5K or not? & TTF module thermal modeling update

Paolo Pierini, Serena Barbanotti INFN Sezione di Milano

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Loads on the 5 K shield

surface for thermal

strapping with small braids



From Webex SCRF meeting on 5 K shield removal

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5 K shield removal: what happens @ 2K?

- From Tom Cryo spreadsheet (Feb07)
 - 2K: 11.4 (1.7 s + 9.7 d) @ 700 W/W
 - 5K: 15.0 (10.6 s + 4.4 d) @ 200 W/W
 - 40K: 153.5 (59.2 s + 94.3 d) @ 16 W/W
 - Sum 14.4 kW plug power for each module (no overcapacity)
- If all 5K load goes into 2K "as is"
 - Plug power increased by 56%
 - Need to provide same efficient radiation shield for the 2K mass, with at least 10 layers MLI protecting the 2K cold mass
- If only radiation flow into 2K (consider factor 2 increase for worse MLI protection) and all conduction intercepted
 - Plug power increased by 15%
 - 5K thermalization for 3 posts, 8-9 couplers, HOM, leads, cables

From Webex SCRF meeting on 5 K shield removal

Operation vs Capital

- Range of effect on plug power (operation cost) is 15% to 55% without redesigning cross section
 - optimistic conditions given the many penetrations that the module has to the 2 K environment, and located at different positions along the transverse section (support at top, couplers to the side)
 - Bulky braids?
 - We need anyway a 5K cryo circuit for 90% of the conduction heat removal



Type I--III

- "Historical" note: One of the most effective cost reduction stategies from generation I to generation II was the elimination of the many braids to perform the shield thermalization
- Sometimes changes that seem minor have heavy implications later in terms of complexity or cost
 - e.g. discussions yesterday/today of modules plug compatibility between regions
 - changes in the shield geometry from TypeII+ to XFEL proto

Example: Type III+ modification



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TTF Thermal analysis with ANSYS

- We did transient thermal analysis 12 years ago on shields only
- Serena developed an ANSYS model for static and transient thermal behavior aimed at
 - static and transient heat loads,
 - thermal gradients on the internals during transient, ...
 - comparison of different cooling procedures
- Opportunity to benchmark with present M3* testing at CMTB
 - The input data (cool down times, flow rates, ...)
 - from CMTB cryogenic system
 - Several cooldowns available
 - A new set of thermal sensor has been included in CMTB

Model overview



Thermal conditions

- In the simulation (both static and transient) we have implemented the following thermal conditions:
 - Cooling provided by convection at the finned Aluminum tubes integrated in both the 5 K and 70 K shields
 - Conduction through penetration and supports (posts, couplers)
 - Thermal radiation load
 - 300 K thermal boundary at top of posts
- Under development: still working on or planning
 - Model so far has double shield and no radiation load at 2 K
 - No single shield model
 - Details of cavity tanks are still missing
 - Imposed temperature at the GRP and connections to tanks

Heat conditions in the transient analysis

- Time dependent convection cooling at the 5 K and 70 K finned tubes and HeGRP
 - Linear T decrease
 - Evaluation of h_f from fluid
 - Imposed linear temperature decrease at the 2 K cavity boundary, with no limit to heat exchange
- Time dependent heat loads:
 - Radiation heat flux acting on the shields surfaces
 - Conduction effects from couplers being implemented at 70 K, 5 K and 2K
 - not modeling real coupler geometry, though
 - heat load at the thermal anchors positions on the shields

Convective heat exchange on 70 K pipe

Derived from fluid properties (T, P, ...) and mass flows





Radiation load through MLI

- CERN data used so far
 - From r.t. to neglibible temperatures using 30 layers MLI
 - 1 W/m²
 - From 80 K to neglibible temperatures using 10 layers MLI
 - 0.05 W/m²
- Scale behavior during cooldown from these data using experimental plots reported in J. Weisend text



From J.Weisend

Figure 3-31 X/X_{nom} effects for nominal warm boundary temperature of 77 K.

Heat flow on 70 K pipe during cooldown



Gradient on 70 K shield

Max gradient on shield: cool down in 40 hours



Work still in progress...

- Further implementation of heat load sources and complexity of loading conditions
- Using CMTB cooldown data
- Getting CMTB data from DESY to be analyzed
 - provides model benchmark
- TO DO: Structural analysis at maximum gradients
 - mechanical interferences
- Model can be extended for exploring different cooldown procedures or thermal intercept strategies
- Big help from W. Maschmann, K. Jensch, R. Lange

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Measured data at CMTB – outer shield



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Measured data at CMTB – inner shield



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Shield radiation



Conduction at couplers



Real data at DESY - CMTB

2K circuit data at CMTB (module 3*)



Fluid parameters, 2 K circuit

2K circuit data at CMTB (module 3*)



Fluid parameters, 5 K circuit



Fluid parameters, 70 K circuits

50 K shield cooldown CMTB data



Results with CMTB cooldown – 70 K



Results with CMTB cooldown – 5 K





Transient Thermal - tutto 60h Time: 2.16e+005 s Items: 10 of 24 indicated 23/4/2008 2:08 PM

В

С

E

F

I

J

A Temperature 300K: 27. °C Convection 4K: -268. °C, 50.414 W/m² °C Convection 70K: -220.5 °C, 99.524 W/m2*°C D Temperature 2K shapes: -271. °C Heat Flux 70K: 1. W/m² Heat Flux 4K: 5.e-002 W/m² G Heat Flow Coupler1_70K: 2.69 W H Heat Flow Coupler2_70K: 2.69 W Heat Flow Coupler3_70K: 2.69 W Heat Flow Coupler4_70K: 2.69 W 0.000 2.000 (m) 1.000 0.500 1.500

Loads

ncommercial use only





Detail of inner shield



Position of coupler load on model

