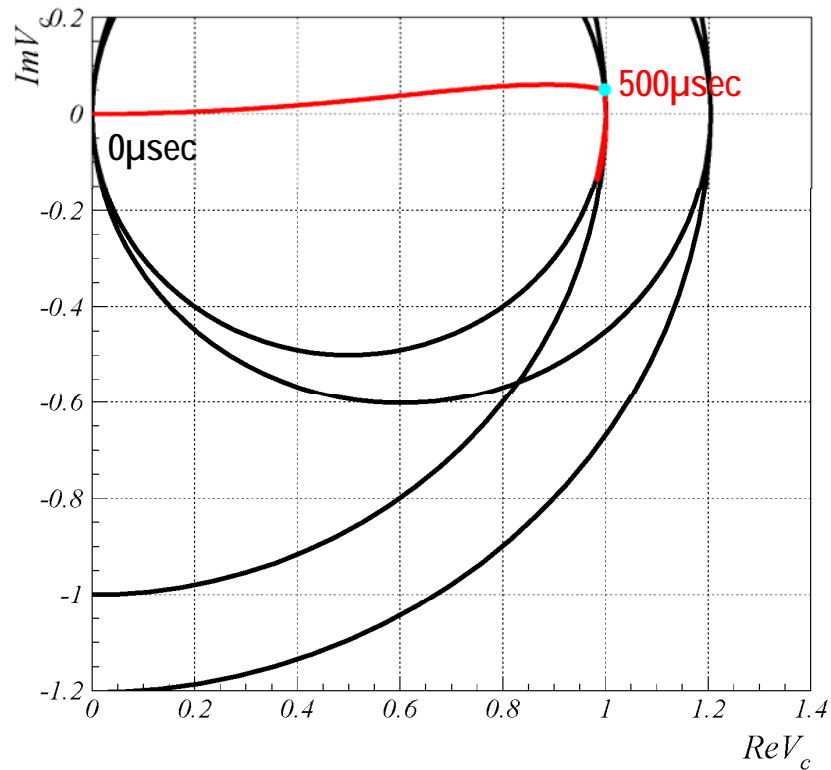
Output data ( $\Psi_{\text{Cavity}}$ )

Time Domain Plot for  $f_{\text{init}}=0\text{Hz}$ ,  $\Delta f_{\text{Input}}=0.3\text{Hz}/\mu\text{sec}$ ,  $-90\text{Hz}/200\text{Hz}$

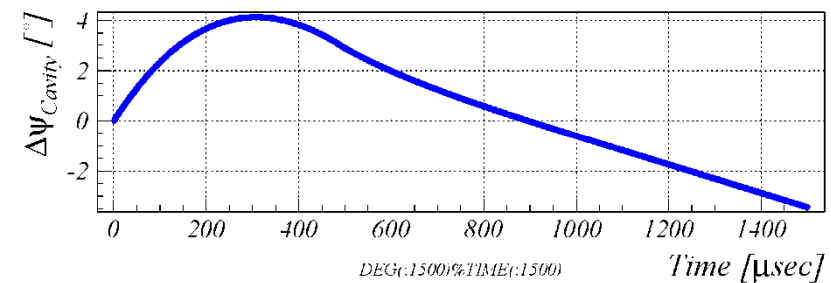
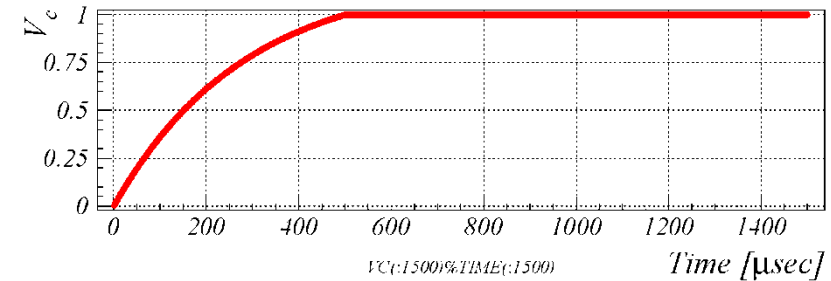
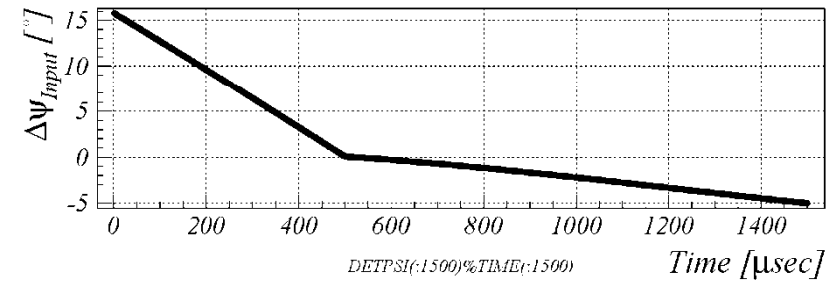
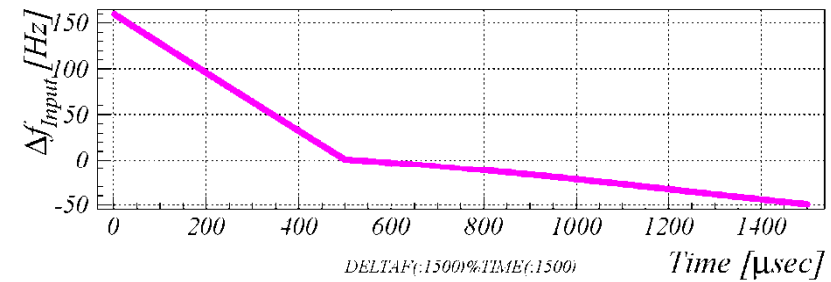


# Case of Flat-top (offset +160Hz, w/o Piezo)

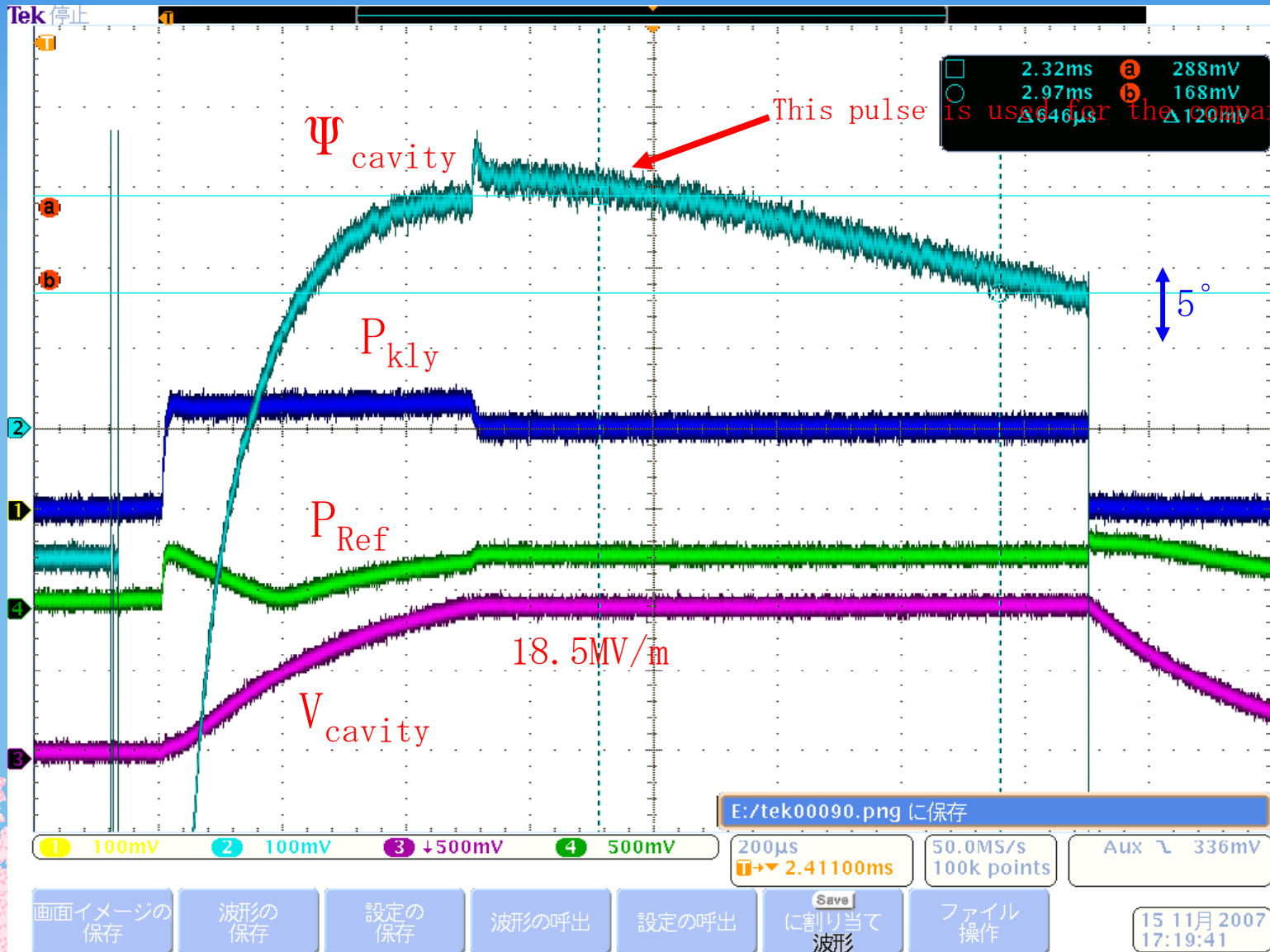
Phaser Diagram for  $f_{init}=-160\text{Hz}$ ,  $\Delta f_{input}=0.3\text{Hz}/\mu\text{sec}$ ,  $-90\text{Hz}/200\text{Hz}$



Time Domain Plot for  $f_{init}=-160\text{Hz}$ ,  $\Delta f_{input}=0.3\text{Hz}/\mu\text{sec}$ ,  $-90\text{Hz}/200\text{Hz}$



# One pulse during High-Power Test (+160Hz Offset, w/o Piezo)



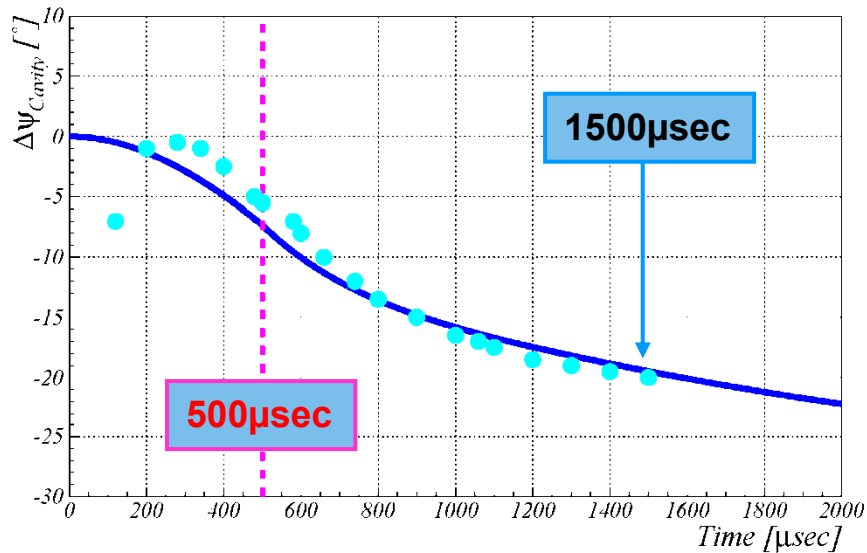
# Comparison between experiment and calculation ①

Preliminary

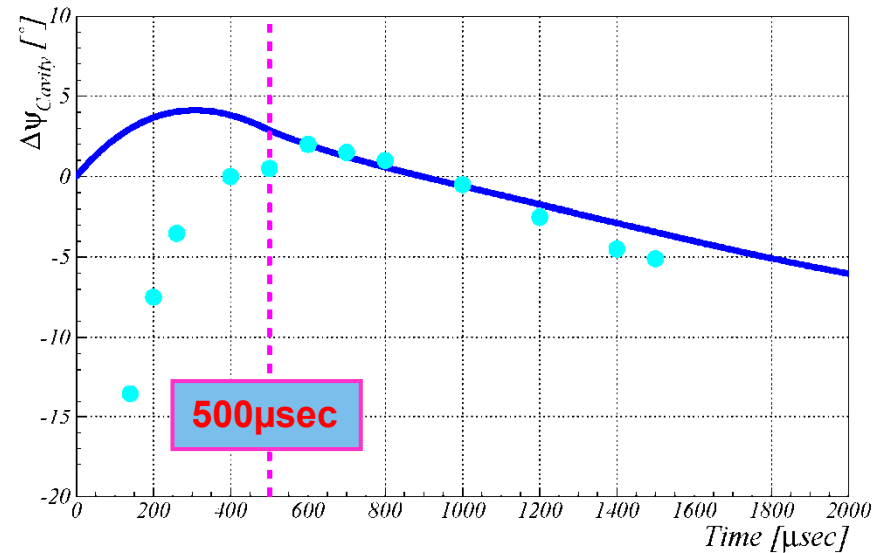
No offset

+160Hz offset

Comparison of Lorentz Detuning between Exp. and Sim.



Comparison of Lorentz Detuning between Exp. and Sim.



Before 500 $\mu\text{sec}$ , the response of the phase detector is probably significant. After that, it is consistent between the experiment and the calculation.

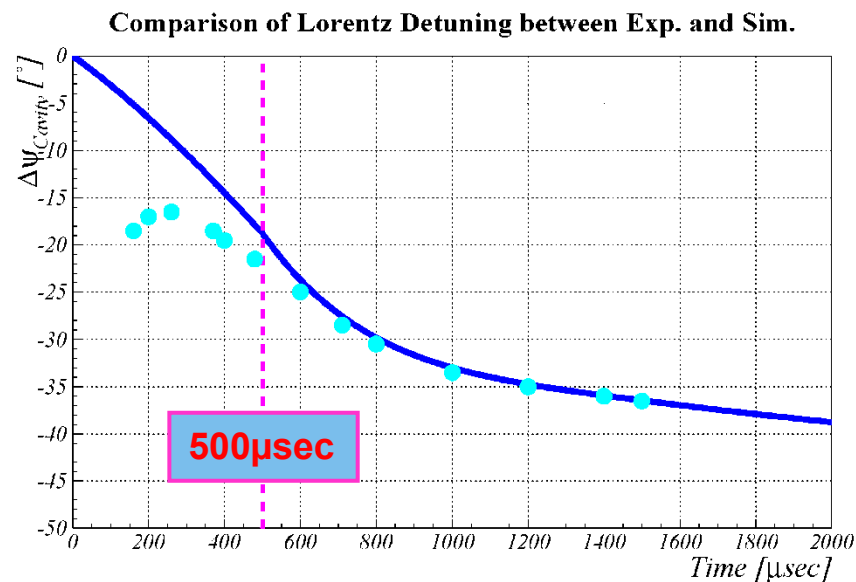
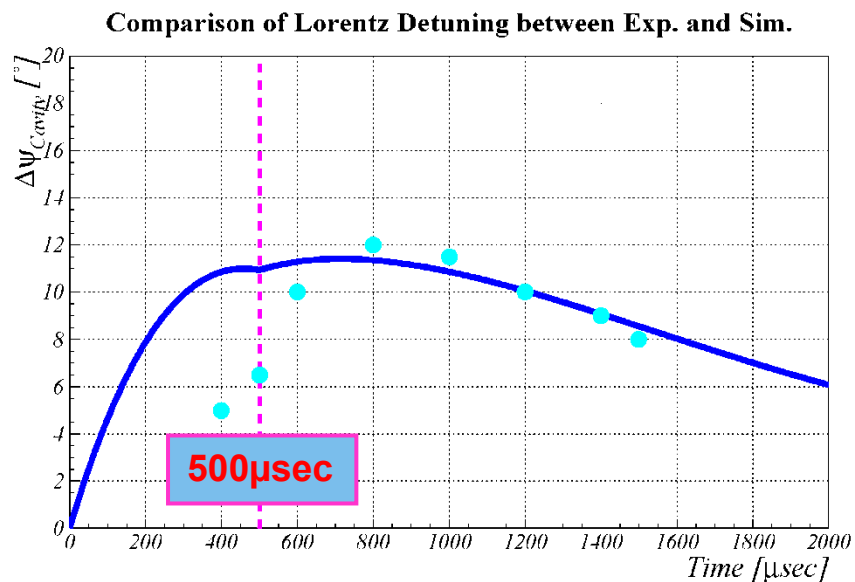
“Two modes model” is valid!

# Comparison between experiment and calculation ②

+300Hz offset

Preliminary

-160Hz offset



“Two modes model” is valid!

For the real operation with Piezo,  
the calculation is modified for a few parameters.

$$E_{\text{acc}} = 18.5 \quad \rightarrow \quad 35\text{MV/m}$$
$$Q_L = 1.15 \times 10^6 \quad \rightarrow \quad 3.00 \times 10^6$$

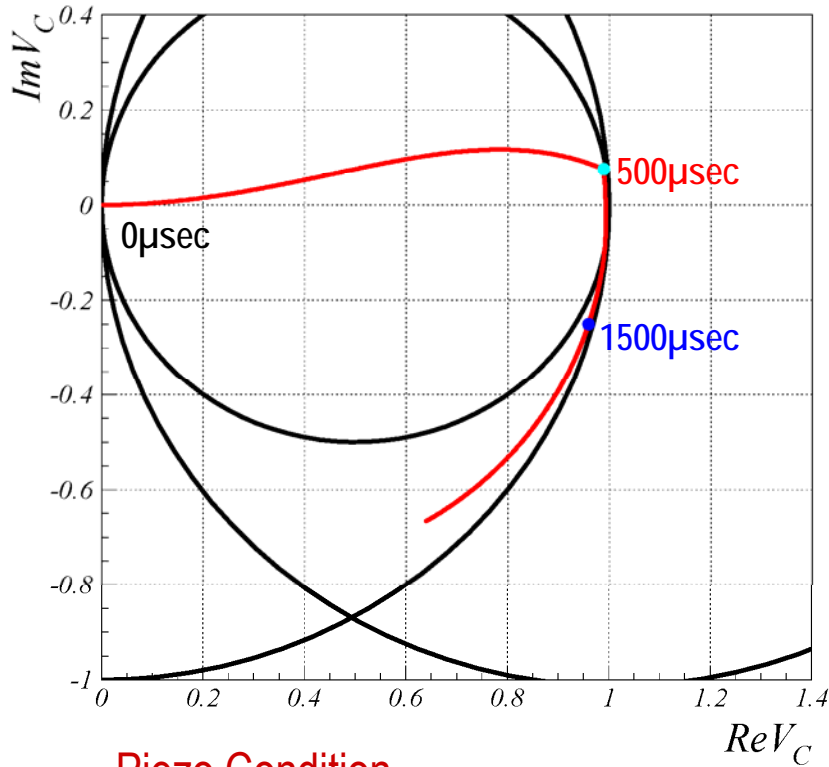
**Sorry! There is not the experimental data around 35MV/m.  
The result around 30MV/m will be obtained in STF Phase-1.0 on June or July.**

# Example of Piezo Compensation (#1)

Preliminary

$Q_L=3.00 \times 10^6$ ,  $f_{orig}=300\text{Hz}$ ,  $\Delta f_{Input}=1.2\text{Hz}/\mu\text{sec}$ ,  $360\text{Hz}/200\text{Hz}$

$Q_L=3.00 \times 10^6$ ,  $f_{orig}=300\text{Hz}$ ,  $\Delta f_{Input}=1.2\text{Hz}/\mu\text{sec}$ ,  $360\text{Hz}/200\text{Hz}$



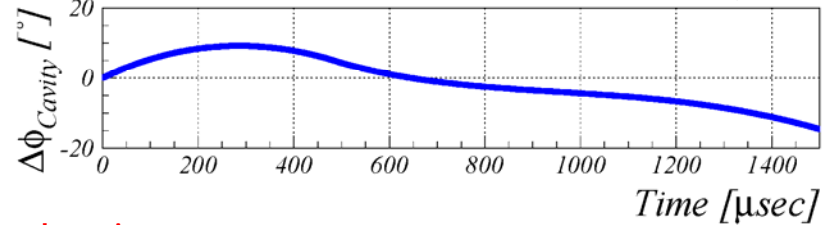
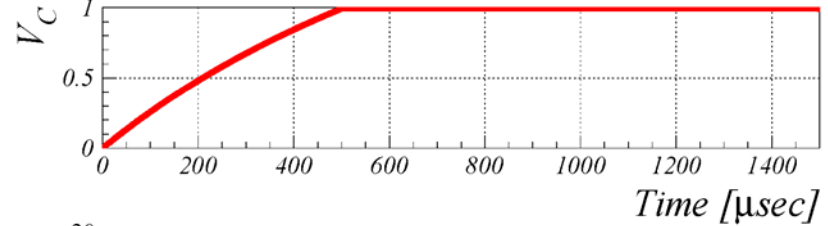
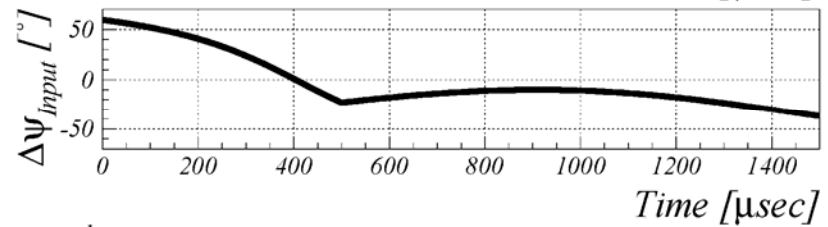
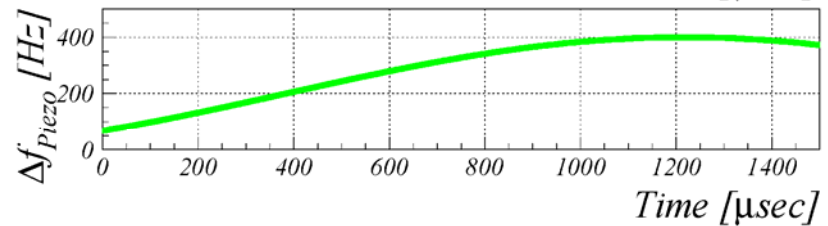
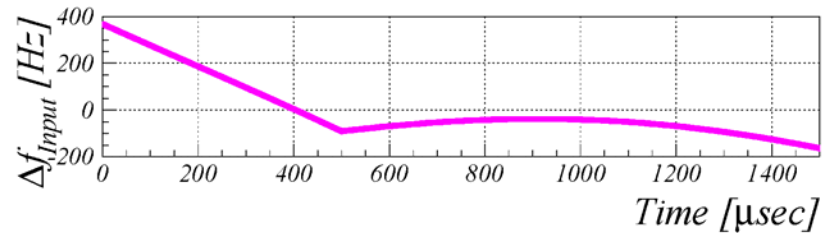
Piezo Condition

Amplitude : 400Hz (300Hz=1μm)

Period : 300Hz

Delay time : -450μsec (fixed!)

Variously changing

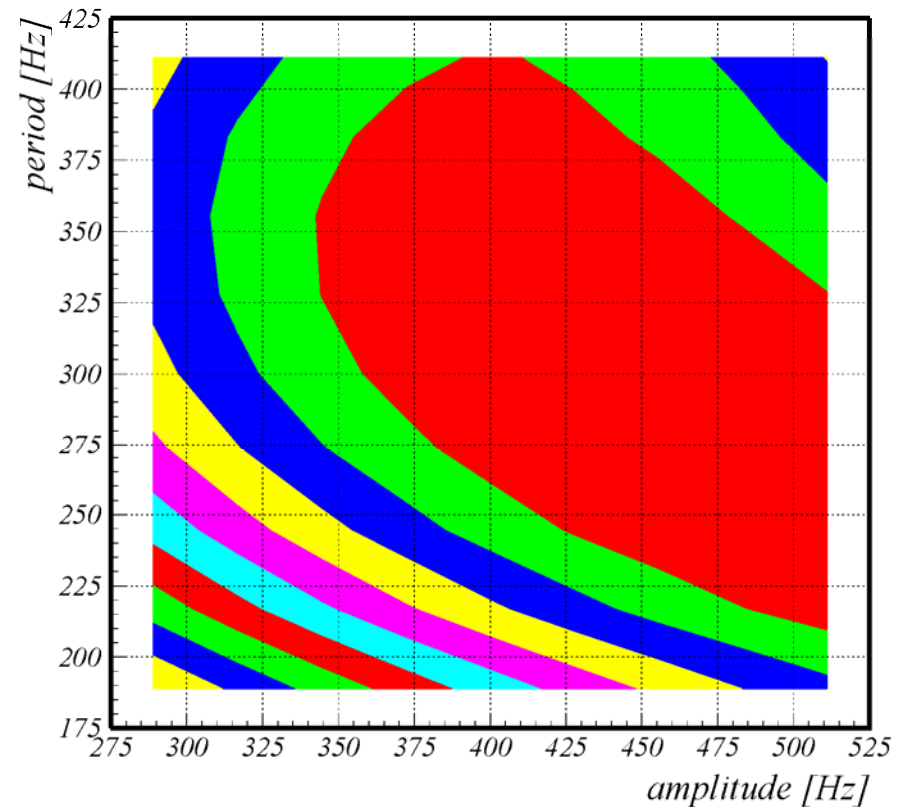
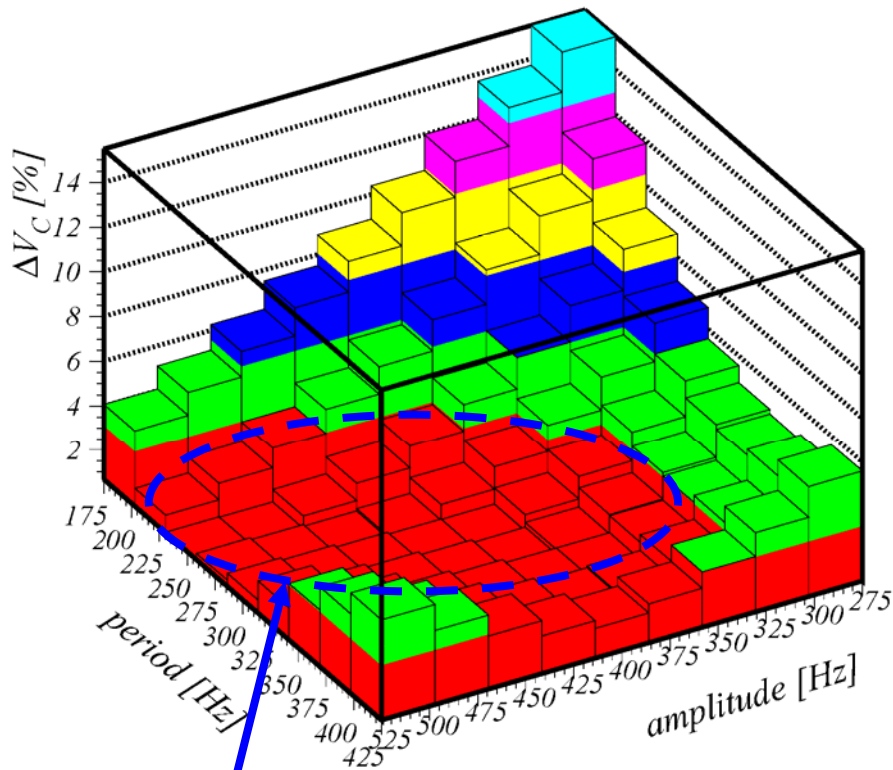


# Criteria of Piezo parameters (#1)

Preliminary

Piezo Criterion at  $E_{acc}=35\text{MV/m}$ ,  $Q_L=3 \times 10^6$ ,  $f_{orig}=300\text{Hz}$ ,  $t_{delay}=-450\mu\text{s}$

Piezo Criterion at  $E_{acc}=35\text{MV/m}$ ,  $Q_L=3 \times 10^6$ ,  $f_{orig}=300\text{Hz}$ ,  $t_{delay}=-450\mu\text{s}$



Good operational region for the stable cavity voltage

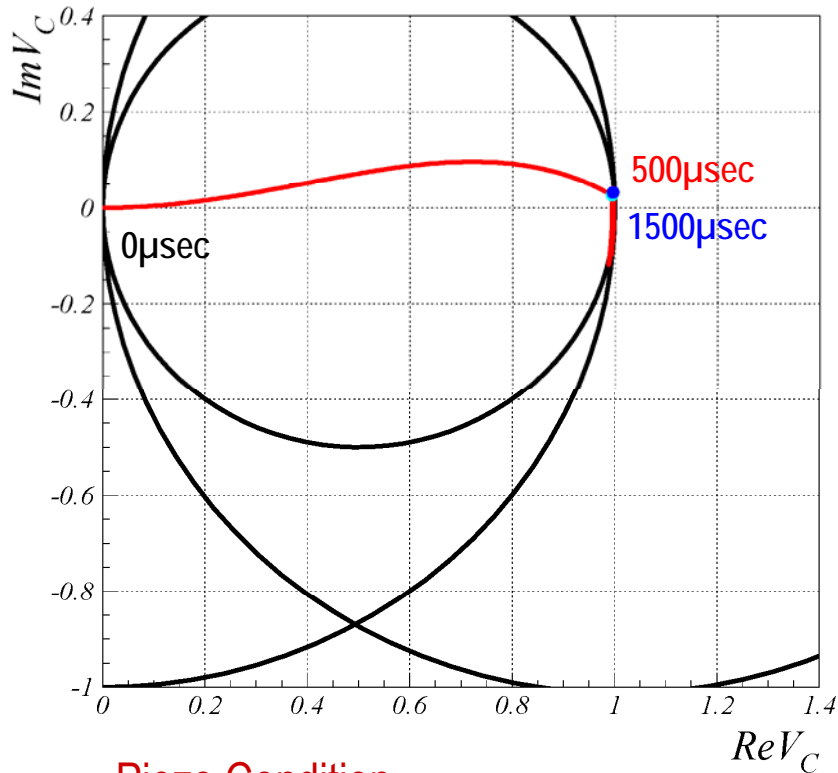


# Example of Piezo Compensation (#2)

Preliminary

$Q_L=3.00 \times 10^6$ ,  $f_{orig}=390\text{Hz}$ ,  $\Delta f_{Input}=1.2\text{Hz}/\mu\text{sec}$ ,  $360\text{Hz}/200\text{Hz}$

$Q_L=3.00 \times 10^6$ ,  $f_{orig}=390\text{Hz}$ ,  $\Delta f_{Input}=1.2\text{Hz}/\mu\text{sec}$ ,  $360\text{Hz}/200\text{Hz}$



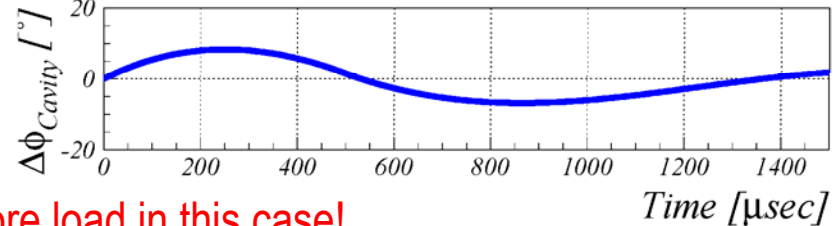
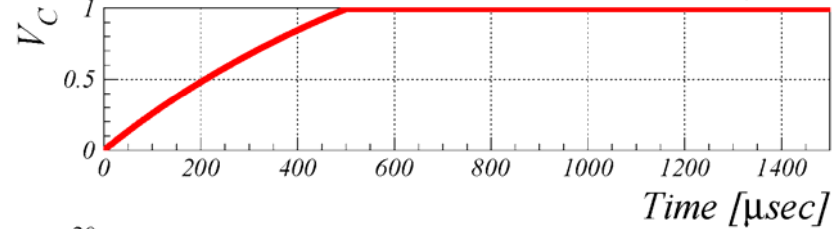
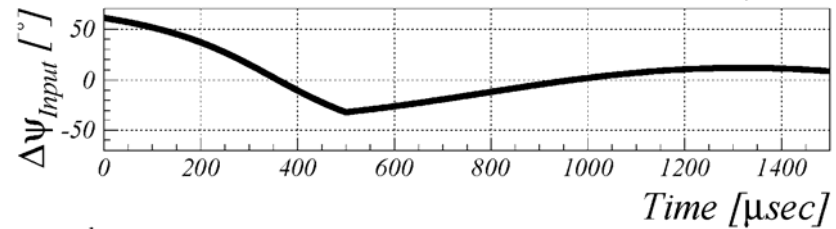
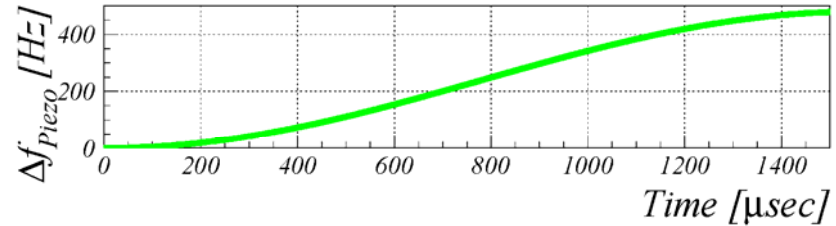
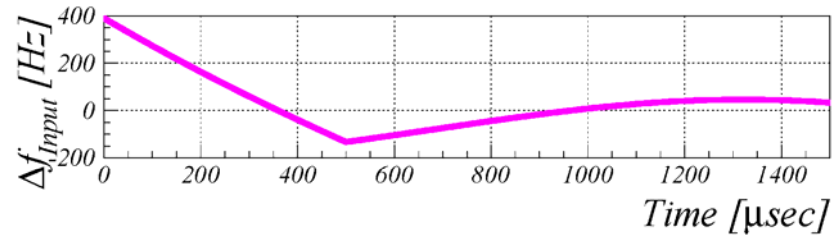
Piezo Condition

Amplitude : 480Hz (300Hz=1μm)

Period : 320Hz

Delay time : 0μsec

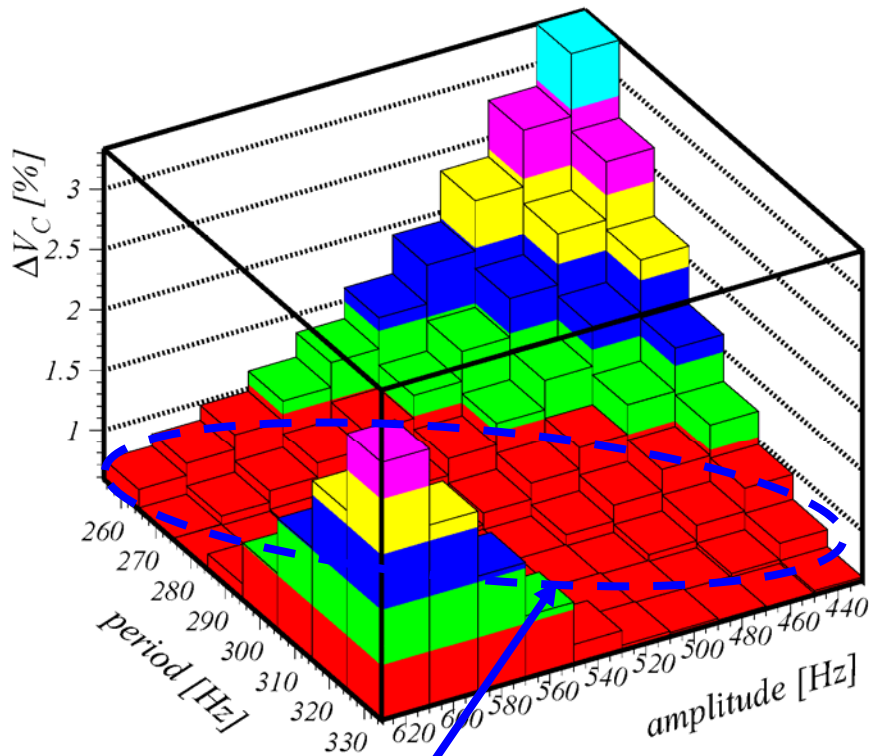
The Piezo is added more load in this case!



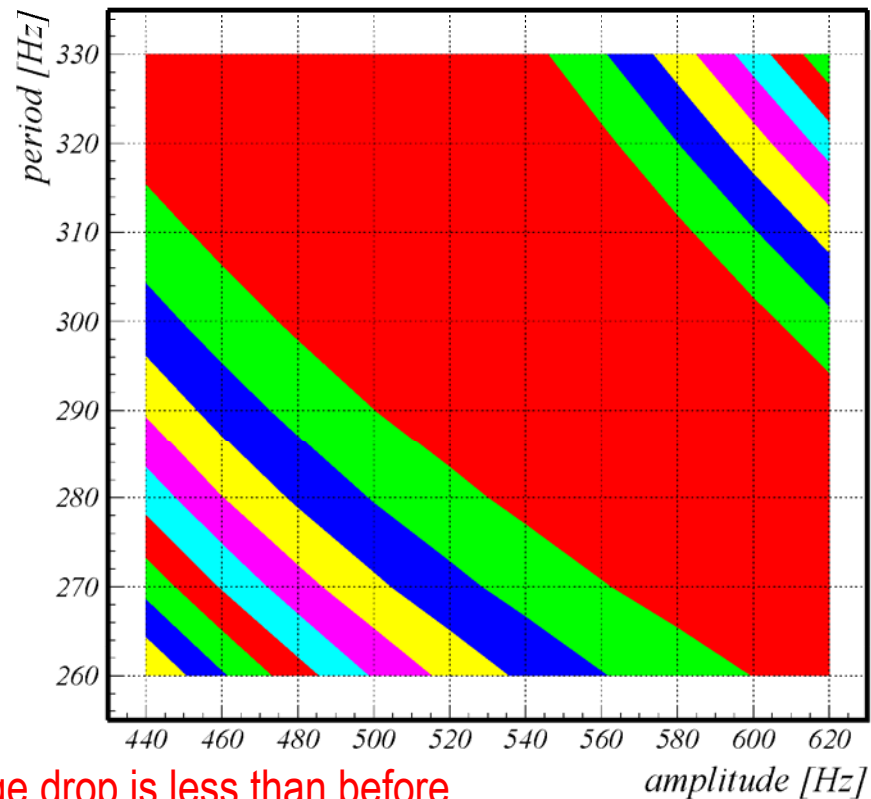
# Criteria of Piezo parameters (#2)

Preliminary

Piezo Criterion at  $E_{acc}=35\text{MV/m}$ ,  $Q_L=3 \times 10^6$ ,  $f_{orig}=390\text{Hz}$ ,  $t_{delay}=0\mu\text{sec}$



Piezo Criterion at  $E_{acc}=35\text{MV/m}$ ,  $Q_L=3 \times 10^6$ ,  $f_{orig}=390\text{Hz}$ ,  $t_{delay}=0\mu\text{sec}$



Good operational region  
for the stable cavity voltage

In this case, the voltage drop is less than before,  
but the added load to the Piezo is larger!

This may cause the breakdown of the Piezo or the lifetime may be shorter.

And, the cavity phase should be also considered!

# Next Measurement Plan

## ❖ Comparing between two types of Piezo actuator

### ❖ High voltage type

– 40 $\mu$ m/1000V@Room Temp. (2 $\mu$ m/1000V@2K)

### ❖ Low voltage type

– 20 $\mu$ m/200V@Room Temp. (? $\mu$ m/1000V@2K)

300Hz/ $\mu$ m for  $\Delta f_{\text{cavity}}$

## ❖ Measurement of the Lorentz detuning around 30MV/m

❖ STF #2 B.L. cavity achieved 29.4MV/m in the V.T.

## ❖ Measurement of the detuning angle during the RF decay

❖ This was already demonstrated in the horizontal test of LL cavity.

## Cavity voltage control using Piezo

❖ If the cavity voltage is dropped, the Piezo may work for the control.

## Checking the response of the phase detector

# Suggestion to the compensation method for the Lorentz Detuning

- ❖ Put the **initial offset** for the cavity frequency
  - ❖ During the filling time, the cavity frequency is gradually decreased by the Lorentz force.
- ❖ Work Piezo with the **small load**
  - ❖ Avoid the breakdown of the Piezo by the larger load
  - ❖ Longer lifetime of Piezo
- ❖ Increase the **mechanical strength** of the cavity support
  - ❖ It is difficult to deform the cavity.

# Summary

- ❖ “Two modes model” is valid for the transient response of the STF B.L. #3 cavity in the horizontal test at STF Phase-0.5.
- ❖ It is effective to increase the mechanical strength of the cavity support structure for the reduction of the Lorentz detuning.
- ❖ It is similarly effective to set the initial offset to the cavity frequency around the high field.
- ❖ In STF Phase-1.0, we will compare between the experimental data around 30MV/m and the simulation.

We will re-examine “two modes model” for more optimization.

# Backup Slides

SCRF Meeting @FNAL 21-25/Apr/2008

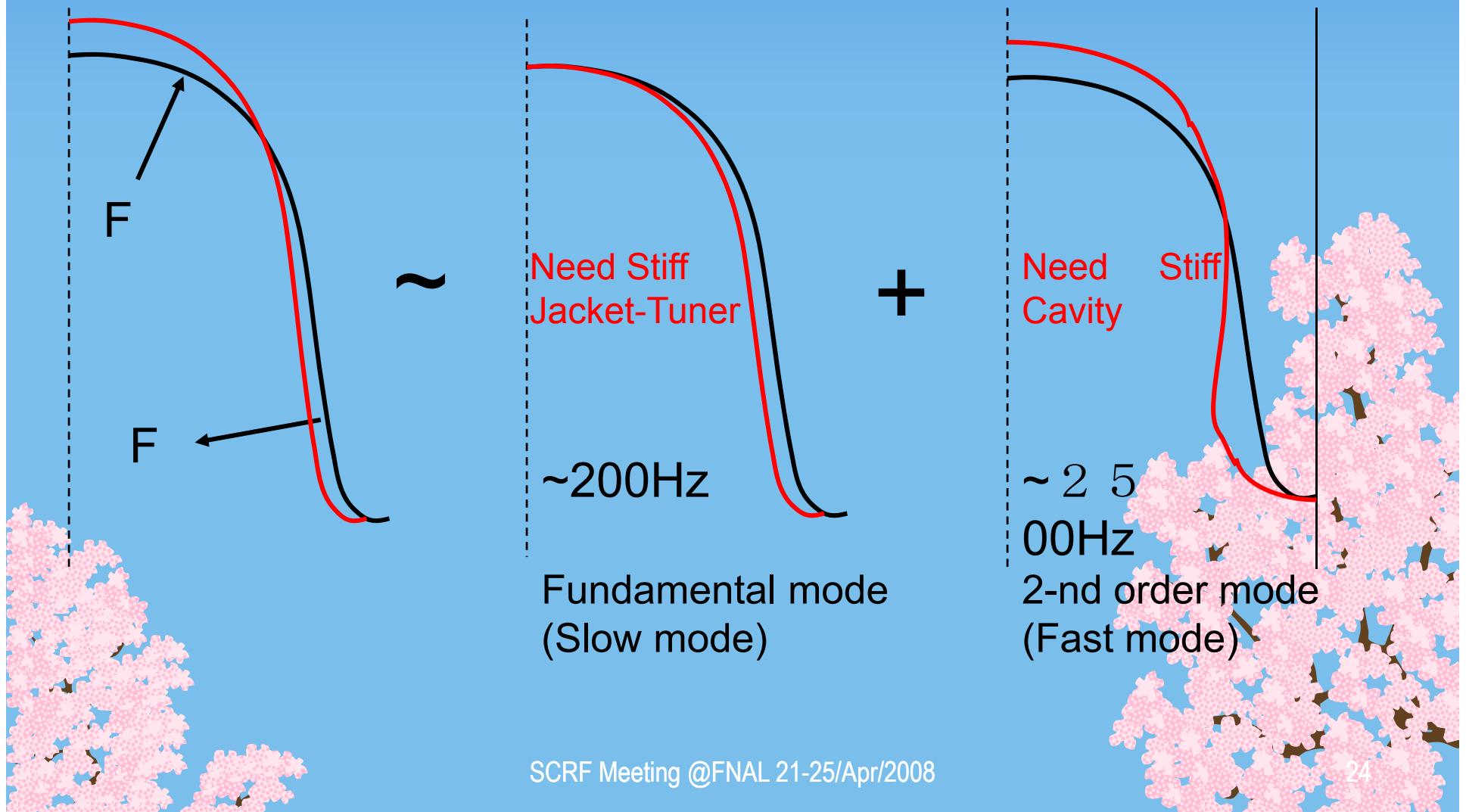
# Mechanical Detuning Equation

$$x(s, t) = \sum_k x_k(s, t); \quad F = \sum_k F_k$$

$$\frac{d^2 x_k}{dt^2} + \frac{\omega_k}{Q_k} \frac{dx_k}{dt} + \omega_k^2 x_k = \frac{F_k}{m_k}$$

It is expected that there are **two modes** from the calculation of the mechanical oscillation. One is the **fast** mode and the other is **slow**.

# Two Dominant Mechanical Modes

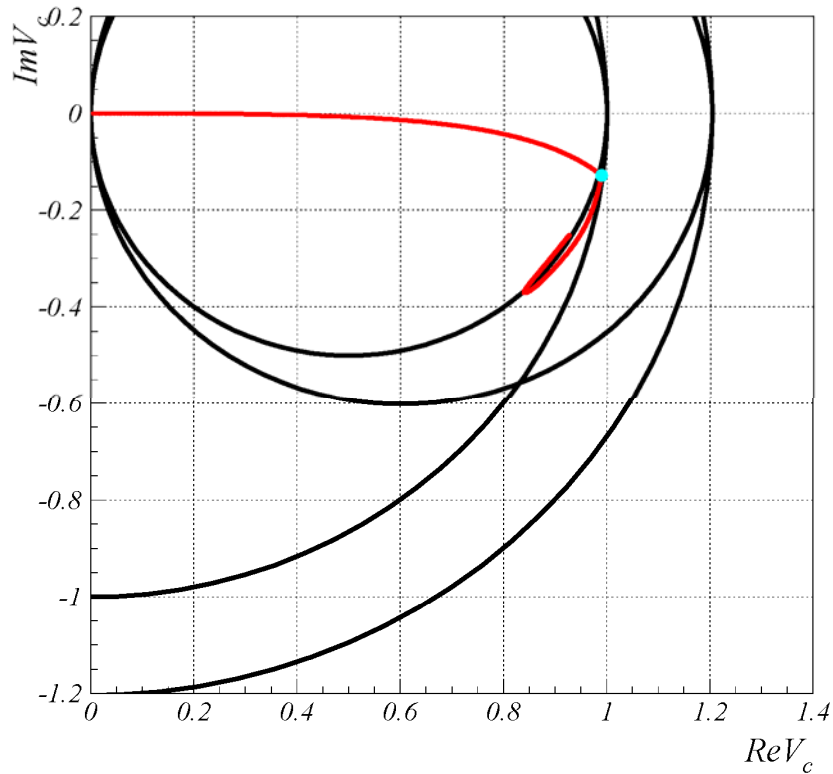




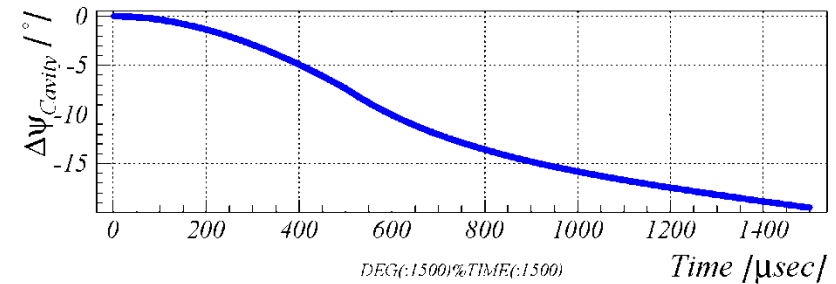
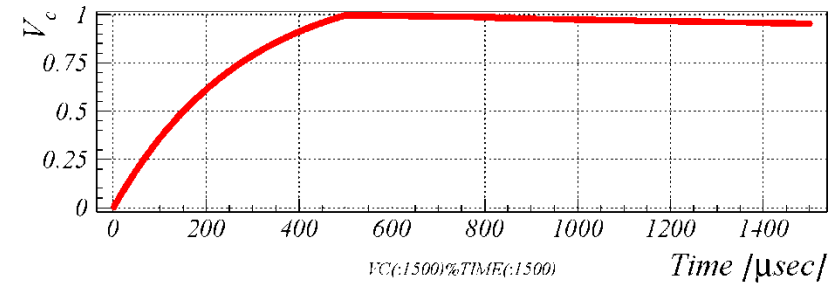
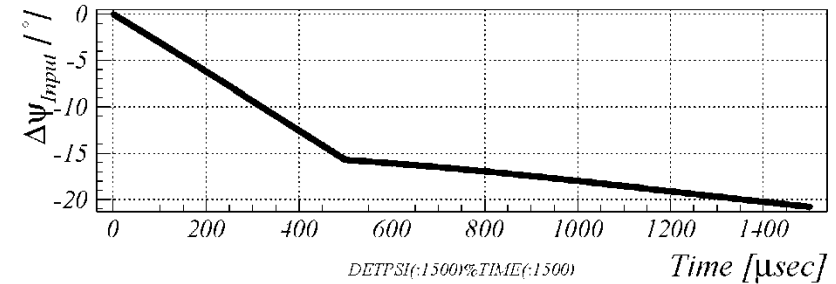
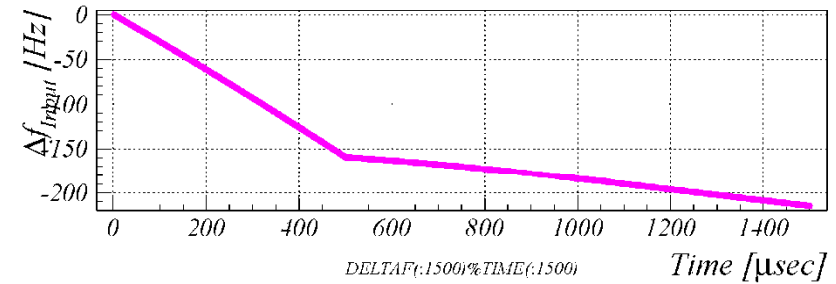
# Case of Flat-top ① (no offset)

## Phaser diagram

Phaser Diagram for  $f_{init}=0\text{Hz}$ ,  $\Delta f_{Input}=0.3\text{Hz}/\mu\text{sec}$ ,  $-90\text{Hz}/200\text{Hz}$

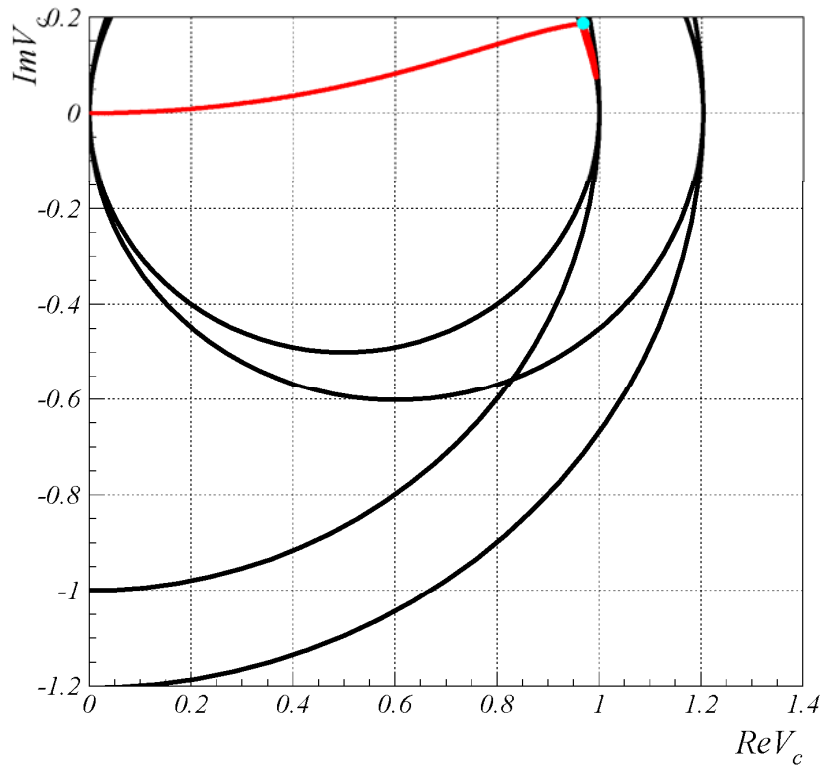


Time Domain Plot for  $f_{init}=0\text{Hz}$ ,  $\Delta f_{Input}=0.3\text{Hz}/\mu\text{sec}$ ,  $-90\text{Hz}/200\text{Hz}$

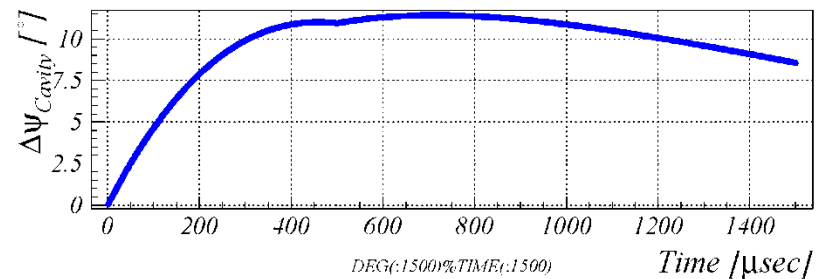
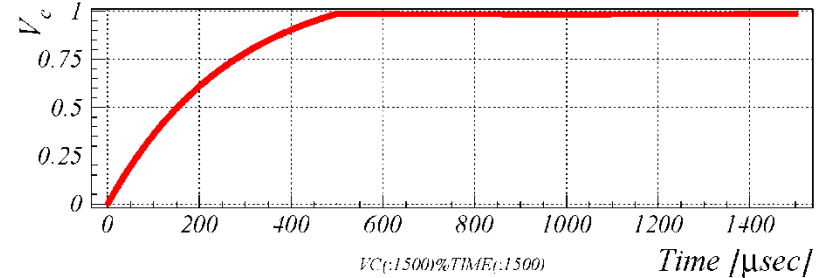
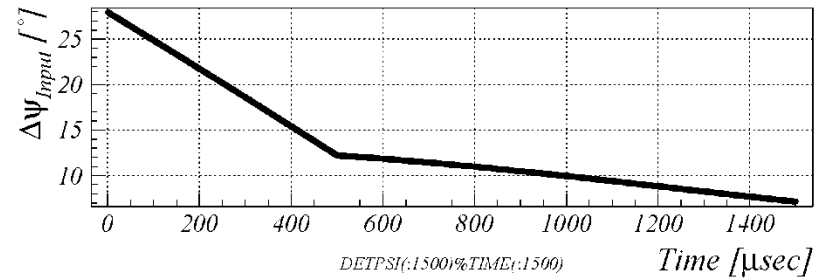
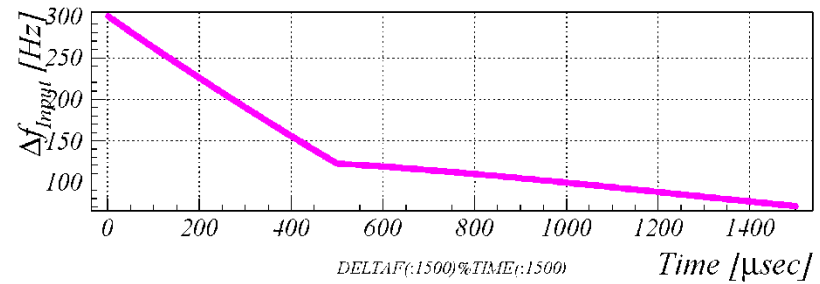


# Case of Flat-top ③ (offset +300Hz)

Phaser Diagram for  $f_{init} = -300\text{Hz}$ ,  $\Delta f_{Input} = 0.3\text{Hz}/\mu\text{sec}$ ,  $-90\text{Hz}/200\text{Hz}$

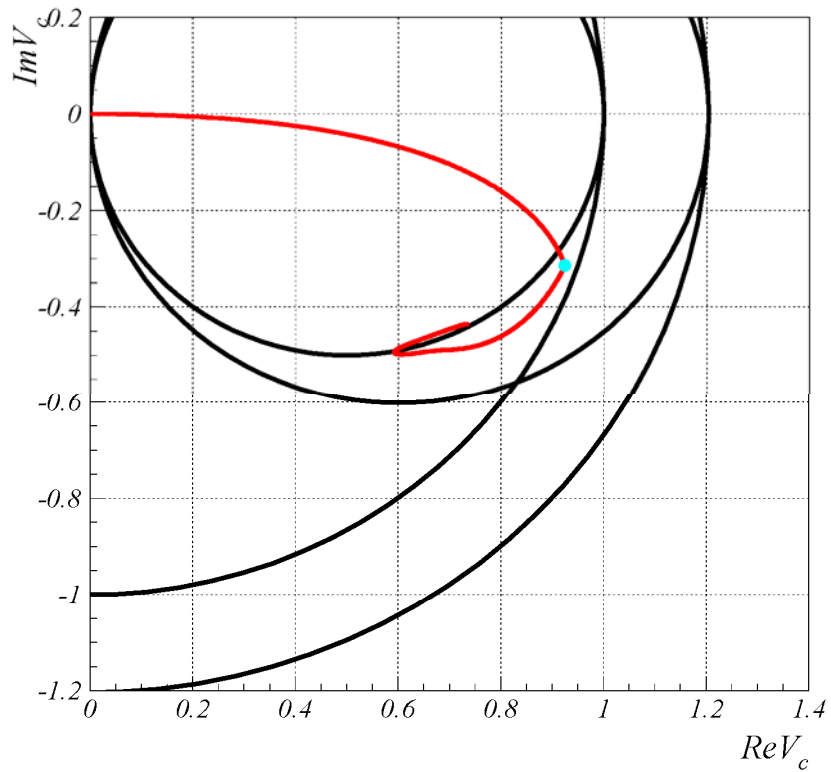


Time Domain Plot for  $f_{init} = -300\text{Hz}$ ,  $\Delta f_{Input} = 0.3\text{Hz}/\mu\text{sec}$ ,  $-90\text{Hz}/200\text{Hz}$

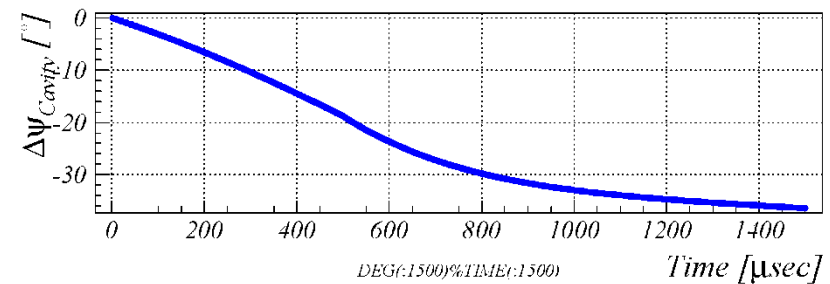
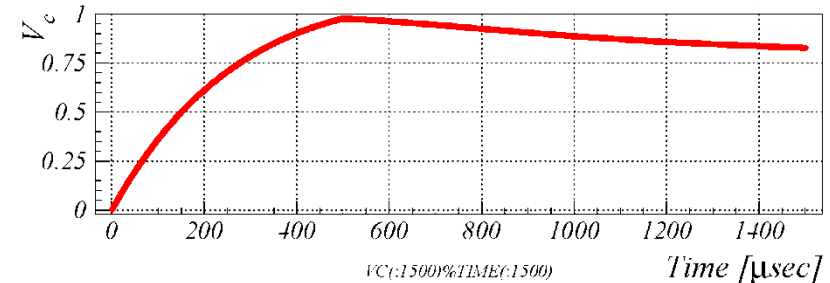
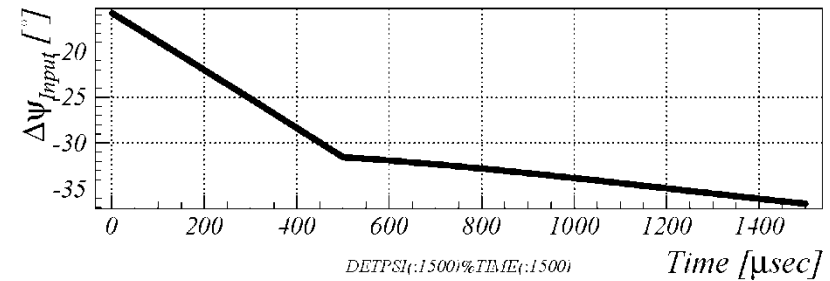
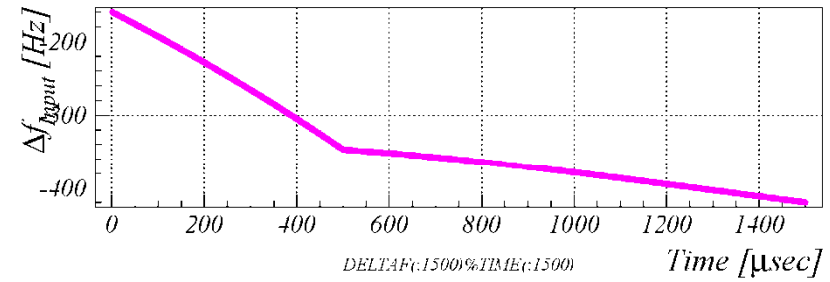


# Case of Flat-top ④ (offset -160Hz)

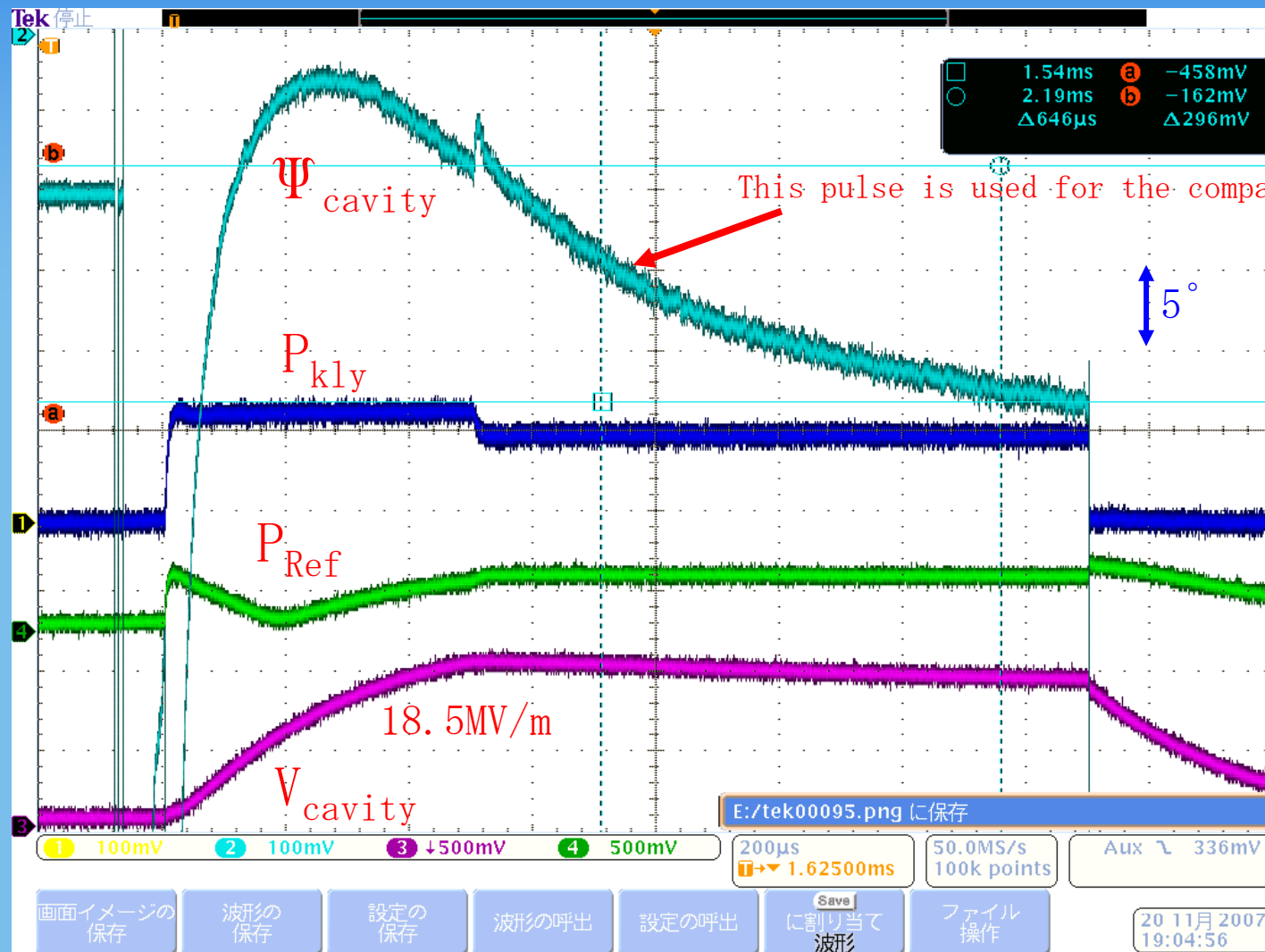
Phaser Diagram for  $f_{init}=+160\text{Hz}$ ,  $\Delta f_{input}=0.3\text{Hz}/\mu\text{sec}$ ,  $-90\text{Hz}/200\text{Hz}$



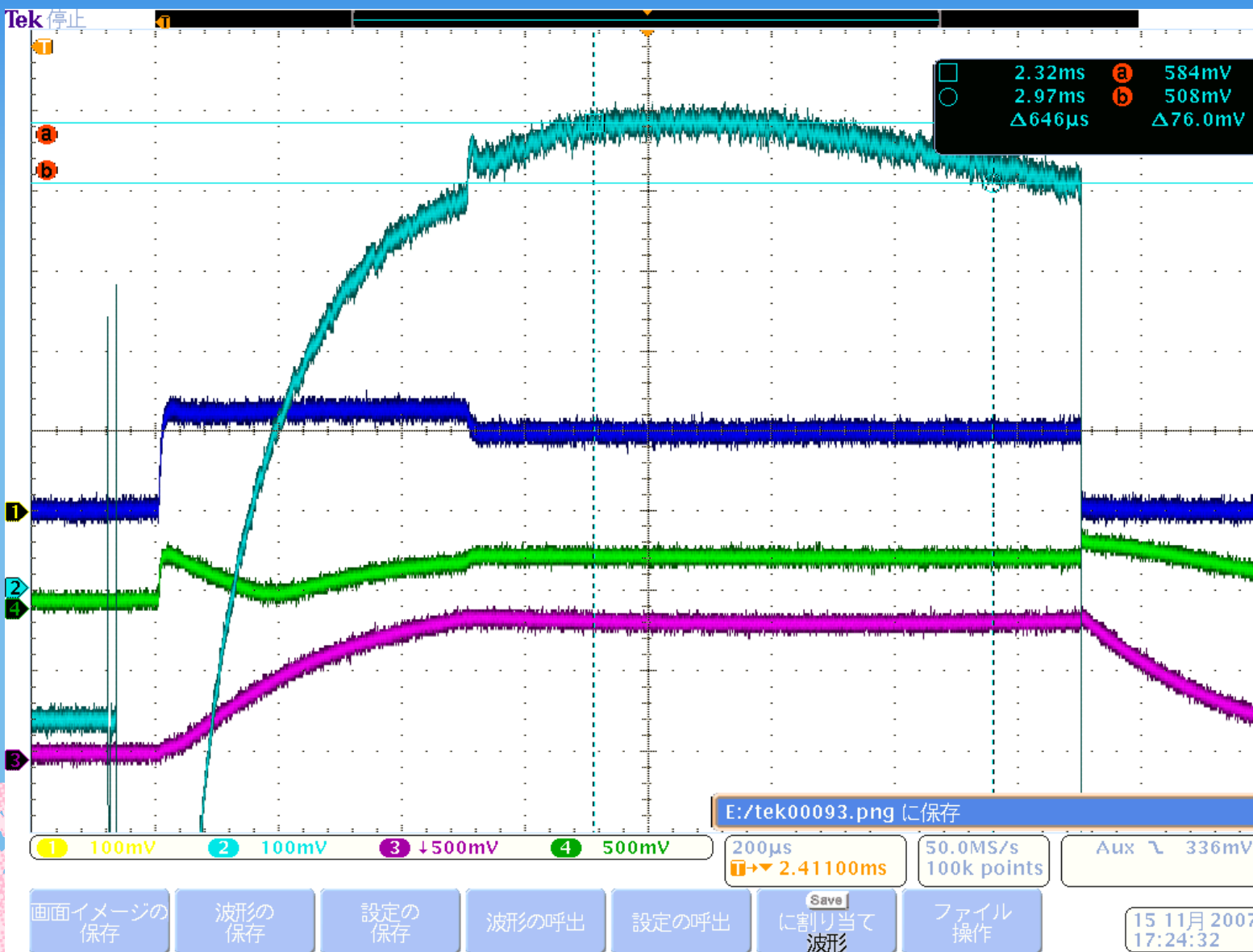
Time Domain Plot for  $f_{init}=+160\text{Hz}$ ,  $\Delta f_{input}=0.3\text{Hz}/\mu\text{sec}$ ,  $-90\text{Hz}/200\text{Hz}$



# One pulse during High-Power Test (No Offset)



# One pulse during High-Power Test (+300Hz Offset)



# One pulse during High-Power Test (-160Hz Offset)

