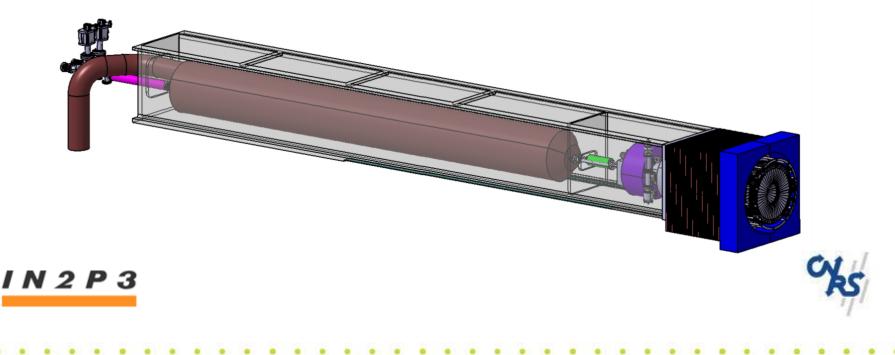




#### **ILD2 square support tube solution**

2<sup>nd</sup> ILD workshop - Cambridge



2<sup>nd</sup> ILD Workshop

M. Joré - ILD2 square support tube

#### Outline



- Requirements on Forward region
- 2 Solutions of a square support tube
  - Why a square tube?
  - Solution 1 : pillar + rails
    - Principle
    - FEA calculations (deformation, stress, natural frequencies)
    - Alignment method
    - Conclusion

#### - Solution 2 : pillar + tie rods

- Principle
- Alignment method
- Conclusion
- Conclusion

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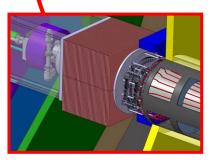
### Forward region



Description QD0 (superconducting magnet) Support tube

Beam line components

- Requirements on support tube
  - Support all the forward components
  - Good vibration performance (QD0 stability)
  - Allowable amplitude
    - Few mm in static load
    - About 50nm for ground motion (IR interface document)
  - Alignment system is needed (in a mm range)



Forward Cals

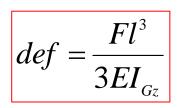
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M. Joré - ILD2 square support tube



- Why a square support tube?
  - Loading is only weight of each forward components
  - Higher moment of inertia allowed to use less material
- Basic calculation (same thickness and external dimension)



		639.
Moment of inertia (I <sub>Gz</sub> )	$\frac{\Pi}{64}(D^4-d^4)$	$\frac{bh^3 - b'h'^3}{12}$
Calculation	$6,77.10^9 mm^4$	$11,5.10^{9} mm^{4}$

→ For same loading and size, deformation is reduced by 40%

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M. Joré – ILD2 square support tube

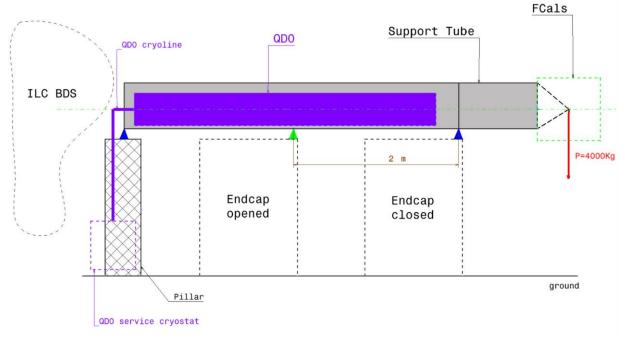




• Supported on

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- Pillar from ground (machine side)
- EndCap

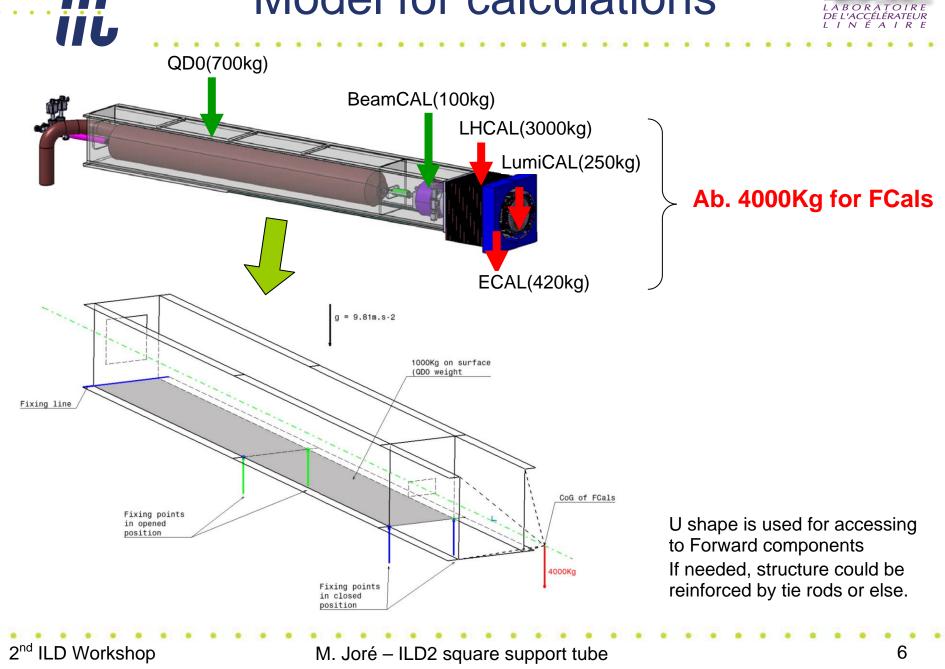


- Compared to cantilever solution
  - Improve vibration stability
  - Reduce deformation and stress

#### Model for calculations

:Ir





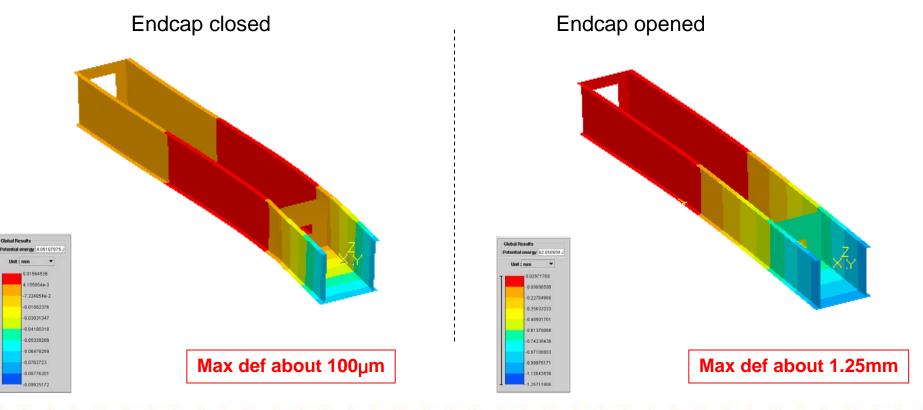
### FEA Calculations (1)



• Conditions

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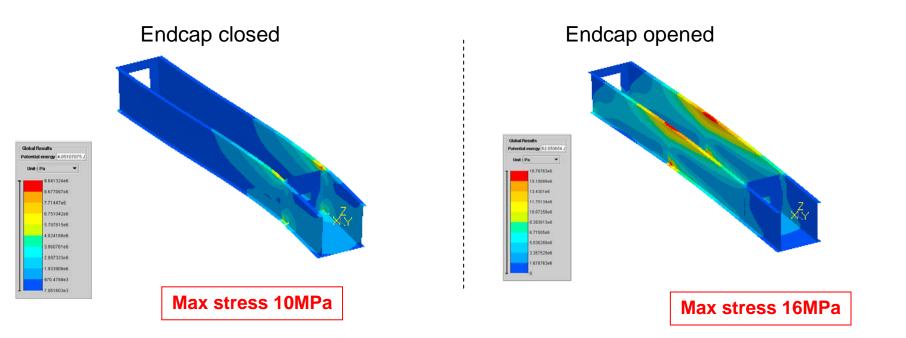
- In both conditions (open/close)
- Stainless Steel (E = 200 GPa)
- Vertical deformation for 50mm thick



# FEA Calculations (2)



• Stress for 50mm thick

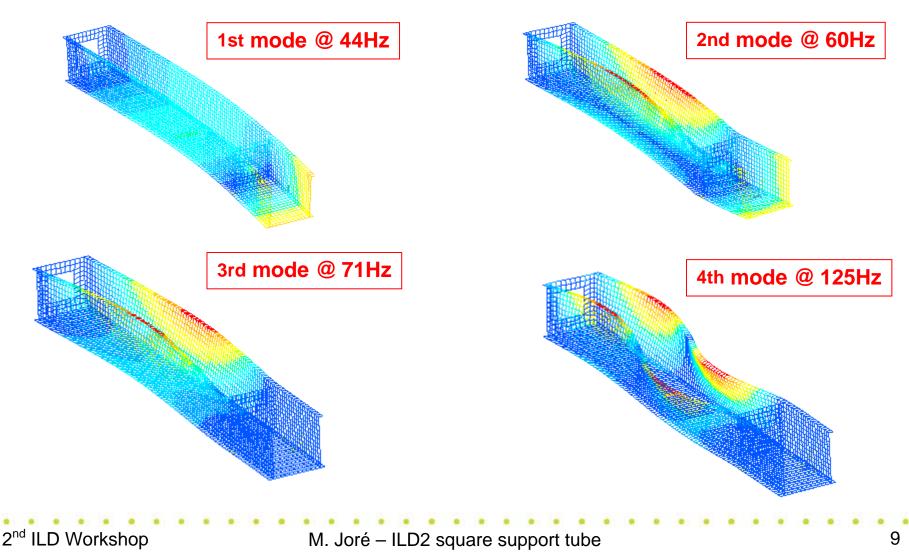


# Natural frequencies



• For 50mm thick and Endcap closed

ilr



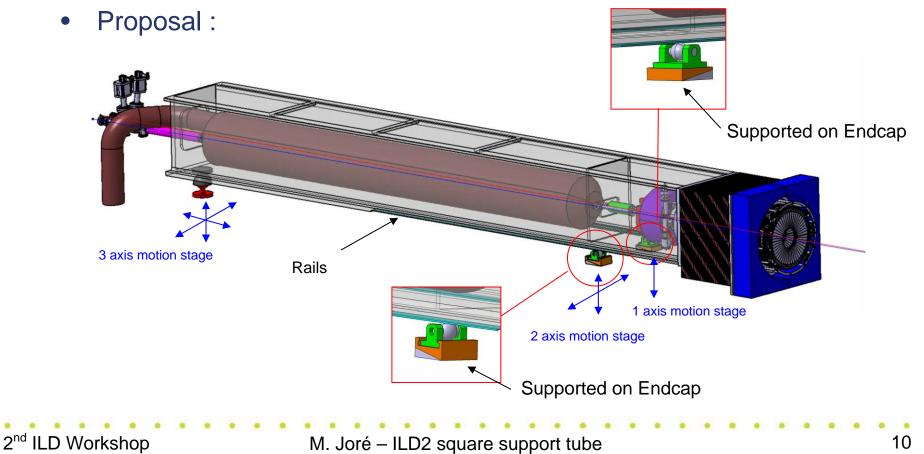
# Alignment method



- Need to adjust the position in a mm range
- Choose of an isostatic devide

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- Allow relative movement of Endcap
- Allow to relax tolerance



# **Conclusions on solution 1**



• Many pros

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- Deformation / stress : OK
- Natural frequencies : OK
- Ground motion calculation under calcultion but seem OK
- We can correct & adjust the position of support tube
- No material in front of Calorimeter
- BUT
  - Need a complex system to align
  - Deformation is a function of the Endcap's position
    - Problems on the forward component
    - On beam tube

#### ⇒ we must discouple Endcap and support tube

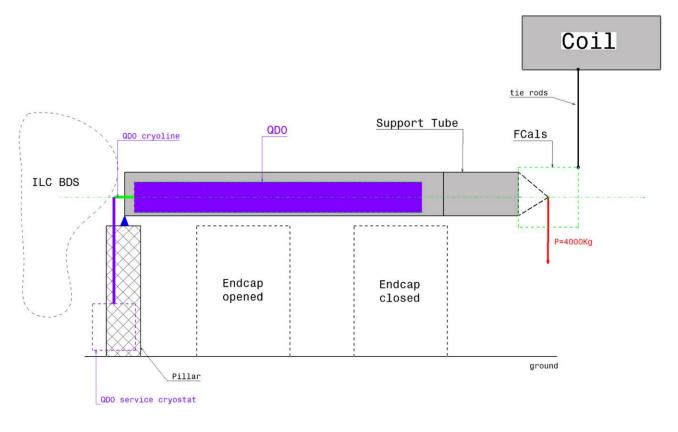


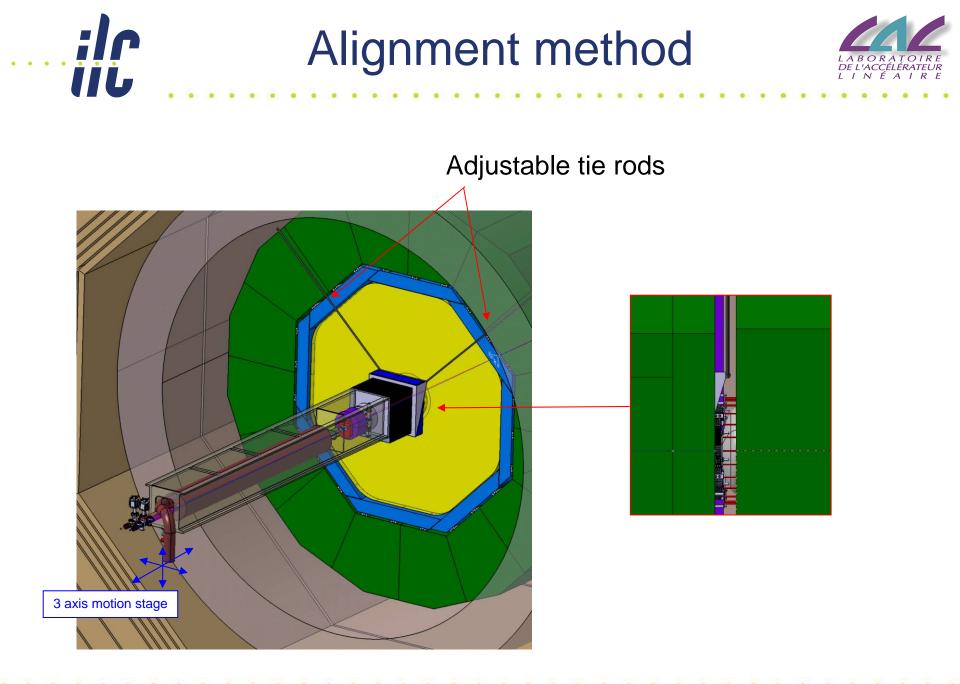


• Supported by

iiL

- Pillar from the ground (like solution 1)
- Tie rods from the magnet to the FCals





## **Conclusions on solution 2**



- Some cons :
  - Add material in front of Forward calos
    - (Possible to use Carbon Fiber for tie rods)
  - Need calculations to optimise the link to support tube
  - Interaction with Ecalring dimension
- But many pros :
  - **Better stability** (fixed at extremity of the tube)
  - Completely independent to the EndCap
  - Easier to adjust with the tie rods
  - No need of active correction
  - Less deformation & stress (results may come)







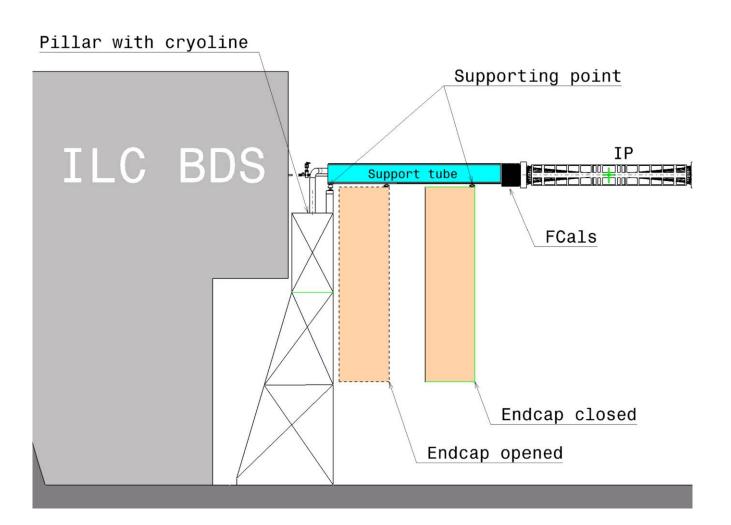
- On using square tube
  - Stiffer than round (ab. 40%)
  - More place for integrating components
- On supporting method
  - Each solution has it's own pros and cons
  - But I think that the 2<sup>nd</sup> one is better for mechanical reason :
    - Less deformation (calculation would be performed)
    - More stability
    - No active correction of alignment
    - ...
  - Do you agree put some material budget in this area ?





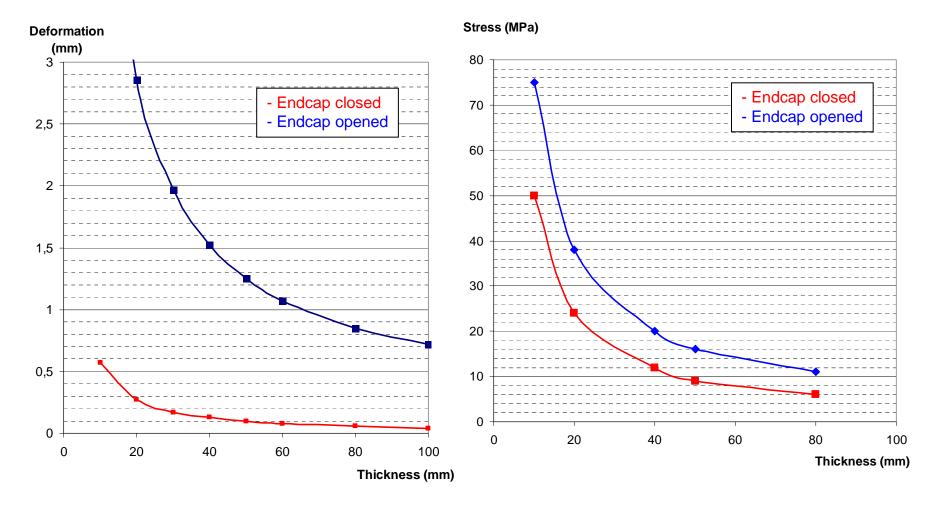
#### Extra slides







• Stress & deformation as function as thickness

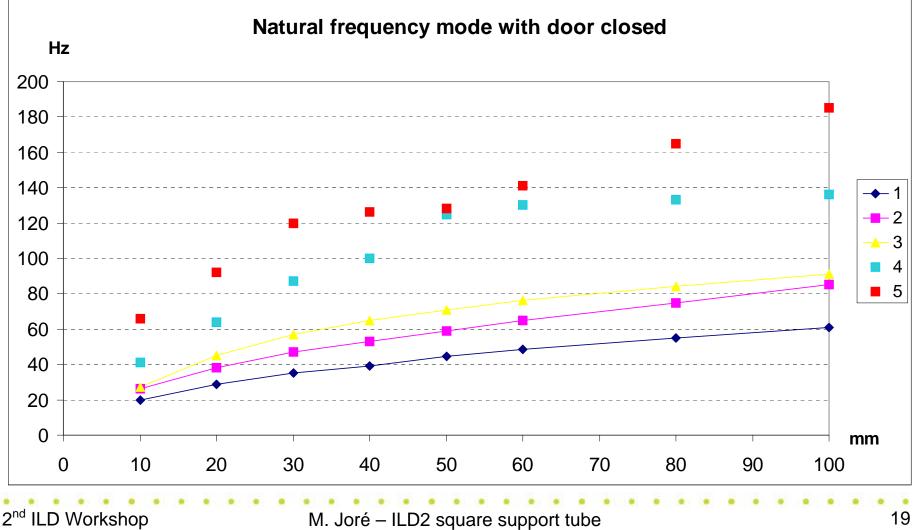


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M. Joré – ILD2 square support tube



Natural frequency mode = f(thickness) 



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