



LLRF for S1 and ilc

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- LLRF for ilc commissioning and operation
- Questionnaire
- LLRF for S1 operation



For ilc



Actual LLRF tuning overhead

RF power budget

- cavity input 8.02 MW (33 MV/m * 1.038 m * 26 cav. * 9 mA)
- reflection from waveguide system 1% (VSWR~1.2)
- non-optimal coupling 2% (if over-coupling x1.3)

(We should also consider the rf-output reduction due to the rf reflection to klystron)

- rf loss 8.54% (should be minimized!)
- beam fluctuation 1% (should be compensated by fast feedforward)
- modulator ripple 2.5% (pulse-to-pulse +/- 0.5%HV ripple)
- cavity detuning 2% (40 Hz peak of Lorentz force and microphonics)

Remained rf power:

$$10 \text{ MW} - 8.02 \text{ MW} * (1.01 * 1.02 * 1.01 * 1.025 * 1.02) / (1 - 0.0854) = 0.47 \text{ MW}$$

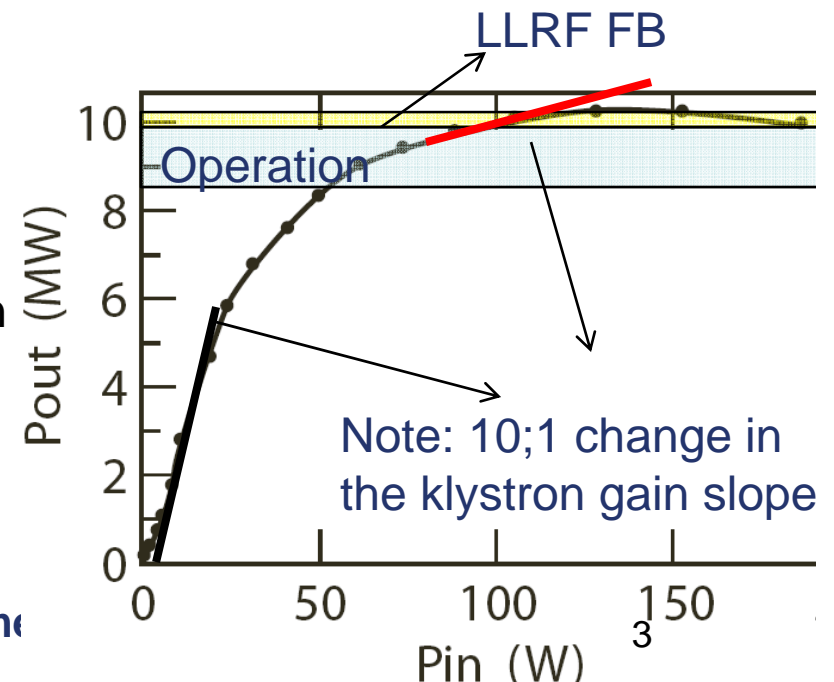
LLRF feedback overhead

$$8.02 * (1.01 * 1.02 * 1.01 * 1.025 * 1.02 * X) / (1 - 0.0854) = 10$$

-> X=1.049 (5%) (2.5% in amplitude)

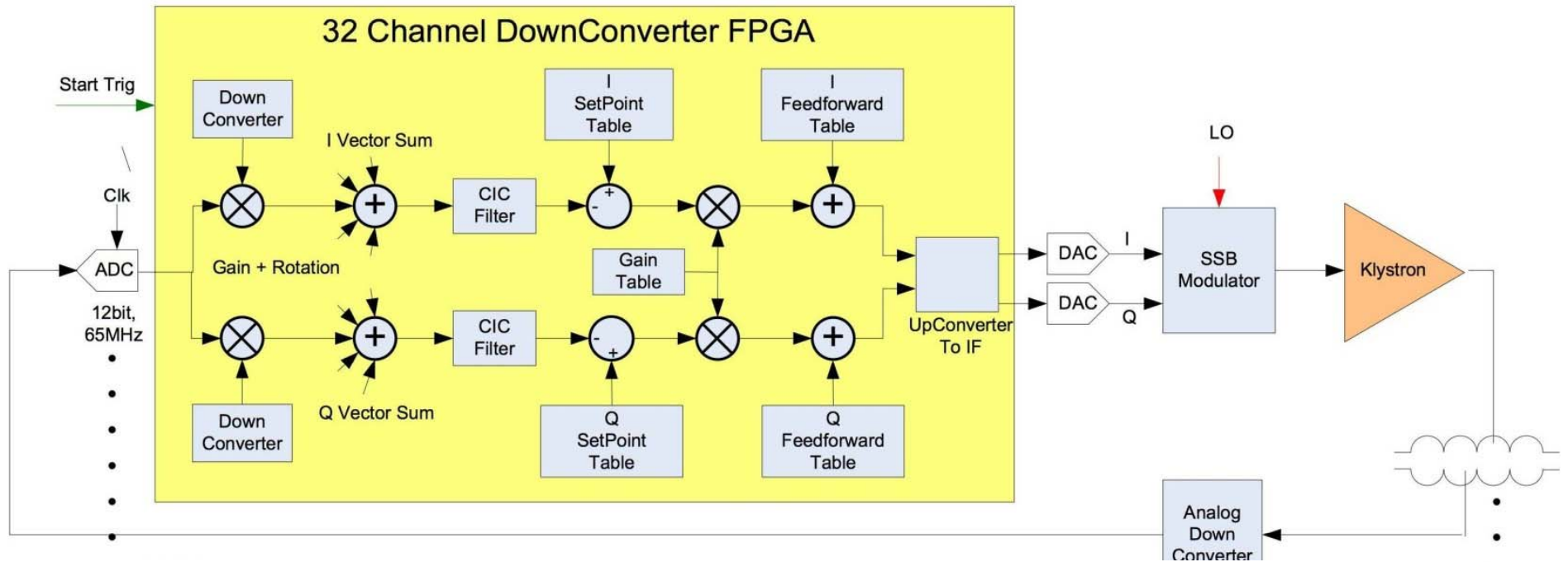
- The overhead is used for field regulation.
- Performance of the field stability depends on
 - feedback gain
 - additional rf power

Strategy for cavity quench or mistuning should be considered.





Power Overhead Budget



- Current FB control consists of feed forward and proportional FB.
- Having proportional gain of P_{gain} , fluctuations can be suppressed $1/P_{gain}$.
(10% fluctuation and $P_{gain}=100$, \rightarrow 0.1% stability)
- Driving power at FB: 0.05% error and $P_{gain}=100$,
 \rightarrow 5% additional amplitude (10% in power)
- Thus 10% is minimum headroom for linear feedback operation.

IX



Brief History of “CCR” from BCD

	Vmax,Vave	Ibeam	# cavities
BCD	35 MV/m, 31.5 MV/m	9.5 mA	24
CCR#20	33.5 MV/m, 31.5 MV/m	9.5 mA	26
RDR	33 MV/m, 31.5 MV/m	9 mA	26

■ At CCR(Change configuration request) #20, Ilrf team estimated some fluctuations. (beam, rf loss,...)

■ We opposed to CCR#20 because of the less Ilrf tuning overhead.

$33.5 \text{ MV/m} * 9.5 \text{ mA} * 1.038 \text{ m} = 330.3 \text{ kW}$ (Cavity Input Power)

* 26 Cavities

* $1 / 0.95$ (Distribution Losses with WR770/WR650)

* $1 / 0.90$ (Tuning Overhead)

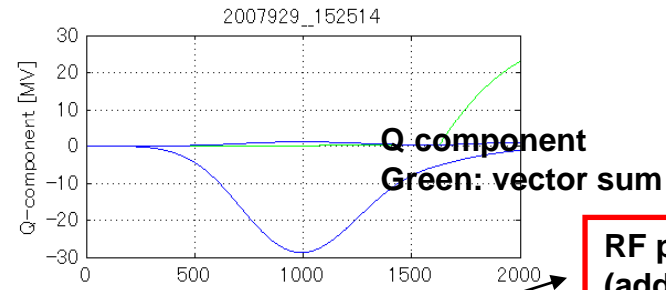
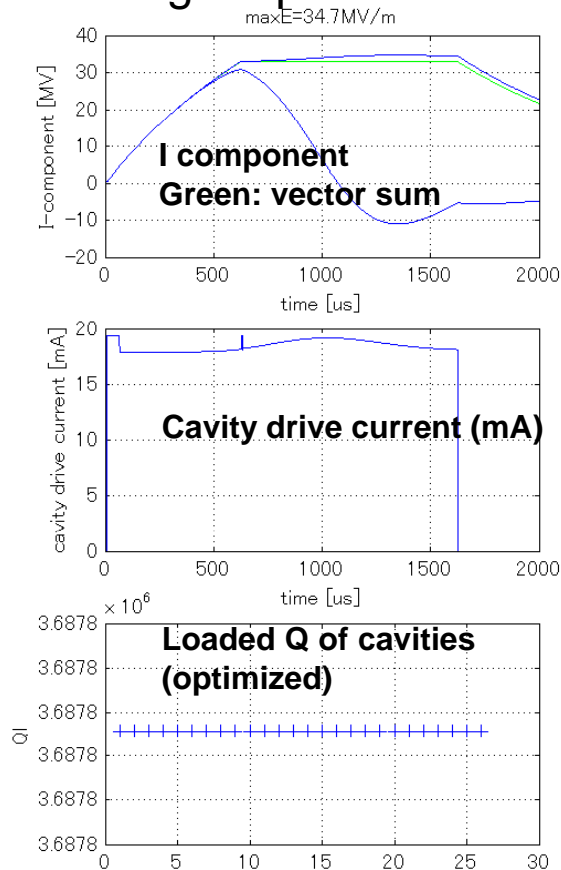
= 10.0 MW

■ Increased power consumption (such as distribution loss, coupling loss), the situation became worse than CCR#20.

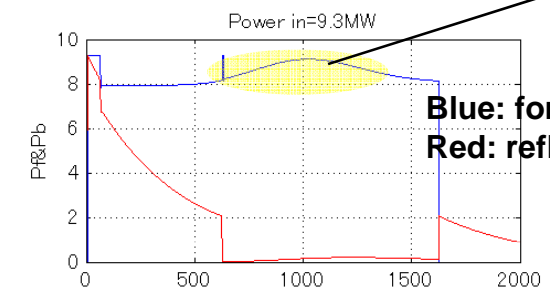


Failure in LFD Piezo Control

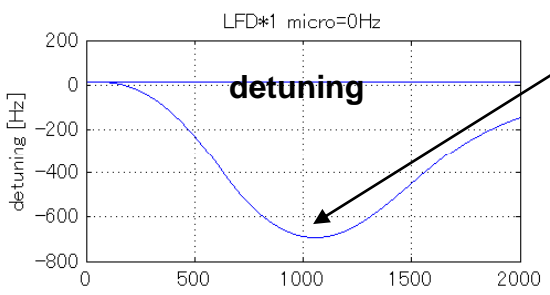
■ If one of 26 cavities **failed detuning control**, other 25 cavities have to compensate during rf operation.



RF power increase from 8 MW to 9.15 MW (additional 13% in power)



Blue: forward rf power [MW]
Red: reflection power [MW]



Un-compensated cavity (-700 Hz detuning)

■ 13% additional rf power is more than 1/3 overhead (5%) in case of 33 MV/m.
-> **Vector-sum gradients cannot be sustained even at one cavity Piezo tuner failure.**



Case study: Piezo failure

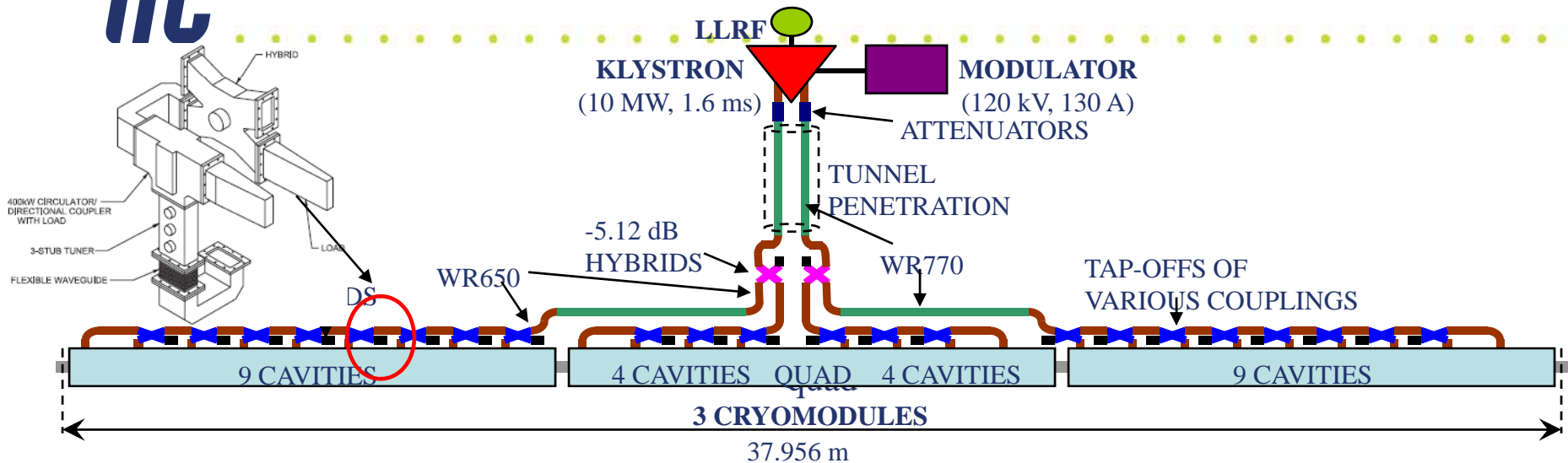
- *If Piezo tuner does not work during rf pulse,*
 - (a) When we have enough power overhead
 - i. We can continue operation during the pulse and check the failure during rf operation.
 - ii. If piezo failure is caused by HV supply, we can replace it with rf operation.

- (b) When we do not have enough power overhead
 - i. RF stability does not satisfy the requirements during the first rf pulse.
 - ii. So we have to detune the cavity and change vector sum set-table (because number of sum decreases.)
 - iii. Diagnose the reason of failure off-line
 - iv. If piezo failure is caused by HV supply, replace it.
 - v. Lower the rf gradient (in order to guarantee the rf stability even if the Piezo control still fails) and change set-table for 26 cavities.
 - vi. Operate with 26 cavities
 - vii. If the failure is completely repaired, we can increase the set-point to the previous value.

-> Smaller power overhead brings a lot of complicated works to do during beam operation.



Questionnaire to HLRF and ML (1)



(1) Strategy of “manual” loaded Q and tap-off (VTO) setting in beam tunnels.
Example)

- 1) determine operational gradient of each cavity
- 2) set load Q and tap-off to optimized value based on the low power data

(2) Procedure of optimization on QI and VTOs commissioning from 0 to 9 mA.

-> How do you set QI and VTOs? (conventional or QI/VTO control?)

(3) How much the residual errors of loaded Q and tap-off control (<+/-3%?)?

Ref)

- 10% residual error in loaded Q induces 4% higher cavity field (need further simulations)
- 10% residual error in rf distribution induces 8.5% higher cavity field (need further simulations)
- Roughly 3%rms residual errors in loaded Q and tap-off coupling causes 3% rms more rf power. (need further simulations)

-> need *motor control of 3-stub tuner and VTO* for fine tuning & less rf dissipation.



Questionnaire to HLRF and ML (2)

.E 2.6-2
nit parameters.

Parameter	Value	Units
Modulator overall efficiency	82.8	%
Maximum klystron output power	10	MW
Klystron efficiency	65	%
RF distribution system power loss	7	%
Number of cavities	26	
Effective cavity length	1.038	m
Nominal gradient with 22% tuning overhead	31.5	MV/m
Power limited gradient with 16% tuning overhead	33.0	MV/m
RF pulse power per cavity	293.7	kW
RF pulse length	1.565	ms
Average RF power to 26 cavities	59.8	kW
Average power transferred to beam	36.9	kW

- • By Christopher Nantista (SLAC)
Main Linac – KOM, Fermilab September 28, 2007

Waveguide Attenuation

Take: .0078 dB/m for WR650 and .0053 dB/m for WR770 (11.6% above theoretical)*.

Horizontal run through penetration (~1.5m+6.75m+~3m = 11.25m WR770):	.0596 dB (1.36%)
Up & down/back & forth, both tunnels (~9m WR650):	.0702 dB (1.60%)
Average tunnel run to cryomodule (6.0m×9/13 = 4.15m WR770):	.0220 dB (0.505%)
Average longitudinal run along cryomodule (1.376m**×3.23 = 4.44m WR650):	.0347 dB (0.795%)
Circulators:	.10 dB (2.28%)
Other feed components (bends, phase shifter, directional coupler):	.020 dB (0.459%)
Flex waveguides (3×0.027dB):	.081 dB (1.85%)
TOTAL Waveguide Loss:	.3875 dB (8.54%)

■ Under **optimal QI and detuning**, klystron output becomes minimum.
-> In other words, additional losses will take place in non-optimal configuration.

■ We hope HLRF group will confirm the waveguide loss (7% or 8.54%) from klystron to input coupler **experimentally** in order to guarantee the LLRF tuning overhead.

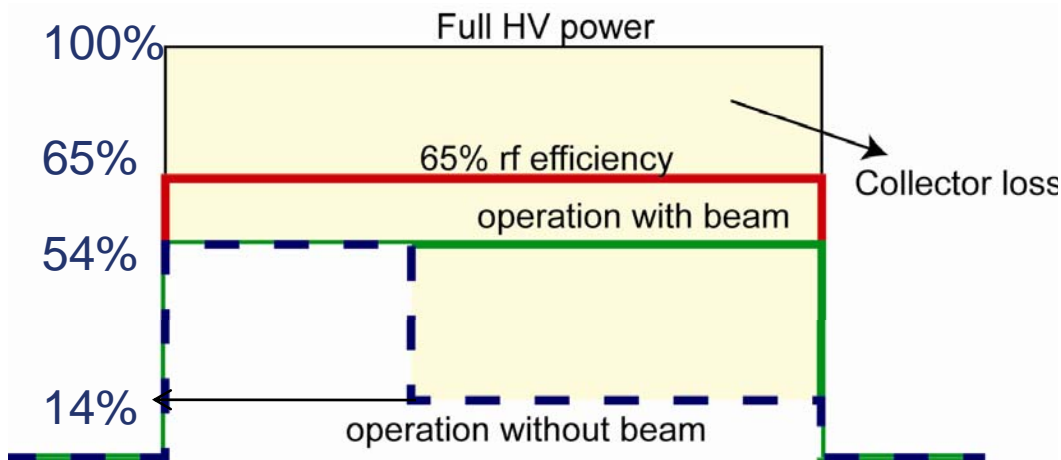
-> If the rf loss in waveguides are higher than expected, improvements of specification (field gradient, or beam current) will be necessary.



What should Ilrf do?

Thermal Phase Shifts

Power estimation:



By Christopher Nantista (SLAC)
at Main Linac – KOM, Fermilab September 28, 2007

	max. available, no atten. power flow	approx. length	V_{RF} / U_{from} from plot	ΔT	$\Delta \phi$	
penetration	5 MW (770)	11.25 m	11° C*	5.52°	14.44° common shift	
up & down	5 MW (650)	9 m	19° C	8.62°		
to cryomodule	3.46 MW (770)	6 m	8° C*	2.14°	6.3° max. diff structure to structure	
to 2 nd & 3 rd feeds	2.88 MW (650) avg.	2.75 m	12° C	1.66°		
to 4 th & 5 th feeds	2.11 MW (650) avg.	2.75 m	9° C	1.25°		
to 6 th & 7 th feeds	1.35 MW (650) avg.	2.75 m	6° C	0.83°		
to 8 th & 9 th feeds	577 kW (650) avg.	2.75 m	3° C	0.42°		
feed	384 kW	3 m	2° C	0.30°		

*Scaled with power dissipation and inversely with perimeter for WR770 (may get much hotter in penetration without cooling)

- diode power (15.4 MW = 10 MW/0.65) -> 120 kW loss @ kly. collector
- operation (with beam) 8.4 MW @ 31.5 MV/m -> 55 kW loss @ kly. Collector
- operation (without beam) 8.4 MW & 2.1 MW -> 86 kW loss @ kly. Collector

What should Ilrf (or trigger) do?

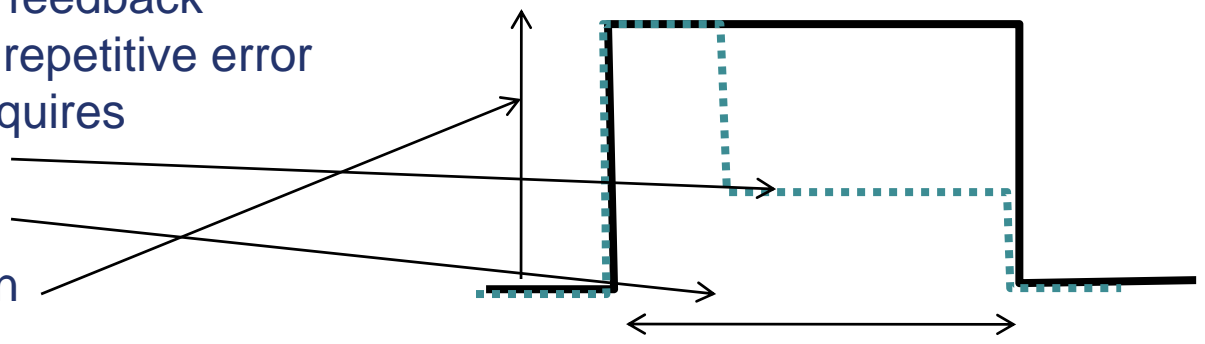
- beam off: change HV width in order to avoid excess klystron collector loss(?)
-> temperature change at waveguide leading to phase drift!!
- rf conditioning: change repetition(?) or control the HV width(?)
- slow LLRF compensation by adaptive FF will be necessary for suppress the effect of phase-shift.

24/04/2008



Adaptive feed-forward (FF) with intelligence

- Feed-forward (FF) is useful to suppress the repetitive error
- Feedback (FB) works for the suppression of non-repetitive error.
- In order to compensate the slow drift (by microphonics, thermal drifts), Adaptive feed forward will be the powerful method for field regulation.
- Adaptive feed forward is
 - to refresh the feed forward table periodically
 - like a pulse-to-pulse feedback
 - useful to reduce the repetitive error
- Adaptive feed-forward requires
 - beam information
 - rf width information
 - field level information



Example)

If “Quench” takes place, we eliminate these pulses from FF table generation

If “beam off” takes place,

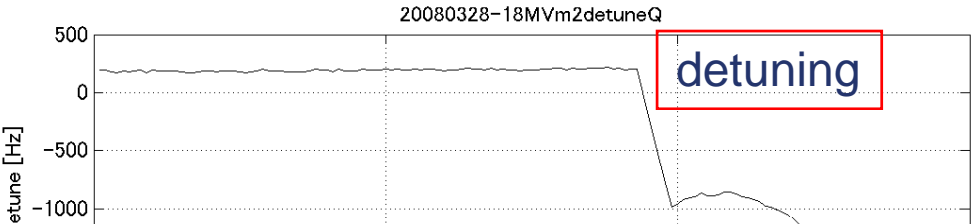
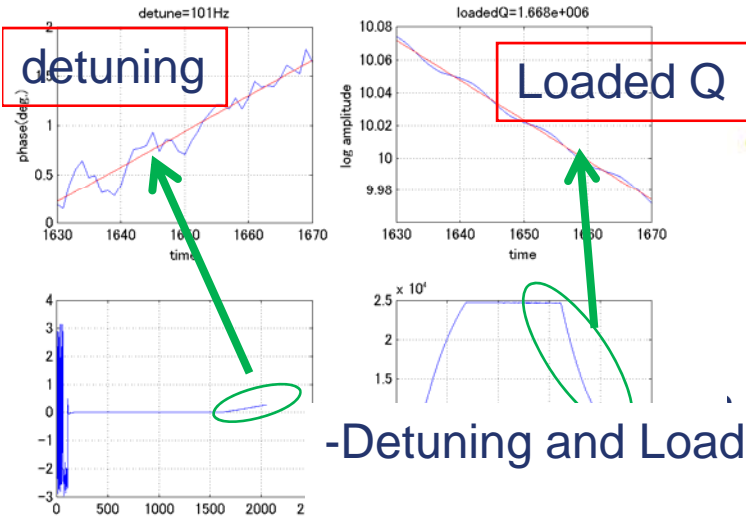


Automation and High Availability (information for software development)

- “For the 4 RF systems at FLASH an rf expert must presently be almost all times available in case of changes in machine settings or if exceptions (for example cavity quenches) occur. *This will not be tolerable for the XFEL and ILC.*” by Stefan Simrock
- Automation study should be considered and more information will be necessary. Examples)
 - How do we detect “Quench”? (from rf ? Or from cryo?)
 - Does llrf have to watch dynamic detuning compensation? (if compensation is not enough, does llrf have to inform it to some machine?)
 - How do we compensate phase drift? (need intelligent adaptive FF?)
 - Does llrf have to change rf pulse-width and set-point (in case without beam)?
 - ...
- These automation software development is not easy because the debugging is only possible at test facility.
- LLRF also needs more information for “high availability”. Examples)
 - What should llrf do when “Quench”? (detune the cavity or stop rf/beam?)
 - What should llrf do when “Piezo failure”? (could not sustain stable op.)

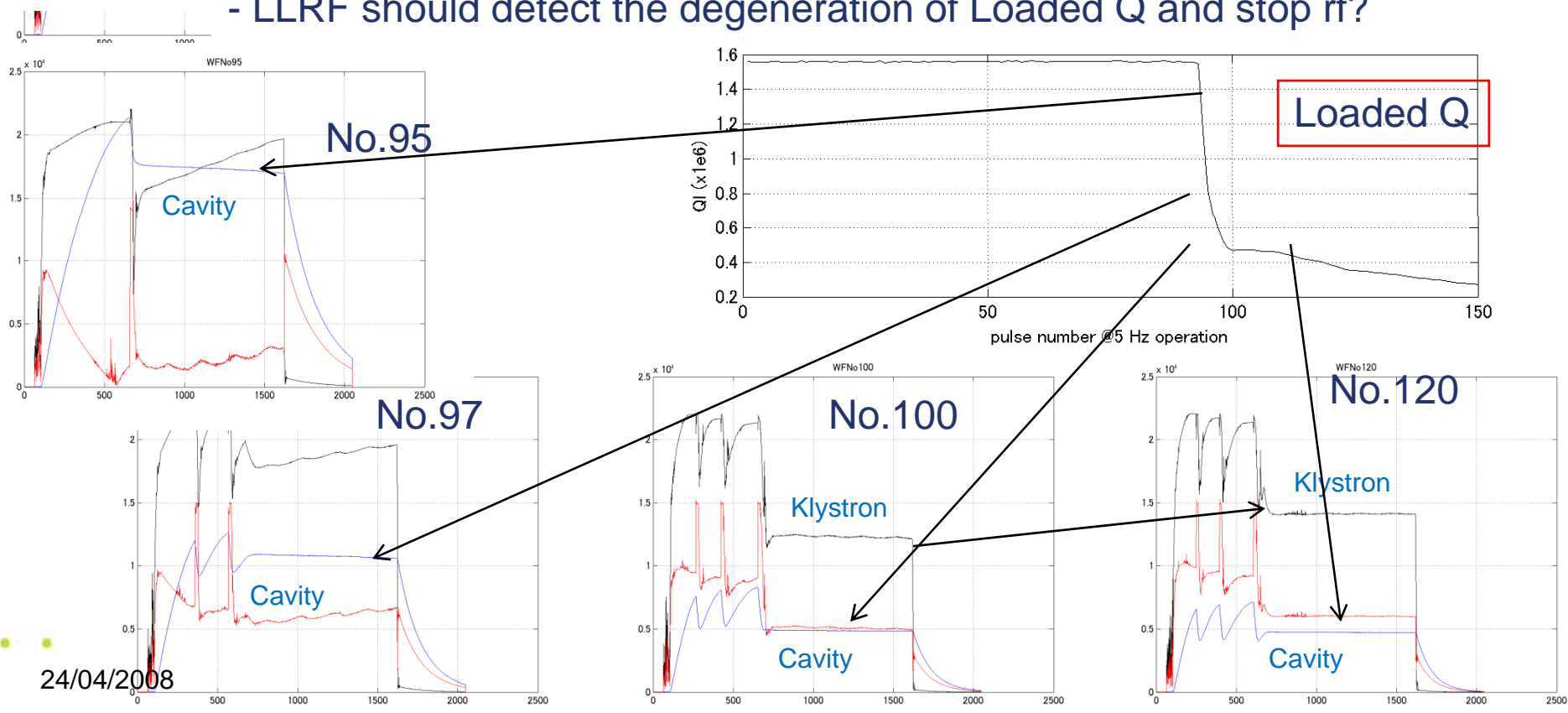
Quench detection

(150 pulses (30 sec.) before rf off)



- Detuning and Loaded Q are calculated from decay curve after the pulse.

- LLRF should detect the degeneration of Loaded Q and stop rf?



24/04/2008

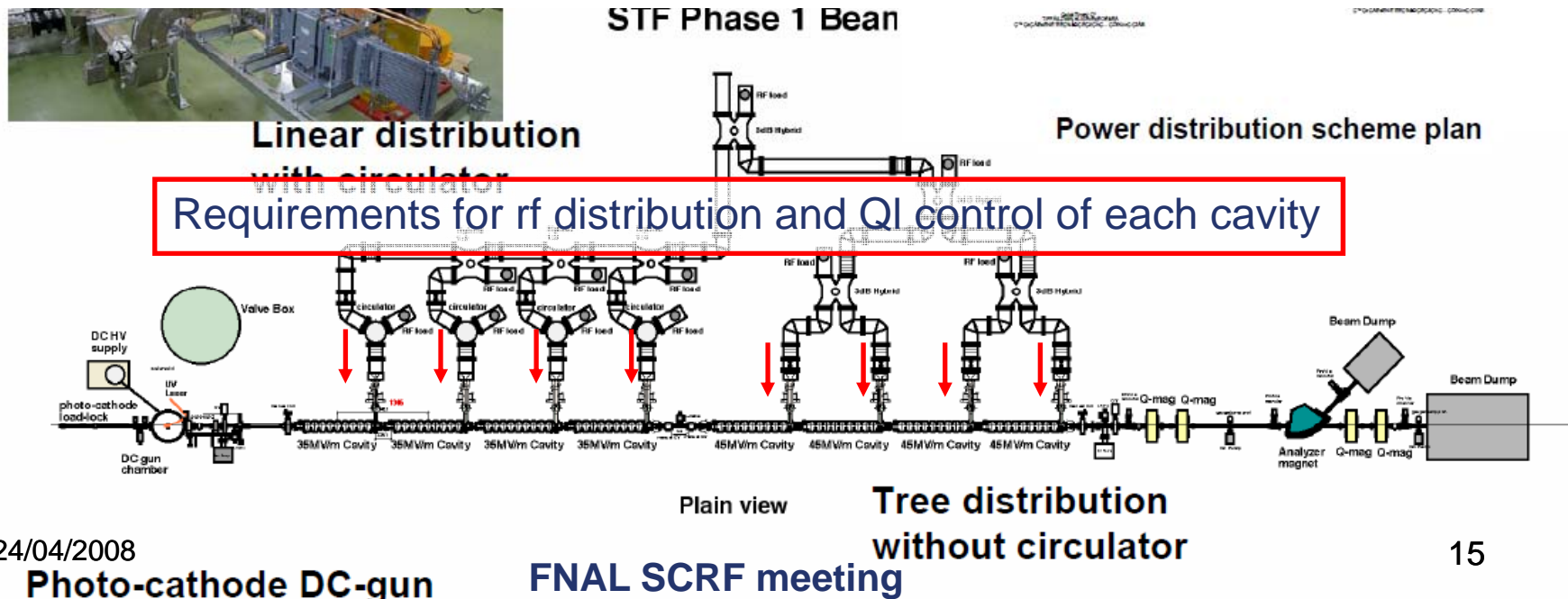


For S1 at KEK



Consideration of S1 at STF

- Eight cavities will be installed.
- Since we have 2 rf sources, 4 cavities (at least) will be driven by each rf source.
(Assumption)
- *Average gradient should be 31.5 MV/m.*
- *Cavities are operated without beam (no beam loading).*
- *Cavity operating gradient can depend on the performance of each cavity and it ranges from 28.5 MV/m to 34.5 MV/m.*
- *Loaded Q of each cavity varies +/-15%.*
- *RF distribution ratio can be controlled by fine tuning (to some extent).*

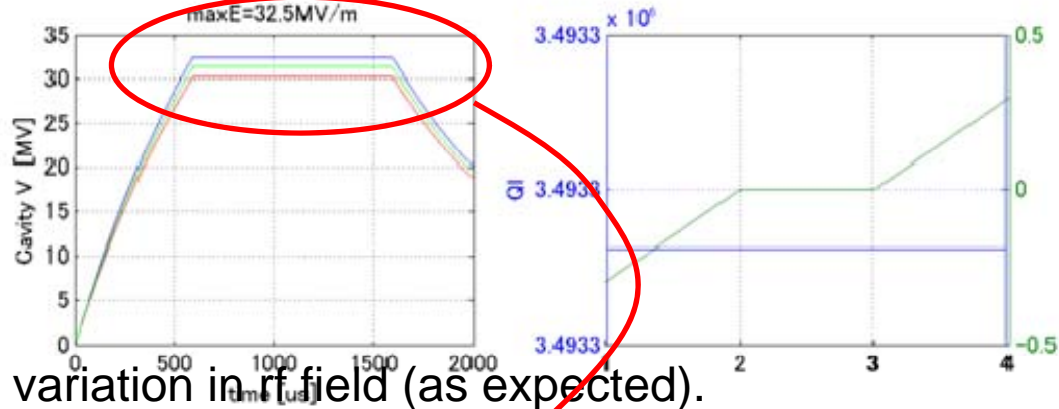




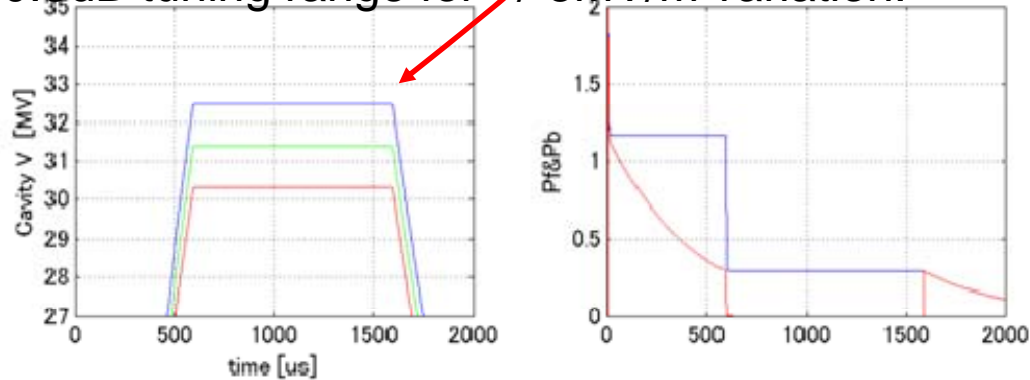
Rf distribution and cavity field gradient

(simulation assumption)

- 4 cavities are driven.
- All cavities have same loaded Q (no variation).
- Rf distribution to cavities are -6.3dB, -6dB, -6dB, -5.7dB.
- Vector sum control without beam



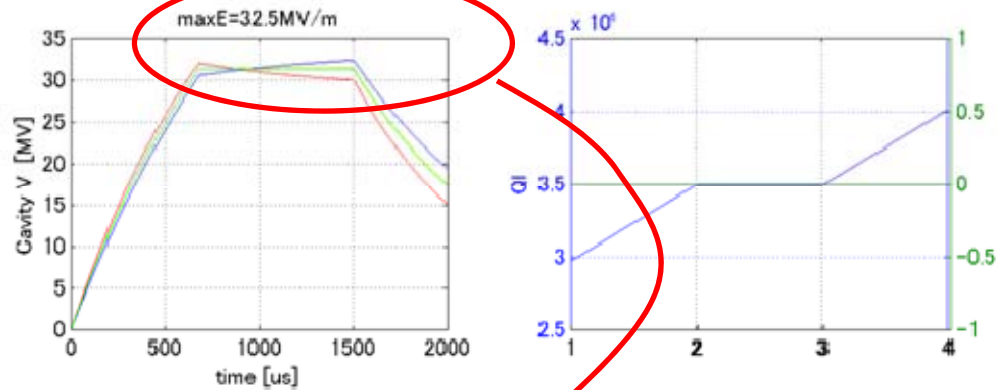
- +/-0.3dB variation in rf field (as expected).
-> need +/-0.8dB tuning range for +/-3MV/m variation.



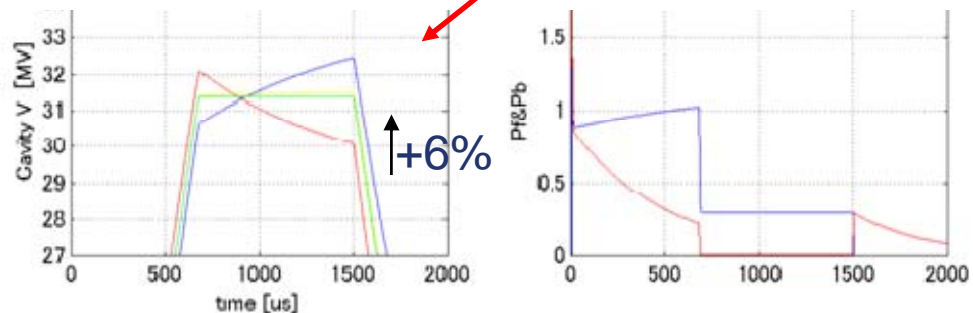


QI variation and cavity field gradient

- All cavities have same rf distribution (-6dB).
- Loaded Q variation of the cavities are -15%,0%,0% and 15%.
- Nominal loaded Q is $3.49e6$.
- Vector sum control without beam



- +6% increase in rf field during rf pulse for higher QI



- QI control by 3-stub will be necessary.



Thank you



Backup slides



Background (required stability)

- Lrf stability requirements (@ ML and BC) are $< 0.07\%$, 0.24deg .
- In order to satisfy these requirements, FB with proper FF control will be carried out.

TABLE 3.9-1

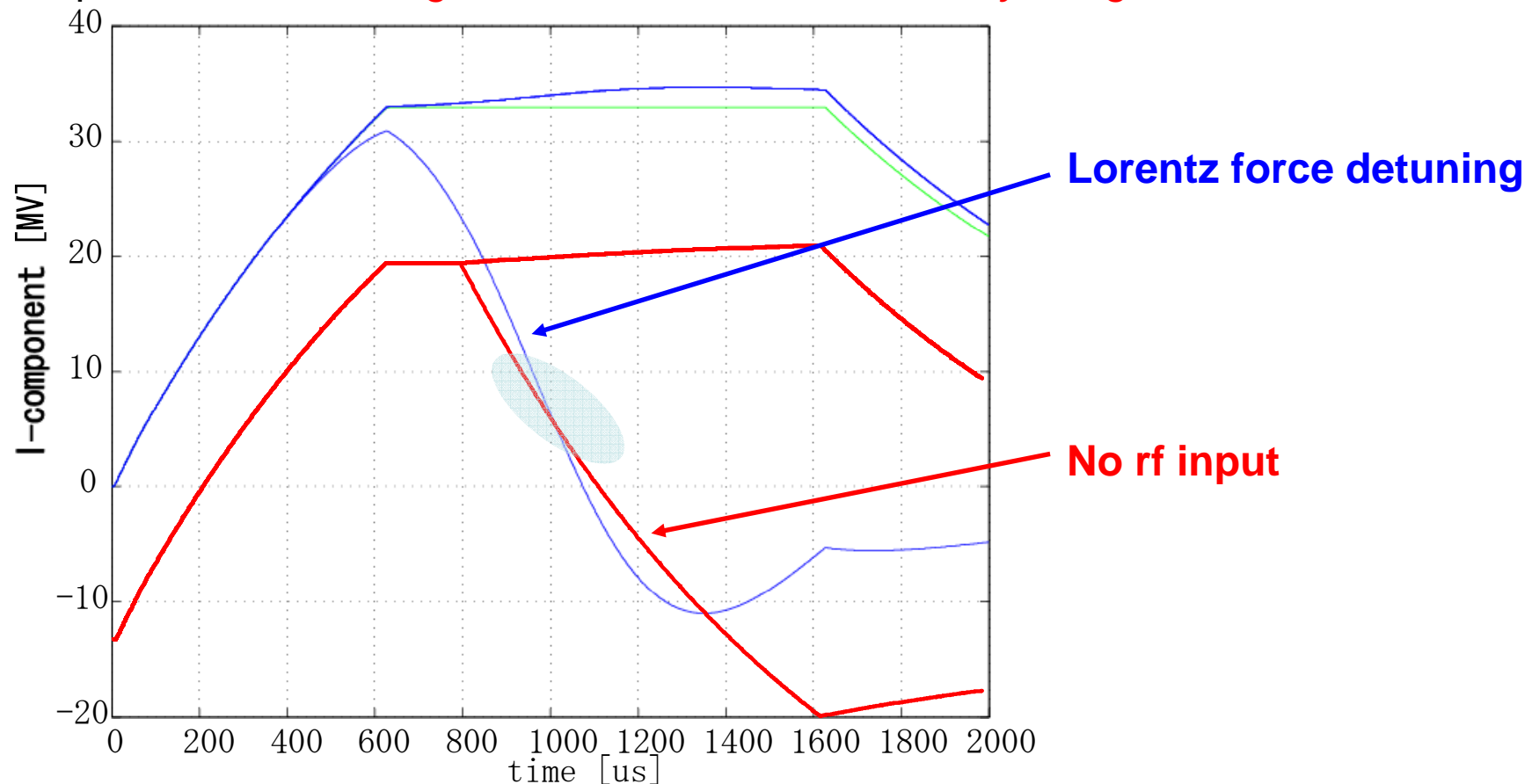
Summary of tolerances for phase and amplitude control. These tolerances limit the average luminosity loss to $<2\%$ and limit the increase in RMS center-of-mass energy spread to $<10\%$ of the nominal energy spread.

Location	Phase (degree)		Amplitude (%)		limitation
	correlated	uncorr.	correlated	uncorr.	
Bunch Compressor	0.24	0.48	0.5	1.6	timing stability at IP (luminosity)
Main Linac	0.35	5.6	0.07	1.05	energy stability $\leq 0.1\%$



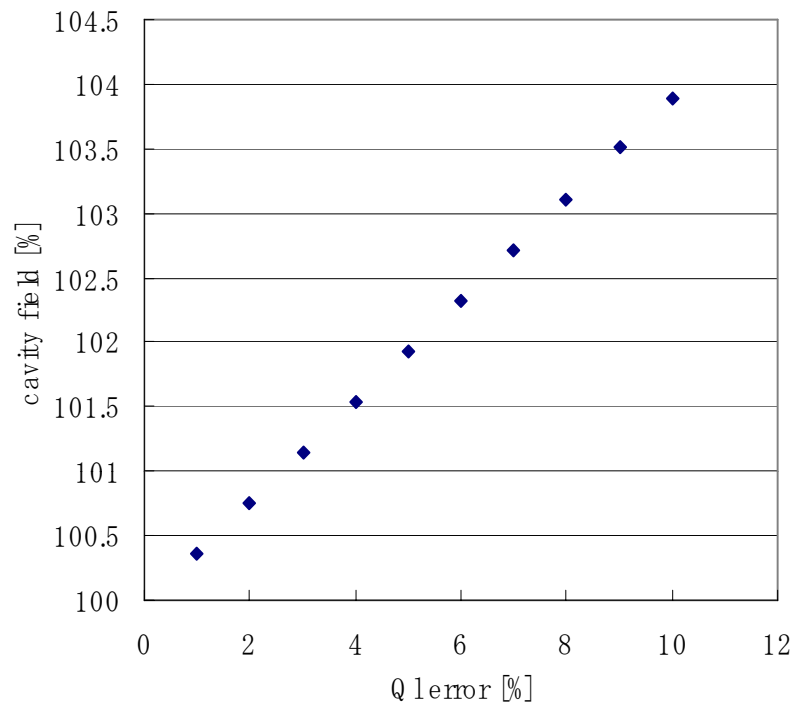
Why we need more rf power at piezo failure?

- Cavity drive current is used for “filling” and “to maintain rf gradient”.
- In case of “Piezo mis-control”, rf gradient change is more rapid than “no rf input”, and *the driving current is used also for “cavity filling”*.





QI variation and cavity field gradient (2)



- If the 6% field increase (+2MV/m) will not acceptable, external QI control system by such as 3-stub should be installed.

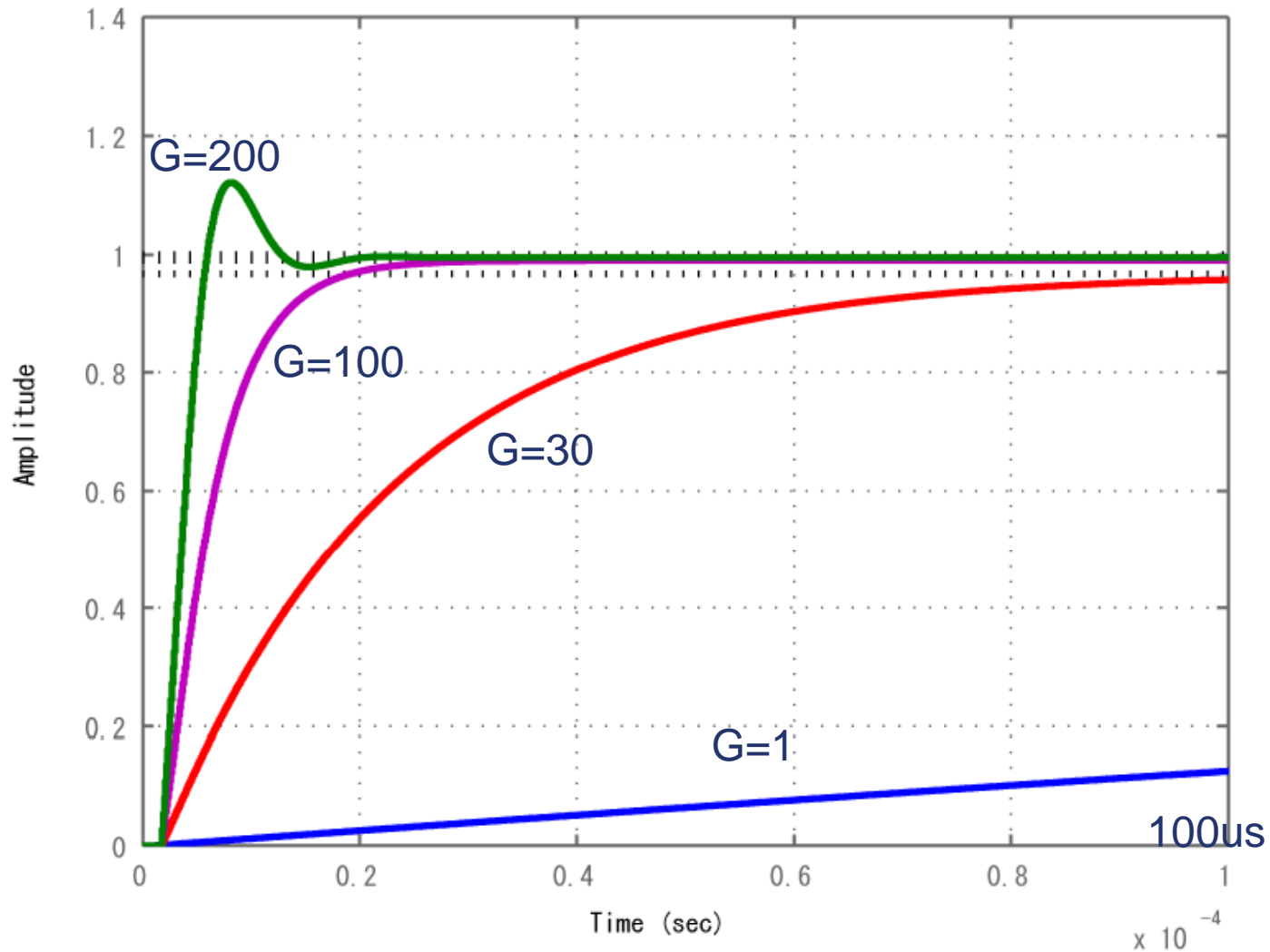
(summary)

- need rf input control of +/-0.8 dB and QI control by 3-stub.



Step response

Step Response



- Faster response at high gain (**but larger drive will be necessary.**)
- Fast FB needs larger driving power.



Perturbations

- In order to evaluate llrf stability (and satisfy llrf requirements), we need further information

- electron beam stability : $<+/-1\%$ (?) Frequency distribution?
- positron beam stability : $<+/-1\%$ (?)

-> 1% increase caused 1% more rf power.

- damping ring rf stability : $<0.3\%$, 0.3deg.rms (?)
- preciseness of beam current monitor at damping ring : $<+/- 0.5\%$ (This will be used for FF table at ML)

-> This precise beam current information is necessary for beam loading compensation.

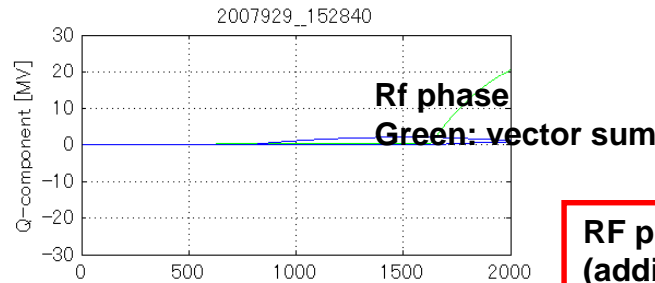
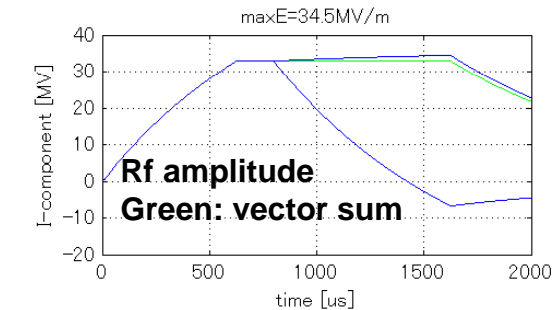
- microphonics level at cavities : <10 Hz (?)
- Lorentz force detuning with correction : $<+/-50$ Hz (?) (including microphonics)

-> $+/-50$ Hz detuning causes $+/-2\%$ additional rf power.

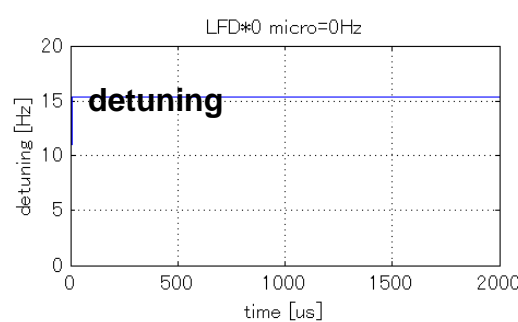
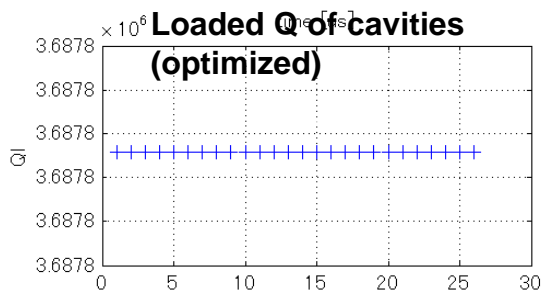
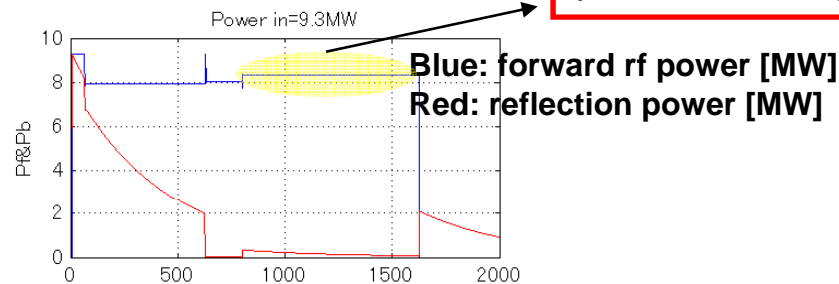
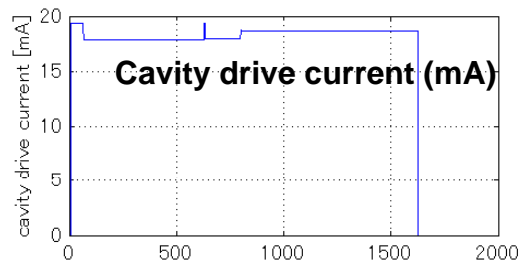


RF stability with one cavity failure

- If one of 26 **cavity input stops**, other 25 cavities have to compensate during rf operation.



RF power increase from 8 MW to 8.35 MW (additional 4% in power)



- In case of slow rf decay, llrf can sustain vector sum rf field by FB.