



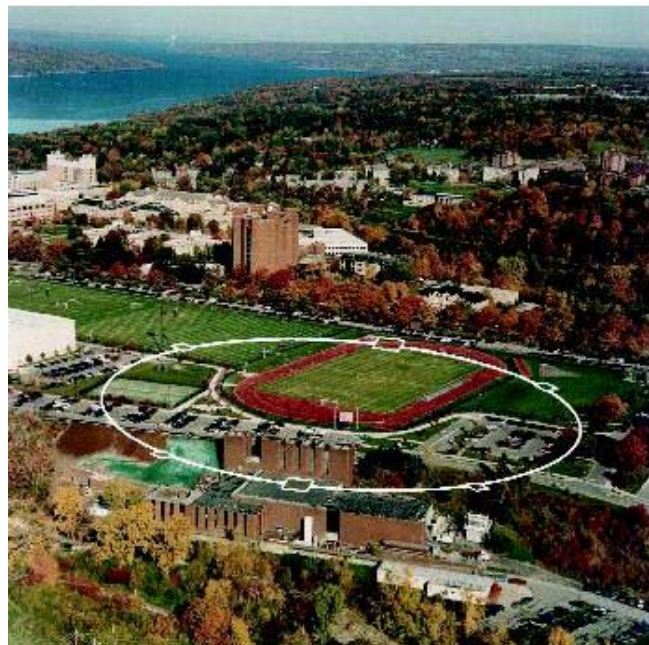
Cornell University
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“AC” Dispersion Measurement

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Traditional dispersion measurement

- Measure orbit
- Change ring energy ($\delta E/E = (\delta f_{rf}/f_{rf})/\alpha_p$)
- Measure again. $\eta_x = \Delta x/(\delta E/E)$

“AC” dispersion

- Drive an energy oscillation by modulating the RF phase at the synchrotron tune
- Measure the phase and amplitude of the vertical and horizontal signal at each BPM that is oscillating at the synchrotron tune
- Use the phase and amplitude information to reconstruct vertical and horizontal dispersion

Advantages:

1. Nondestructive

Use a signal bunch to measure dispersion without disturbing all of the other bunches in the ring

2. Fast - Changing the ring energy via the RF frequency is slow, especially with high Q cavities

3. Better signal to noise (Filter all but signal at synch tune)



“AC” dispersion

Note that dispersion is z-x and z-y coupling

Use transverse coupling formalism to analyze dispersion

Review of transverse coupling formalism and measurement

$T=VUV^{-1}$ (T is 4X4 full turn transport, U is block diagonal)
propagates the phase space vector (x,x',y,y')

$$V = \begin{pmatrix} \mathcal{M} & C \\ -C^+ & \mathcal{M} \end{pmatrix} \quad \bar{C} = G_b^{-1} C G_a \quad G = \begin{pmatrix} \sqrt{\beta_a} & 0 \\ -\alpha/\sqrt{\beta_a} & 1/\sqrt{\beta_a} \end{pmatrix}$$

In the absence of coupling, $C=0$, $V=I_{4X4}$, $U=T$



To measure x-y coupling

Drive beam at horizontal [a-mode] (or vertical [b-mode]) frequency.

The beam responds resonantly

Measure x and y amplitude and phase of the a-mode (b-mode) at each BPM

Finite y_{amp} indicates coupling

- The relative phase tells us something about its source

We find that:

$$\bar{C}_{12} = \frac{y_{amp}}{x_{amp}} \sin(\varphi_y - \varphi_x) \qquad \bar{C}_{22} = \frac{y_{amp}}{x_{amp}} \cos(\varphi_y - \varphi_x)$$

If we drive the b-mode we can extract \bar{C}_{11}

Note: \bar{C}_{12} is insensitive to BPM tilts

If there is no coupling, but a BPM is tilted,

then $y_{amp} \neq 0$, but $\phi_y = \phi_x \rightarrow \bar{C}_{12} = 0$



To measure x(y) - z coupling

Construct the matrix that propagates x-z motion. Again
 $T=VUV^{-1}$ (T is 4X4 full turn transport, U is block diagonal)

But here T propagates the phase space vector $(x, x', 1, \delta)$ [or $(y, y', 1, \delta)$]

As before we can write:

$$V = \begin{pmatrix} \mathcal{M} & C \\ -C^+ & \mathcal{M} \end{pmatrix} \quad \bar{C} = G_b^{-1} C G_a \quad G = \begin{pmatrix} \sqrt{\beta_a} & 0 \\ -\alpha/\sqrt{\beta_a} & 1/\sqrt{\beta_a} \end{pmatrix}$$

Here, the a-mode corresponds to horizontal[vertical] motion
and the b-mode is synchrotron motion

Now $C=0 \rightarrow$ no coupling of longitudinal and horizontal motion,
That is, zero dispersion



It turns out that in the limit $Q_s \rightarrow 0$

$$C_{12}(z-x) = \eta_x, \quad C_{22}(z-x) = \eta'_x$$

$$C_{12}(z-y) = \eta_y, \quad C_{22}(z-y) = \eta'_y$$

Drive beam at synchrotron tune (z-mode)

Measure x, y (and z?) amplitude and phase at each BPM

Then as with transverse coupling

$$\bar{C}_{12} = \frac{x_{amp}}{z_{amp}} \sin(\varphi_x - \varphi_z)$$

Is related to the horizontal dispersion according to

$$\bar{C} = G_b^{-1} C G_a \sim \eta / (\beta_a \beta_b)^{1/2}$$

$$\bar{C}_{12} = \frac{y_{amp}}{z_{amp}} \sin(\varphi_y - \varphi_z)$$

to the vertical dispersion (η_y)



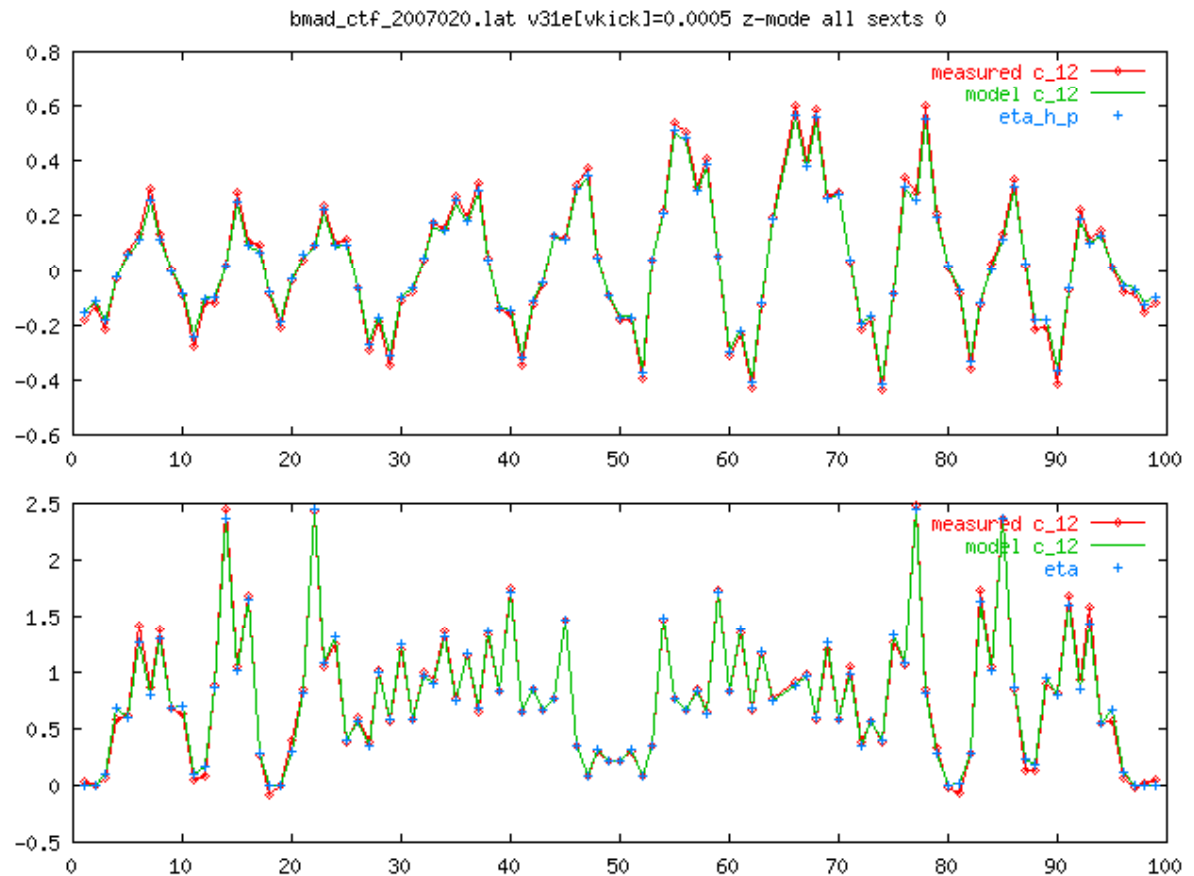
- Simulation of “AC” dispersion measurement

Introduce a vertical kick into CEsrTA optics to generate vertical dispersion

-Drive synchrotron oscillation by modulating RF at synch tune (In the simulation: apply an energy kick modulated at synch tune) and track for >30k turns

-“Measure” vertical & horizontal amplitudes and phases of synch tune signal at BPMs

- Construct C_{12}



“measured c_{12} ” - 30k turn simulation

“model c_{12} ” - Model y-z and x-z coupling

“model eta” - Model dispersion



We measure x_{amp} and ϕ_x , y_{amp} and ϕ_y

But we are unable (so far) to measure z_{amp} and ϕ_z with sufficient resolution

Longitudinal parameters come from the design lattice

(Perhaps with new BPM system we will be able to extract ϕ_z from $2f_s$)

—

$$z_{\text{amp}} = \sqrt{a_z \beta_z}, \quad 13\text{m} < \beta_z < 14.6\text{m} \quad (\text{CesrTA optics})$$

→ z_{amp} is very nearly constant - there is an overall unknown scale (a_z)

$$0 < \phi_z < 36^\circ.$$

We compute ϕ_z from the design optics at each BPM

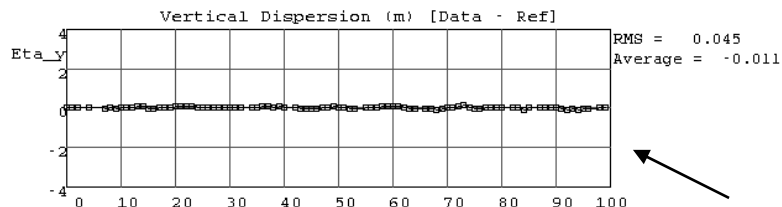
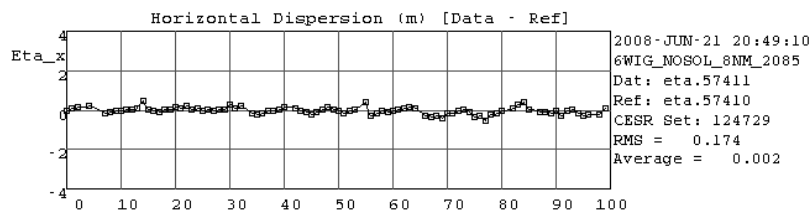
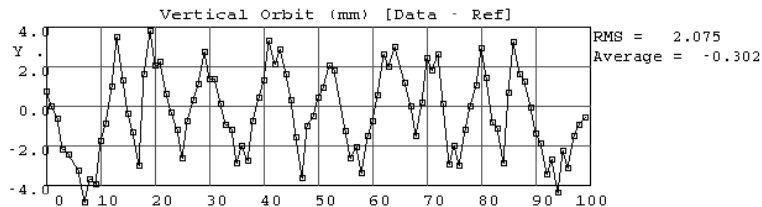
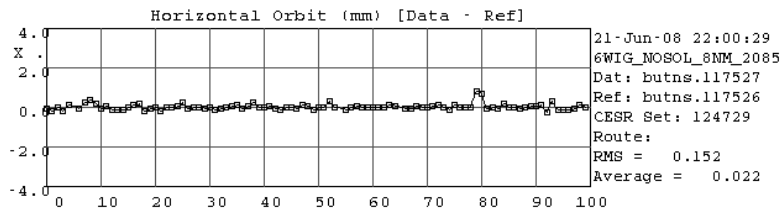
- there is an overall unknown phase offset (ϕ_0)

- Determine a_z , ϕ_0 by fitting x - data to model horizontal C_{12}

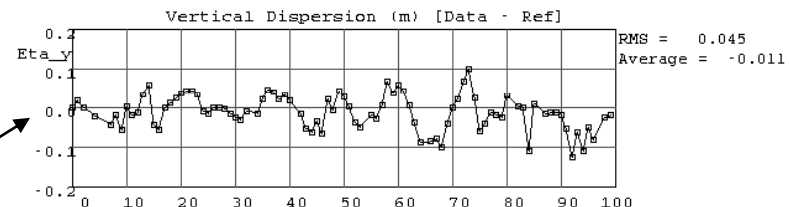
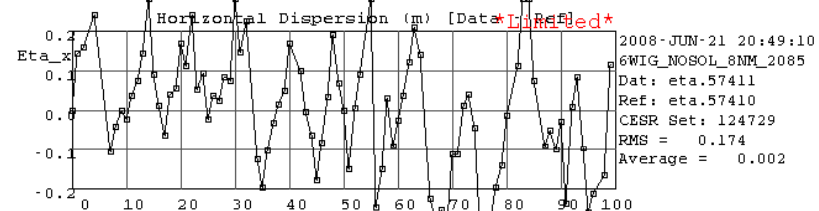
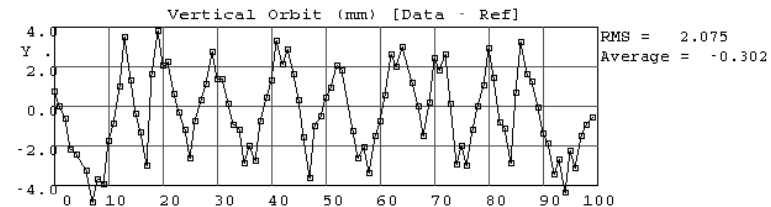
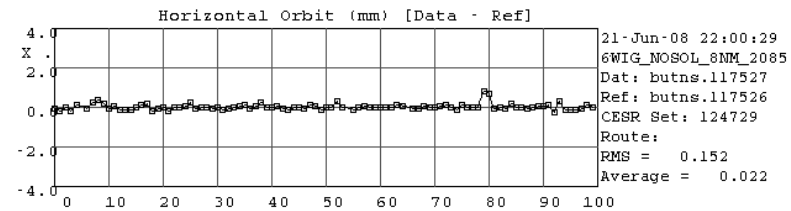
- Then use fitted parameters to determine vertical C_{12}



data v31e=200cu
ref: v31e=0



data v31e=200cu
ref: v31e=0



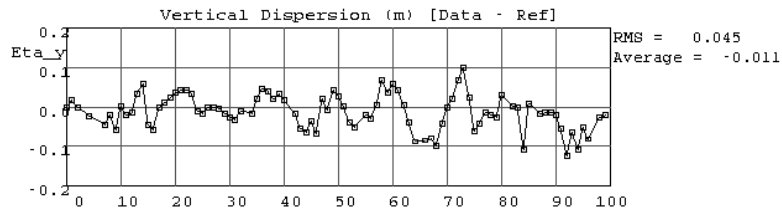
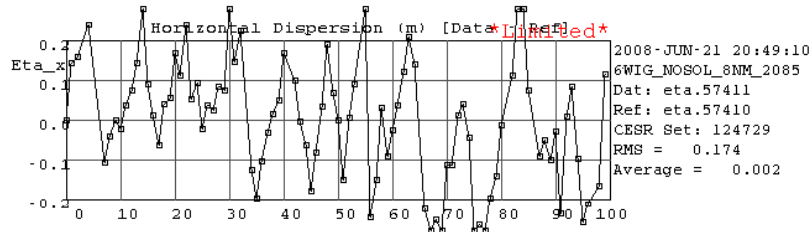
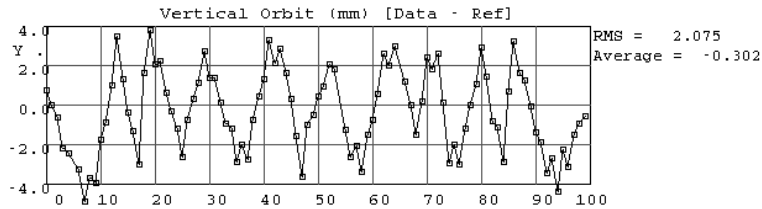
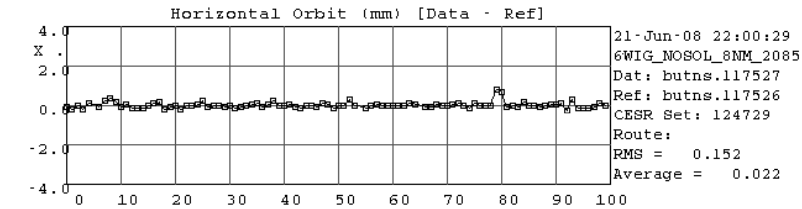
Same data - different scales

Change vertical steering 31e +200cu and measure orbit and “ac” dispersion (data).
Restore vert 31e to zero and remeasure orbit and dispersion (ref)



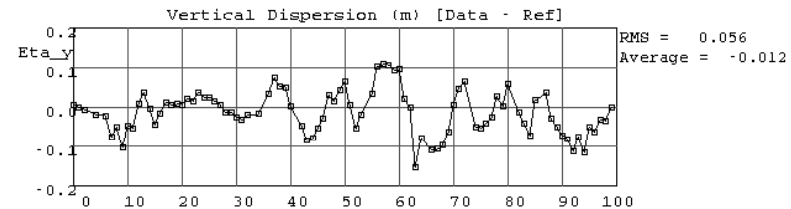
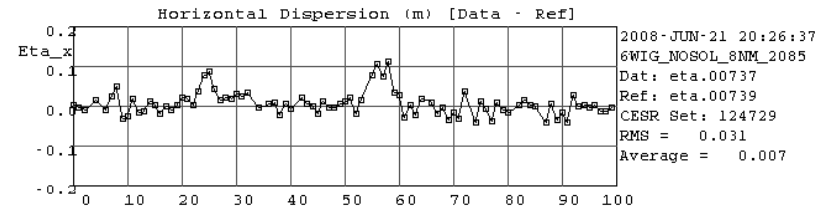
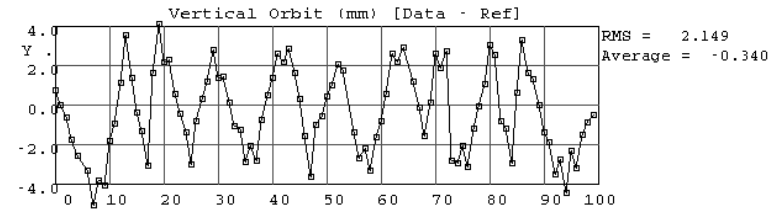
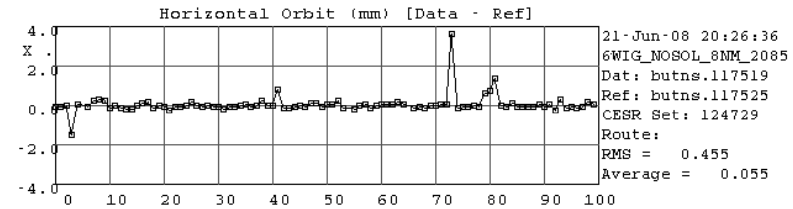
“AC” and “DC” measurements

data v31e=200cu
ref: v31e=0



“ac” dispersion
(same as last slide)

data: v31e=+200cu
ref: v31e=0 DC



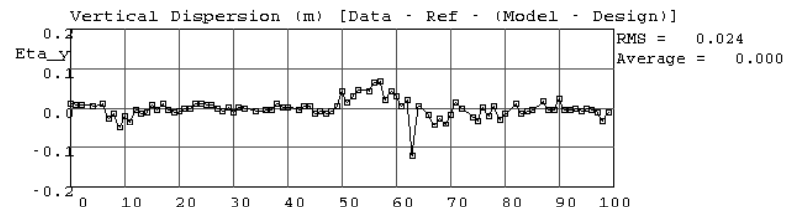
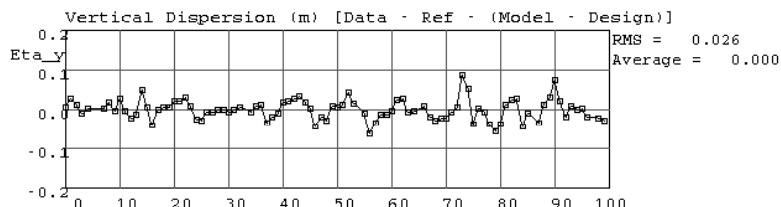
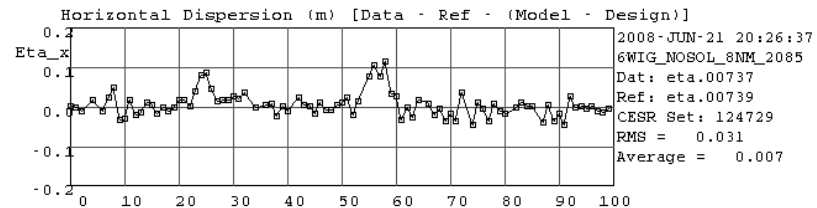
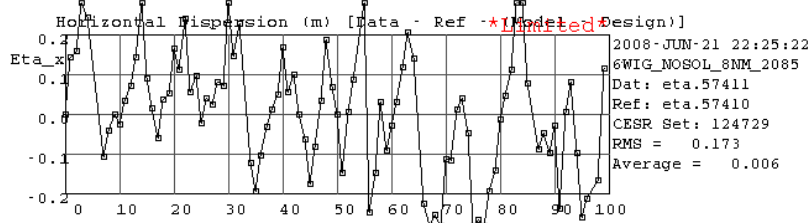
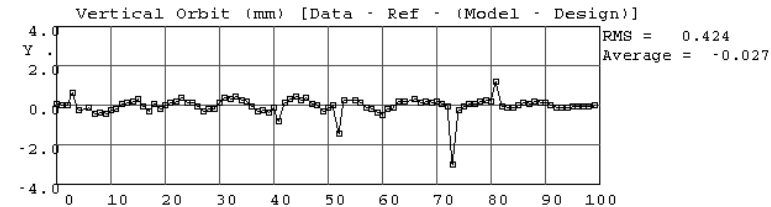
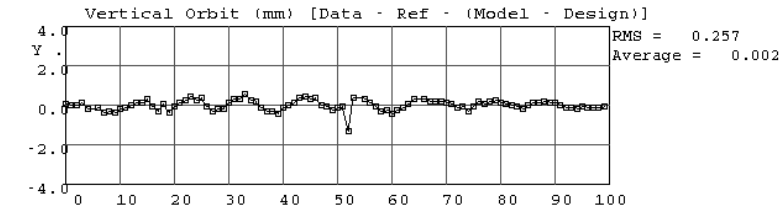
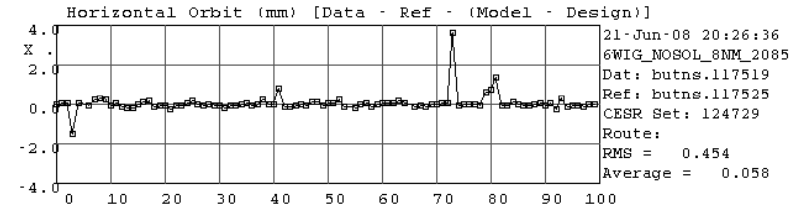
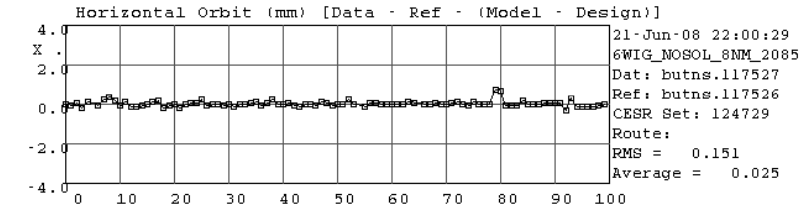
“dc” dispersion

Same steering change with “DC” dispersion measurement



data: v31e=+200cu
ref v31e=0
(Data-ref)-model

data: v31e=+200cu
ref: v31e=0 (measurement) - v31e=200cu (model)



“ac” measurement

“dc” measurement

“Data”: measurement with v31e=200cu

“Ref”: measurement with v31e=0

“Model”: modeled orbit and dispersion with v31e=200cu



- **Conclusions**

Dispersion is coupling of longitudinal and transverse motion

Measurement

- Drive synchrotron oscillation by modulating RF at synch tune
- Measure vertical & horizontal amplitudes and phases of signal at synch tune at BPMs

Then

$$\{\eta_v/\beta_v\} = (y_{\text{amp}}/z_{\text{amp}}) \sin(\varphi_y - \varphi_z)$$
$$\{\eta_h/\beta_h\} = (x_{\text{amp}}/z_{\text{amp}}) \sin(\varphi_h - \varphi_z)$$

Advantages?:

1. Faster (30k turns) (RF frequency does not change)
2. Better signal to noise - (remains to be seen)
filter all but signal at synch tune
3. Nondestructive (RF frequency does not change)
Witness bunch?