

Experience with *Echotek* Digital Receivers for High Performance Beam Position Measurements

– ATF Damping Ring BPM Upgrade –

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Fermilab**

for the ATF DR BPM Upgrade Collaboration

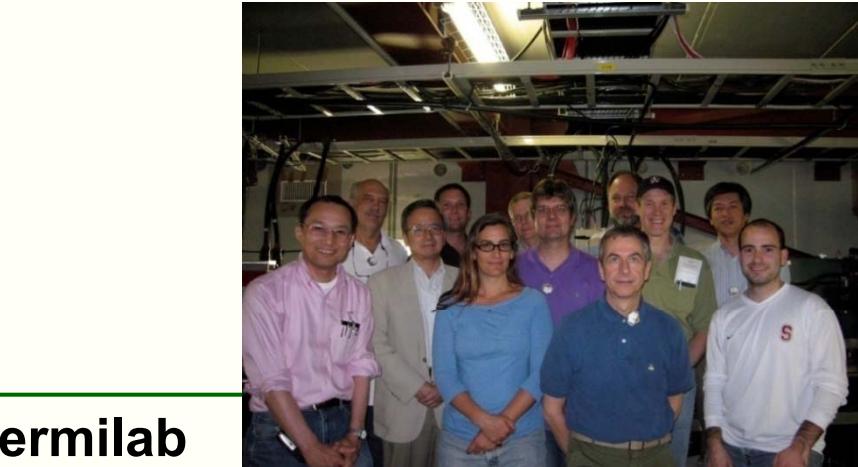


KEK

- Nobuhiro Teranuma
- Junji Urakawa

SLAC

- Doug McCormick
- Joe Fisch
- Justin May
- Janice Nelson
- Andrei Seryi
- Tonee Smith
- Mark Woodley



Fermilab

- Charlie Briegel
- Nathan Eddy
- Eliana Gianfelice
- Bill Haynes
- Peter Prieto
- Dennis Nicklaus
- Ron Rechenmacher
- Duane Voy
- Manfred Wendt

...and many others!

- ILC damping ring R&D at KEK's Accelerator Test Facility (ATF):
 - Investigation of the beam damping process (damping wiggler, minimization of the damping time, etc.)
 - Goal: generation and extraction of a **low emittance beam ($\epsilon_{\text{vert}} < 2 \text{ pm}$)** at the nominal ILC bunch charge
- A major tool for low emittance corrections:
a high resolution BPM system
 - Optimization of the closed-orbit, beam-based alignment (BBA) studies to investigate BPM offsets and calibration.
 - Correction of non-linear field effects, i.e. coupling, chromaticity,...
 - Fast global orbit feedback(?)
 - Necessary: a state-of-the-art BPM system, utilizing
 - a broadband turn-by-turn mode (< 10 μm resolution)
 - a narrowband mode with high resolution ($\sim 100 \text{ nm}$ range)

The ATF Damping Ring

Machine and Beam Parameters

beam energy $E = 1.28 \text{ GeV}$

beam intensity, single bunch $\approx \sim 1.6 \text{ nC} \equiv 10^{10} \text{ e}^- (\equiv I_{\text{bunch}} \approx 3.46 \text{ mA})$

beam intensity, multibunch (20) $\approx \sim 22.4 \text{ nC} \equiv 20 \times 0.7 \times 10^{10} \text{ e}^- (\equiv I_{\text{beam}} \approx 48.5 \text{ mA})$

accelerating frequency $f_{\text{RF}} = 714 \text{ MHz}$

revolution frequency $f_{\text{rev}} = f_{\text{RF}} / 330 = 2.1636 \text{ MHz} (\equiv t_{\text{rev}} = 462.18 \text{ ns})$

bunch spacing $t_{\text{bunch}} = t_{\text{RF}} / 2 = 2.8011 \text{ ns}$

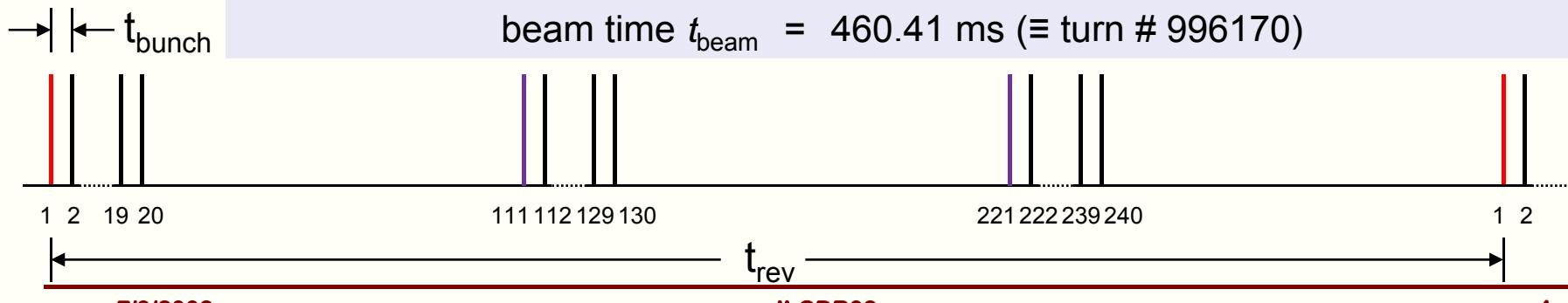
batch spacing $t_{\text{batch}} = t_{\text{rev}} / 3 = 154.06 \text{ ns}$

horizontal betatron tune $\approx 15.204 (\equiv f_h \approx 441 \text{ kHz})$

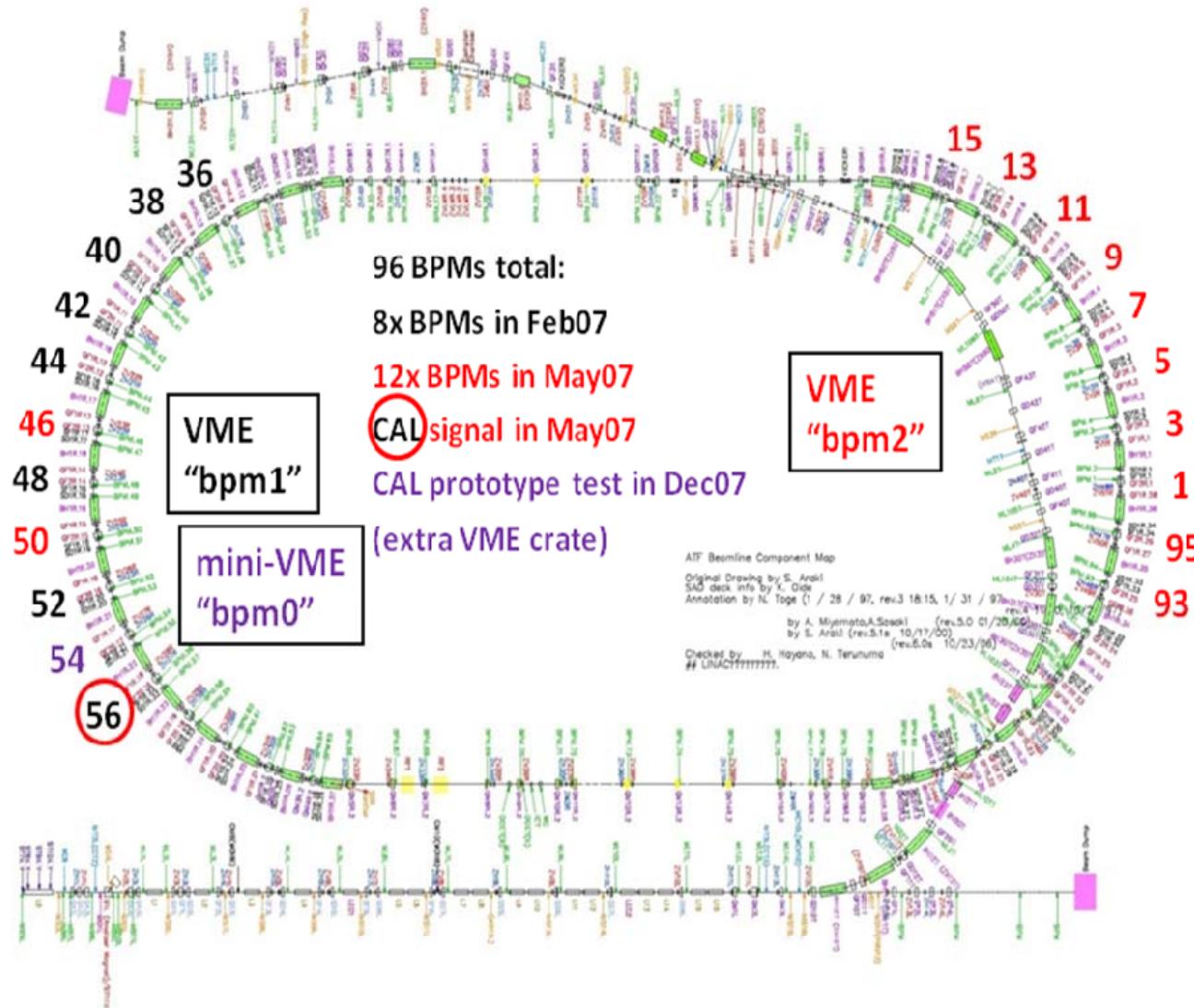
vertical betatron tune $\approx 8.462 (\equiv f_v \approx 1000 \text{ kHz})$

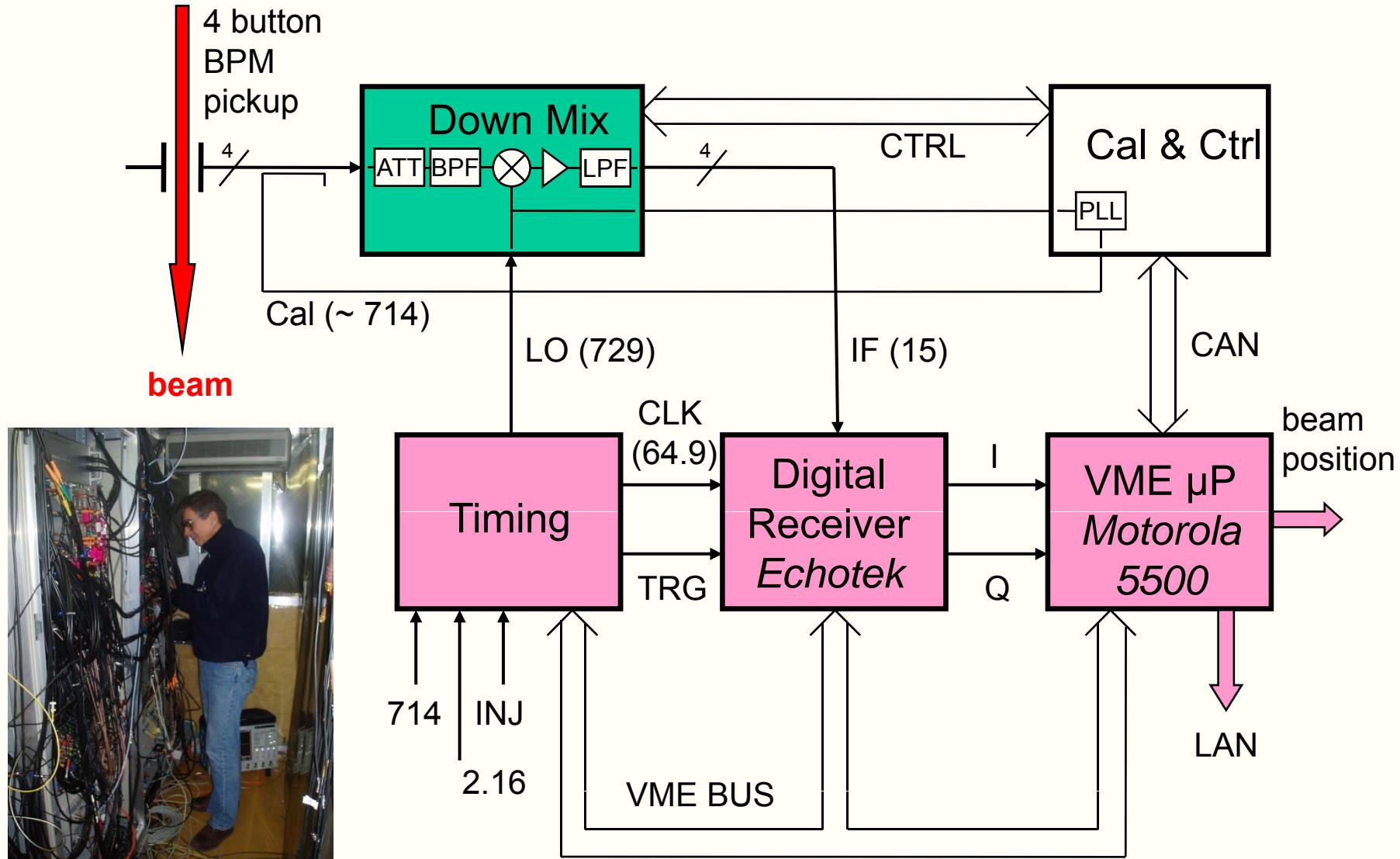
synchrotron tune $\approx 0.0045 (\equiv f_s \approx 9.7 \text{ kHz})$

repetition frequency $f_{\text{rep}} = 1.56 \text{ Hz} (\equiv t_{\text{rep}} = 640 \text{ ms})$

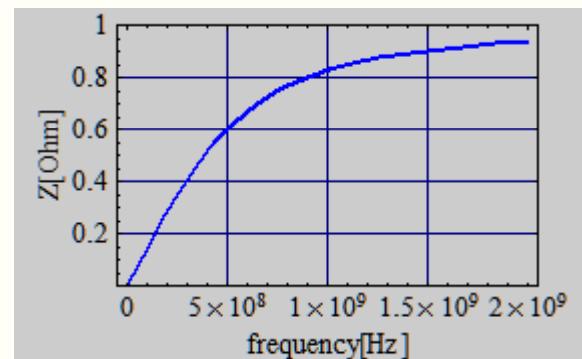
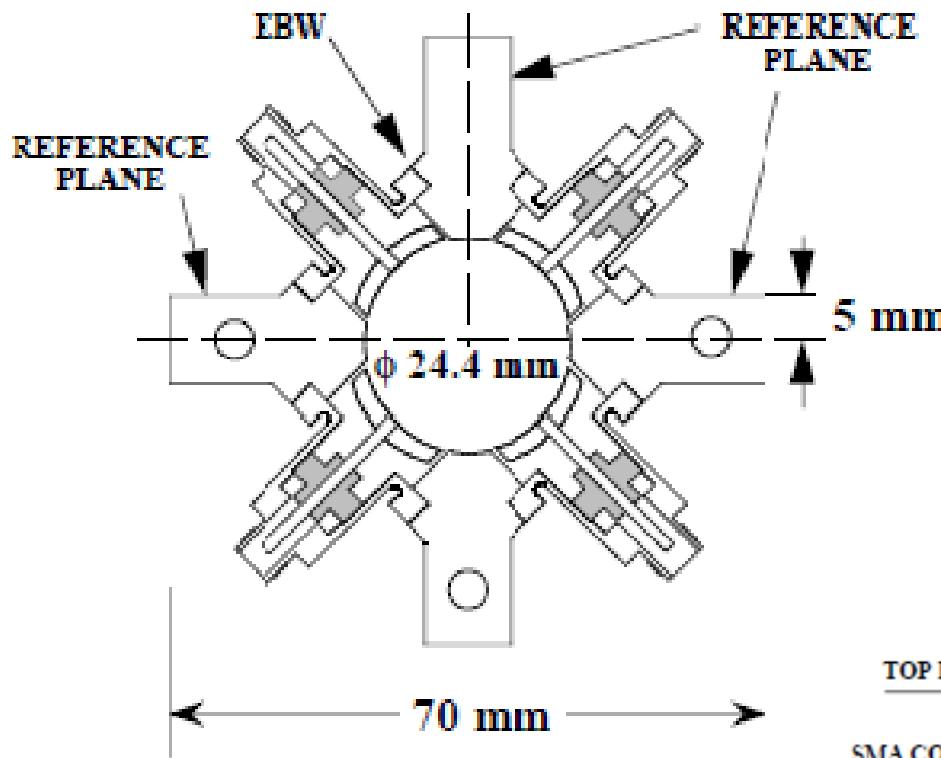


The ATF Damping Ring

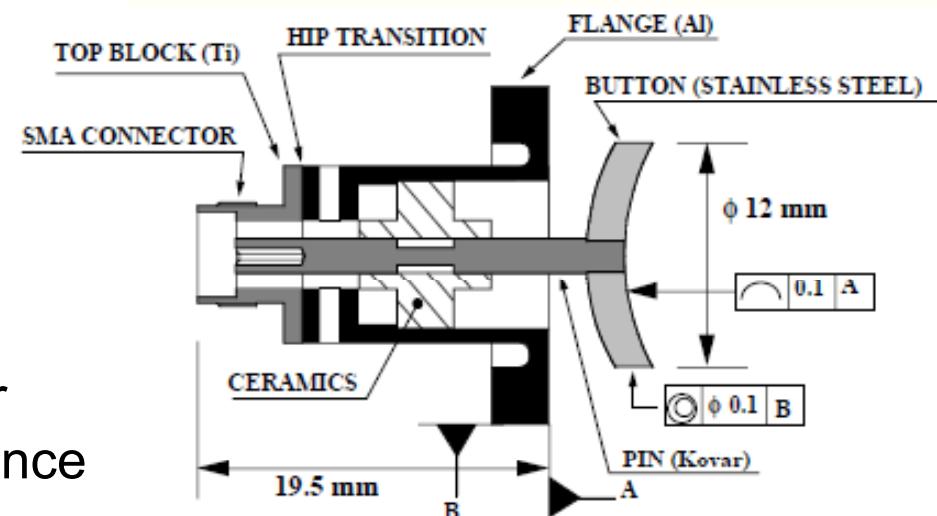
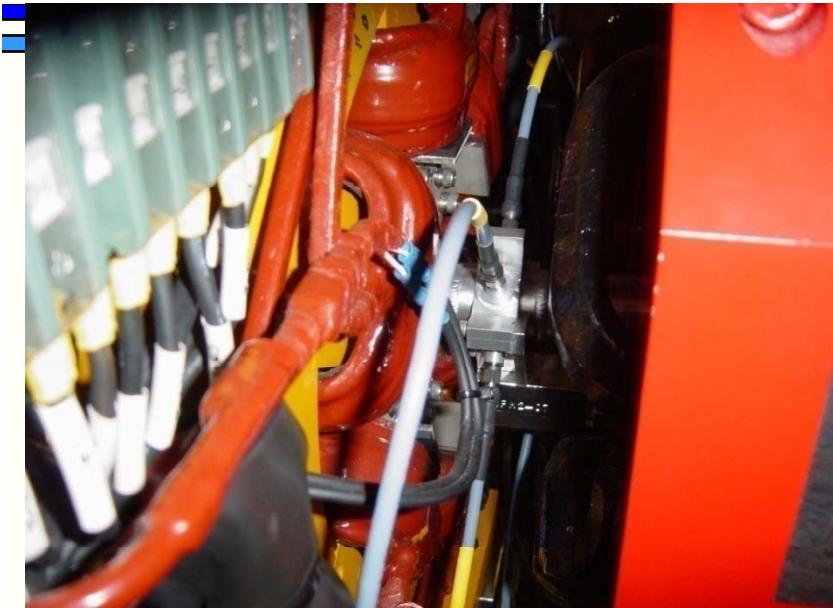




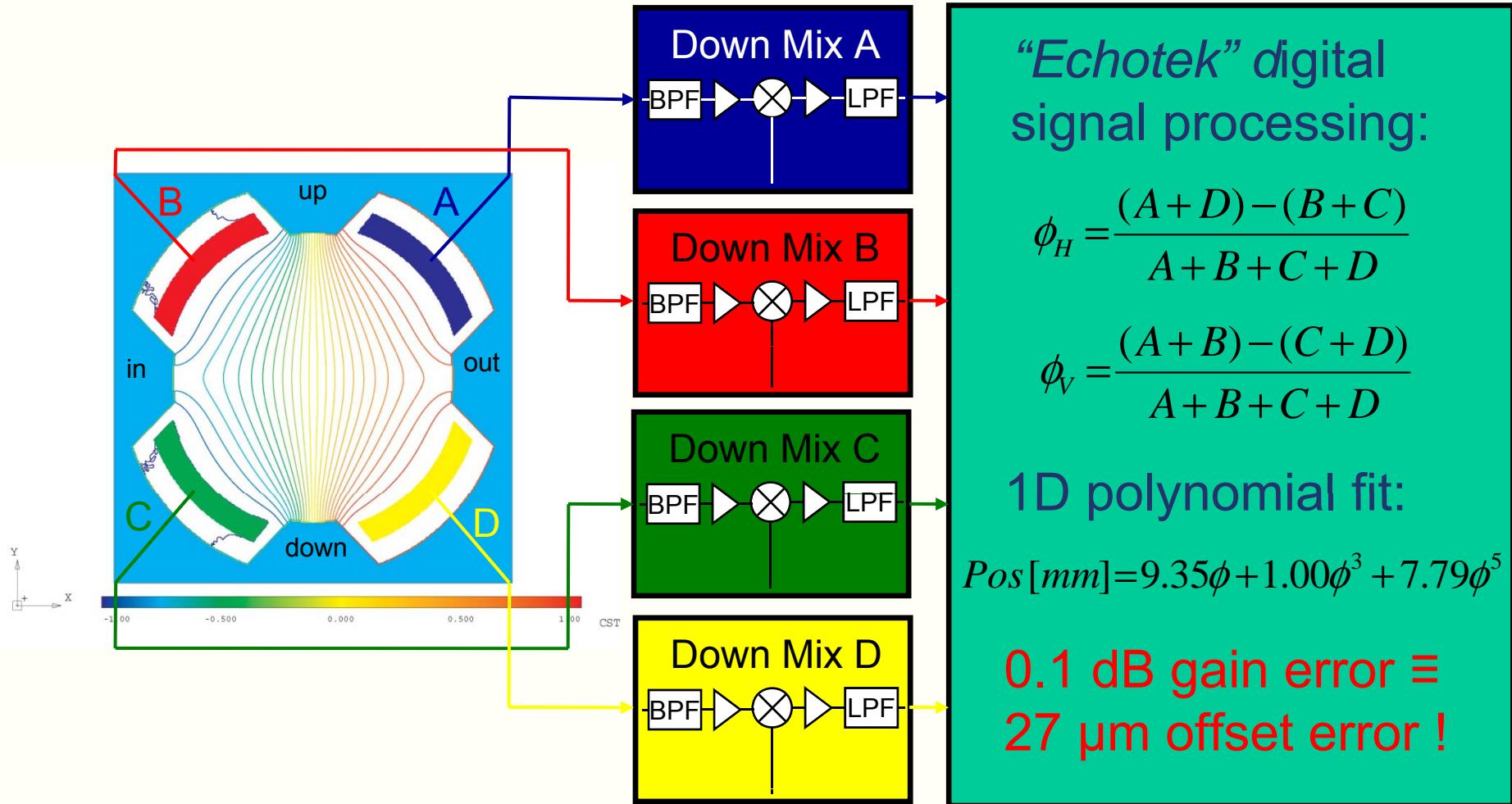
Button-style BPM Pickup

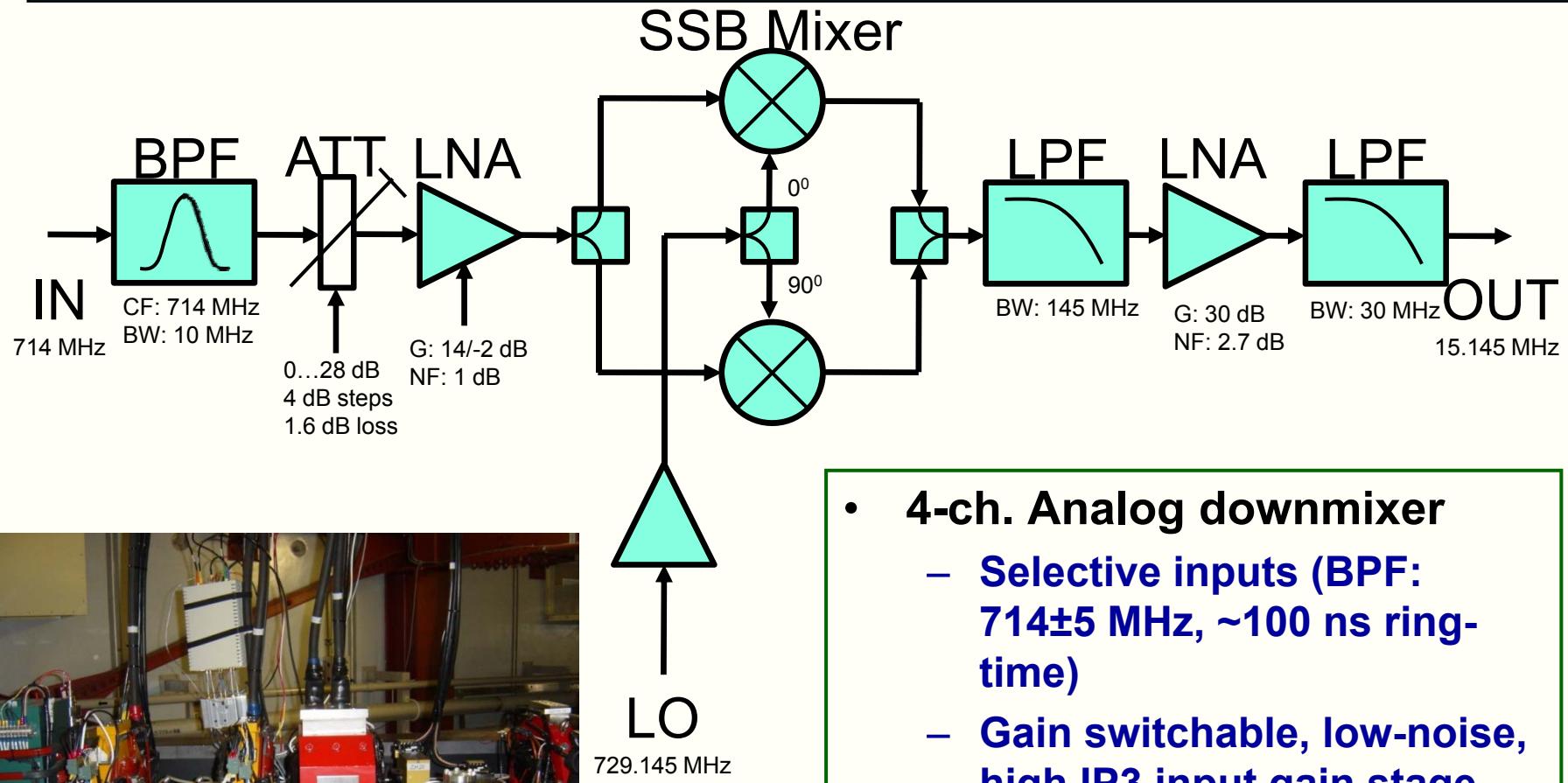


Button:
transfer
impedance

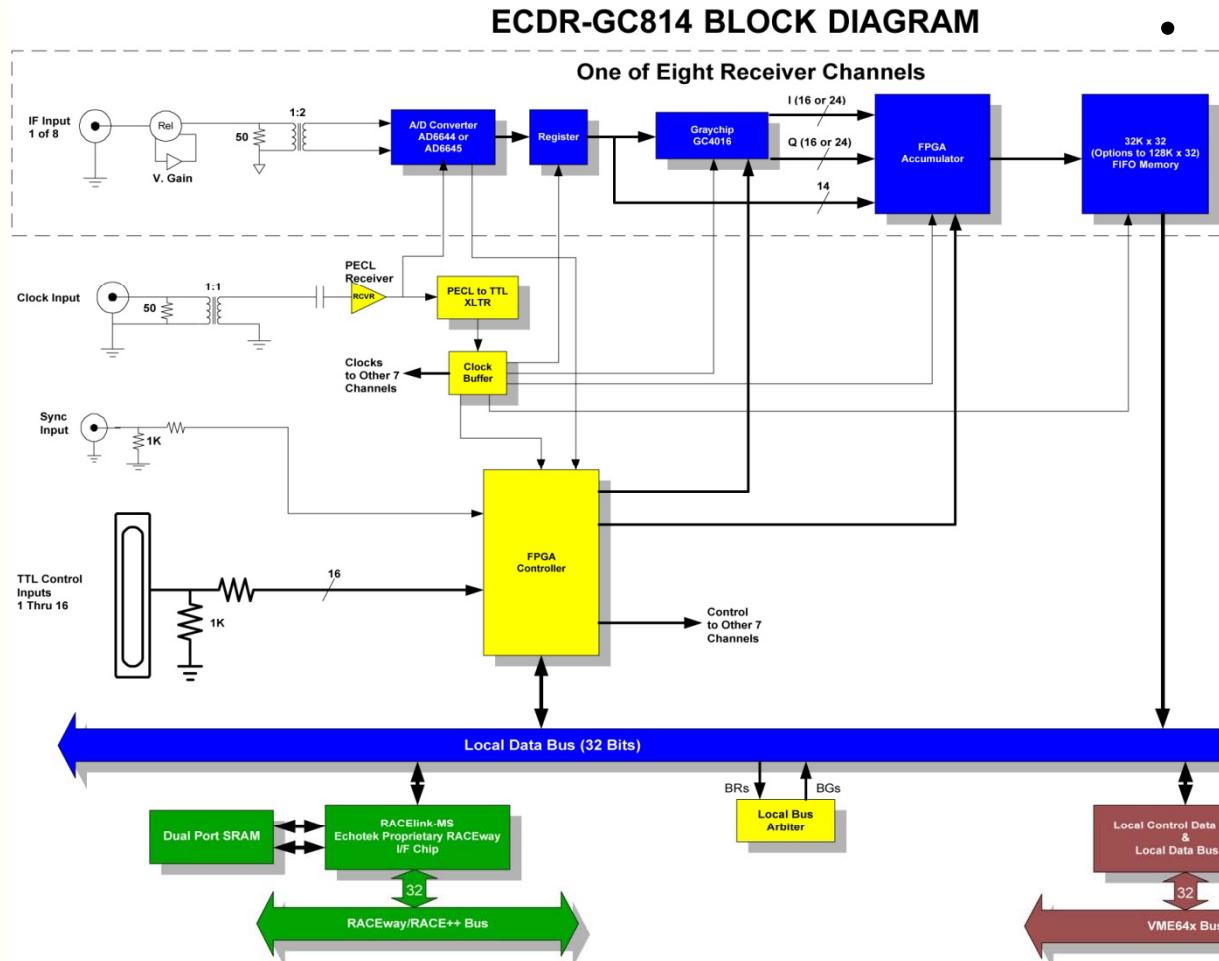


ilc Beam Position Signal Processing



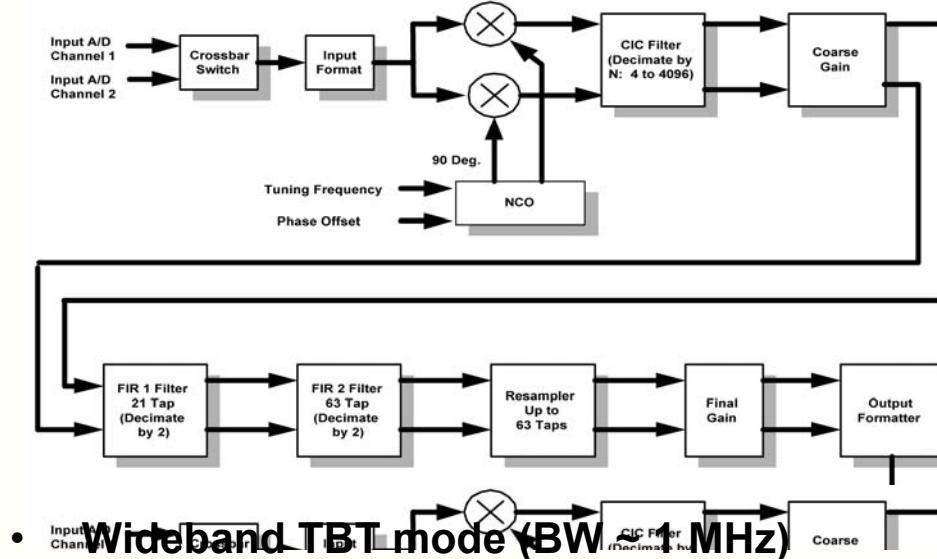


- **4-ch. Analog downmixer**
 - Selective inputs (BPF: 714 ± 5 MHz, ~100 ns ring-time)
 - Gain switchable, low-noise, high IP3 input gain stage
 - Image rejection (SSB) mixer
 - 15.1 MHz high gain, ultralinear IF stage



- **Echotek digital receiver**
 - 8-ch VME64x module
 - Analog Devices 14-bit 105 MS/s AD6645
 - Each ADC channel: *Texas Instruments 4-ch GC4016 “Graychip” digital downconverter*
 - 128 kWord FIFO



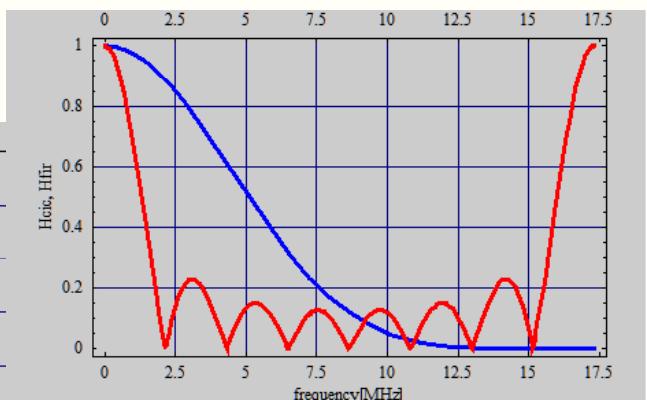
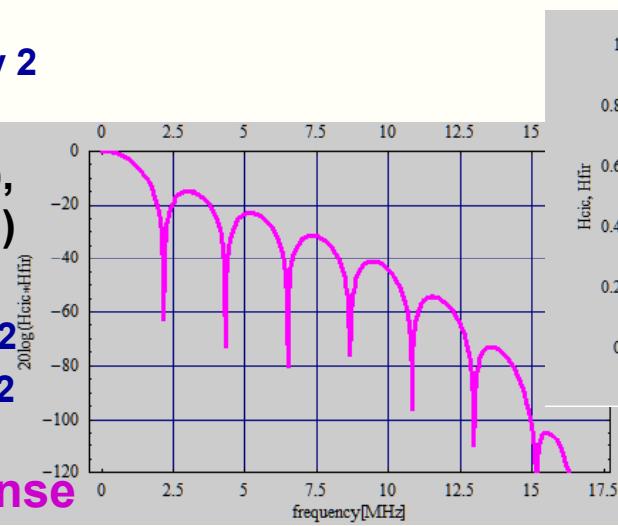


• **Wideband TBT mode (BW ~ 1 MHz)**

- 5 stage CIC: decimate by 4
 - CFIR: 7-tap boxcar, decimate by 2
 - PFIR 1-tap, no decimation
- **Narrowband mode (BW ~ 1 kHz), $t_{dec} = 158.7 \mu\text{s}$, 1280 pt (~200 ms)**
- 5 stage CIC: decimate by 2746
 - CFIR: 21-tap RRC, decimate by 2
 - PFIR: 63-tap RRC, decimate by 2

WB mode magnitude response

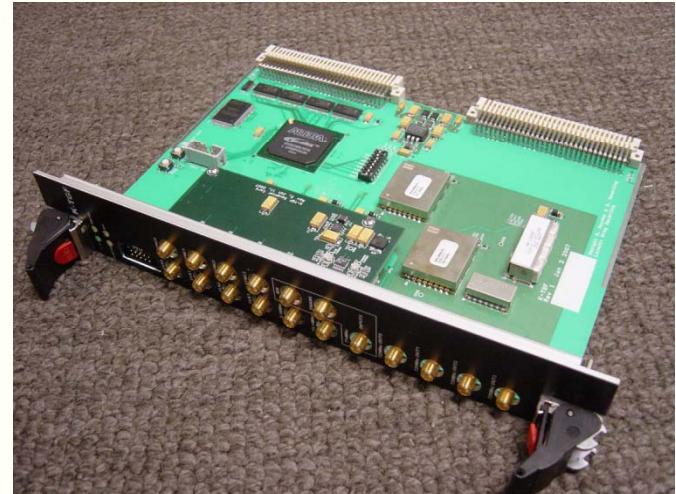
- **Graychip digital downconverter**
 - 4 independent channels per ADC
 - NCO set to $f_{IF} = 15.145 \text{ MHz}$ (downconvert to DC baseband)
 - ADC clock set to 32 samples per revolution: $f_{CLK} = 32 \times f_{rev} = 69.2 \text{ MHz}$
 - Decimation and filtering for wide- and narrowband mode using CIC and FIR digital filters
 - Simultaneous DDC operation of beam and calibration signals!

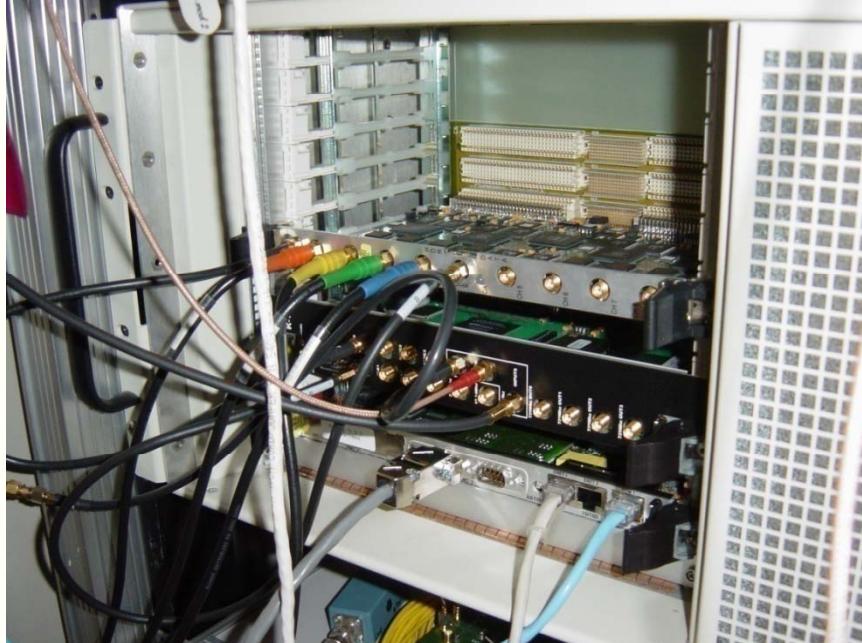


WB CIC response

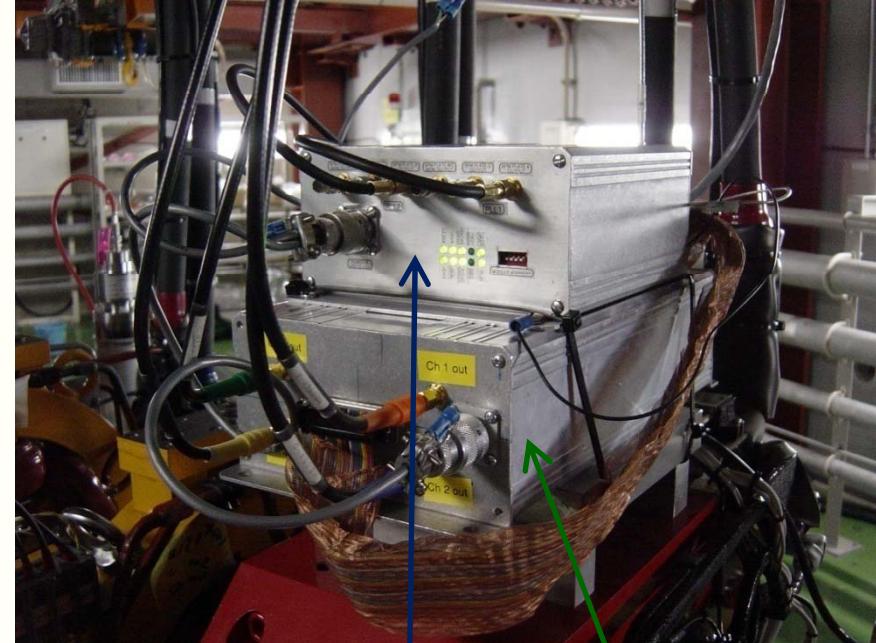
WB FIR response

- **VME Timing module:**
 - $f_{\text{CLK}} = f_{\text{RF}} * 32 / 330 = 69.236 \text{ MHz}$ clock signals (4x)
 - $t_{\text{rev}} = 462.2 \text{ ns}$ turn marker signals (4x),
0...115 double-buckets (2.8 ns) delayable
 - To f_{RF} phase-locked $f_{\text{LO}} = 729.145 \text{ MHz}$
 - Auxiliary f_{rev} and f_{IF} signals
- **Motorola 5500 VME CPU:**
 - Data collection and normalization
 - Box-car post-processing filter (20 ms)
 - Local diagnostic and control software
 - EPICS control interface
- **Calibration & remote control unit (prototype):**
 - To f_{RF} phase-locked $f_{\text{CAL}} \approx 714 \text{ MHz}$ (*Analog Devices ADF4153*)
 - In-passband, through button-BPM, or reflected signal calibration
 - 2nd and 3rd *Graychip* channels for CAL signal downconversion
 - CAN-bus remote control functions (attenuation, temperature, etc.)

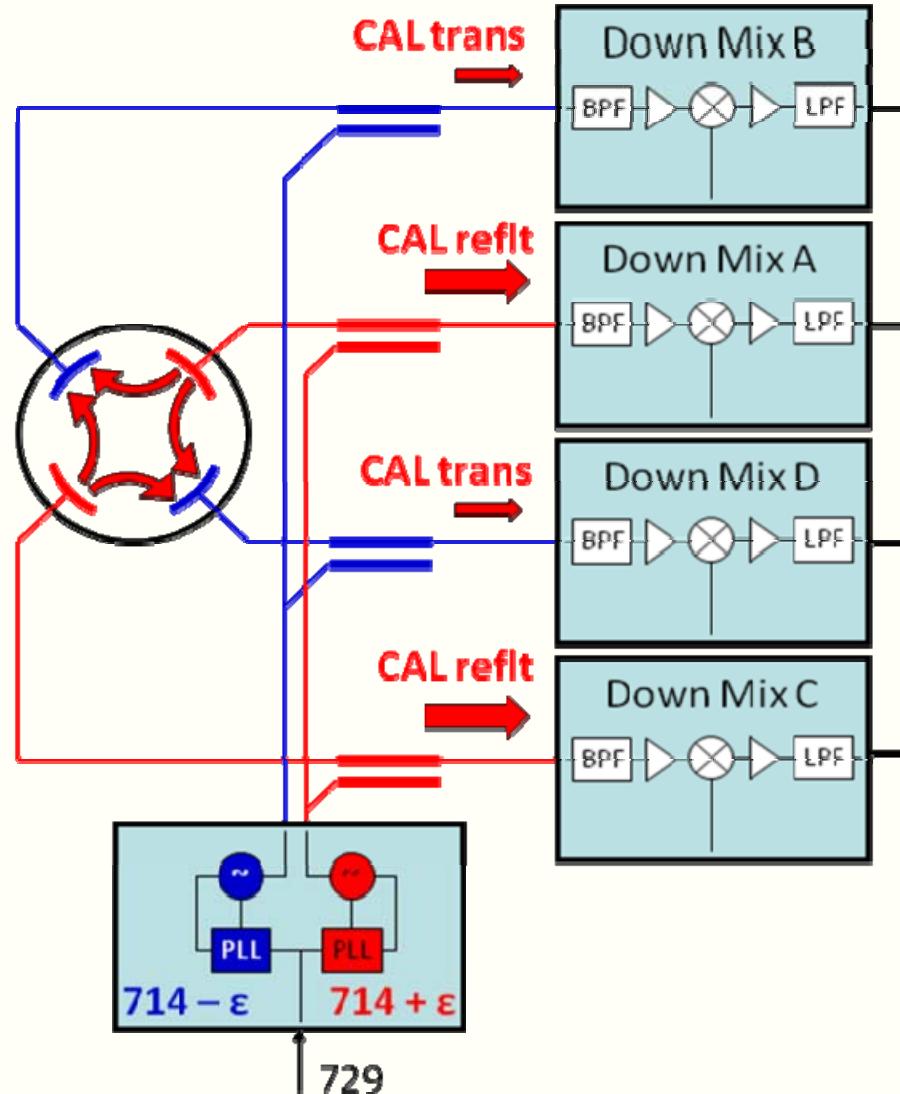




- Mini VME crate accommodating:
 - **Motorola 5500 CPU**
 - **PMC CAN bus interface ECAN-2**
 - **Timing module TGF**
 - **Echotek digital receiver module**



- BPM #54 prototype installation (temporary):
 - **CAN bus remote control & CAL signal**
 - **PLL unit (Fermilab)**
 - **4 ch. Downconverter unit (SLAC)**



- **2 calibration tones:**
 - $714 + \epsilon$ MHz
 - $714 - \epsilon$ MHz
- In passband of the downconverter
- Coupled through the button BPM
- Alternative: Reflected CAL signal
- **On-line calibration**
 - In presence of beam signals
 - Available only in narrowband mode
 - Using separate Graychip channels

- **Calibration tone frequencies:**

- $f_{\text{CALx}} = 713.6 \text{ MHz}$
 - $f_{\text{CALy}} = 714.4 \text{ MHz}$

- **Calibration procedure:**

- **Correction values:**

$$A_{\text{Corr}} = \frac{A_{\text{CAL}} + B_{\text{CAL}} + C_{\text{CAL}} + D_{\text{CAL}}}{4A_{\text{CAL}}}$$

$$C_{\text{Corr}} = \frac{A_{\text{CAL}} + B_{\text{CAL}} + C_{\text{CAL}} + D_{\text{CAL}}}{4C_{\text{CAL}}}$$

$$B_{\text{Corr}} = \frac{A_{\text{CAL}} + B_{\text{CAL}} + C_{\text{CAL}} + D_{\text{CAL}}}{4B_{\text{CAL}}}$$

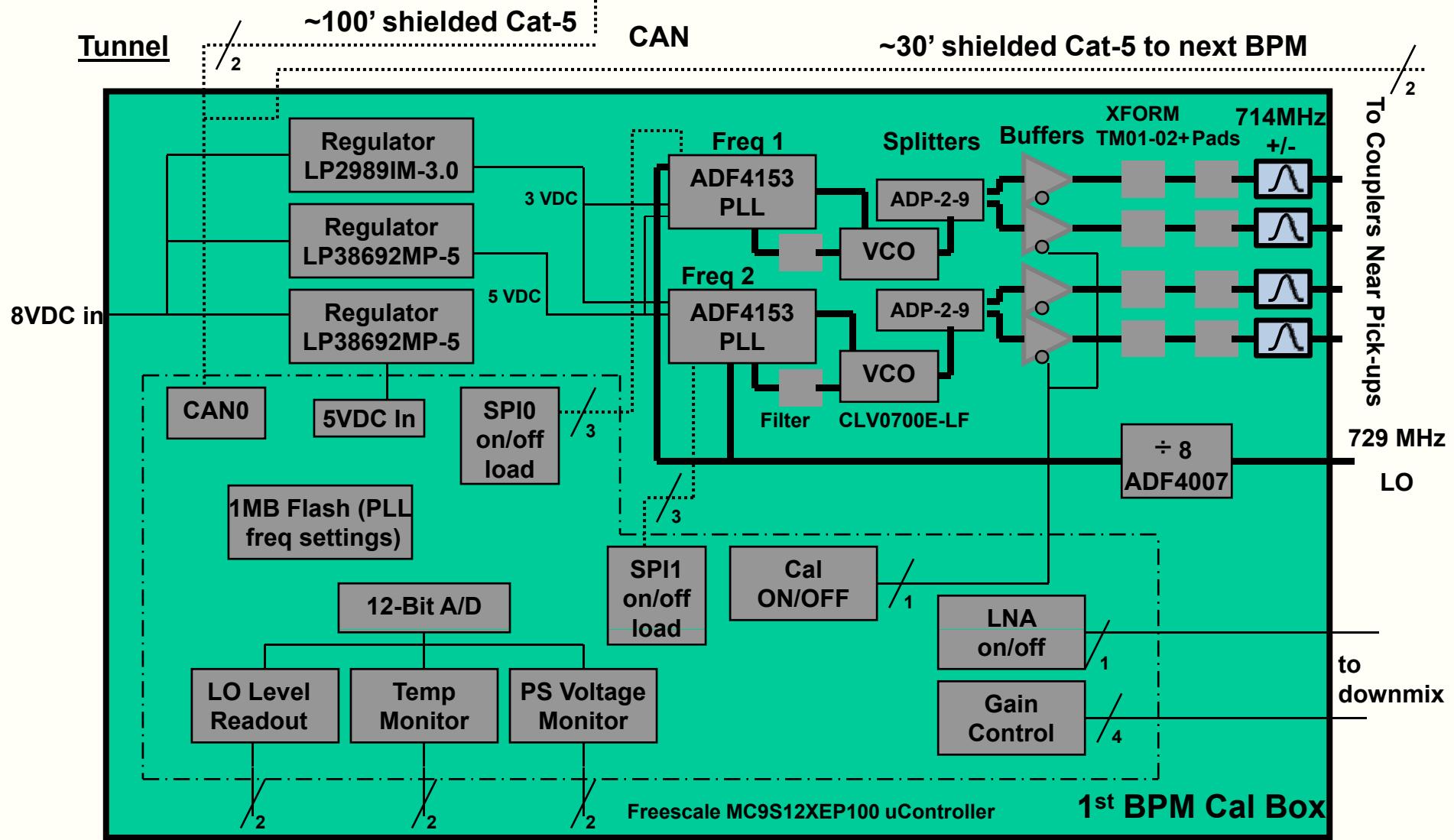
$$D_{\text{Corr}} = \frac{A_{\text{CAL}} + B_{\text{CAL}} + C_{\text{CAL}} + D_{\text{CAL}}}{4D_{\text{CAL}}}$$

- **Corrected beam positions:**

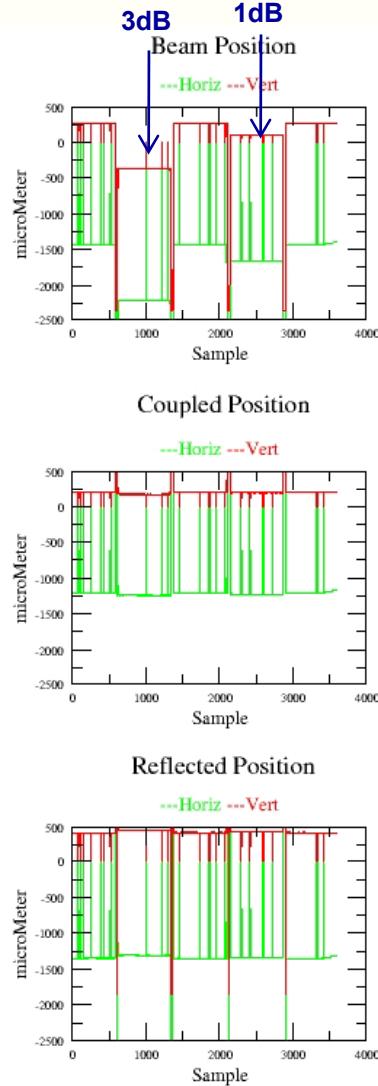
$$\phi_{H\text{corr}} = \frac{(AA_{\text{Corr}} + DD_{\text{Corr}}) - (BB_{\text{Corr}} + CC_{\text{Corr}})}{AA_{\text{Corr}} + BB_{\text{Corr}} + CC_{\text{Corr}} + DD_{\text{Corr}}}$$

$$\phi_{V\text{corr}} = \frac{(AA_{\text{Corr}} + BB_{\text{Corr}}) - (CC_{\text{Corr}} + DD_{\text{Corr}})}{AA_{\text{Corr}} + BB_{\text{Corr}} + CC_{\text{Corr}} + DD_{\text{Corr}}}$$

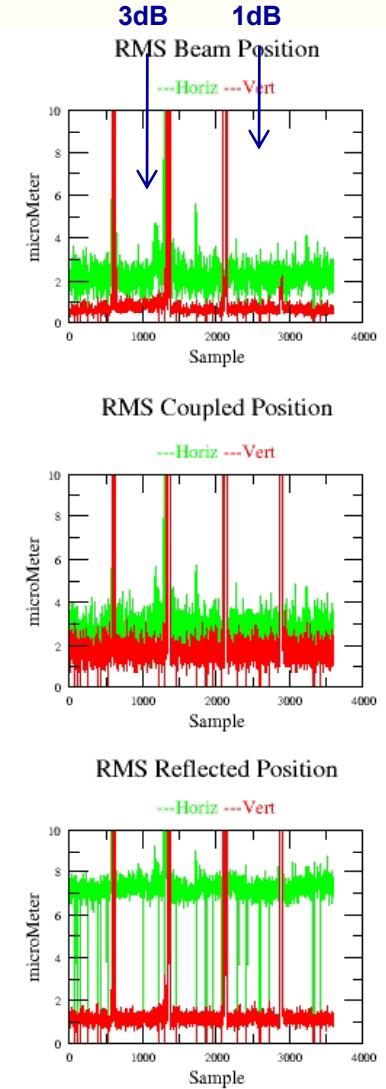
Block Diagram



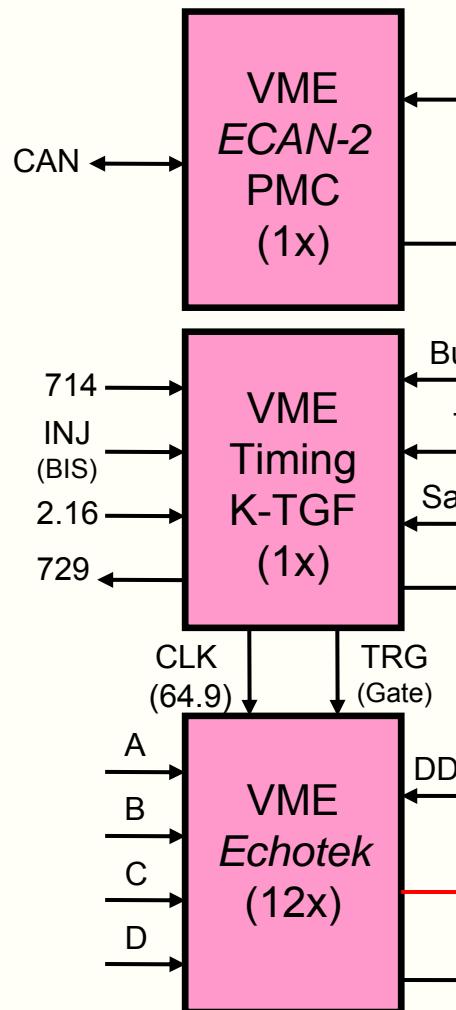
- **PMC-ECAN-2 Bus controller**
 - Commercial PMC CAN bus controller
 - VxWorks PPC driver support
- **Freescale MC9S12XEP100 16-bit µController**
 - Serial interface support (CAN, I²C, RS485, etc.)
 - 8/10/12-bit ADC's (2x16 ch.), timers, I/O, etc.
 - Up to 1M flash, 64k RAM, 4k EEPROM
- **Analog Devices AD4153 fractional PLL**
 - Successfully tested the calibration generation during the last run (729 MHz locking, $714 \pm \epsilon$ MHz CAL signals).
 - Selectable frequency, on/off switch, acceptable phase noise and spurious harmonics.



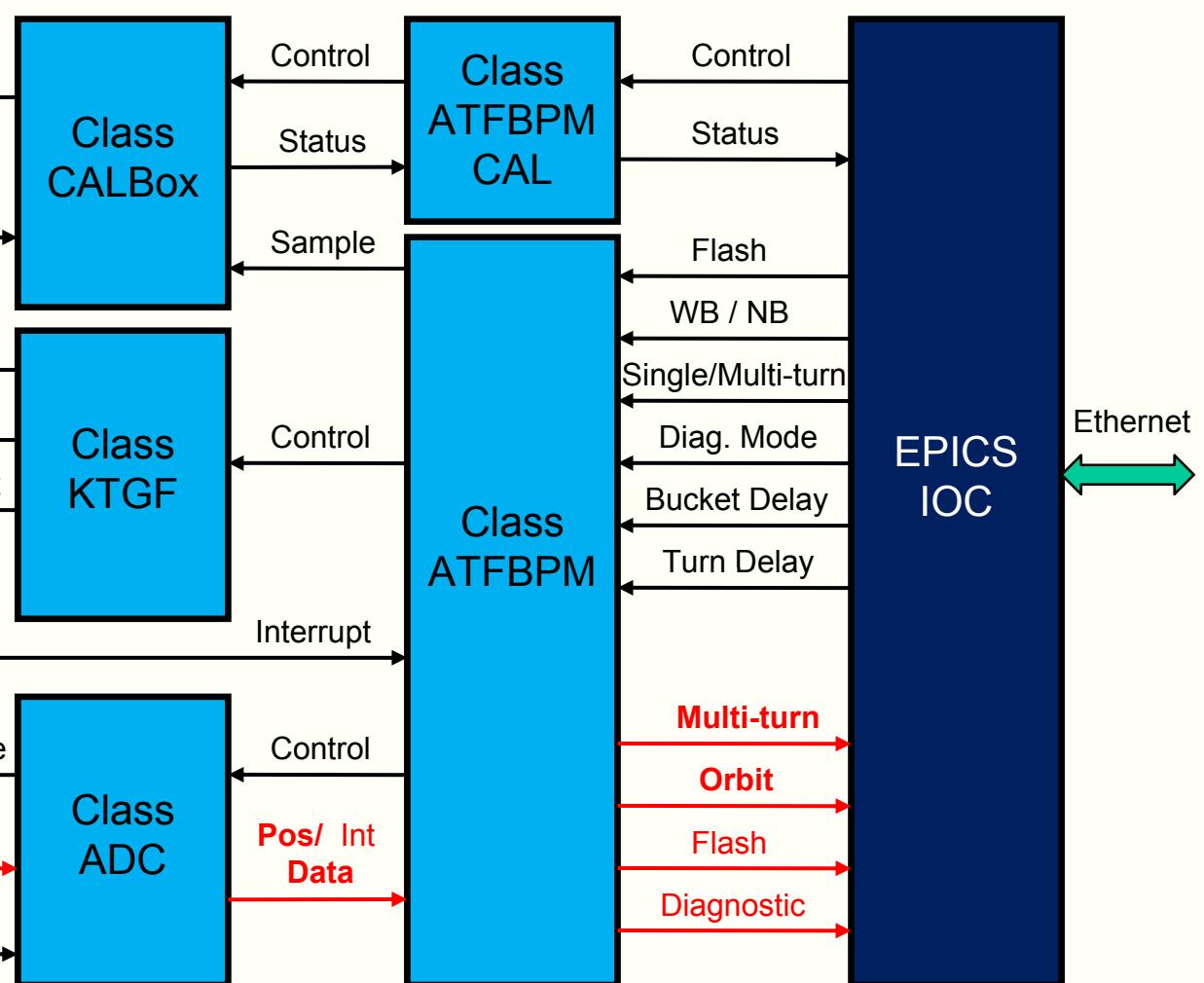
- Calibration on, datalogger on
- Comparing uncorrected, corrected (coupled-through), and corrected (reflected)
- Introduce large 3 & 1 dB gain errors.
- Automatic correction compensates the gain error almost completely!!
- Corrected beam position shows a slight increase of the RMS error (to be further studies!).



VME Hardware



Motorola 5500 µP Software (VxWorks)



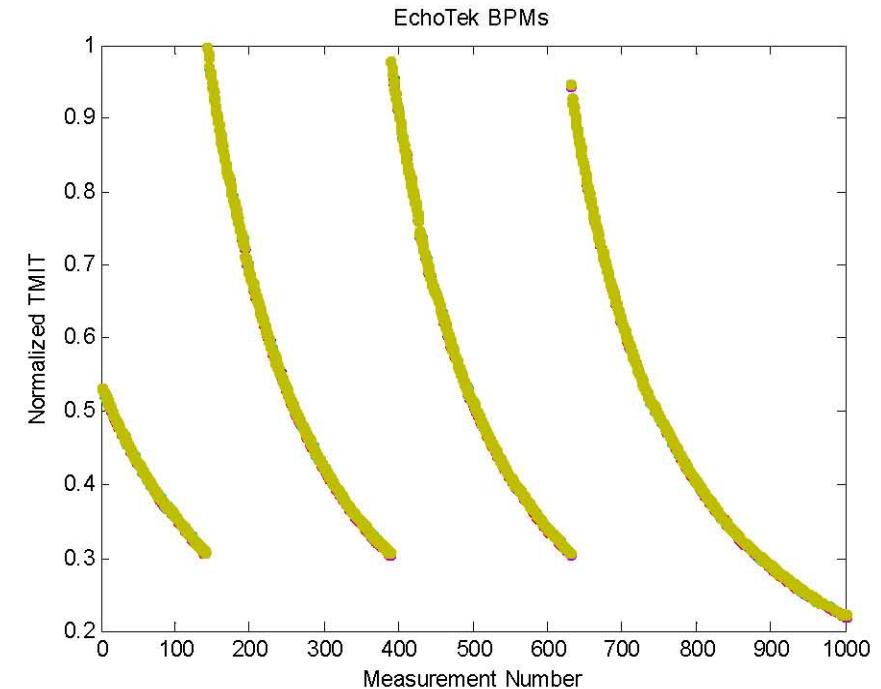
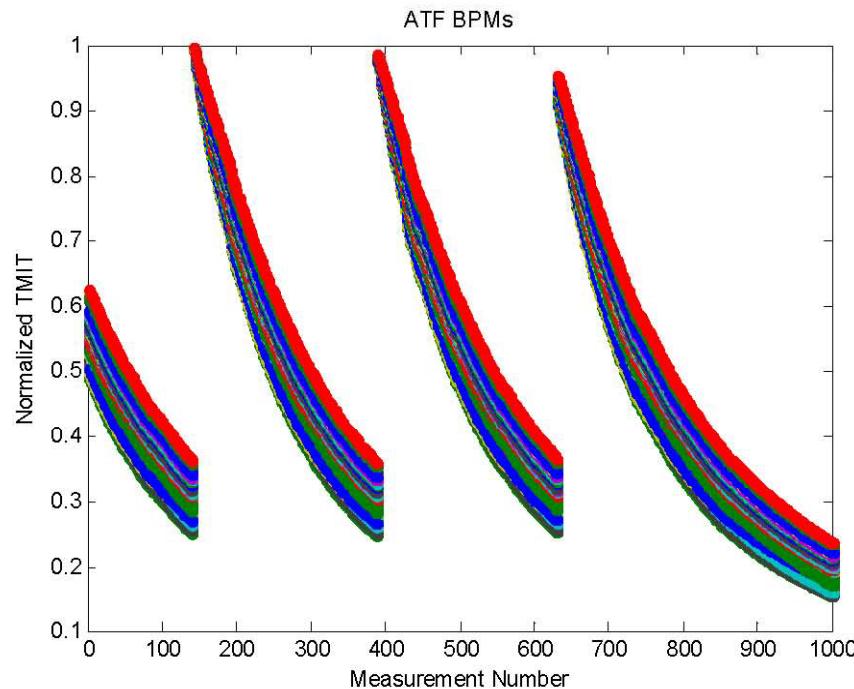


EPICS Data Acquisition



	Multi-turn	Orbit	Flash
Wide-Band	Samples: 4096 Samples/turn: 4 Turns: 1024 POSITION Intensity	Average Samples: 4096 Turns: 1024 POSITION (RMS & StdDev) Intensity (RMS & StdDev)	N th Sample (1) POSITION Intensity
Narrow-Band	Samples: 1280 μsec/Sample: 158.73 Turns: 439600 POSITION Intensity	Average Samples: 126 (50 Hz Boxcar) Turns: 43273 POSITION (RMS & StdDev) Intensity (RMS & StdDev)	N th Sample (1) POSITION Intensity

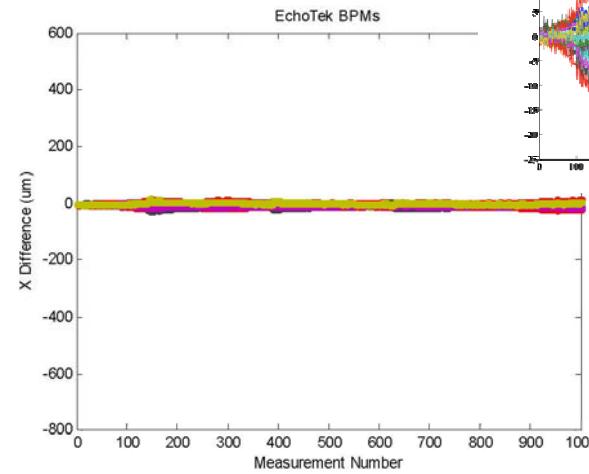
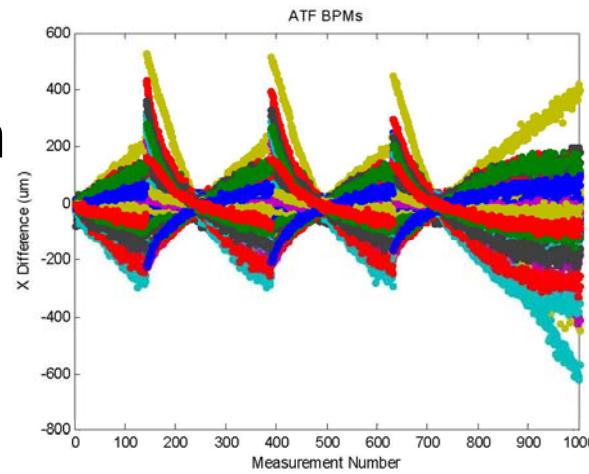
Normalized Intensities



Scrubbing Mode, Positions

070518

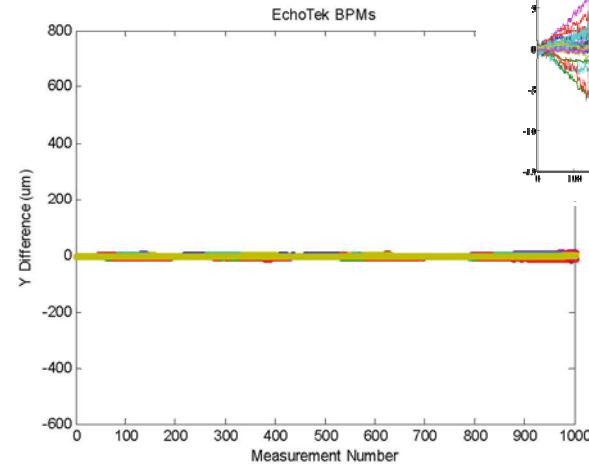
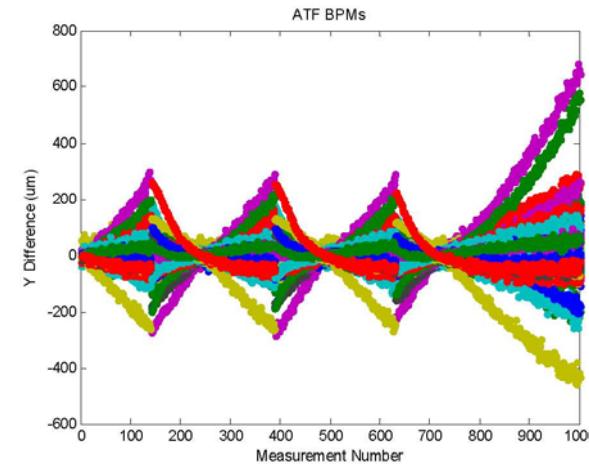
$\pm 700 \text{ }\mu\text{m}$



$\pm 25 \text{ }\mu\text{m}$

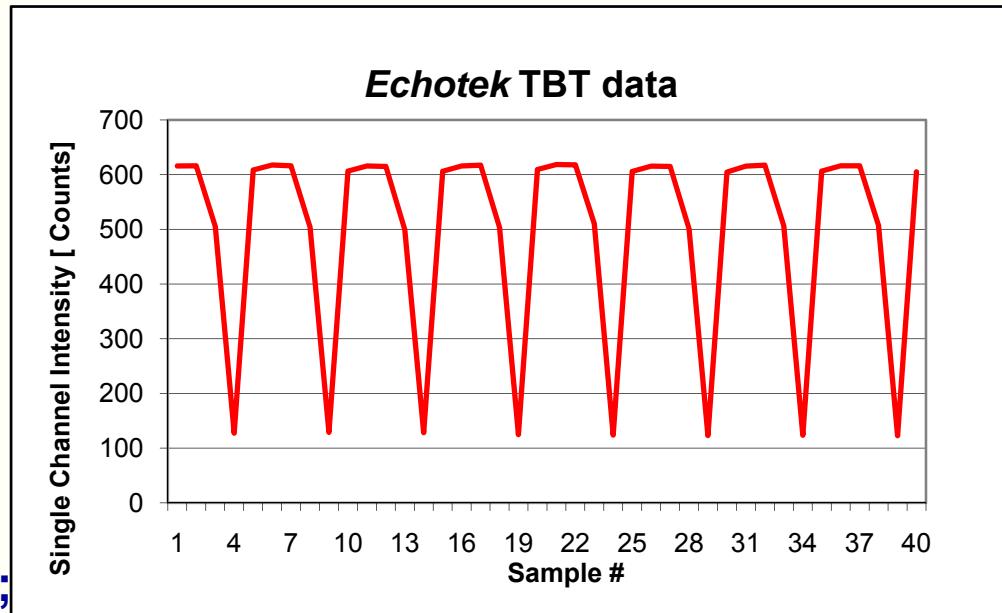
Vertical Position

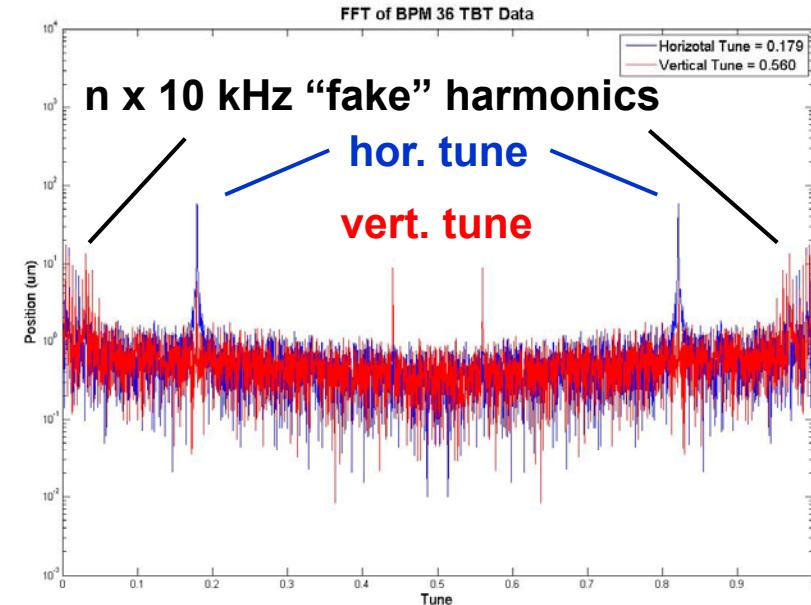
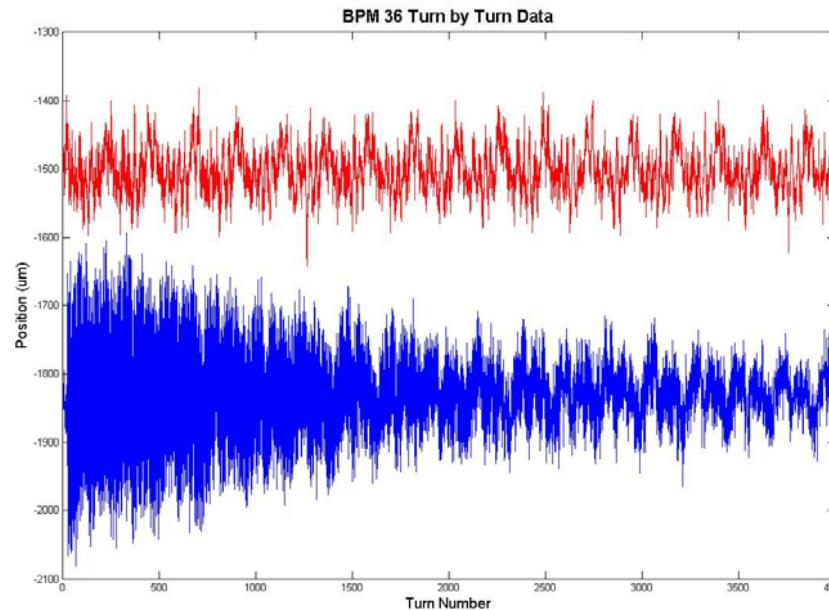
$\pm 700 \text{ }\mu\text{m}$



$\pm 15 \text{ }\mu\text{m}$

- Several “issues” had to be resolved:
 - CIC & FIR digital filter impulse responses to resolve true turn-by-turn data (no “smearing”)
 - Timing issues, e.g. channel-to-channel, as well as between BPMs and “houses” (VME crates); and of course the usual “seam” problem.
- In particular for the kicked beam TBT response tests:
 - Vertical beta at pinger is 0.5 m (12 times smaller than the horizontal one): we had to resort to injection oscillations -> lower resolution.





- Turn-by-Turn data BPM #36 (pinger: On)
- Identifying hor. and vert. tune lines (387 kHz, 1.212 MHz).
- Observed short time, broadband TBT resolution: few μm !
- Observation of “fake” harmonics at $n \times 10$ kHz (not f_s), due to power supply EMI in the analog downconverter unit!

- TBT data at the j^{th} BPM following a single kick in the z-plane ($z \equiv x, y$):

$$z_n^j = \frac{1}{2} \sqrt{\beta_z^j} e^{i\Phi_z^j} A_z e^{iQ_z(\theta_j + 2\pi n)} + c.c.$$

– with

$$n \equiv \text{turn number}, \quad A_z = |A_z| e^{i\delta_z} \equiv \text{constant of motion}$$

$$\Phi_z \equiv \mu_z - Q_z \theta \quad (\text{periodic phase function})$$

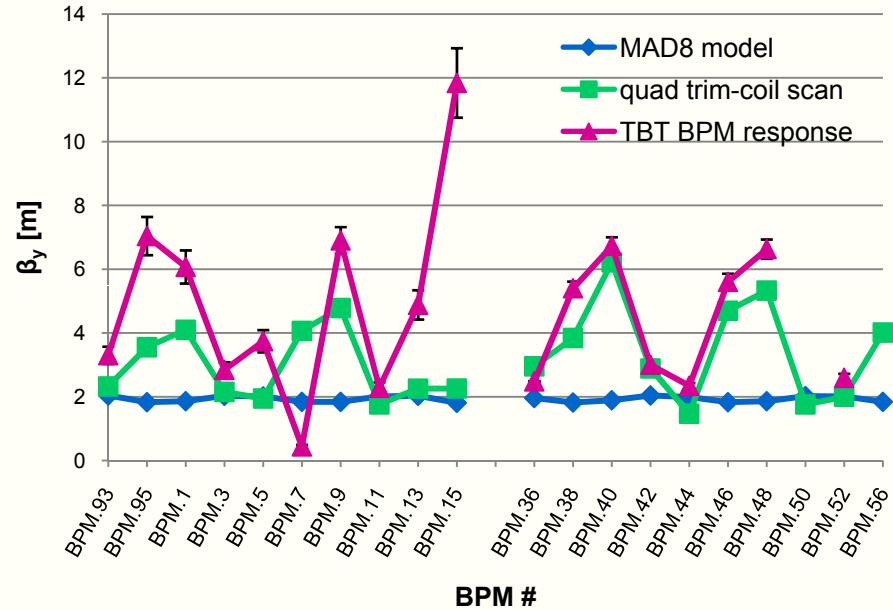
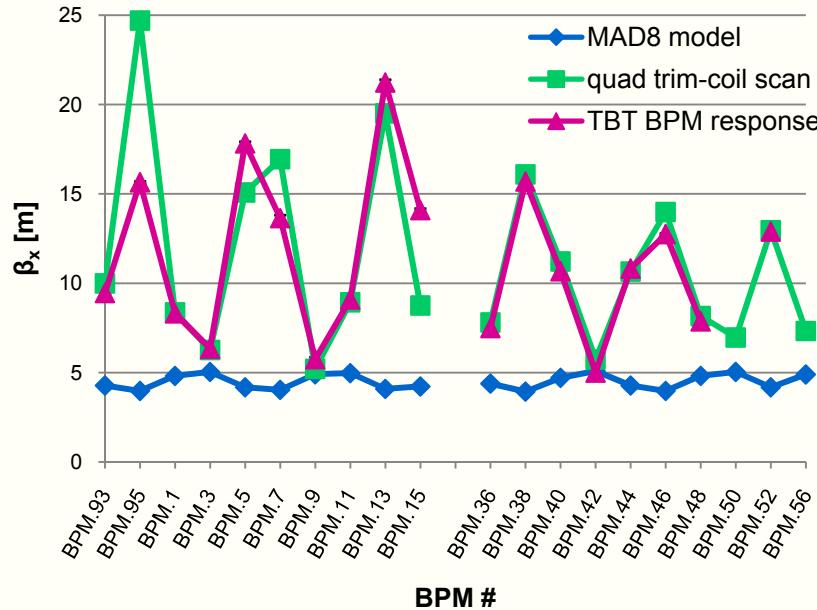
- Twiss functions:

$$\beta_z^j = |Z_j(Q_z)|^2 / A_z^2 \quad \mu_z^j = \arg(Z_j) - \delta_z$$

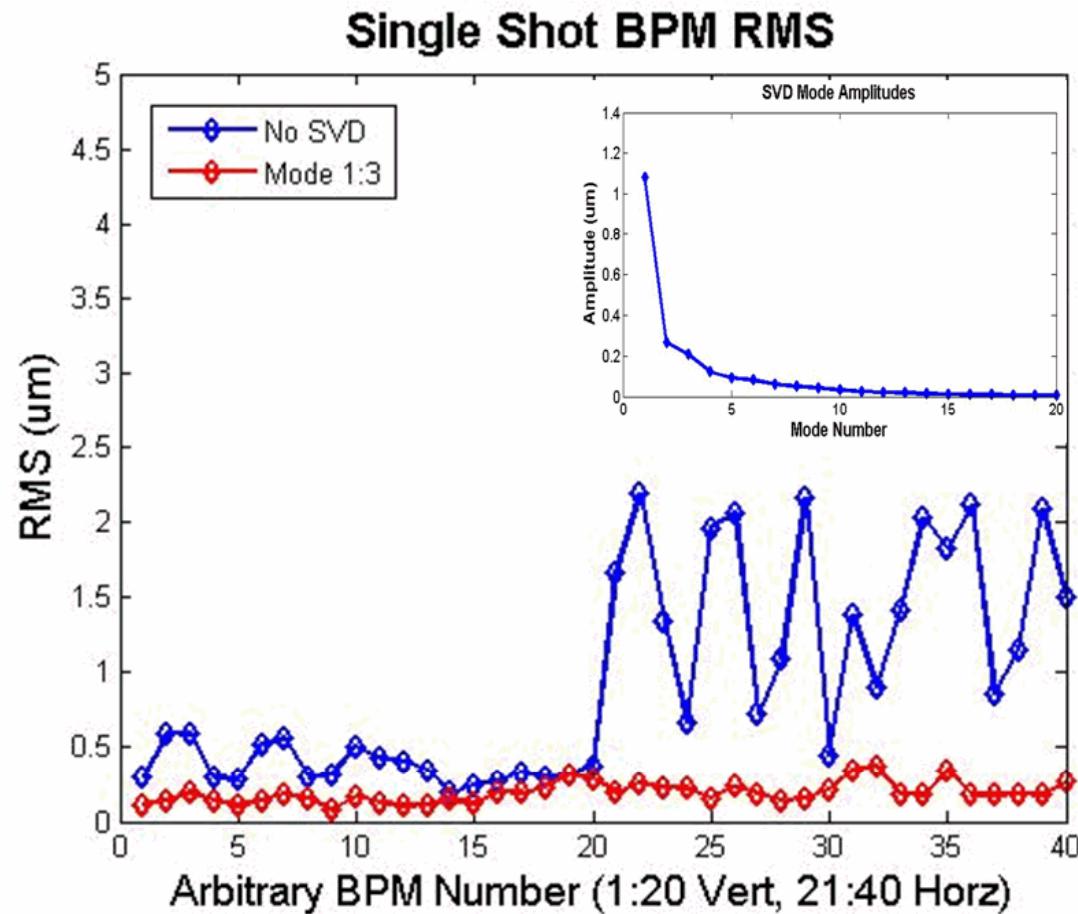
$Z_j(Q_z)$ \equiv Fourier component of z_j

- Amplitude fit:

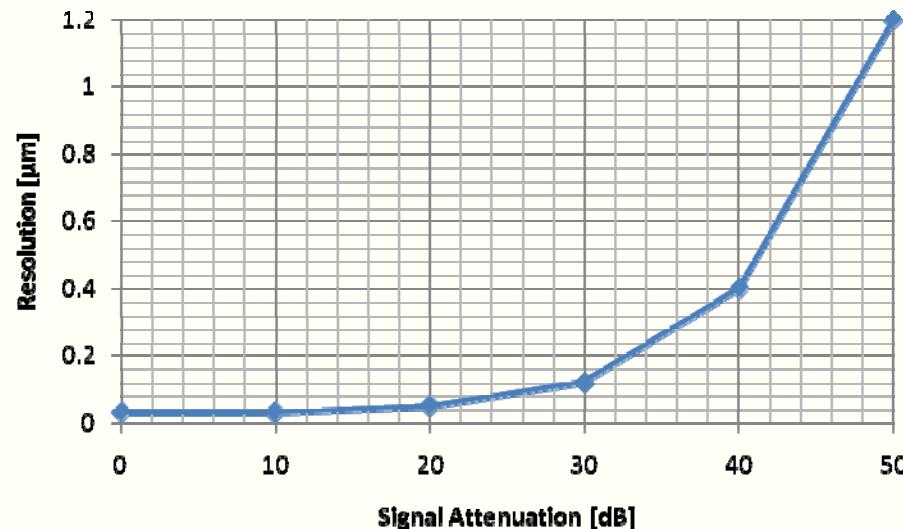
$$|A_z|^2 = \frac{\sum_j 1/\beta_z^{0j}}{\sum_j 1/|Z_j(Q_z)|^2}$$



- **MAD8 model (M. Woodley, marginal differences wrt. Kuroda SAD model).**
- **Nearby quadrupole trim coil scan (May 2008).**
- **TBT Fourier analysis, amplitude by fit to beta measured through trim coil scan (April 2008).**



- Triggered at turn #500,000
- ~200 ms position data per shot (1280 narrowband mode BPM measurements).
- 126 tap box car filter to reject 50 Hz:
 - ~800 nm resolution
- SVD analysis, removing modes with hor./ vert. correlation:
 - ~200 nm resolution



Theoretical:

- ADC SNR: 75 dB
- Process gain: 40.4 dB
- NF 1st gain stage: ~ 1 dB
- CAL tone level: -10 dBm
- Splitter attenuation: 6 dB
- Effective gain: ~ 100 dB
- BPM sensitivity: 240 μm/dB
- Calculated equivalent resolution: ~ 20 nm

**CAL tone resolution measurement
on BPM #56: ~30 nm(!) equiv. resolution
(no beam operation at ATF!, magnets off)**

- **Resolve known issues and defects**
 - Two defect downmix units
 - EMI interference into downmix electronics
- **Publish a revised plan to continue the BPM upgrade!**
 - Integrated downmix-CAL prototype, simplified RF housing and cabling.
 - **Proposal: Next upgrade step to a total 48 BPMs**
 - Install only improved downmix & CAL hardware into the ATF tunnel.
 - Utilize spare *Echotek* digital receivers
or new low-cost VME digitizers (Fermilab development)
for DDC of the BPM signals.
 - Increase ADC clock rate (32 -> 40 samples / turns)
- **Most soft-/firmware activities & beam studies:**
Remote operation!
- **Still need to demonstrate the long term offset drift stabilization.**