

NSLS-II Lattice Design Strategies

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07/10/08

Acknowledgement:

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Outline

- 1. Introduction to the linear lattice**
- 2. Linear lattice grid**
- 3. Nonlinear requirements: injection and Touschek scattering**
- 4. Minimum needed sextupole families**
- 5. Required physical aperture**
- 6. Effects of the multipole field errors**

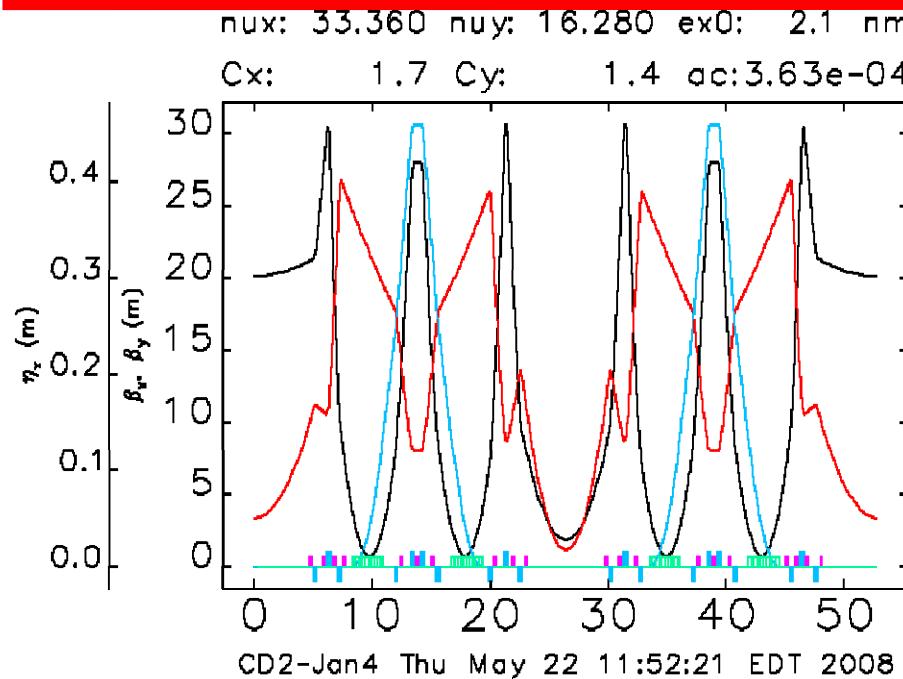
Method:

Simulation using Elegant

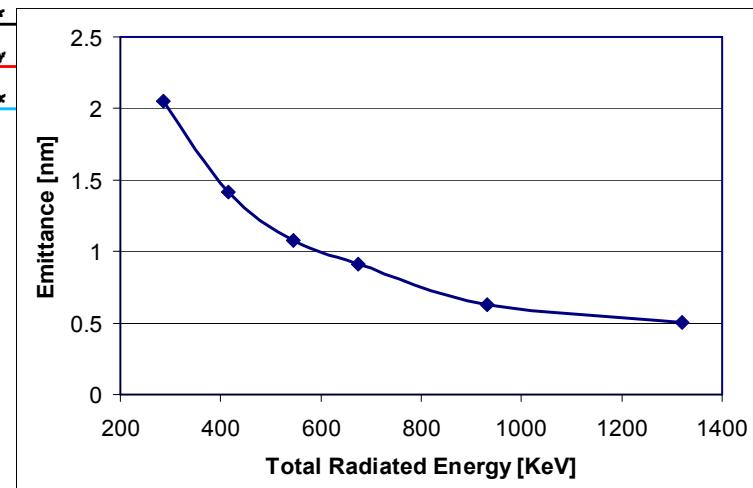
Main Design Parameters

Beam Energy	3 GeV
Circumference	792 m
Circulating current	500 mA
Total number of buckets	1320
Lifetime	3 hours
Electron beam stability size	10% beam
Top-off injection current stability	<1%
ID straights for undulators	>21
Straight length	9.3/6.6 m

Magnets and lattice



Natural emittance with 0, 1, 2, 3, 5 and 8 DWs added



Courtesy of S. Kramer

Quad. Family: 8, 10 magnets per cell

Sext. Family: 9, 10 magnets per cell

Chromaticity per cell: -3.4/-1.4

Linear Lattice design approaches

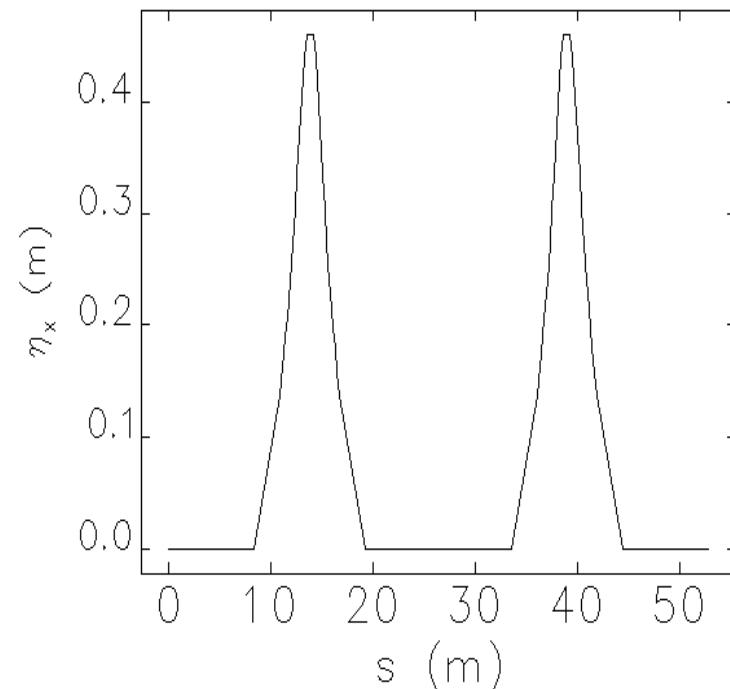
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1. Large bending radius enhances the effect of the damping wiggles

$$B = 0.4T, \rho = 25m, \begin{cases} D_x = \rho(1 - \cos \theta) \\ D_x' = \sin \theta \end{cases}$$

2. Strict double-bend-acromat

Two reasons NSLS-II is sensitive to the residual dispersion:

- 1nm emittance. For $\beta_x = 2$ m, $\eta_x = 4.5$ cm, $\beta_x \varepsilon_x \sim (\eta_x \sigma_\delta)^2$
- Damping wiggler has quantum excitation effect



Tunability: An Ensemble of Stable Solutions

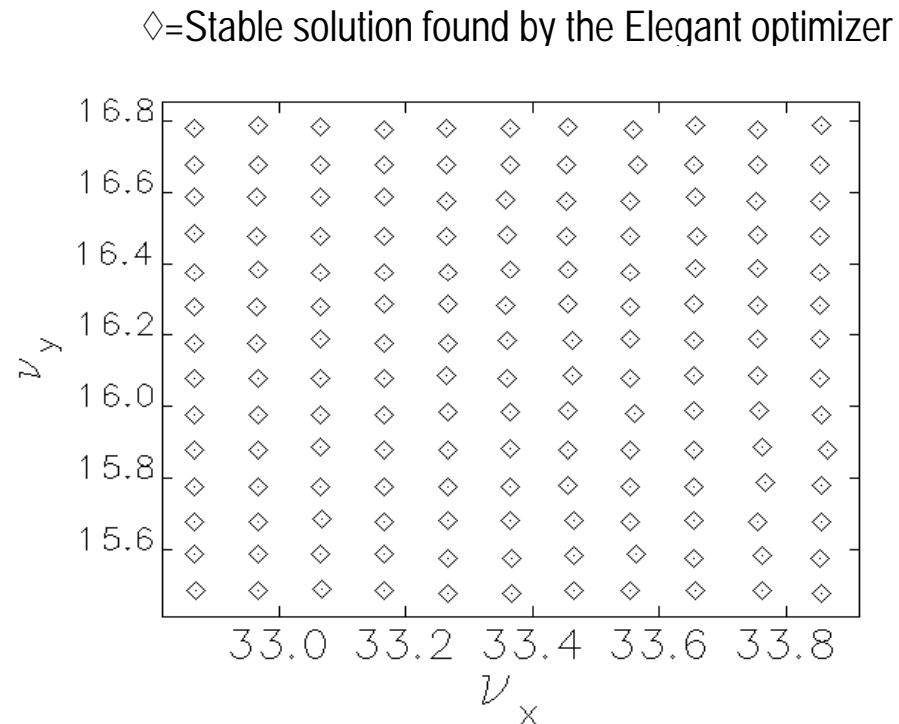
Tune scan: $\nu_x \sim 33$, $n_v \sim 16$

$$\nu_x \pm 0.5$$

$$\nu_y \pm 0.5$$

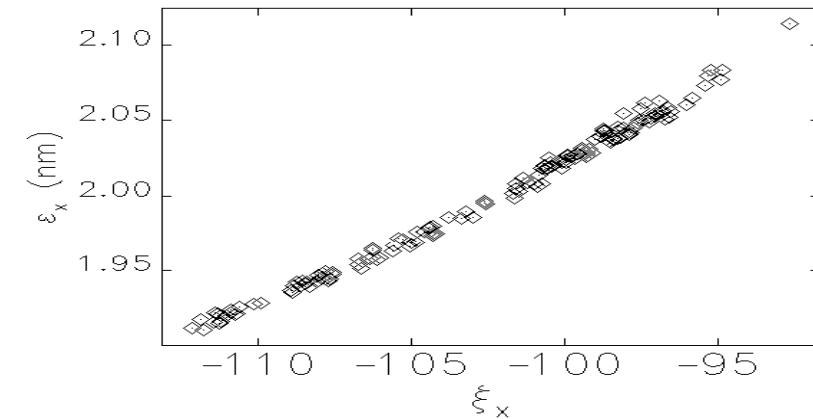
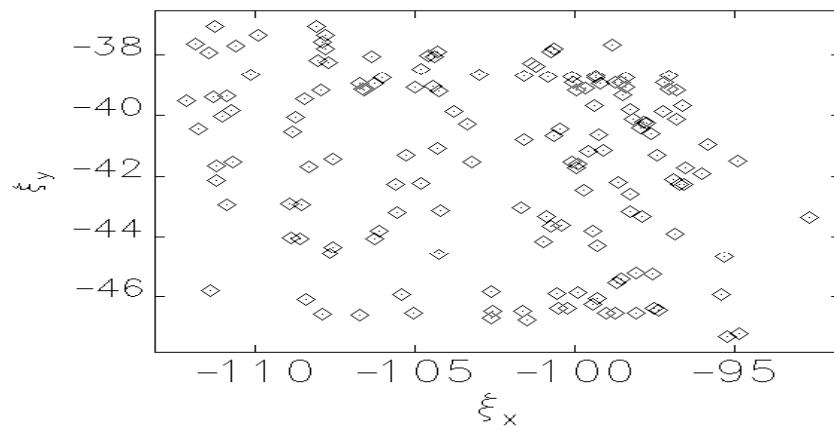
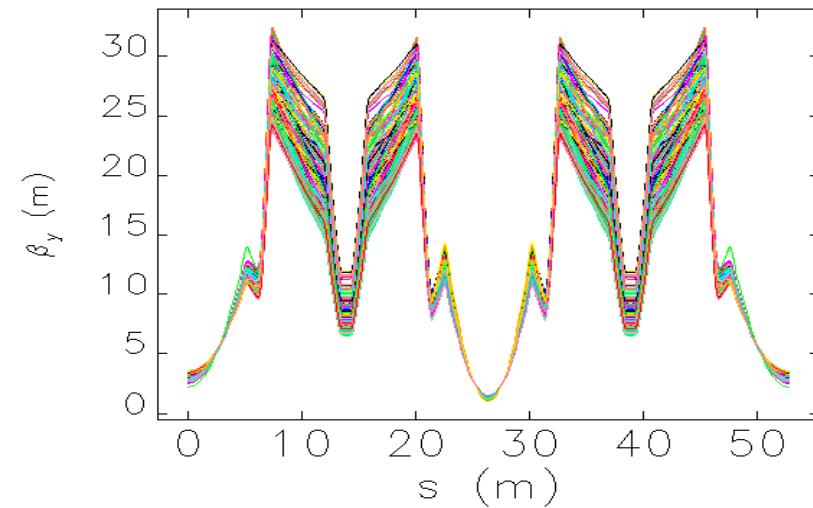
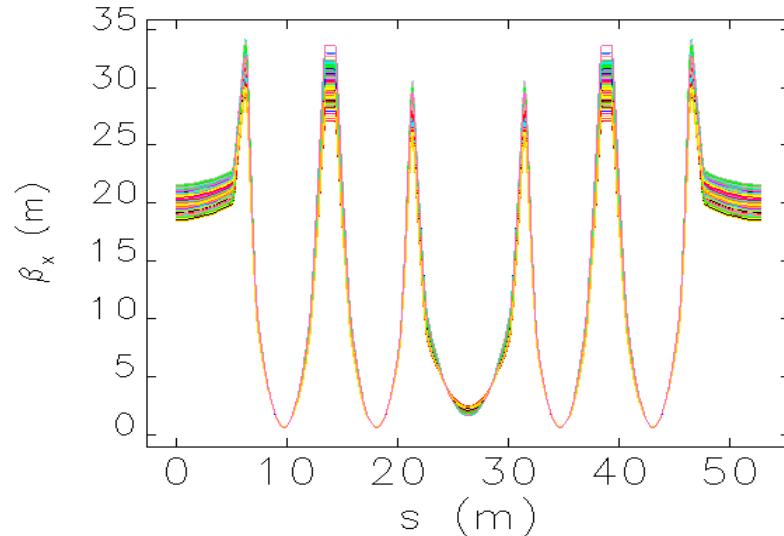
$\Delta\nu_x/\nu_x = \pm 1.5\% \text{ in horizontal}$

$\Delta\nu_y/\nu_y = \pm 3\% \text{ in vertical}$

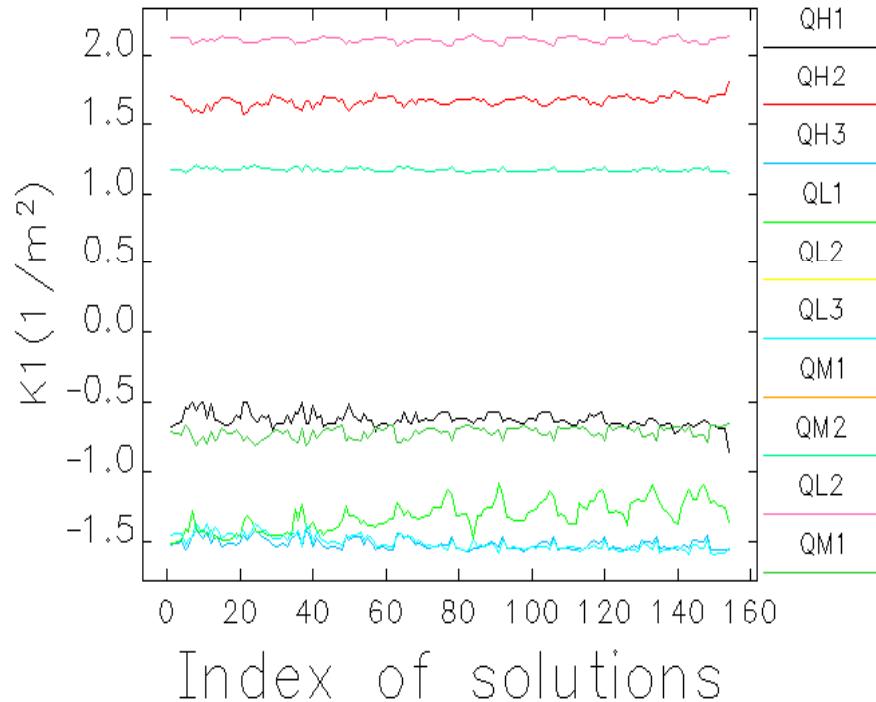


- Each solution meets the requirements on the emittance, symmetry, chromatic conditions, beta functions, and chromaticity
- This ensemble of solutions is used as input for the dynamic aperture optimization

Lattice Functions of the Solutions



Quadrupole Strength Variation Range

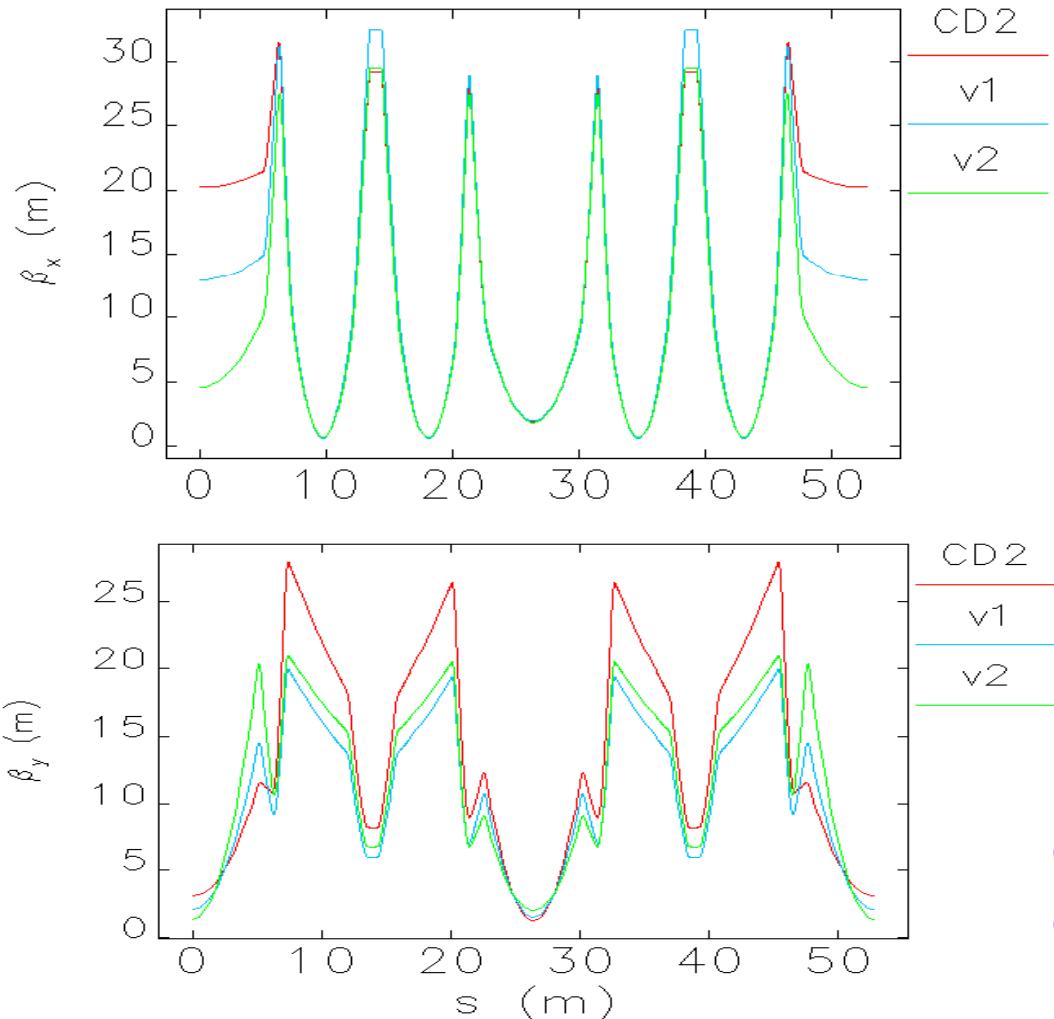


Quad	min	max	ave	$\frac{sig}{ave.}$ (%)	$\frac{max. - min.}{2 * ave.}$ (%)
QH1	-0.861	-0.500	-0.625	7.8	28.9
QH2	1.572	1.800	1.662	2.0	6.9
QH3	-1.570	-1.423	-1.520	2.5	4.8
QL1	-1.513	-1.086	-1.320	7.8	16.2
QL2	2.066	2.150	2.112	0.9	2.0
QL3	-1.597	-1.374	-1.511	3.5	7.4
QM1	-0.814	-0.657	-0.717	5.7	10.9
QM2	1.150	1.199	1.169	1.1	2.1

Variation of K_1 ($1/m^2$)

Conclusion: Although we are tuning in a large range, the relative change of the quadrupole Strength is <30%. This allows us to use weaker power supplies for certain quadrupoles.

K1 Margin for the Customization of β_x



Quad	ave	$\frac{v1 - ave}{ave} \%$	$\frac{v2 - ave}{ave} \%$
QH1	-0.625	103.06	146.55
QH2	1.662	17.58	26.35
QH3	-1.520	7.19	15.15
QL1	-1.320	7.52	11.26
QL2	2.112	1.23	1.56
QL3	-1.511	1.31	1.38
QM1	-0.717	6.32	7.54
QM2	1.169	1.22	1.44

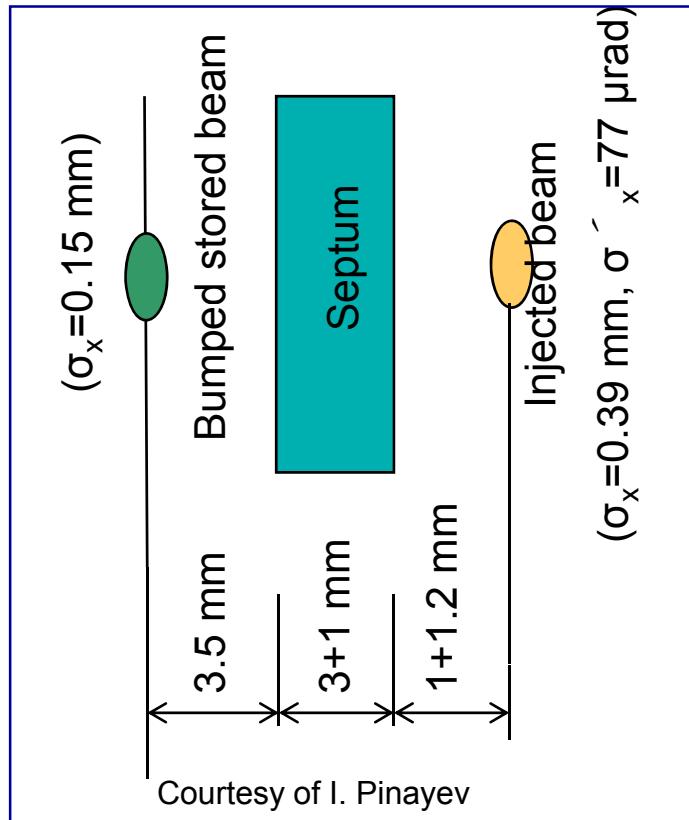
Variation of K1 ($1/m^2$)

QH2, QL2: $K1 < 2.2$, 37% margin

QM1: $K1 < 1.3$, ~ 25% margin

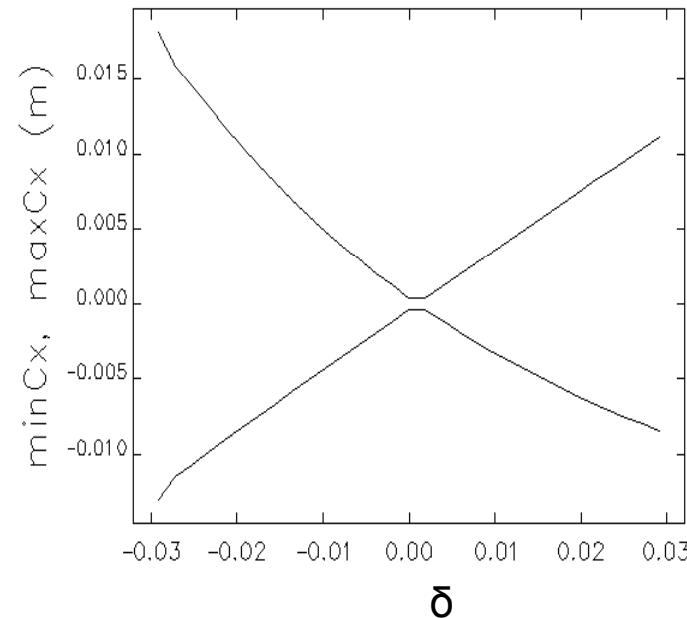
Rest: $K1 < 2$, ~25% margin

Nonlinear Design Goal



1. Sufficient dynamic aperture ($>11\text{mm}$) for injection

On momentum particle



Minimum required dynamic aperture

2. Sufficient dynamic aperture to keep Touschek scattered particles with $\delta = \pm 2.5\%$

Off momentum particle

Source of the nonlinearity

Frist order chromatic terms (5)

$$h_{11001} \rightarrow \xi_x^{(1)}$$

$$h_{00111} \rightarrow \xi_y^{(1)}$$

$$h_{10002} \rightarrow D^{(2)}$$

$$h_{20001} \rightarrow \frac{d\beta_x}{d\delta}$$

$$h_{00201} \rightarrow \frac{d\beta_y}{d\delta}$$

Amplitude tune dependence

$$\frac{\partial \nu_{x,y}}{\partial J_{x,y}}$$

Second order chromaticity

$$\xi_x^{(2)} = -\frac{1}{2}\xi_x^{(1)} + \frac{1}{8\pi} \int ds \{ K_2 D^{(2)} \beta_x - [K_1 - K_2 D^{(1)}] \frac{d\beta_x}{d\delta} \}$$

$$\xi_y^{(2)} = -\frac{1}{2}\xi_y^{(1)} - \frac{1}{8\pi} \int ds \{ K_2 D^{(2)} \beta_y + [K_1 - K_2 D^{(1)}] \frac{d\beta_y}{d\delta} \}$$

Frist order geometric terms (5)

$$h_{21000} \rightarrow \nu_x$$

$$h_{30000} \rightarrow 3\nu_x$$

$$h_{10110} \rightarrow \nu_x$$

$$h_{10020} \rightarrow \nu_x - 2\nu_y$$

$$h_{10200} \rightarrow \nu_x + 2\nu_y$$

Number of chromatic sextupole families

$$\Delta \xi^{(1)}_{x,y} = \pm \int ds K_2 D^{(1)} \beta_{x,y}$$

$$D^{(2)} = -D^{(1)} + \frac{\sqrt{\beta}}{2 \sin(\pi\nu)} \int ds (K_1 - \frac{K_2}{2} D^{(1)}) D^{(1)} \sqrt{\beta} \cos(|\Delta\Psi| - \pi\nu)$$
$$= -D^{(1)} + \frac{\sqrt{\beta}}{2 \sin(\pi\nu)} \int ds K_1 D^{(1)} \sqrt{\beta} \cos(|\Delta\Psi| - \pi\nu) - c \times \Delta \xi_x^{(1)}$$

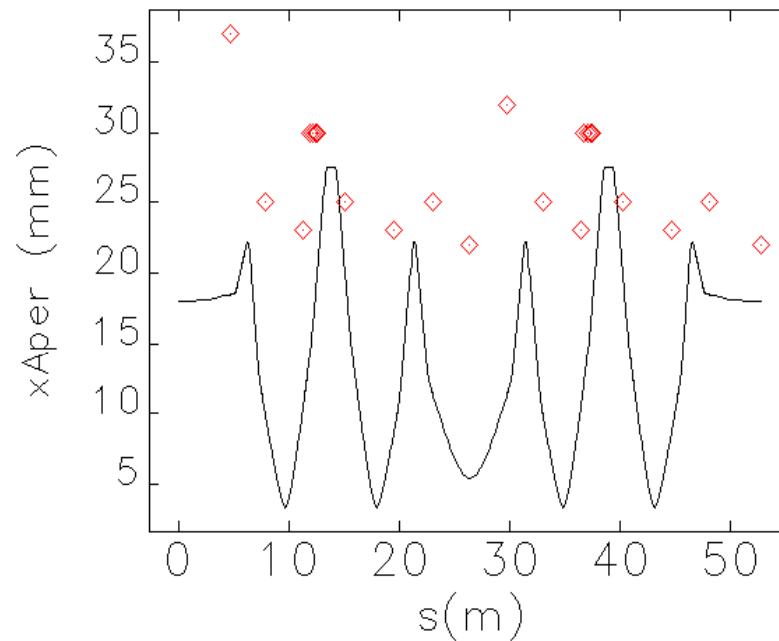
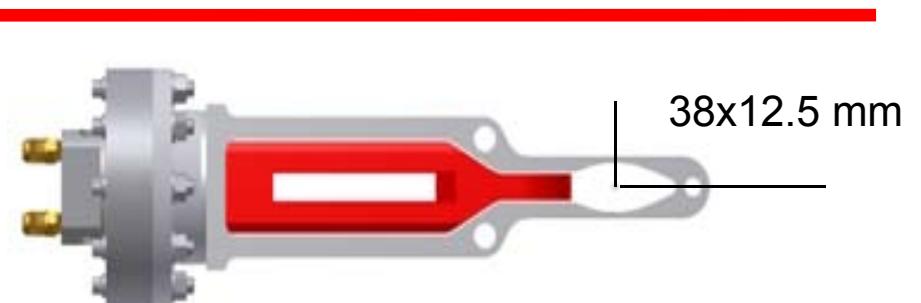
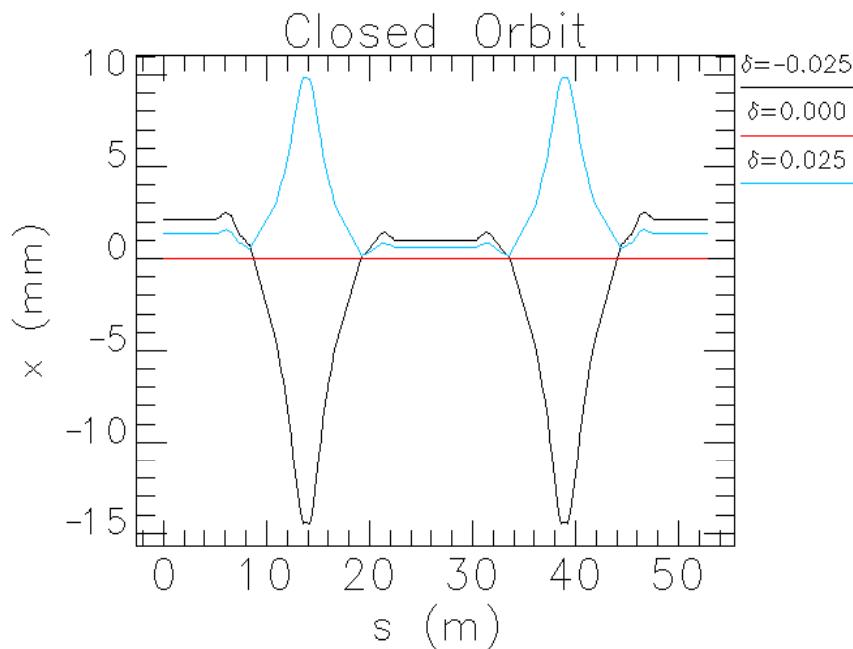
$$\frac{d\beta_x}{d\delta} = \frac{\beta_x}{2 \sin(2\pi\nu)} \int ds (K_1 - K_2 D^{(1)}) \beta_x \cos(2|\Delta\Psi| - 2\pi\nu)$$

$$\frac{d\beta_y}{d\delta} = \frac{-\beta_y}{2 \sin(2\pi\nu)} \int ds (K_1 - K_2 D^{(1)}) \beta_y \cos(2|\Delta\Psi| - 2\pi\nu)$$

Conclusion:

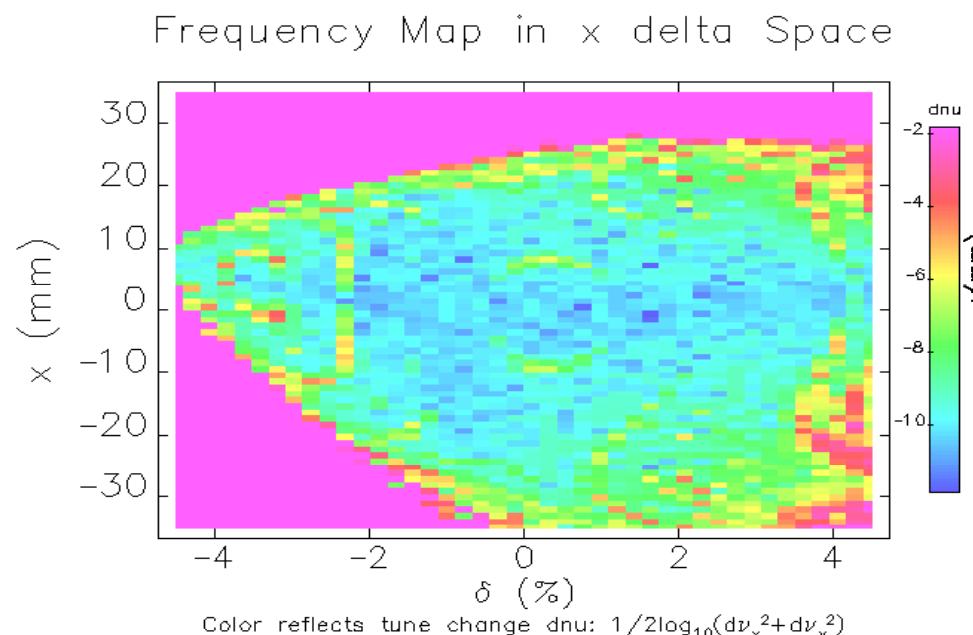
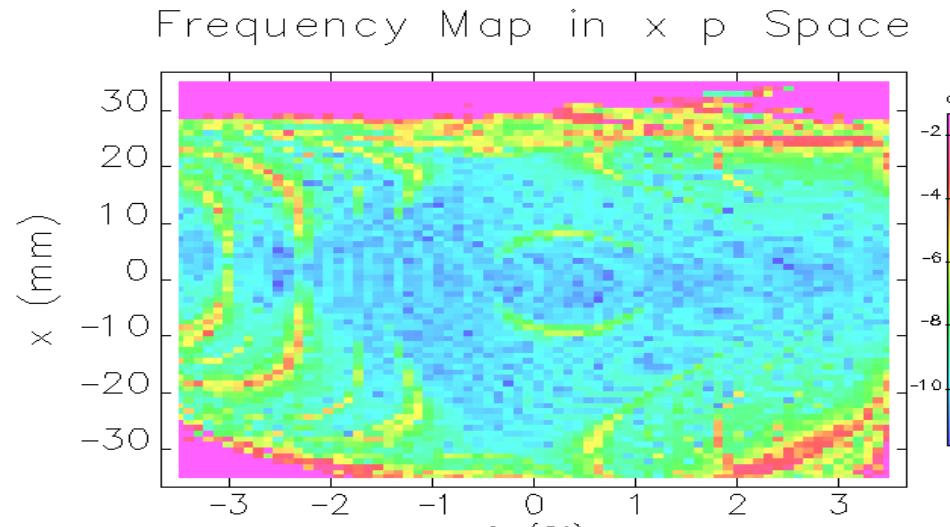
Because the betatron phase advance in the dispersive region is small ($x: \sim 10^\circ$, $y: \sim 20^\circ$),
the five chromatic terms have only two degree of freedom. → 7~8 sextupole families

Stay-clear aperture



$$x_{c.o.}(s) + x_{c.o.}(s_0) \sqrt{\frac{\beta(s)}{\beta(s_0)}}$$

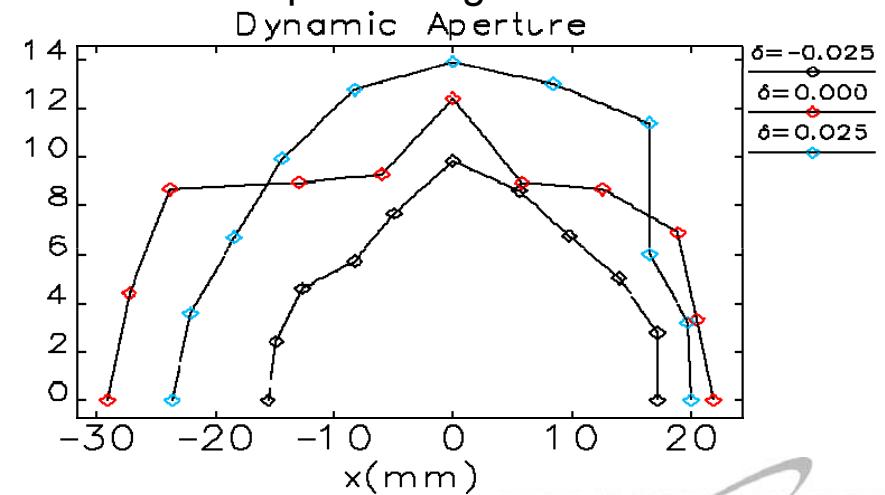
Dynamic Aperture with Multipole Error



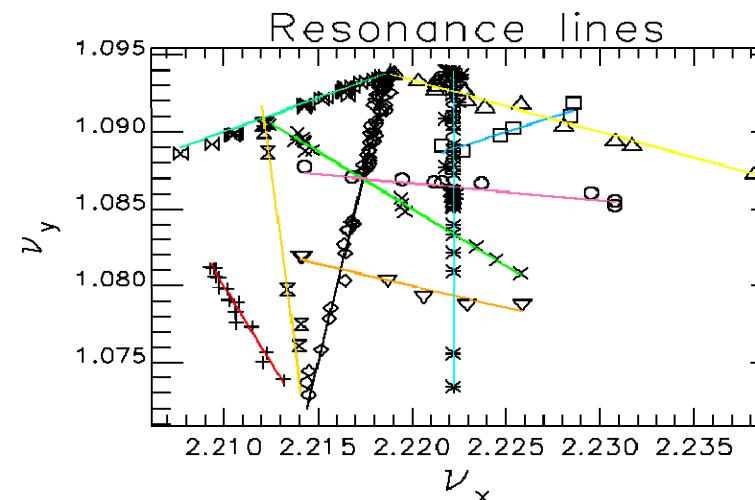
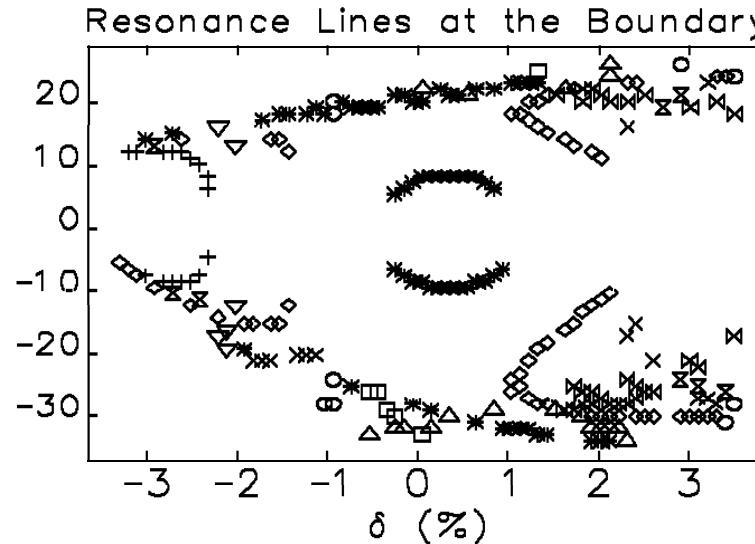
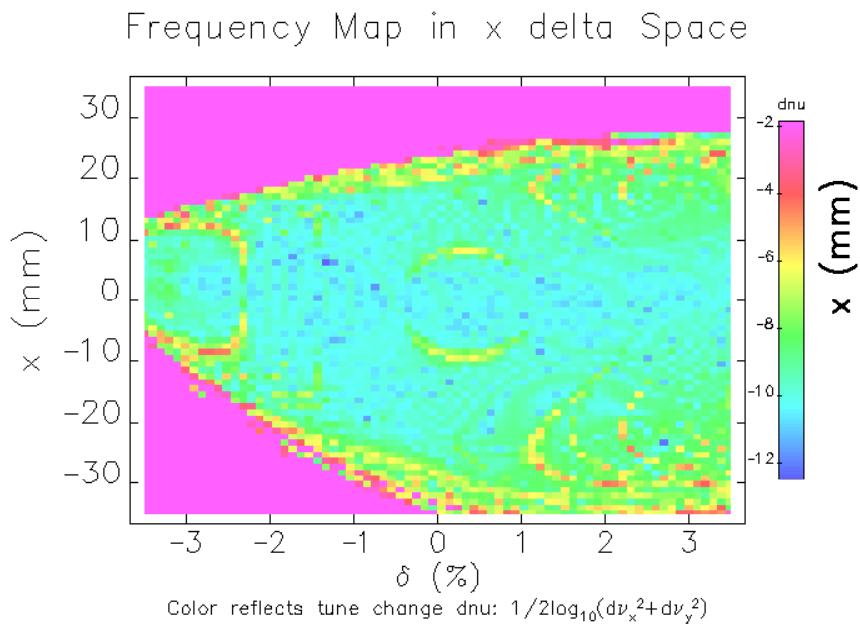
The Feb.-08 multipole components at 25 mm

Magnet Type	Magnet Aperture (mm)	Multipole Order	Relative Strength ($\times 10^{-4}$)
Quad	66	6	1
Quad	66	10	3
Sext	68	9	1
Sext	68	15	2

DA collapse at negative momentum

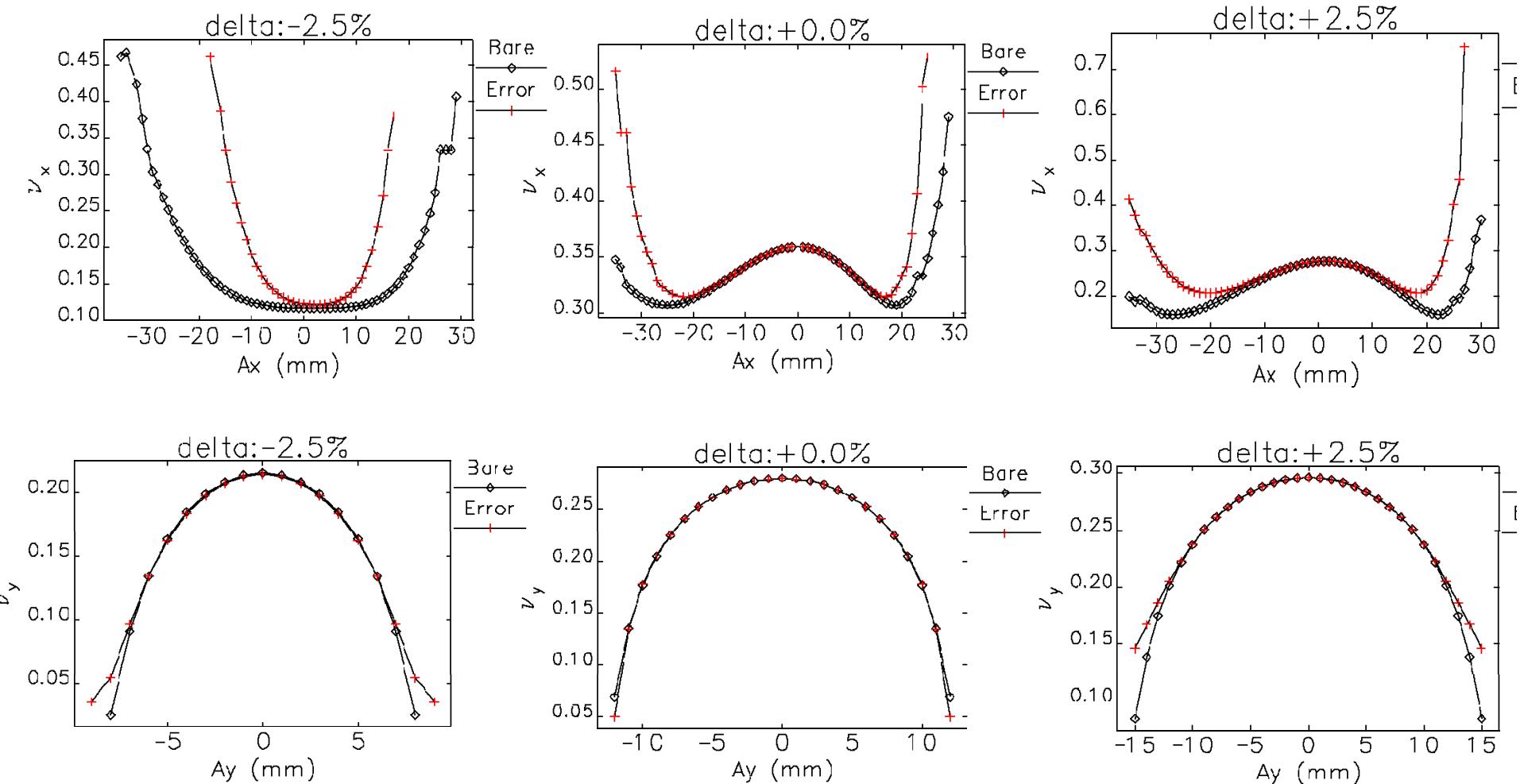


Effects of Multipoles



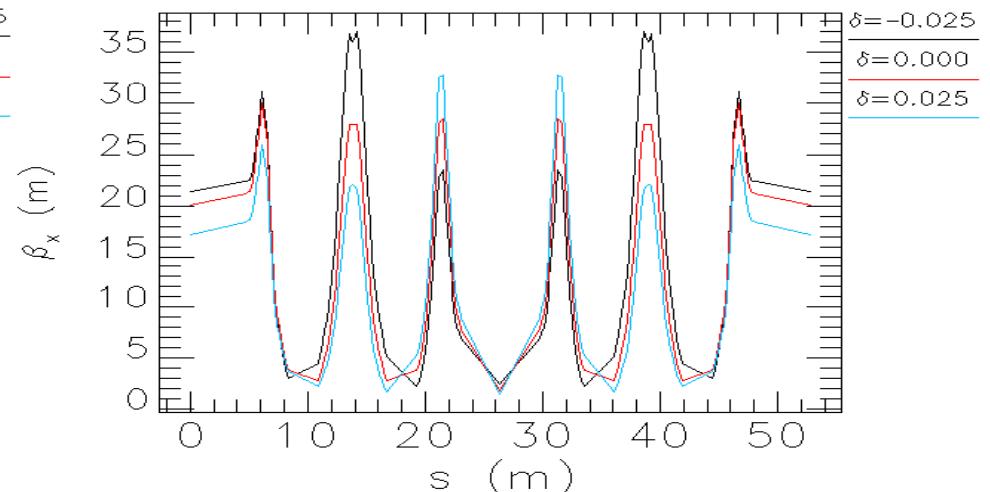
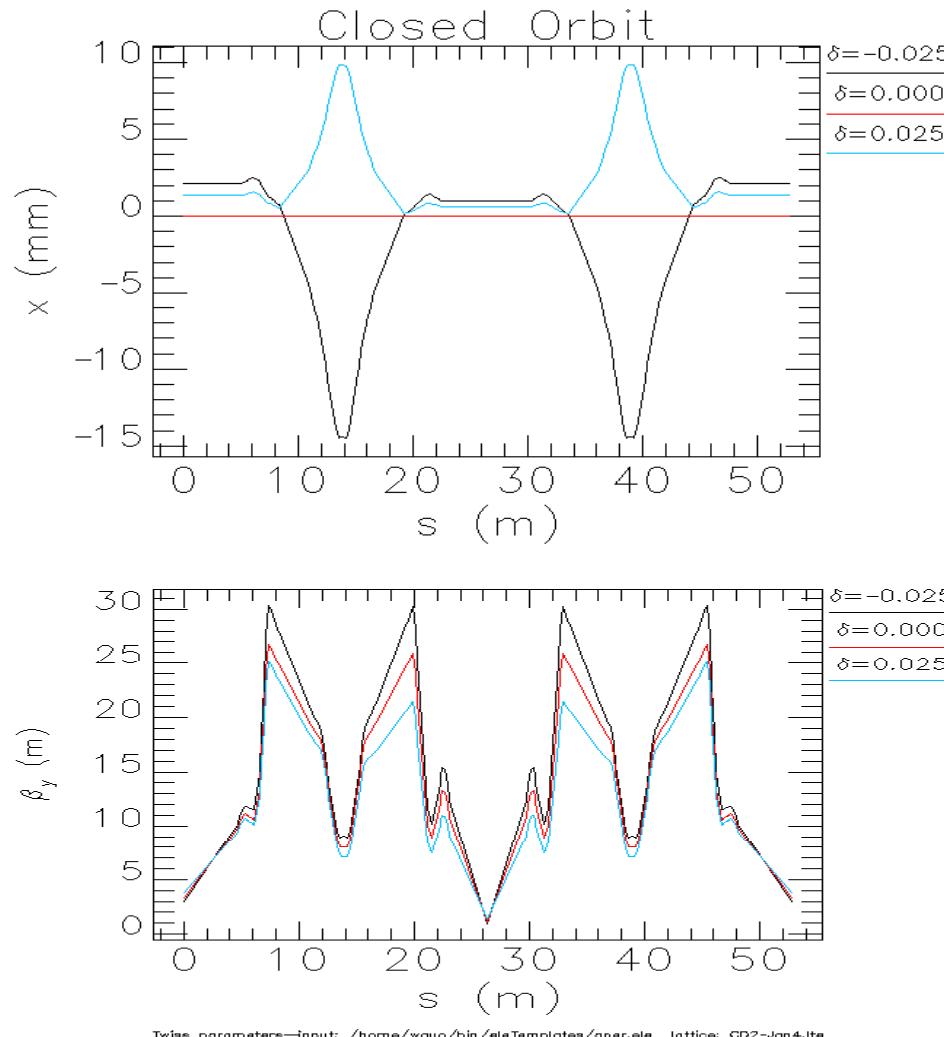
Conclusion:
introducing systematic
multipole errors doesn't add
resonance lines.

Amplitude Tune Dependence



Conclusion: Multipole terms changes the tunes at large amplitude dramatically, and makes the stable area smaller.

Why Negative Momentum?



Twiss parameters—input: /home/wguo/bin/eleTemplates/aper.ele lattice: CD2-Jan4.lte

$$H_{10} = -\frac{1}{B\rho} \frac{1}{10!} \frac{\partial^9 B_y}{\partial x^9} (x^{10} - 45 x^8 y^2 + \dots),$$

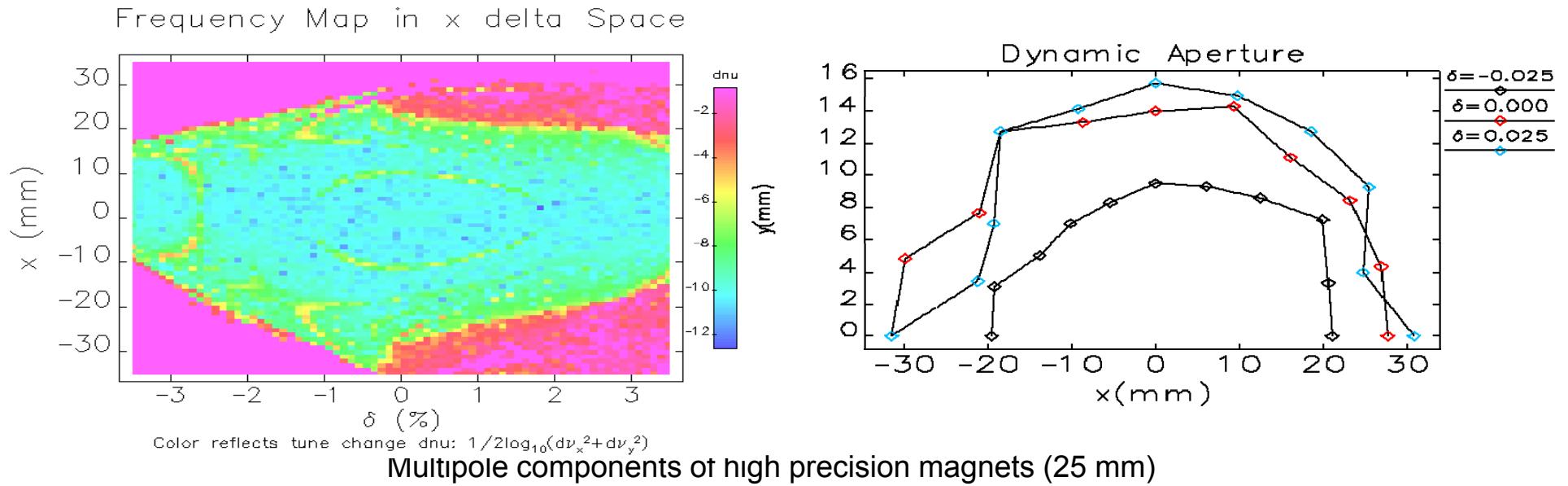
$$x = x_{c.o.} + x_\beta$$

$$\nu_{10} = \frac{1}{2\pi} \frac{\partial}{\partial J_x} < H_{10} >$$

$$= -\frac{1}{2\pi} \frac{1}{B\rho} \frac{1}{10!} \frac{\partial^9 B_y}{\partial x^9} \times$$

$$\sum_{k=1}^5 k C_{10}^{2k} x_{c.o.}^{10-2k} (2\beta)^k < \cos^{2k} \phi > J_x^{k-1},$$

New Specifications



Magnet Type	Magnet Aperture (mm)	Multipole Order	Relative Strength ($\times 10^{-4}$)
Quad	90	6	1
Quad	90	10	0.5
Quad	90	14	0.1
Sext	76	9	0.5
Sext	76	15	0.5
Sext	76	21	0.5

Summary

- Linear lattice is designed to enhance the effects of the damping wiggles
- A grid of stable solutions is used to determine the power supply specifications; and for nonlinear optimization
- Nonlinear design goal to provide sufficient dynamic aperture for injection and Touschek scattered particles up to $\delta=2.5\%$
- There are 8 sextupole families in the lattice, one more might be added.
- The physical aperture is conservatively retained.
- The reduction of the dynamic aperture due to multipole errors is shown to be the momentum related tune shift with amplitude.
- Further optimization of the dynamic aperture is proceeding.