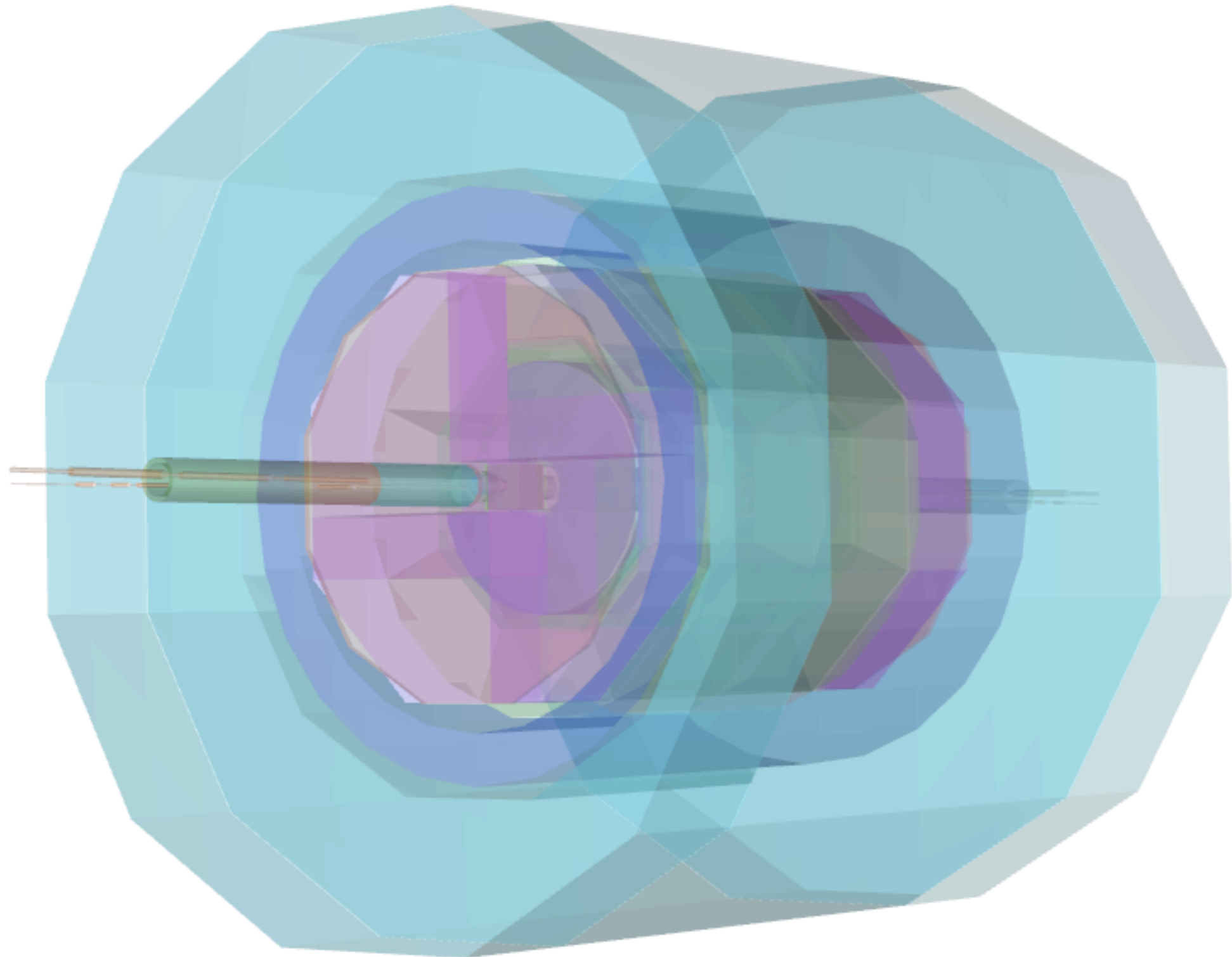


# Status of ILD Detector MDI work

T. Tauchi,

LCWS2008, UIC, Chicago, 17 November 2008

# ILD00 - Mokka 3D model for simulation



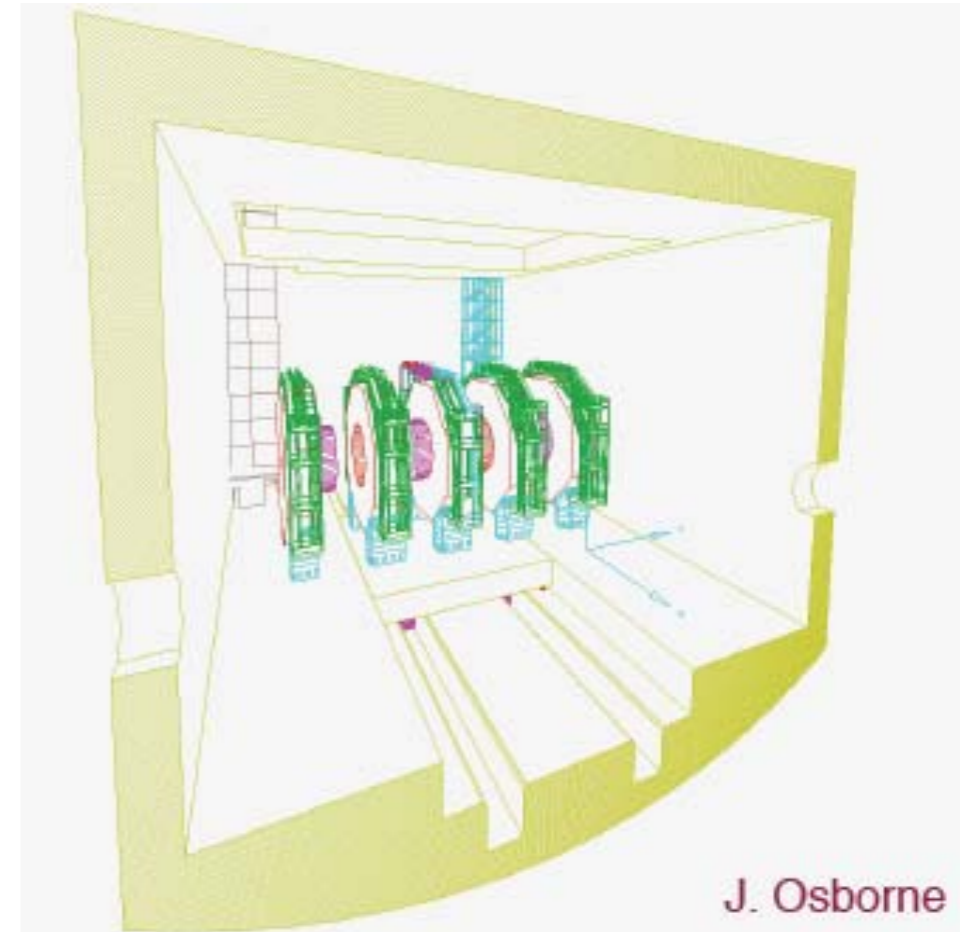
Overall size : 8.88m in diameter, 8.09m in total length ( Tentative, Nov.08)

# MDI issues in ILD

1. platform in the push pull scheme : A.Herve, John
2. background : Adrian
  - minijets (T.Barklow,Jan.04) for positive ion in TPC
  - anti-DID
3. beam pipe : Sugimoto, Suetsugu, M.Winter, FCAL-collab.
  - heating
  - vacuum pump system
  - passive anti-DID option
  - engineering design
4. self-shield for radiation in ILD : Sanami
5. iron structure : Uwe, Yamaoka
  - tail catcher - M.Thompson's study
  - CMS style for surface assembly
  - gaps (assembly, cables, cooling pipes) and stray field

# Push Pull

- Platform
  - Would make movement of detector easier
  - Need  $\sim 2\text{m}$  deeper hall (quite expensive)
  - So far no work on-going within ILD
  - Preliminary work at SLAC on stability and strength of platform on hold
  - Will assume platform for LOI
  - Check whether detector design is compatible with no platform
- Concern by F. Kircher
  - Vibrations may destroy coil titanium support structures. Need careful design
    - > previous talk



# Vertex Detector – Results

## Hits on the vertex detector

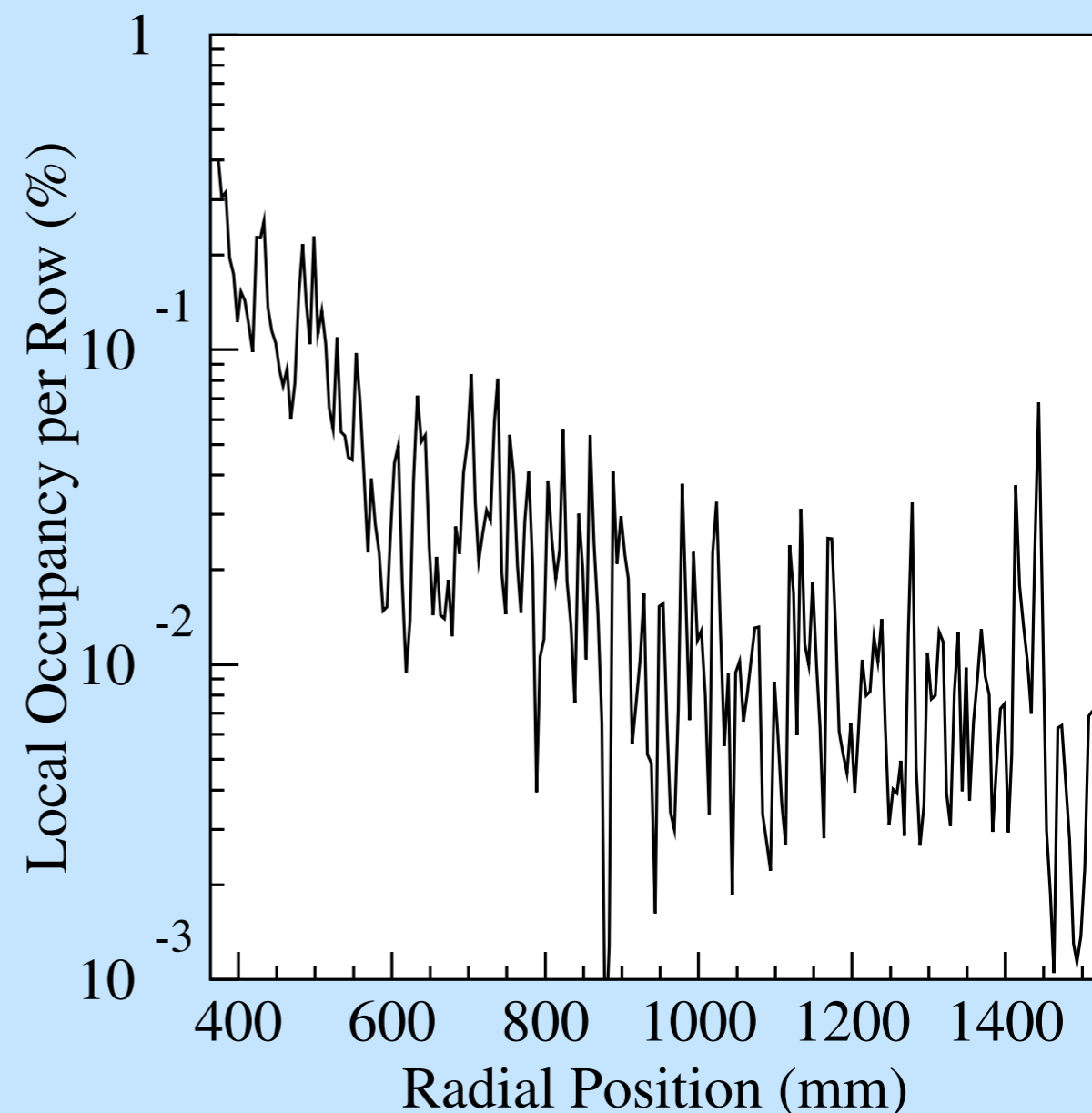
- innermost layer has 400–800 hits / BX
- most hits direct, but also from backscatterers
- background levels drive the VTX design
- resulting backgrounds are still manageable

## Neutron fluence in the vertex detector

- extrapolation from 100 BX to 500 fb<sup>-1</sup> total run time
- energy-dependent weighting of neutrons (NIEL model)
- fluence ( $10^8$  n / cm<sup>2</sup>) is uncritical for all layers

# TPC – Occupancy

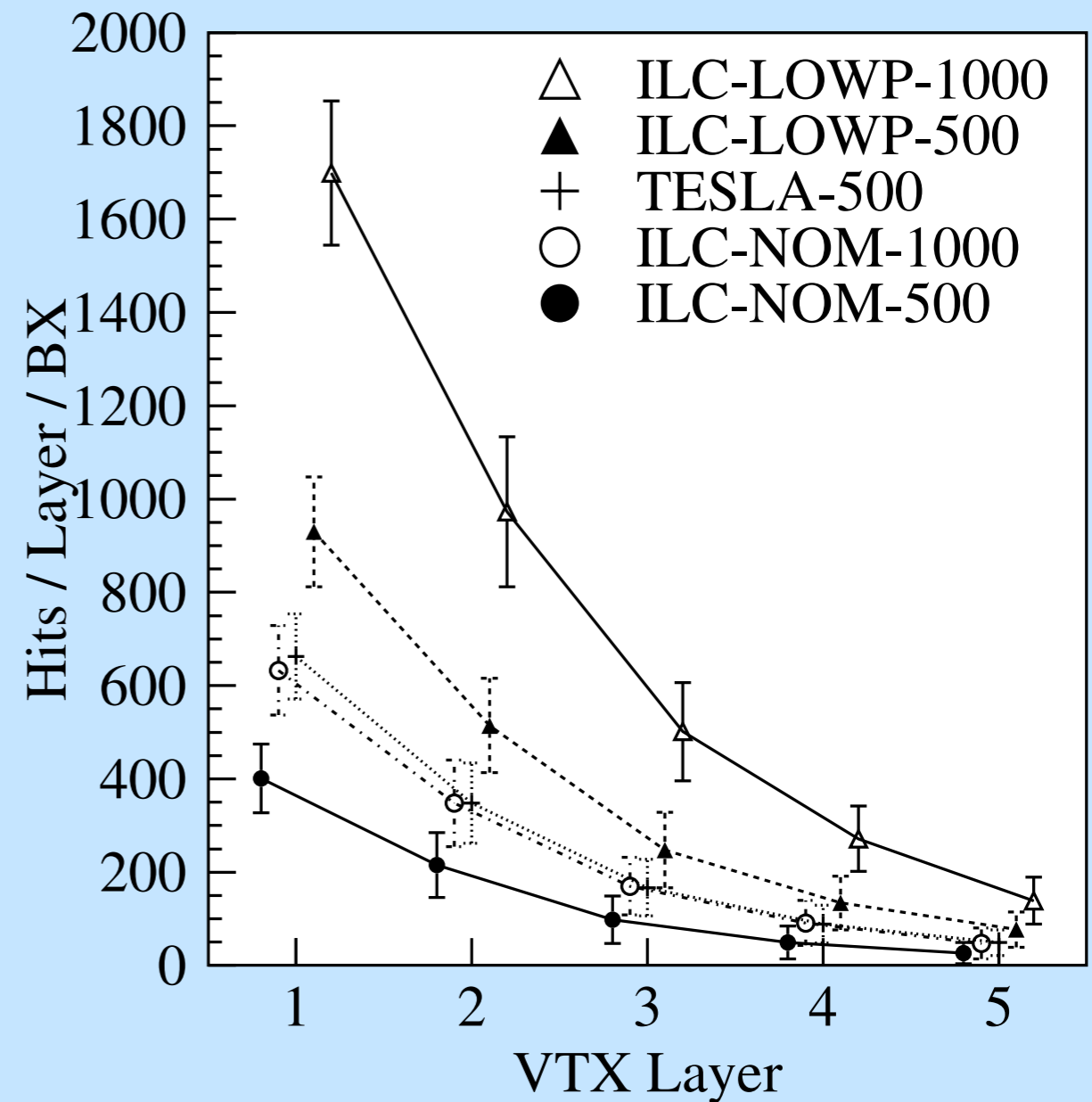
- highest occupancies at small radii
- overall value stays very well below 1 %
- outside-in tracking always possible
- n-p scattering gives negligible contribution
- backgrounds will be no problem for the TPC



Overlay of 100 BX

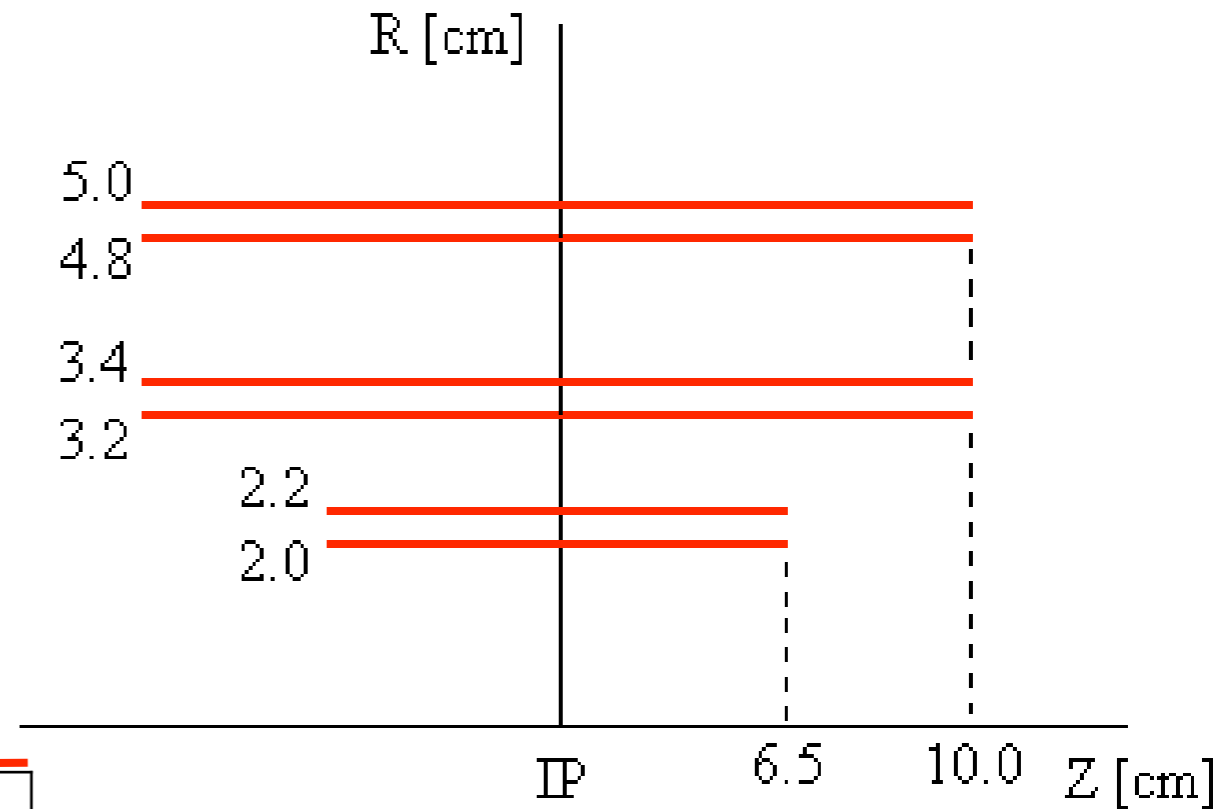
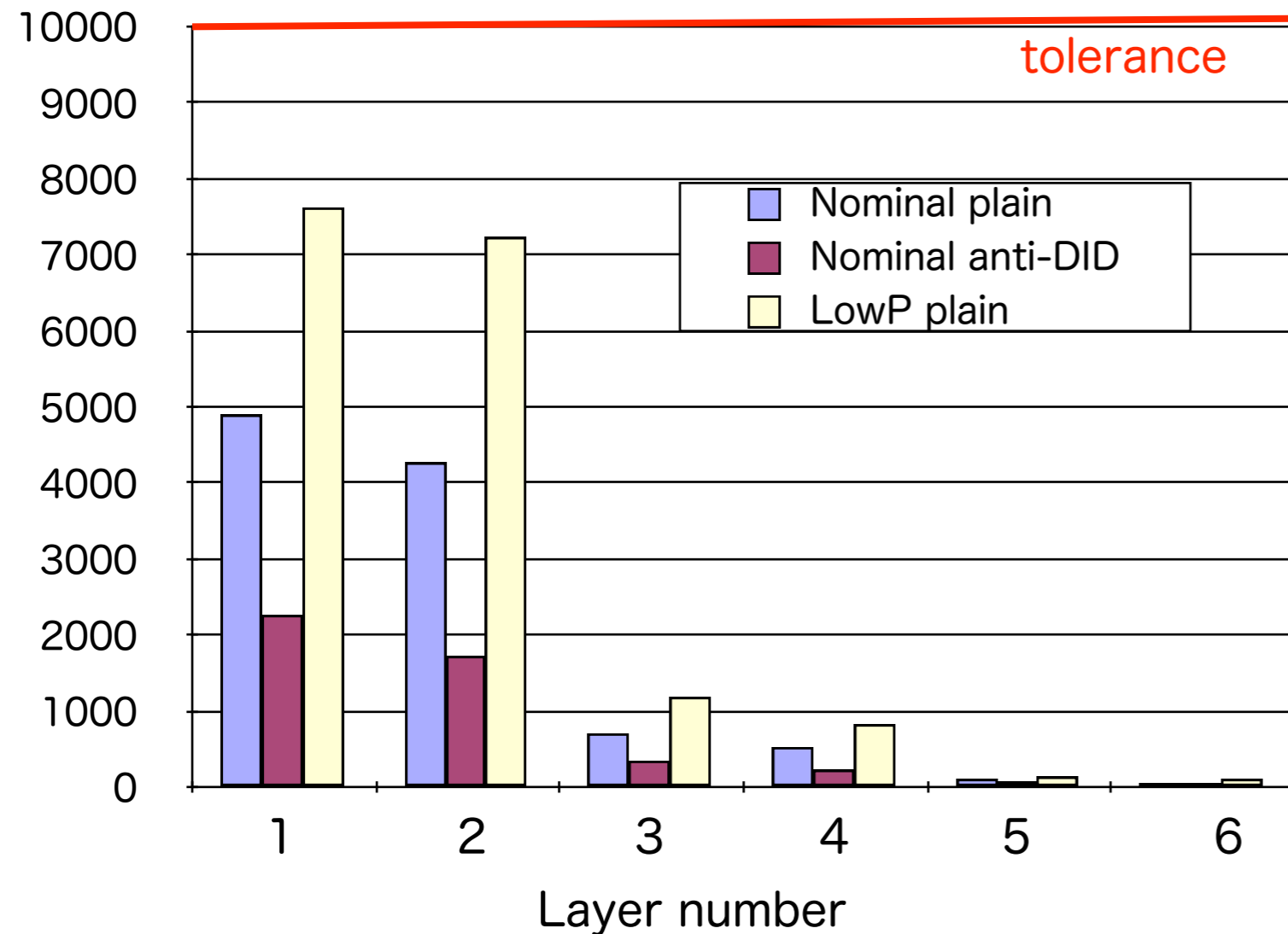
# ILC Beam Parameters – Backgrounds

- “Low Power” option:  
2.5 times more hits
- But: half the number  
of bunches per train
- Integrated backgrounds  
(over a fixed time)  
do not change much
- Upgrade to 1000 GeV:  
2 times more hits



# VTX hit distribution

hits/cm<sup>2</sup>/train



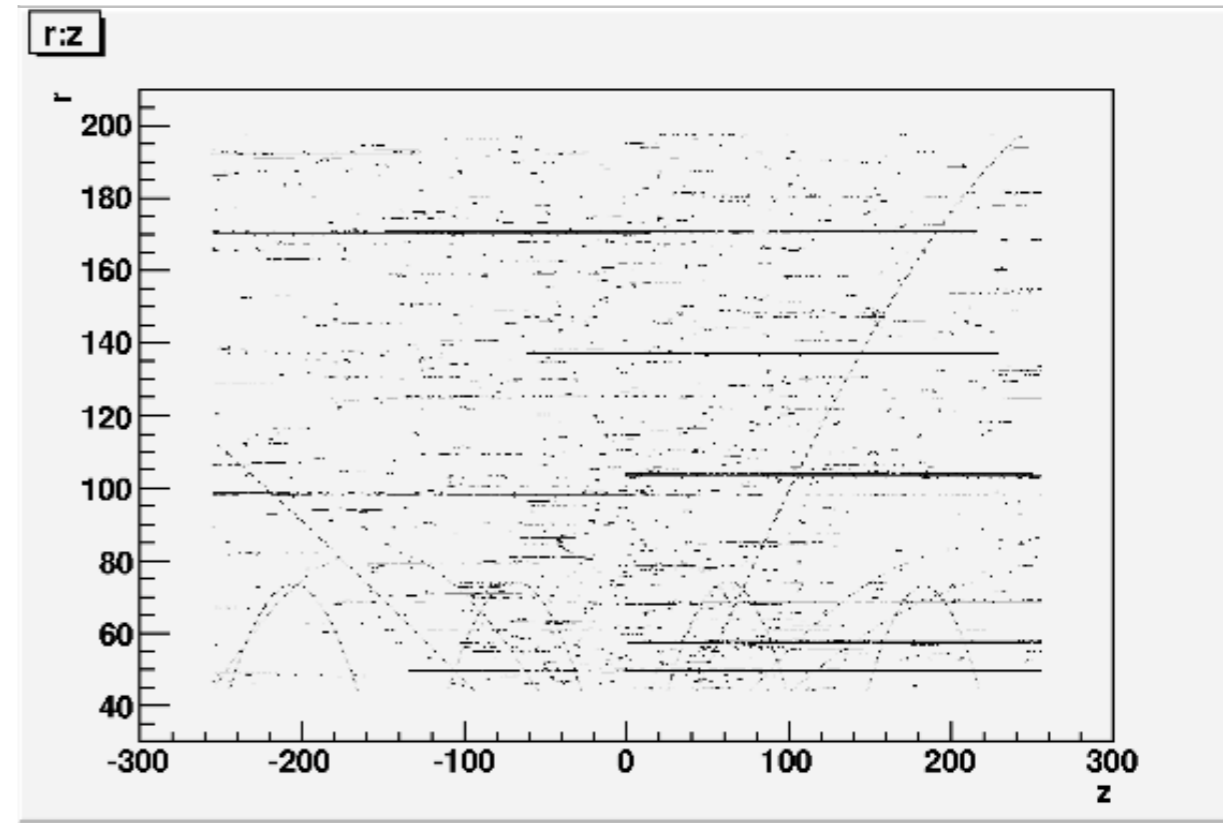
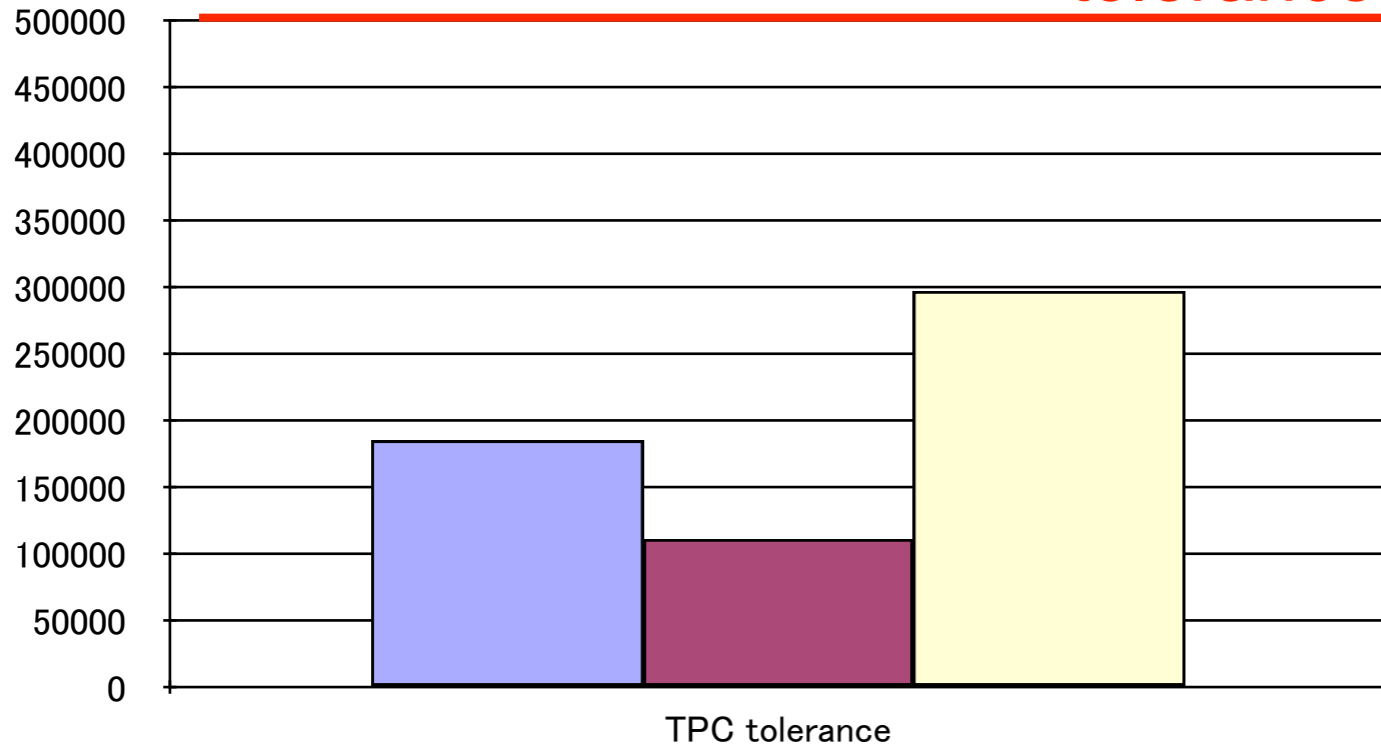
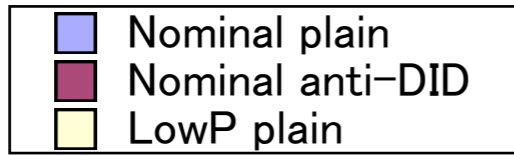
Nominal plain: 20 bunch

Nominal anti-DID: 10 bunch

Low P plain: 1 bunch



# TPC hit

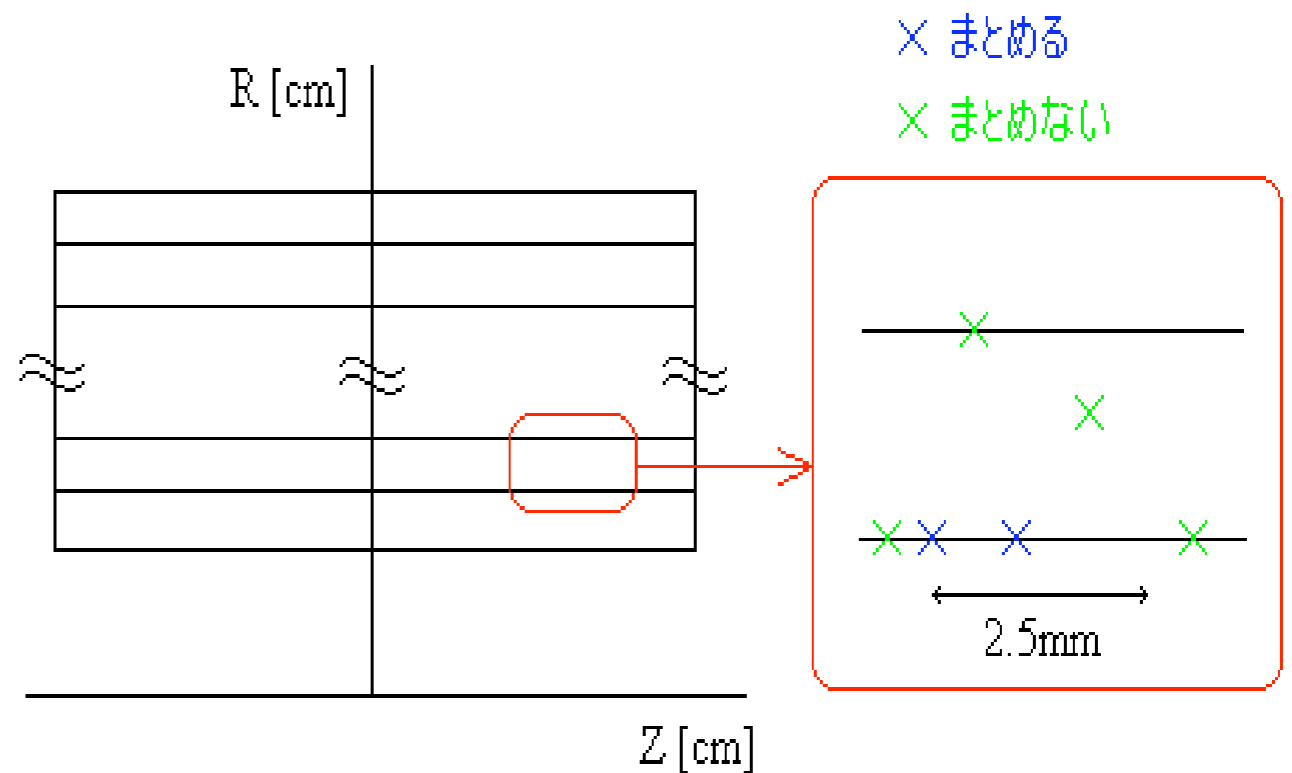


## TPC digital hits

Nominal plain: 20 bunch

Nominal anti-DID: 10 bunch

Low P plain: 1 bunch

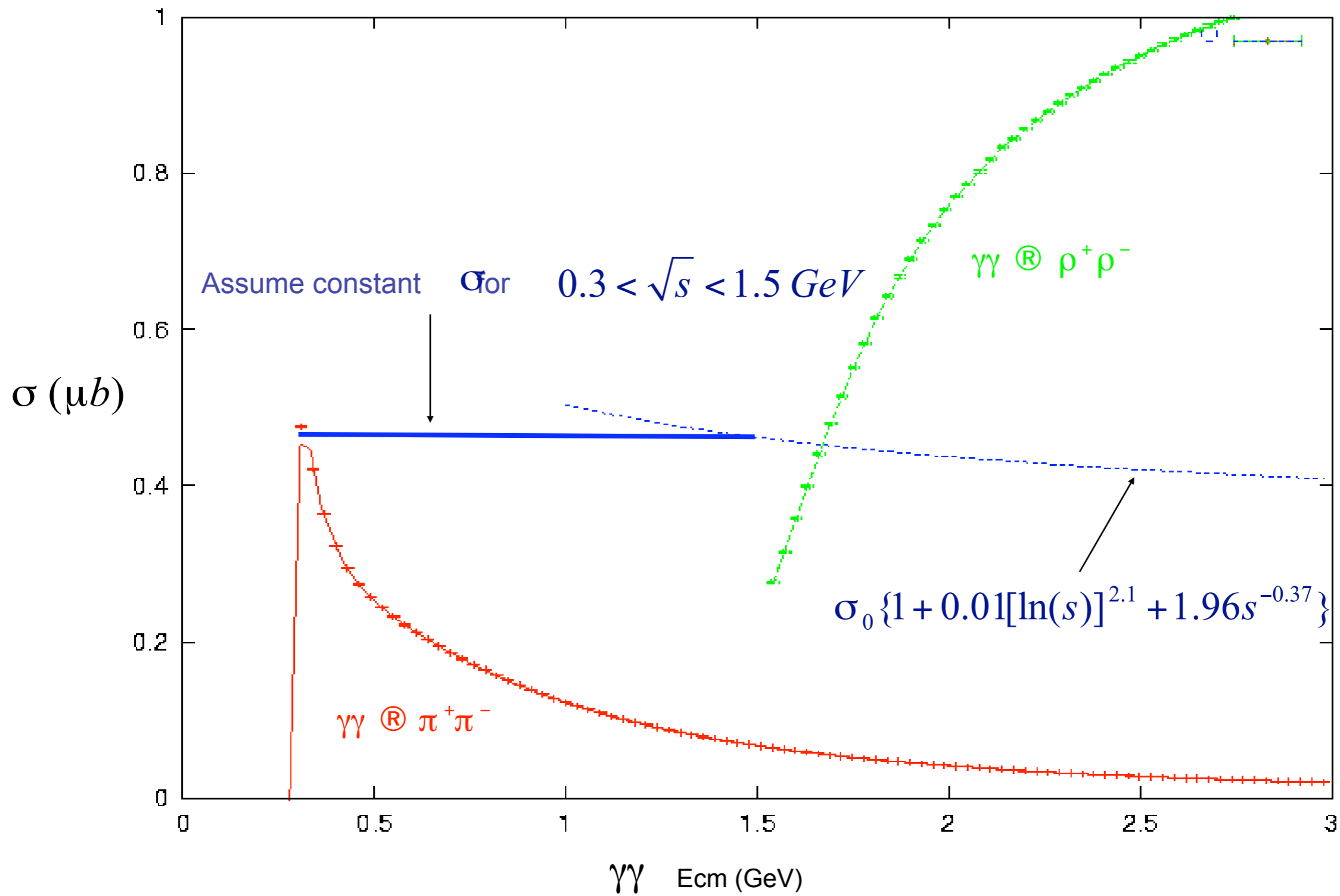


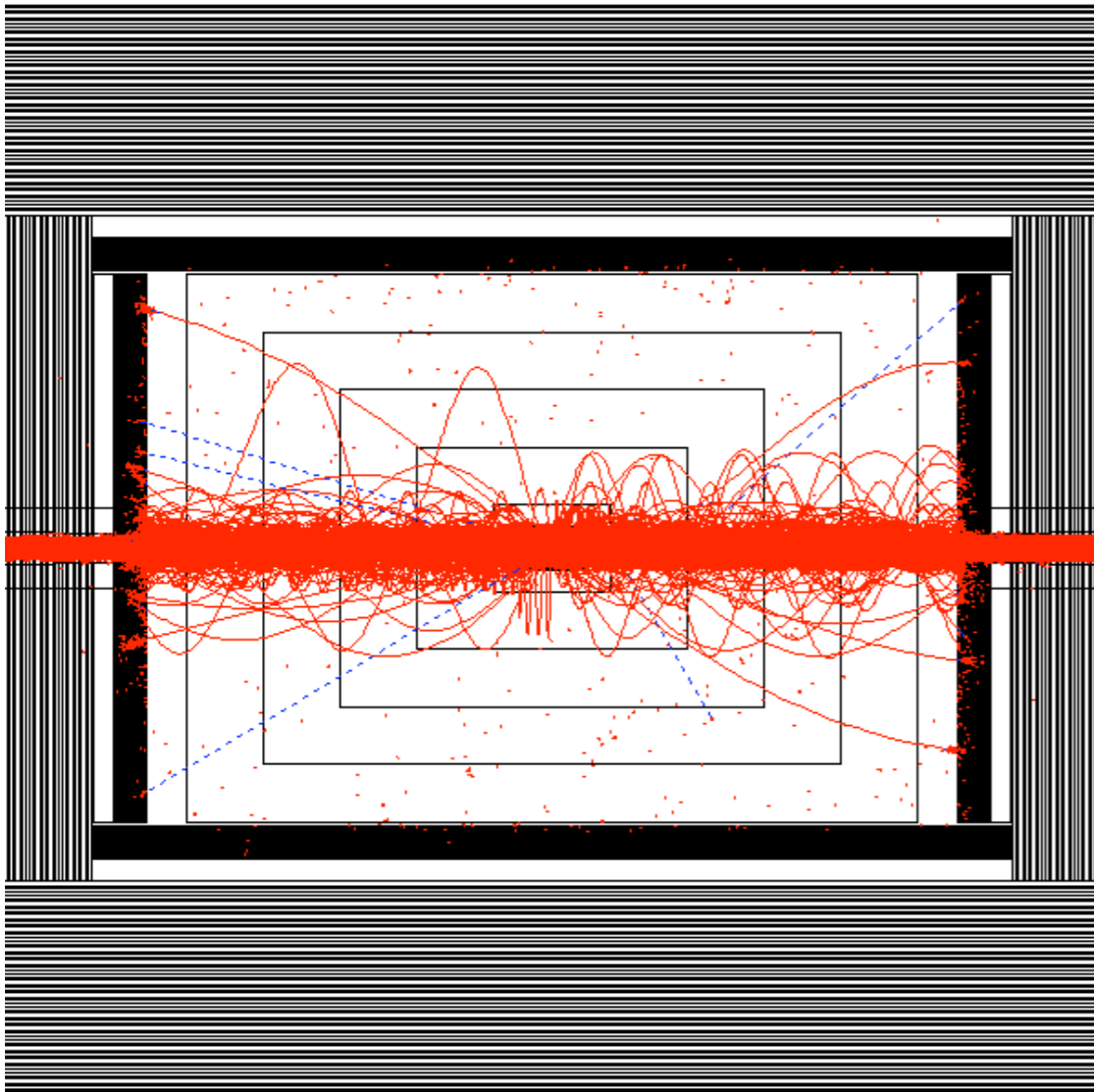
# Update on $\gamma\gamma$ $\otimes$ *hadrons* Calculation

Tim Barklow

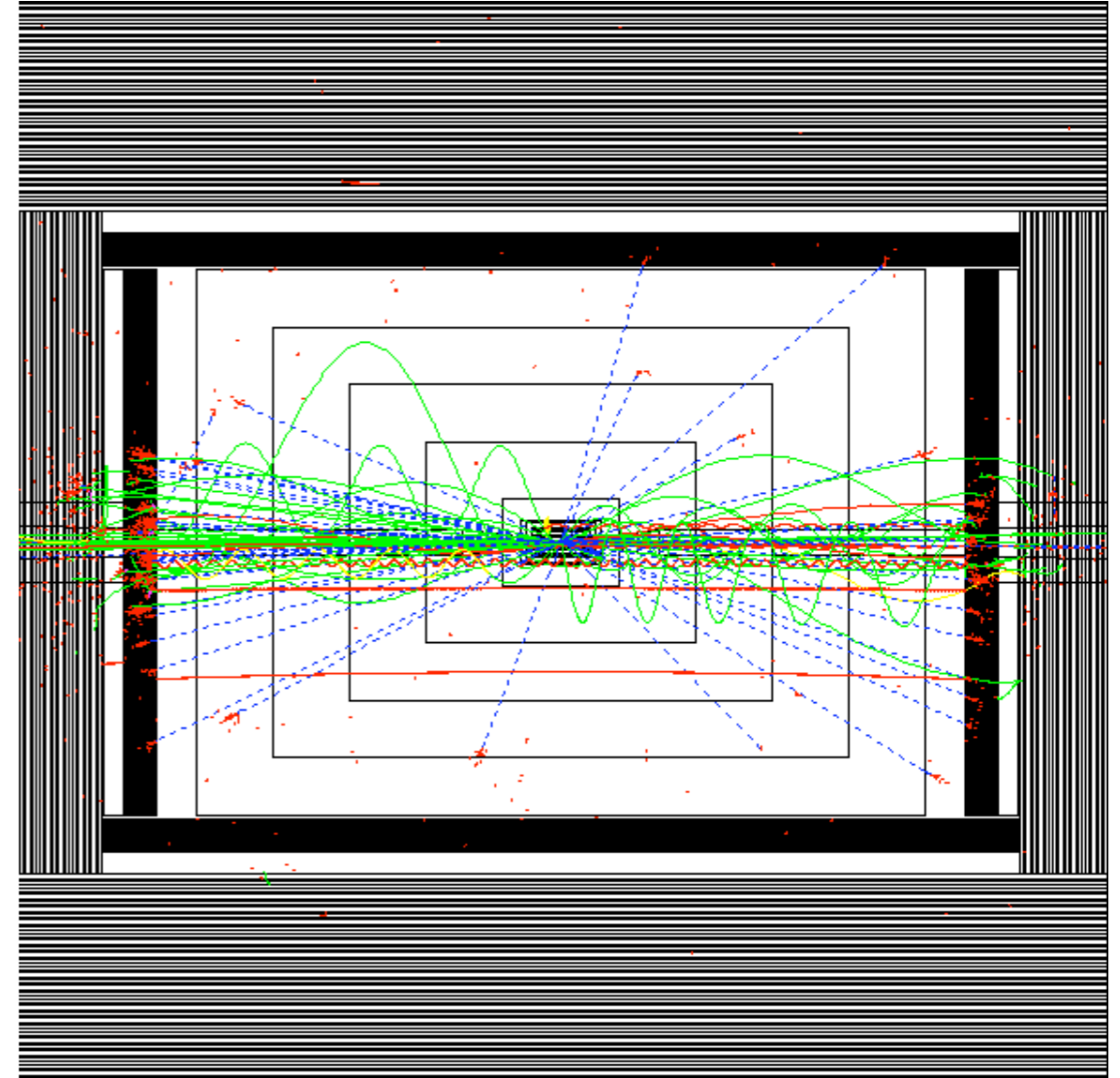
SLAC

January 8, 2004

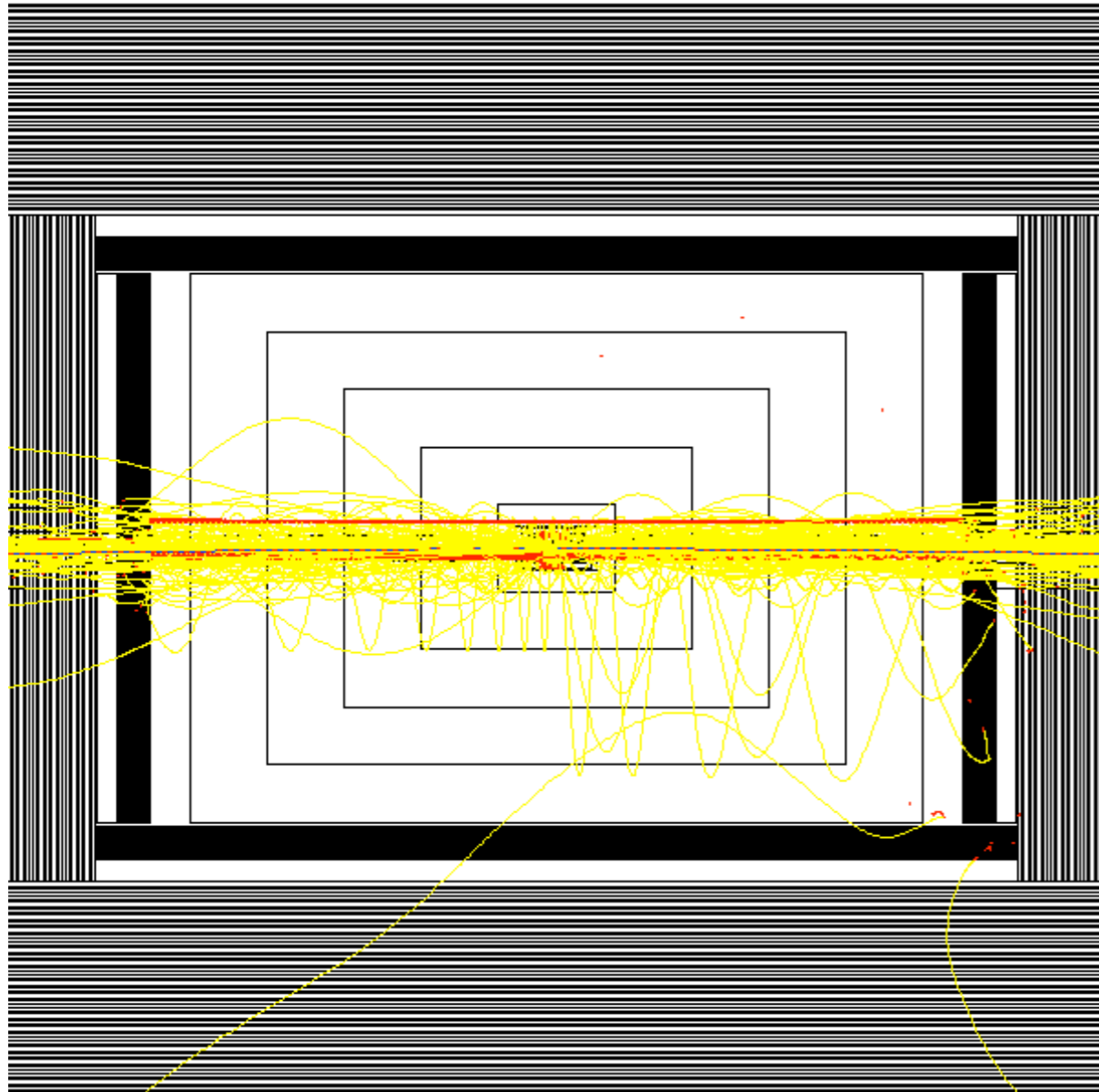




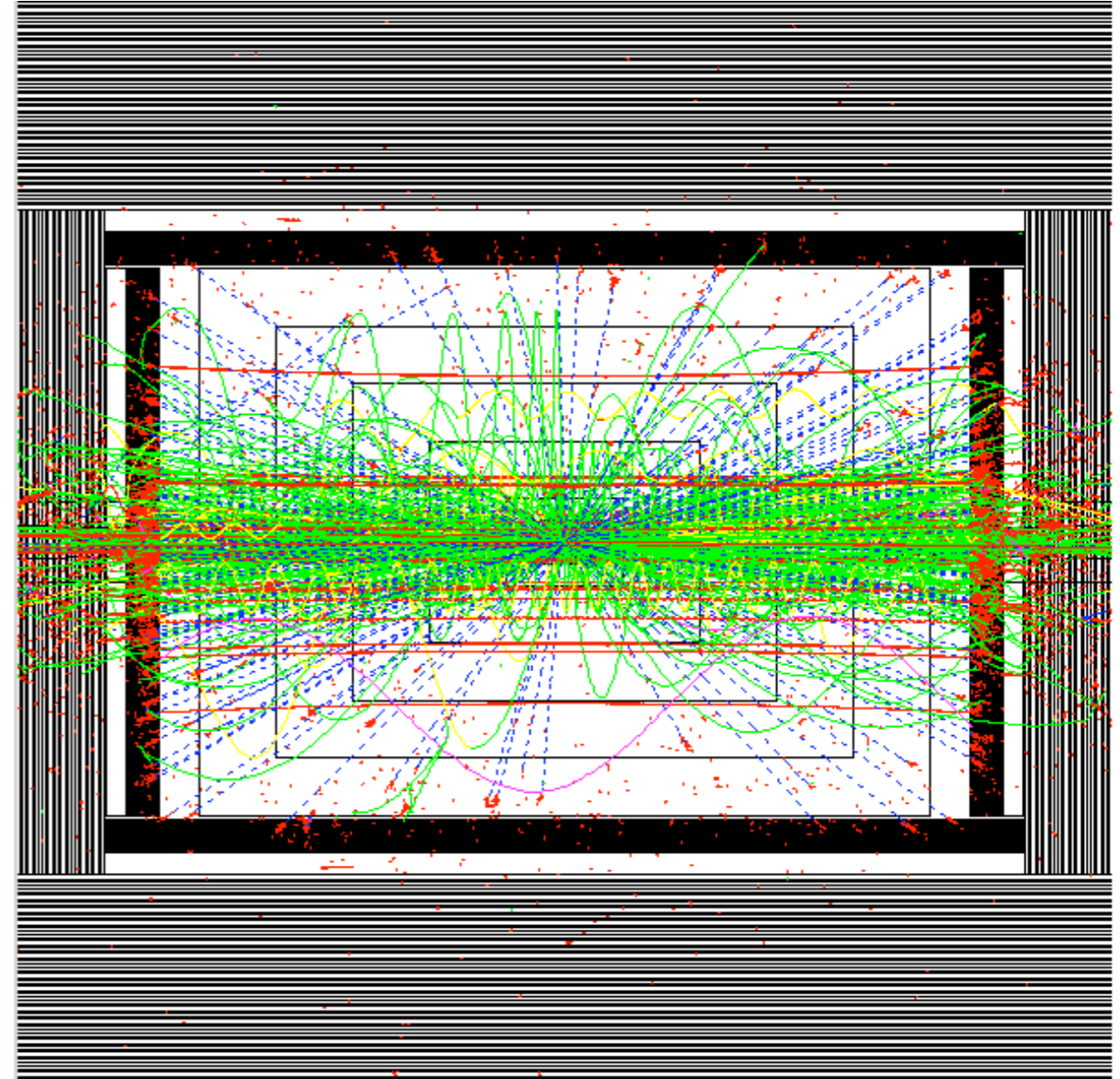
8600  $e^+e^-$  pairs / train strike detector



1.8 hadronic events / train with  $pt > 2.2 \text{ GeV}$   
(TESLA TDR definition of hadronic bkgnd)  
79 GeV / train detected energy  
14.6 detected charged tracks / train



154  $\mu^+ \mu^-$  pairs / train  
 56 GeV / train detected energy  
 24 detected charged tracks / train



56 hadronic events / train  
 no pt cut;  $E_{cm}$  down to  $\pi^+ \pi^-$  threshold  
 454 GeV / train detected energy  
 100 detected charged tracks / train

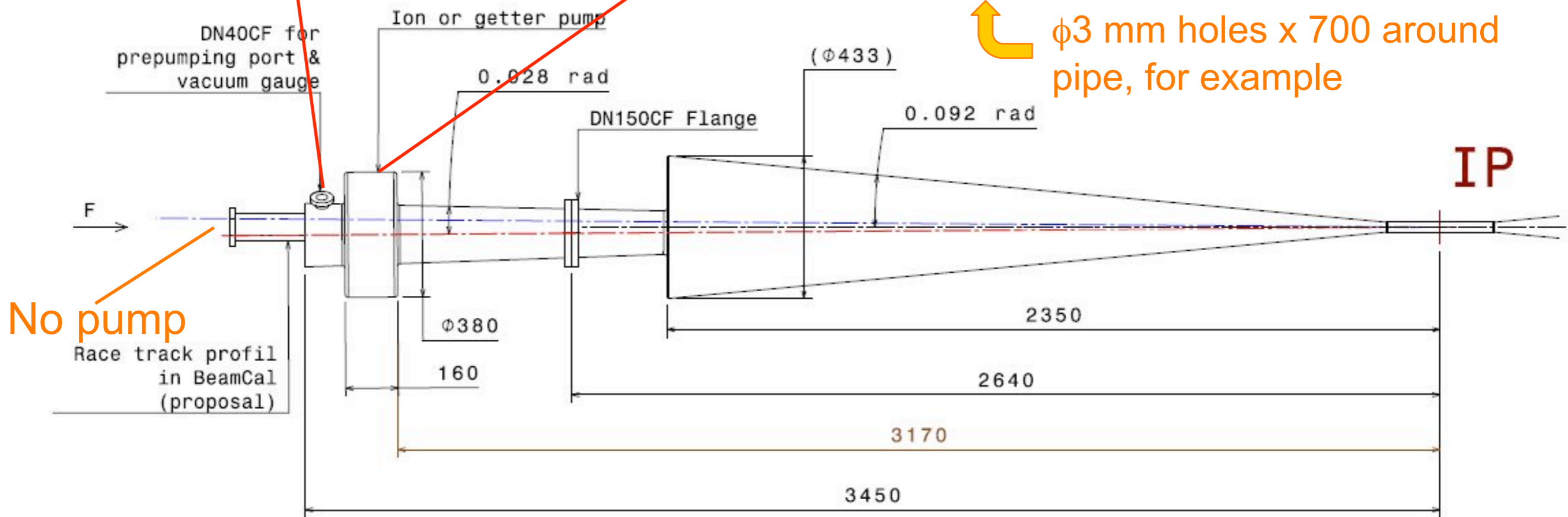
- Pumps

- **NEG strip** : ST707 (SAES Getters), for ex.
- **Aligned at the circumference of pipe**

To a small ion pump  
(and rough pumps)

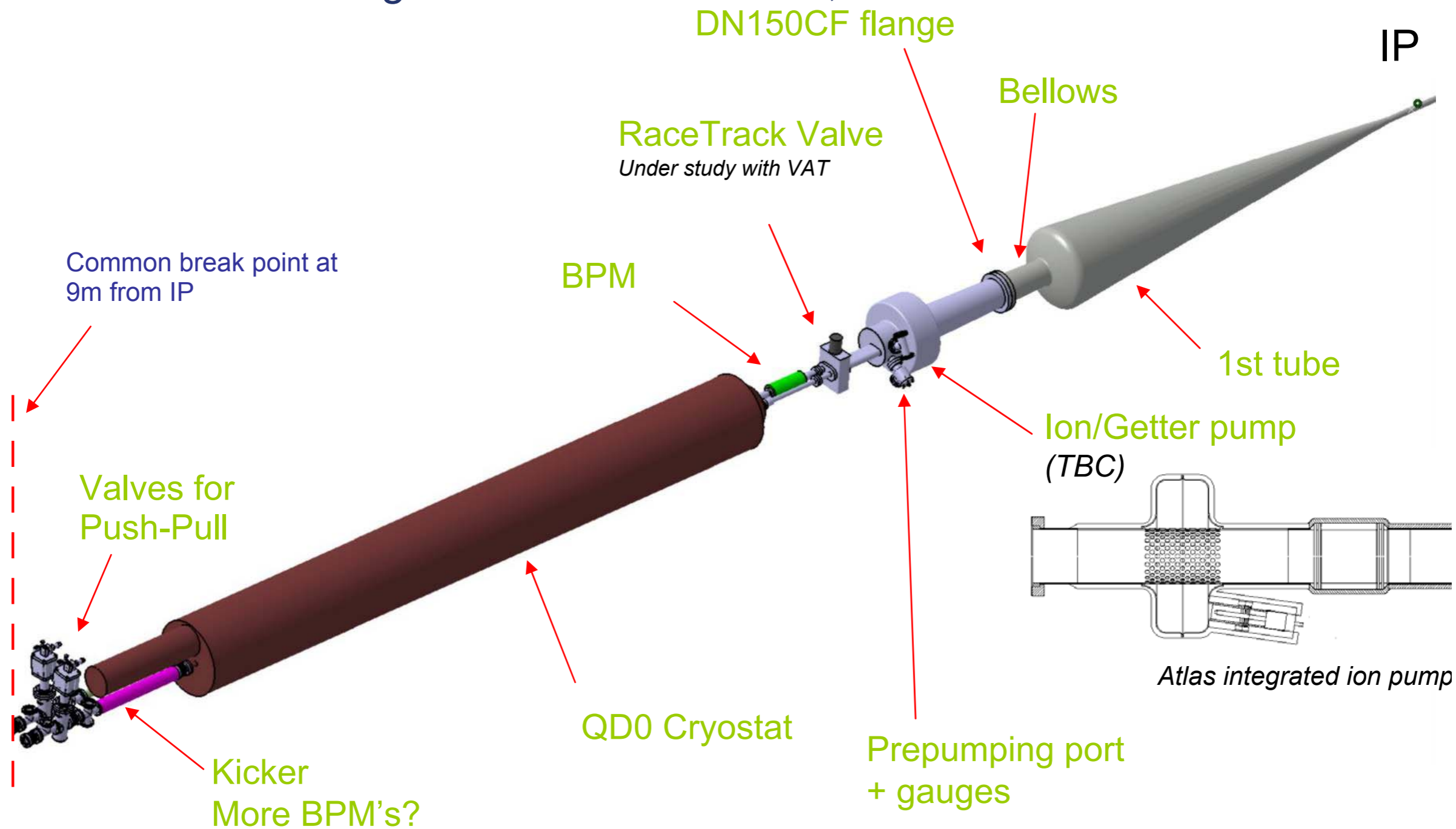
4m NEG strip in total  $S_{\text{eff}} =$   
 CO:  $0.2 \text{ m}^3/\text{s}$ ,  $C = 0.3 \text{ m}^3/\text{s} \rightarrow 0.12 \text{ m}^3/\text{s}$   
 H<sub>2</sub>:  $2 \text{ m}^3/\text{s}$ ,  $C = 1.1 \text{ m}^3/\text{s} \rightarrow 0.72 \text{ m}^3/\text{s}$

$\phi 3 \text{ mm}$  holes x 700 around pipe, for example

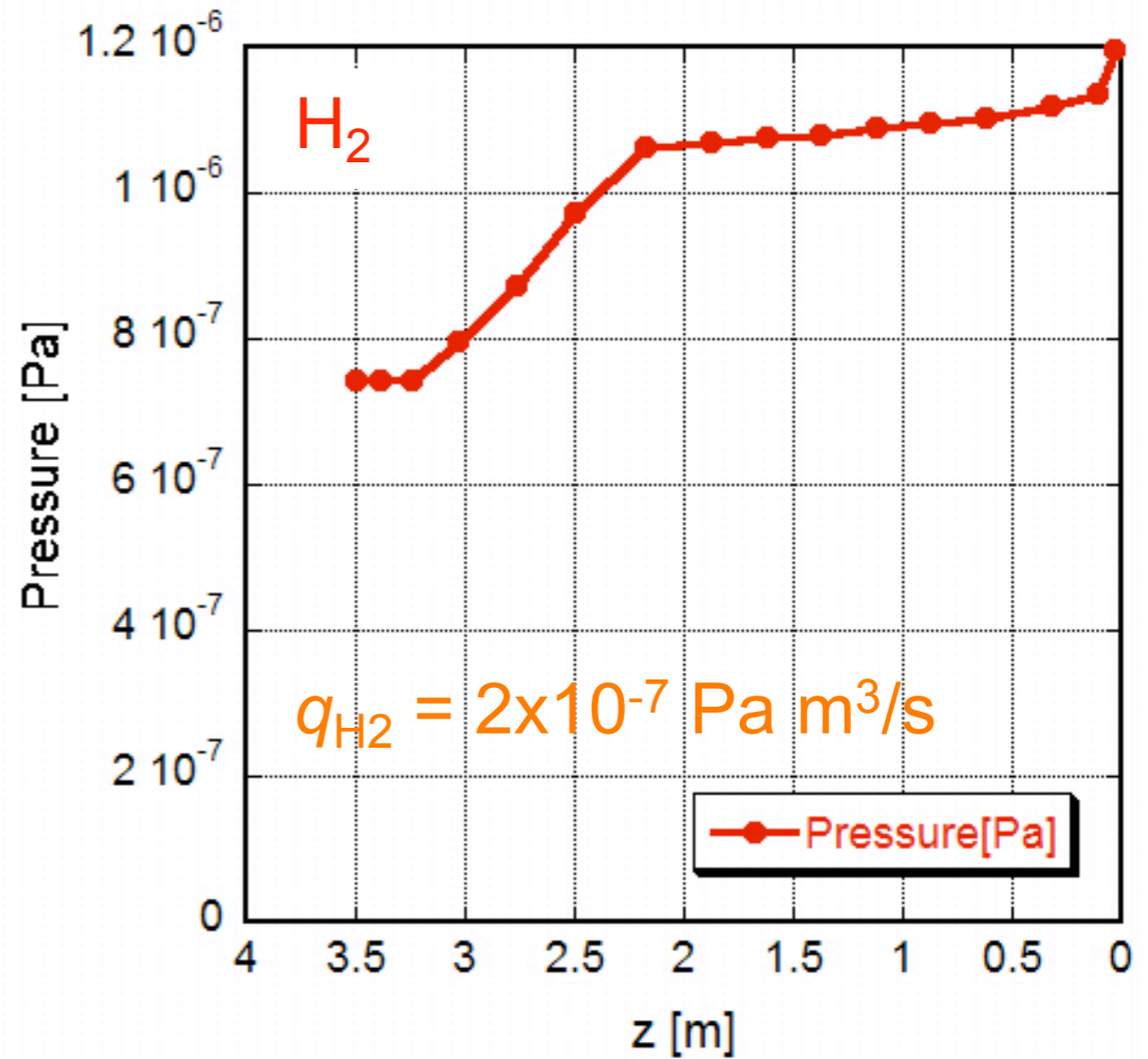
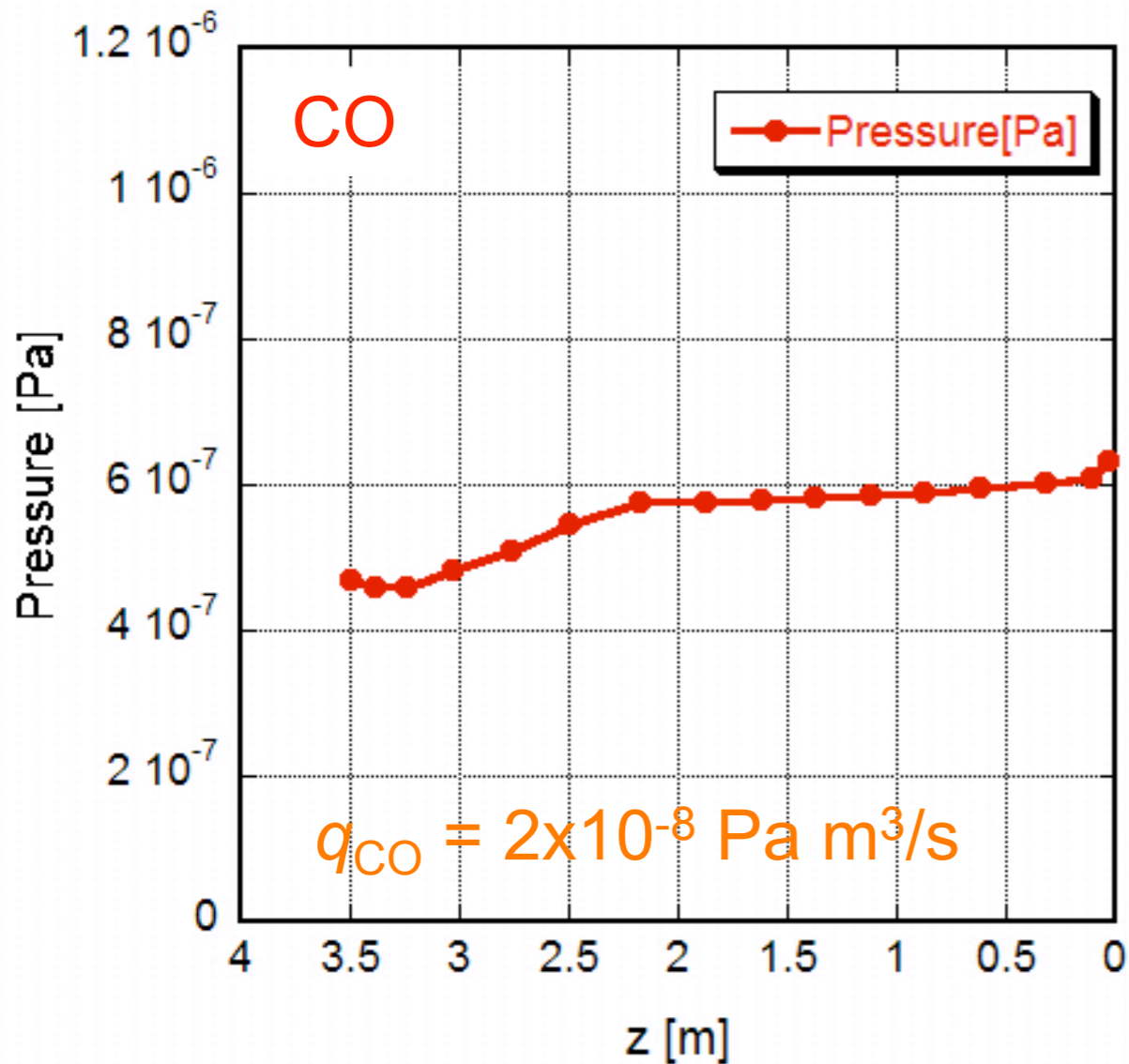


No pump

- Beam line design for 14mrad and  $L^* 4,5\text{m}$



- Results



$P \sim 1 \times 10^{-6} \text{ Pa}$  for H<sub>2</sub>.

The assumed pumping speed is the minimum.

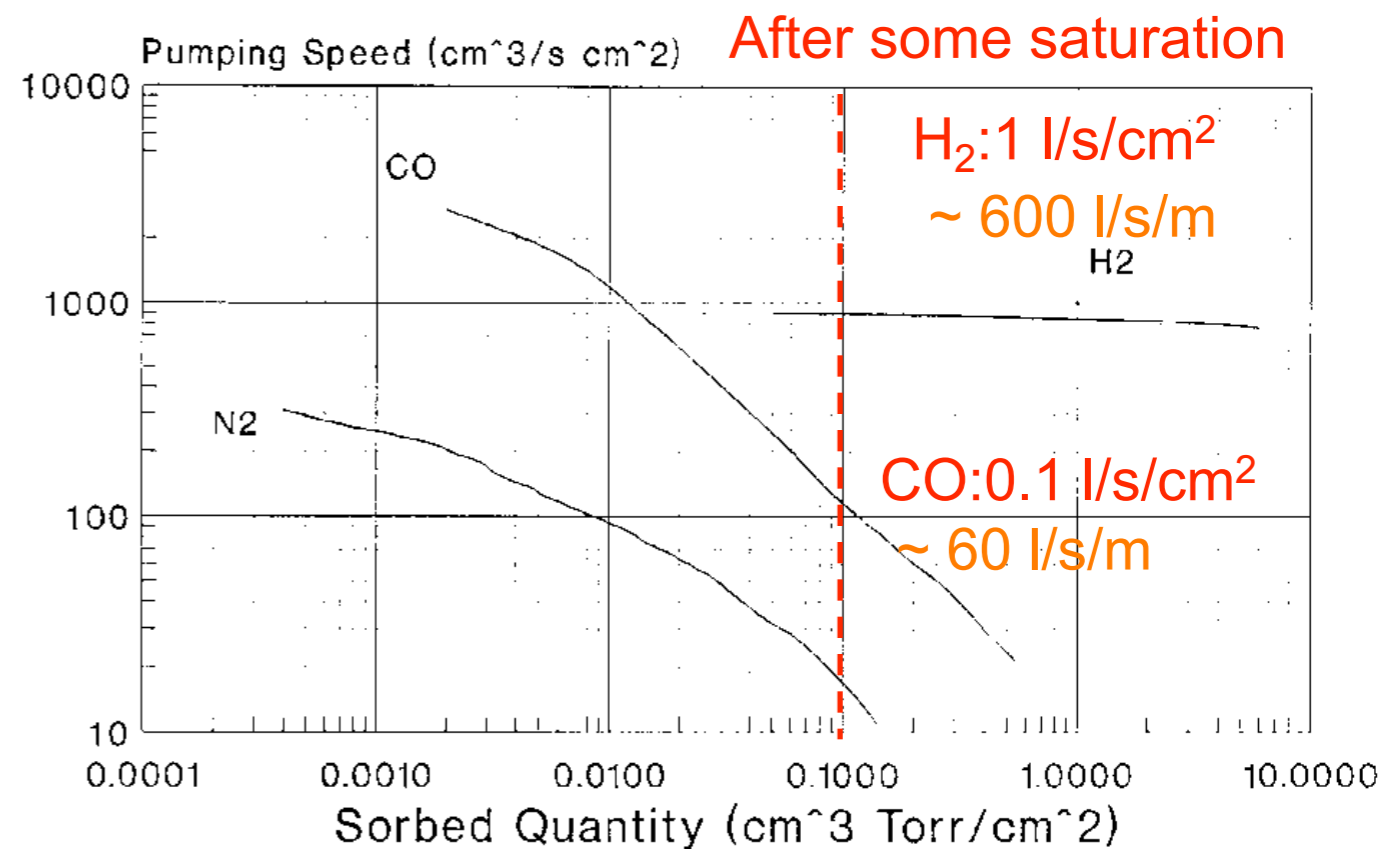
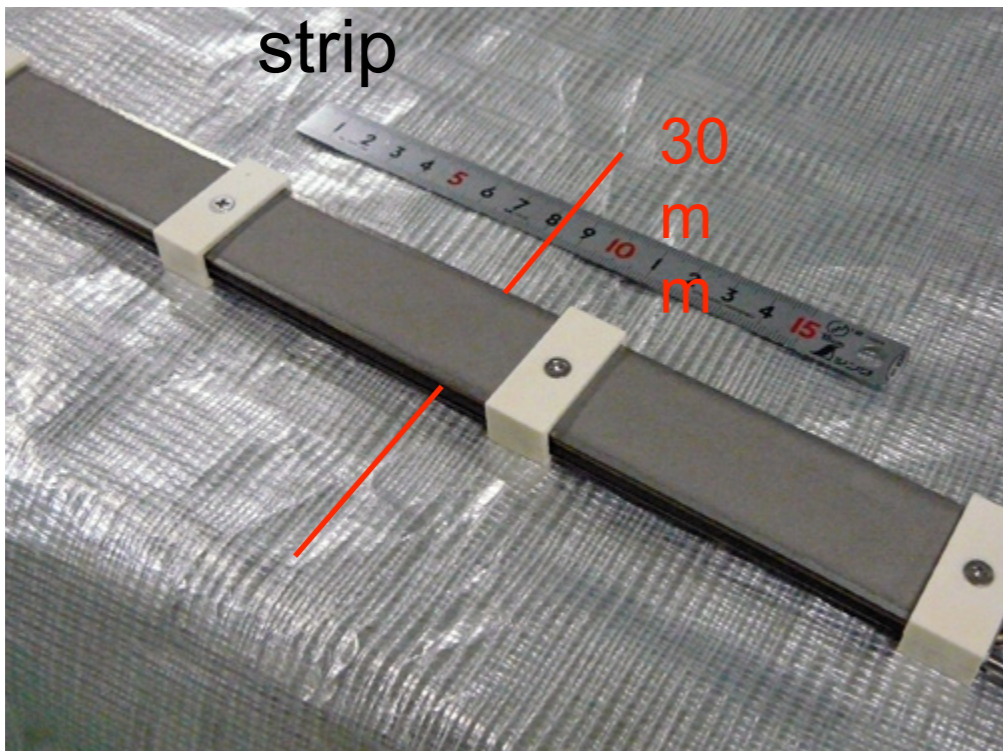


- Assumptions

- **Distributed pumping** to effectively evacuate these **conductance-limited beam pipes**
- Use **NEG strip** : **ST707 (SAES Getters)**, for ex.

ST 707/CTAM/30D Strip  
Typical Sorption Curves

St707 NEG  
strip



Activation : 450 C x 45 min  
Sorption : T= 25 C P= 3E-6 Torr  
Ref. M.FSPT.0004 Rev.0 Jan 5, 1994



PREP. *Wentzel*

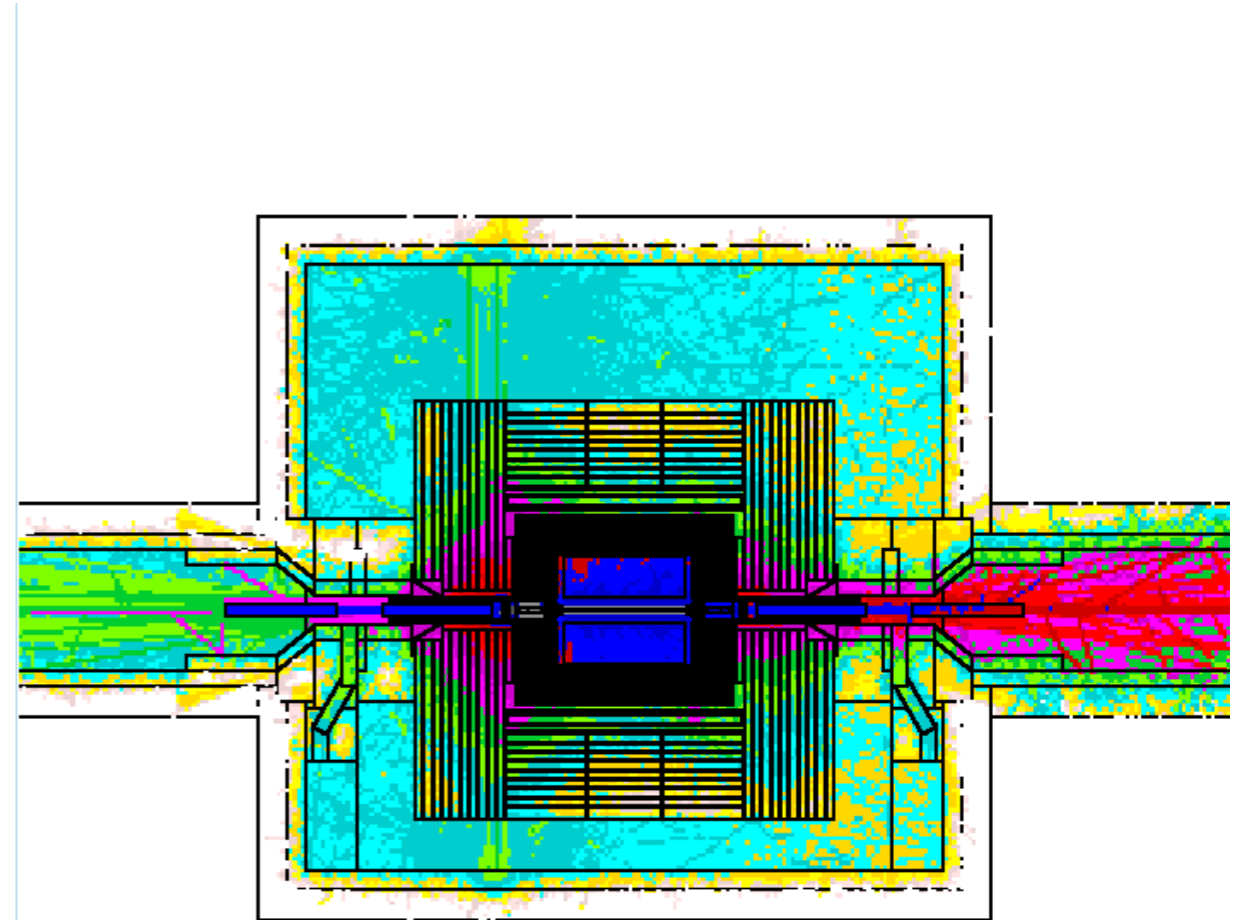
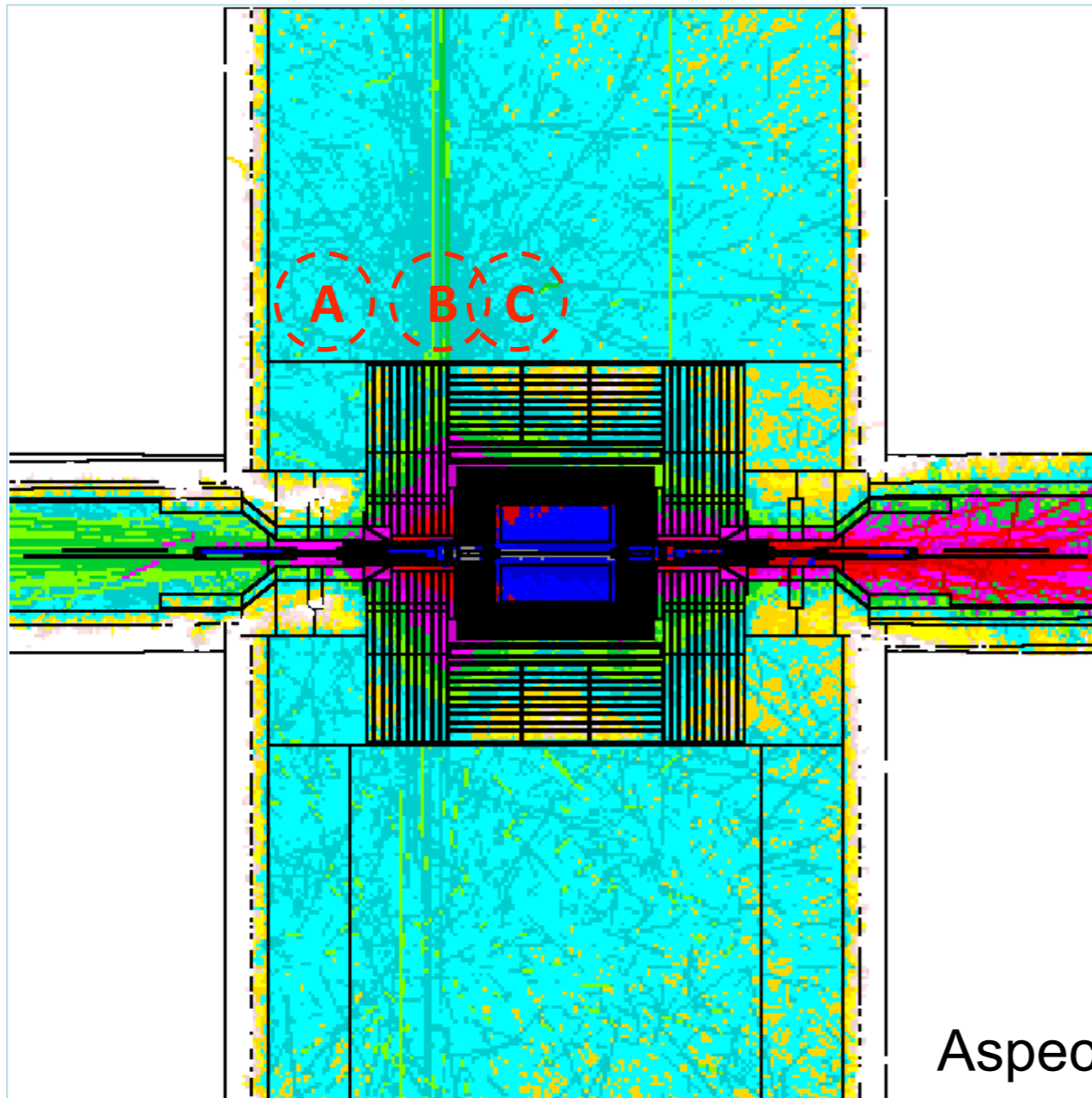
# Radiation Shield of Detector

- (1) Self-shielded or additional local fixed/movable shielding wall
- (2) Nominal operation :  $< 0.5 \mu\text{Sv}(0.05 \text{ mrem})/\text{hour}$  near the offline detector
- (3) Accident case :
  - $< 250 \text{ mSv}(25\text{rem})/\text{hour}$  for maximum credible beam  
( simultaneous loss of both beams anywhere near IP )
  - The integrated dose  $< 1\text{mSv}(100\text{mrem}) / \text{accident}$
- (4) Remarks
  - gaps in CMS style assembly and PACMAN at beam line

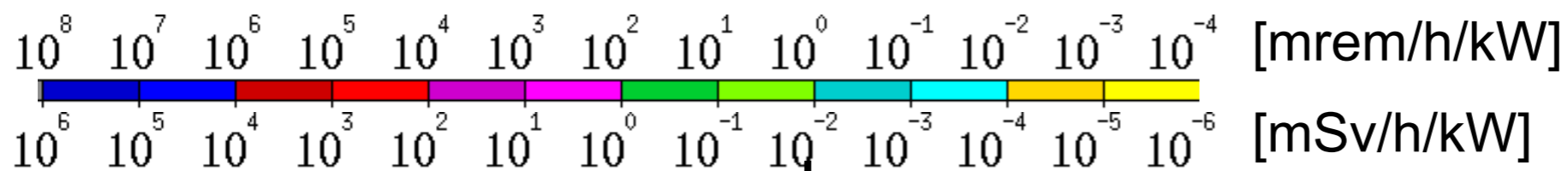
# Result of dose rate evaluation in IR hall

Plan view

Elevation view



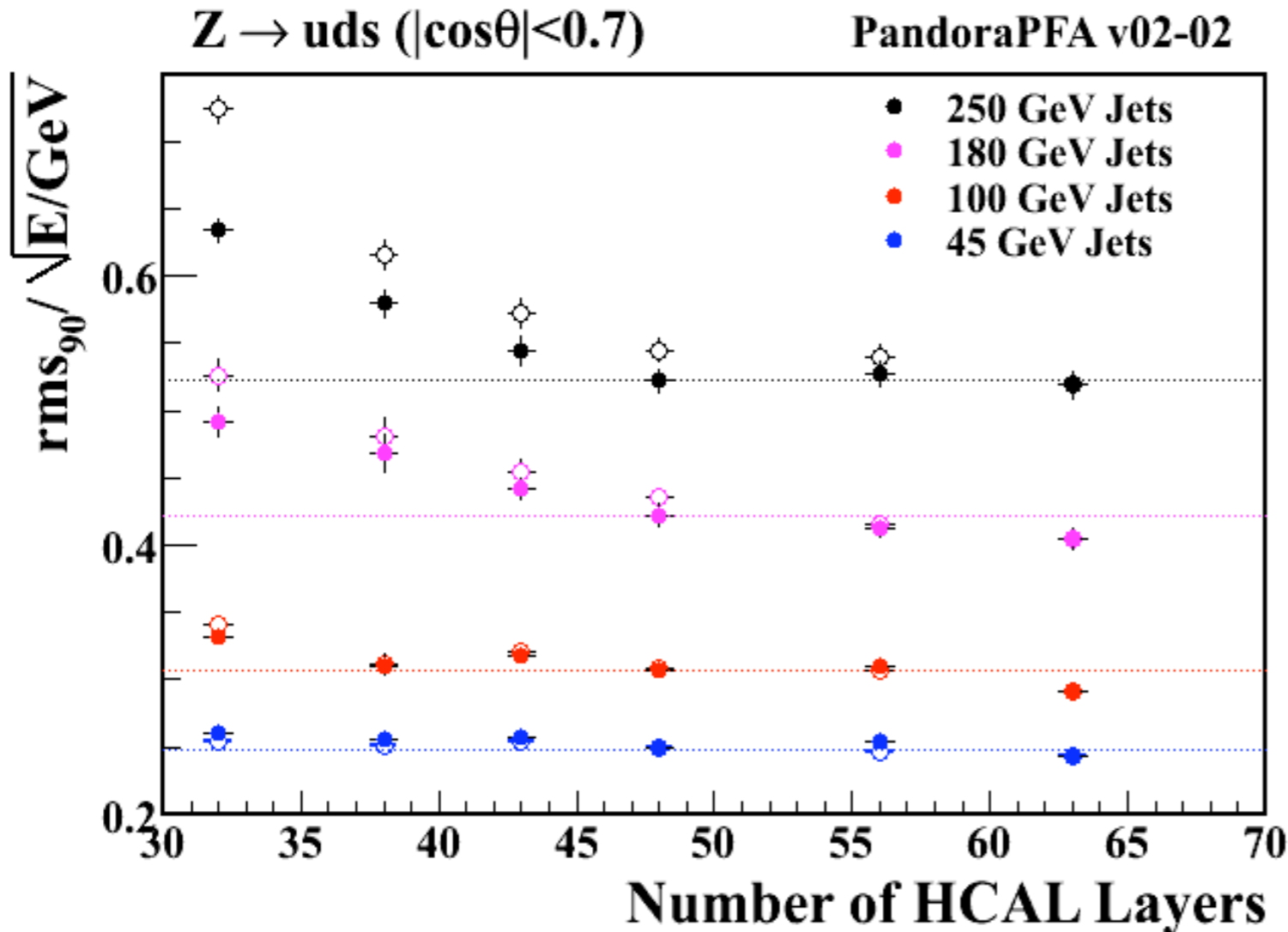
Aspect ratio 1:1 (20 m x 20m)



$1.39 \times 10^{-2}$  [mSv/h/kW] (250mSv/h / 18 MW)

# HCAL Depth Results

- Open circles = no use of muon chambers as a “tail-catcher”
- Solid circles = including “tail-catcher”



HCAL Layers	$\lambda_I$	
	HCAL	+ECAL
32	4.0	4.8
38	4.7	5.5
43	5.4	6.2
48	6.0	6.8
63	7.9	8.7

ECAL :  $\lambda_I = 0.8$

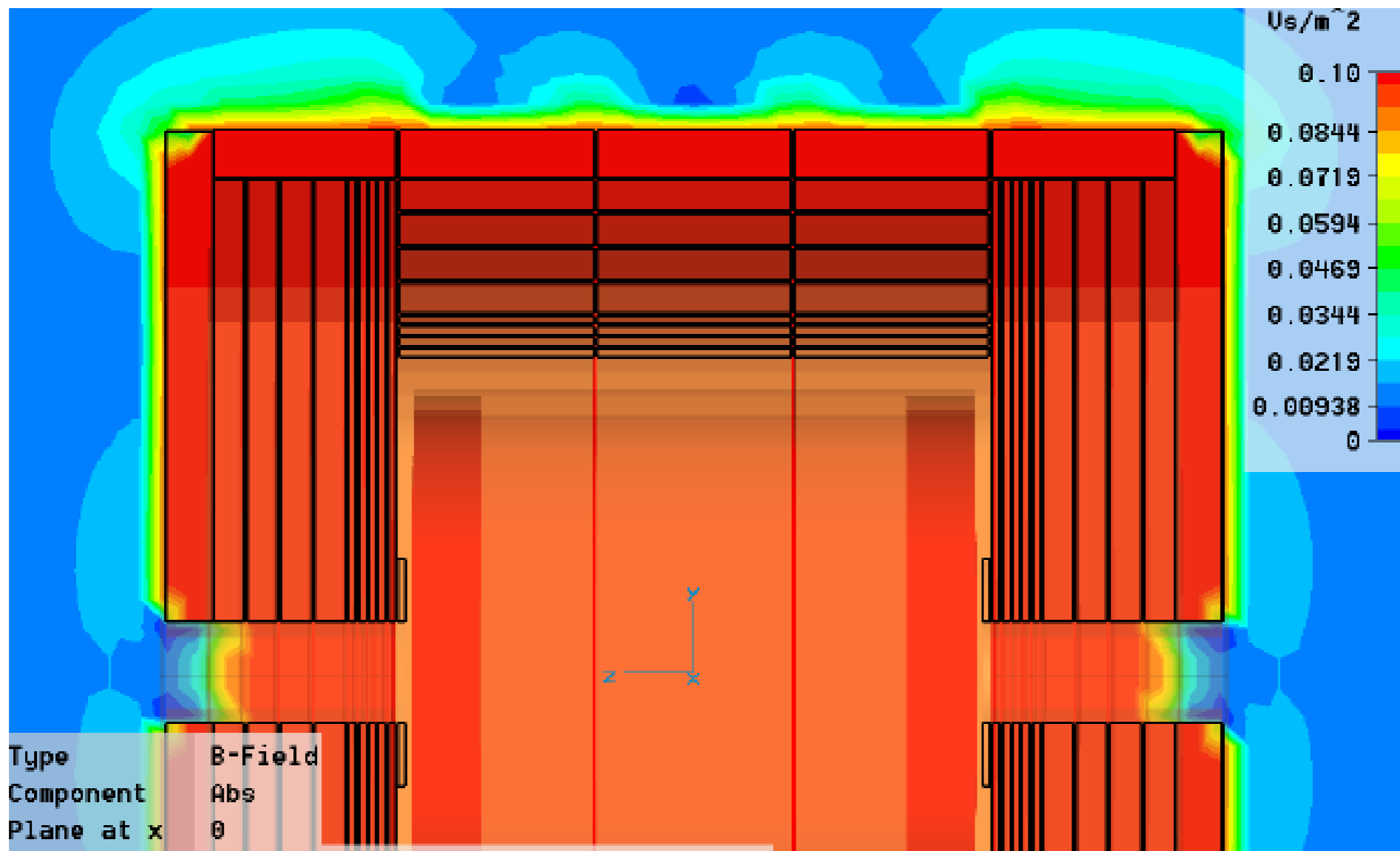
HCAL :  $\lambda_I$  includes scintillator

- ★ Little motivation for going beyond a 48 layer ( $6 \lambda_I$ ) HCAL
- ★ Depends on Hadron Shower simulation
- ★ “Tail-catcher”: corrects ~50% effect of leakage, limited by thick solenoid

For 1 TeV machine “reasonable range” ~ 40 – 48 layers ( $5 \lambda_I - 6 \lambda_I$ )

# B Field Calculations

Added 60cm of iron to reduce stray field, bounding box 15m



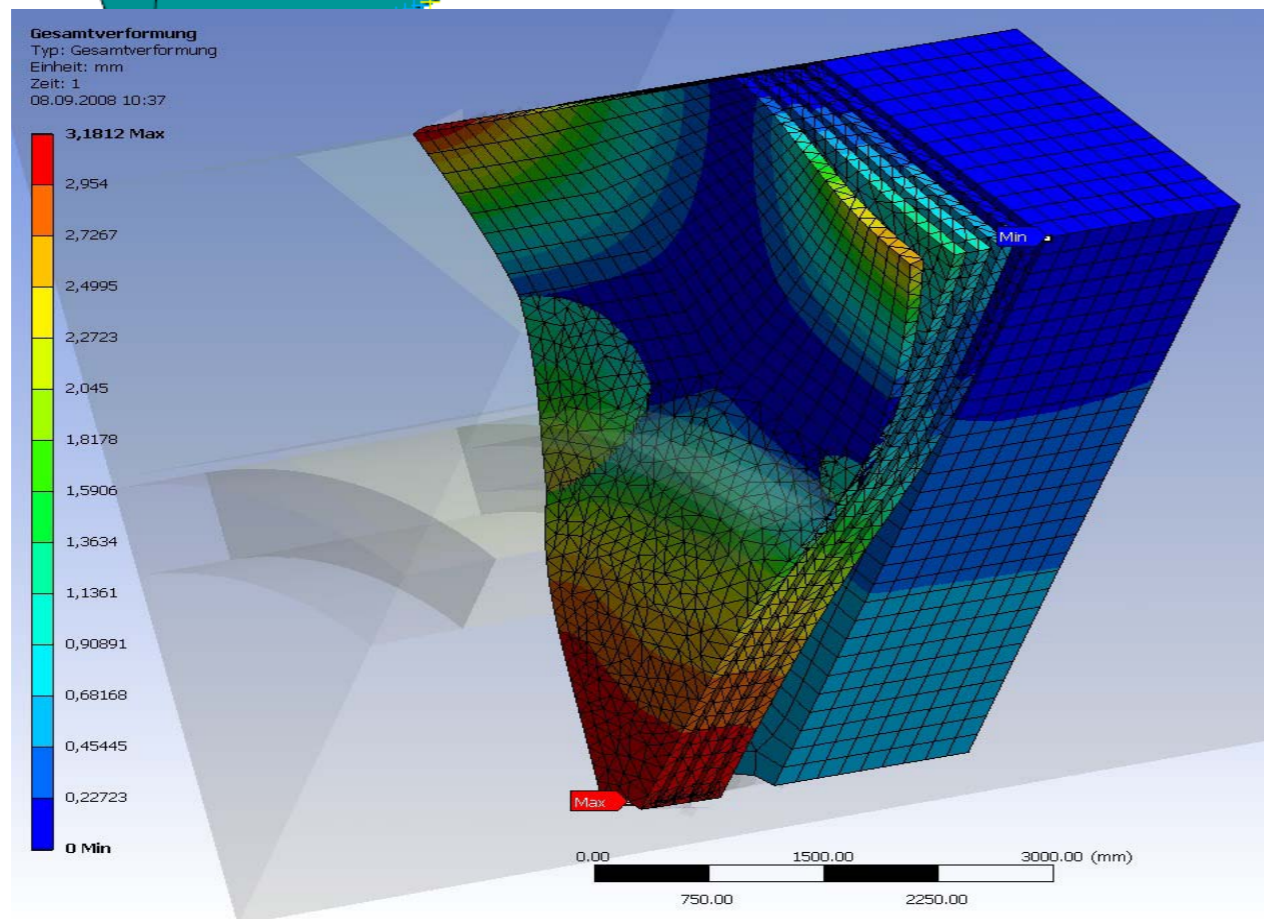
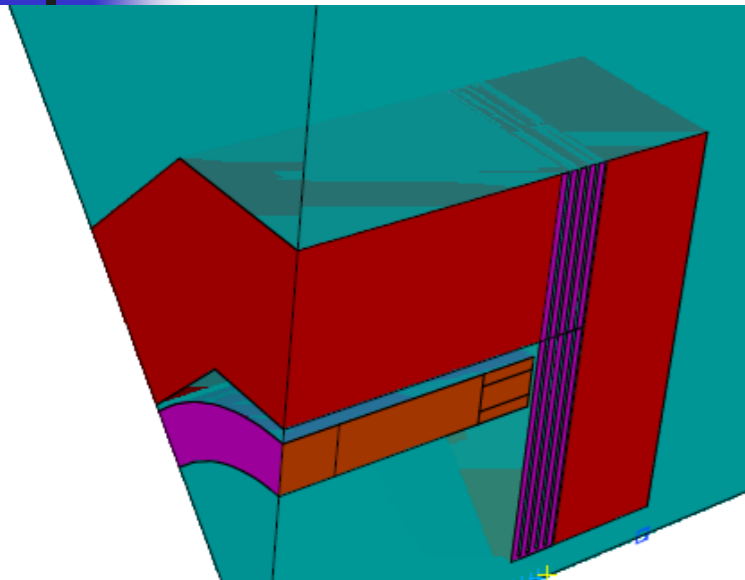
# Deformation due to Magnetic Forces

C.Martens

Deformation of inner thin end-cap section with radial rips

- So far not connected to outer end-cap
- Plates connected at inner tube
- Very preliminary results max. deformation
  - 3mm at 3T
  - 4.5mm at 4T

Confident that a 'thin' plate inner end-cap can be built



6. solenoid; 3.5T operation but design at 4T  
: Francois Kircher, Yamaoka (cryostat, coil support )
  - strong coil support for the push pull
  - coil design for stability
  - uniformity
7. anti-DID : B.Parker, Iwashita for passive anti-DID
8. support of final quadrupole magnets, forward calorimeters :  
Yamaoka, Matthieu
9. assembling/installation and maintenance method :  
Sugimoto, Yamaoka, Uwe, Henri
  - period - 5 years as in the RDR
10. option in machine parameters : Karsten, Henri, Tauchi
  - new Low-P
  - $L^* = 7 - 8$  m

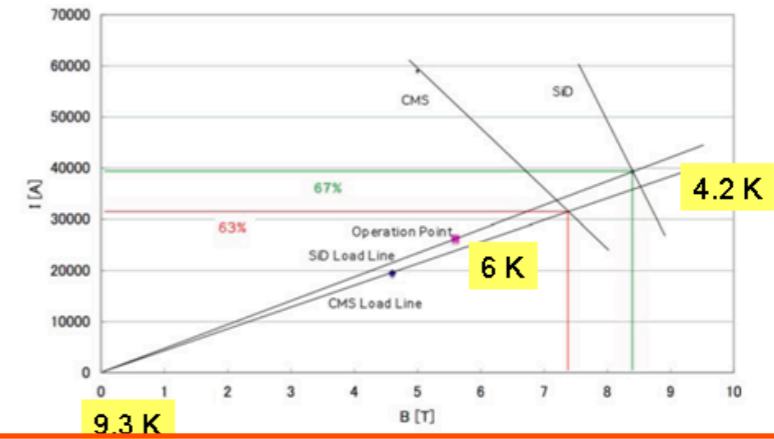
# SC Coil Design

Superconducting Magnets  
for ILC Detectors

A. Yamamoto (KEK)

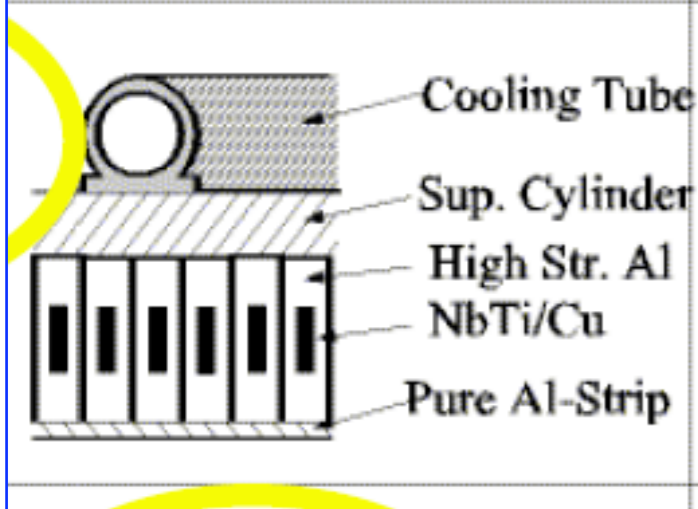
To be presented at ACFA Meeting,  
Beijing, Feb. 4, 2007

## NbTi Superconductor Facing Limit with Temperature Margin

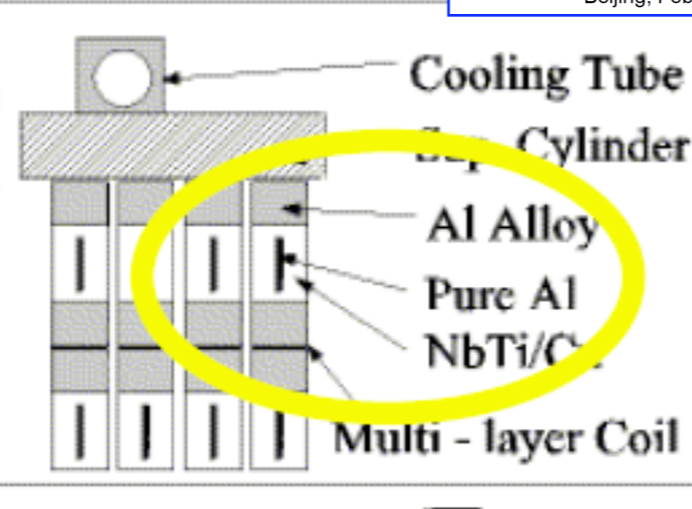


- A load line ratio of  $< 70\%$  should be kept to keep a temperature margin of  $>> 1\text{ K}$ .
- A useful field of  $5\text{ T}$  reaching the practical limit of NbTi

### SDC / ATLAS



### CMS

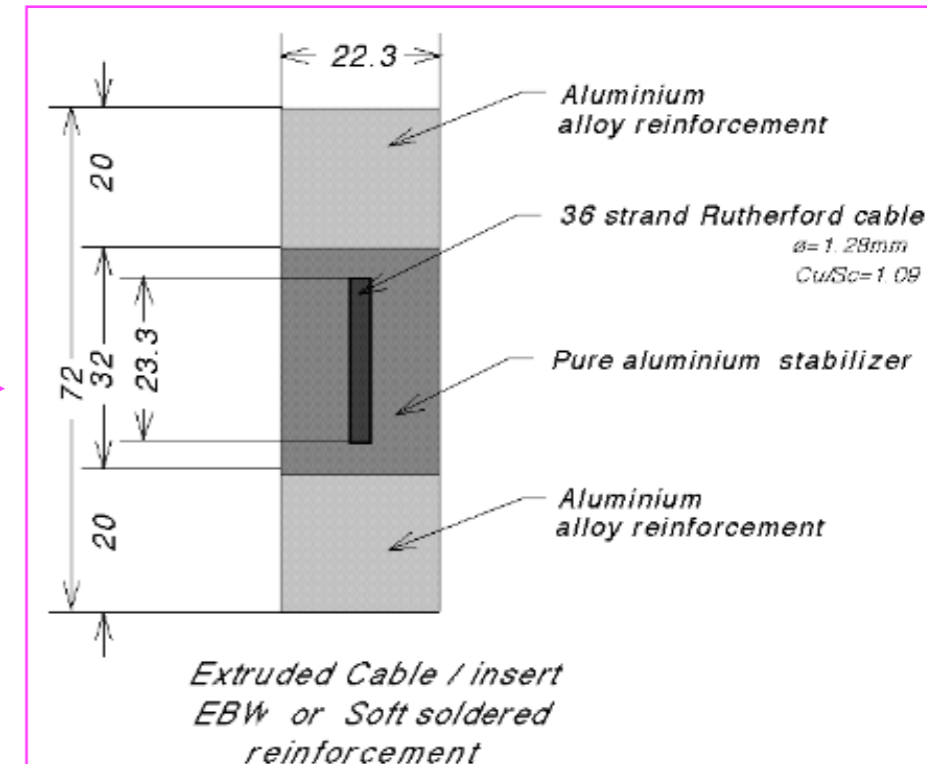


Ref: [CMS: The Magnet Project - Technical Design Report](#)

#### 12.3 Mechanical consideration

The thin, aluminium stabilised solenoids developed in the past 15 years show common characteristics. As an example for all these magnets (CDF, TOPAZ, VENUS, H1, ZEUS, DELPHI, ALEPH, etc.) This solution minimises the bonding area between conductors and reinforcement leading to **some disadvantages**.

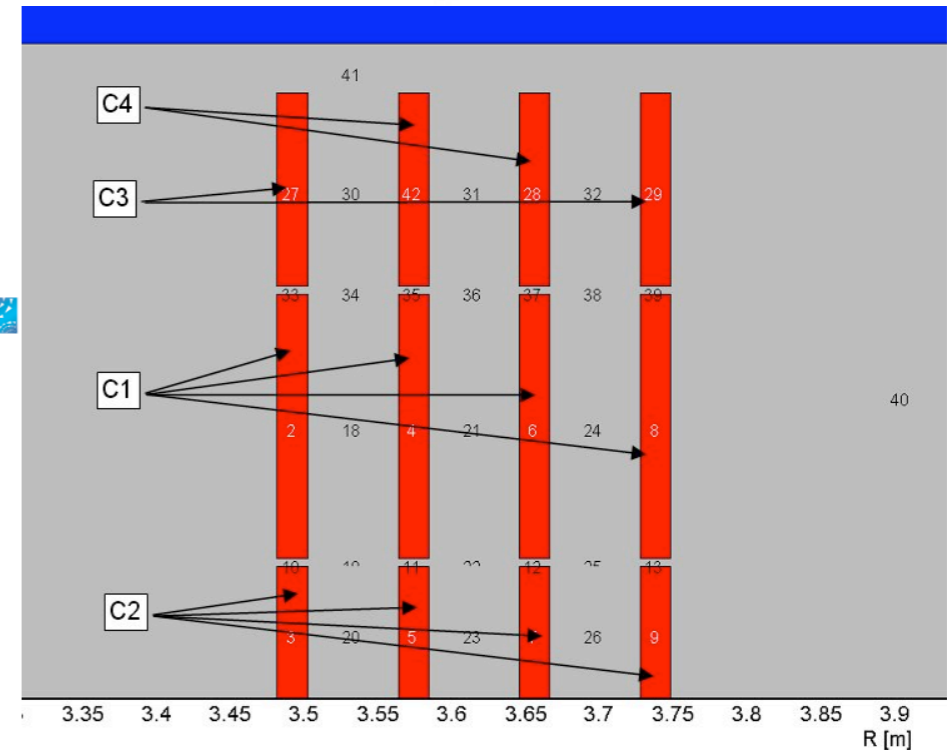
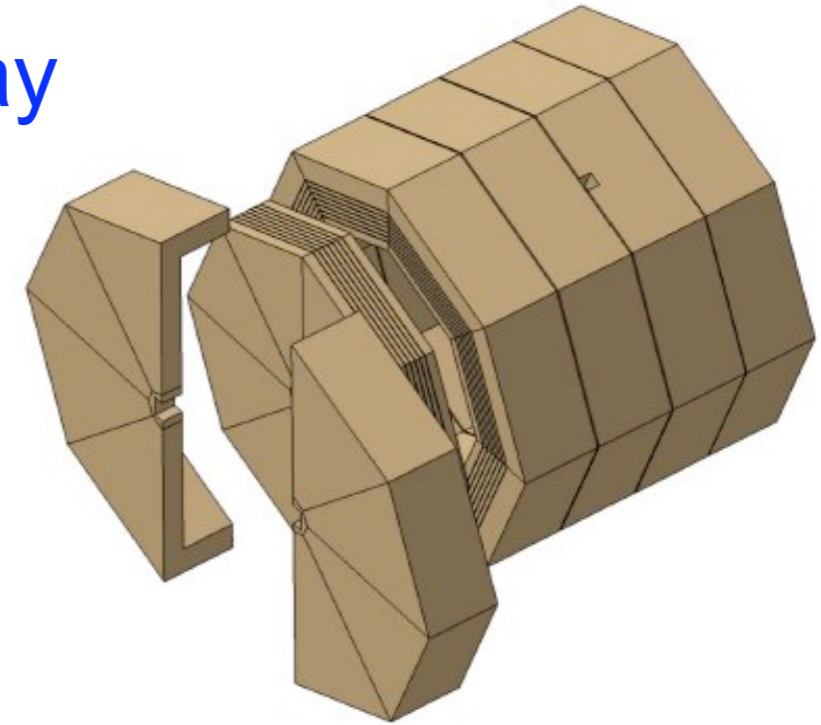
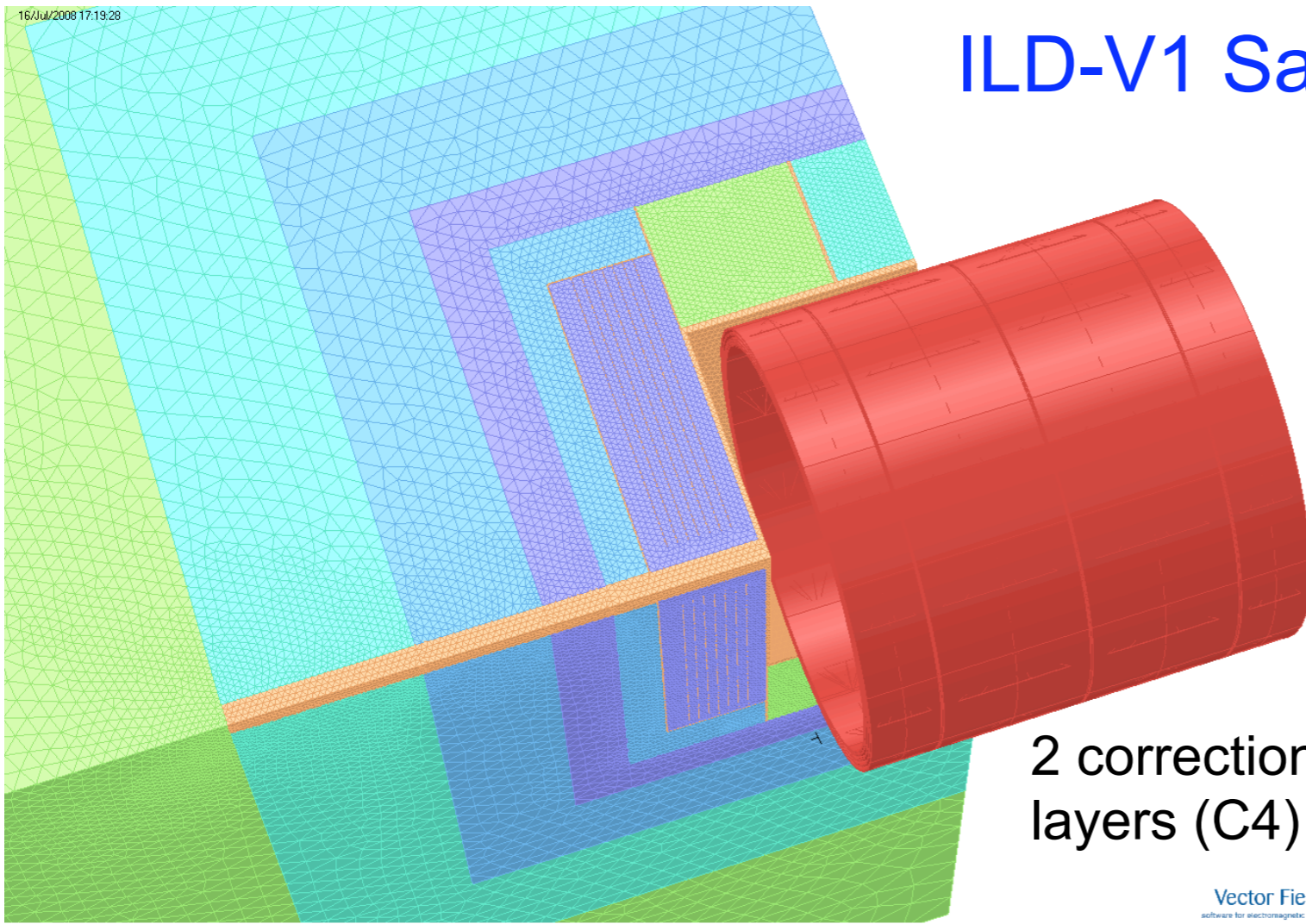
- The structural part is far from the conductor, so that its heat capacity plays no role (or a minor role) in determining the stability margins.
- The total axial force (147 MN) is transferred to the reinforcement through the bonding of the outermost layer. This bonding becomes very critical for the shear strength resistance.
- The axial thermal contraction of the coil, affected by the insulating material, does not match the cylinder thermal contraction, leading to a further increase of the shear stress at the cylinder-winding bond.



→ As the CMS, Hybrid type is better, but  $B < 5\text{ Tesla}$ .



# ILD-V1 Saclay

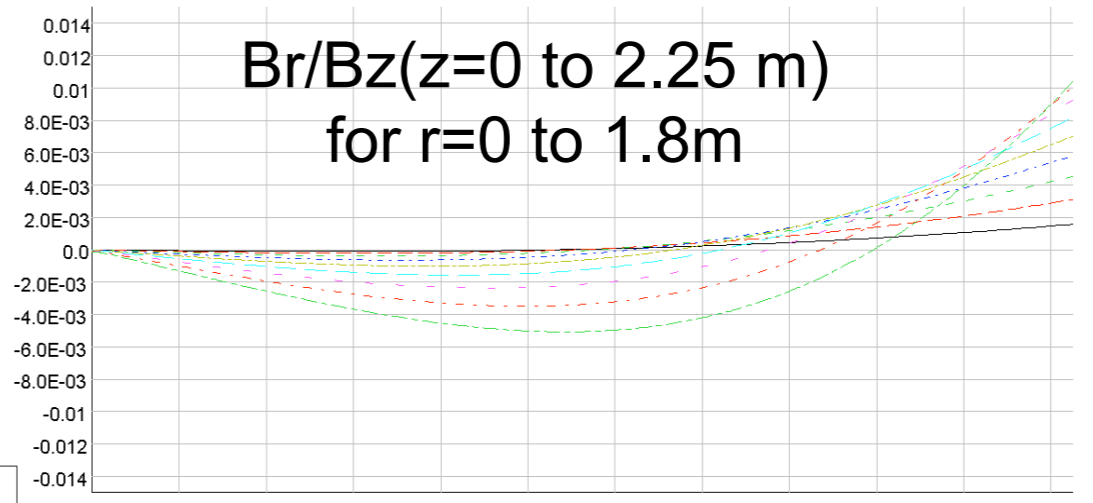
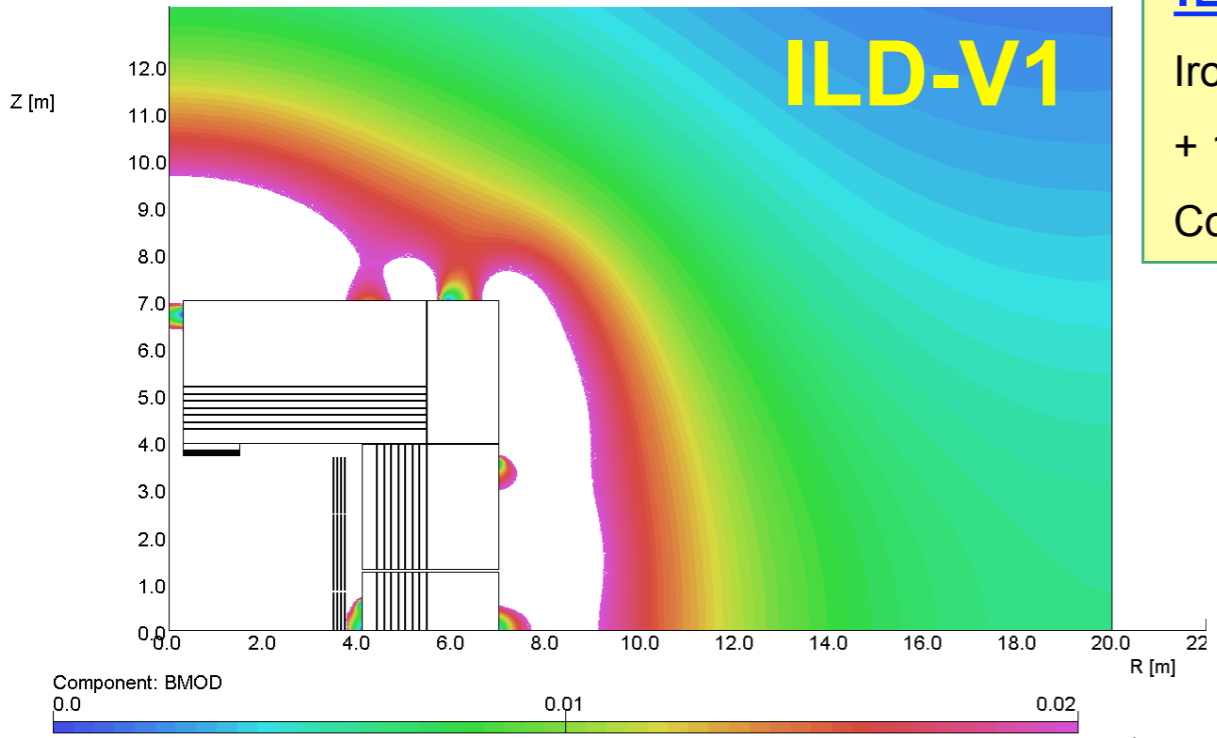


Current distribution :		2 correction layers		
12948	12948	12948	12948	12948
32136	12948	12948	12948	32136
32136	12948	12948	12948	32136
12948	12948	12948	12948	12948

	NI (MA)	J (A/mm <sup>2</sup> )	N (turns/layer)	I per turn (kA)	I correction (kA)	Length (m)
<b>C1</b>	1.29	40.0	100	12.9	0	1.65
<b>C2</b>	0.65	40.0	50	12.9	0	1.65
<b>C3</b>	0.95	40.0	73	12.9	0	1.21
<b>C4</b>	2.35	93.0	73	32.1	19.2	1.21

# ILD-V1 configuration

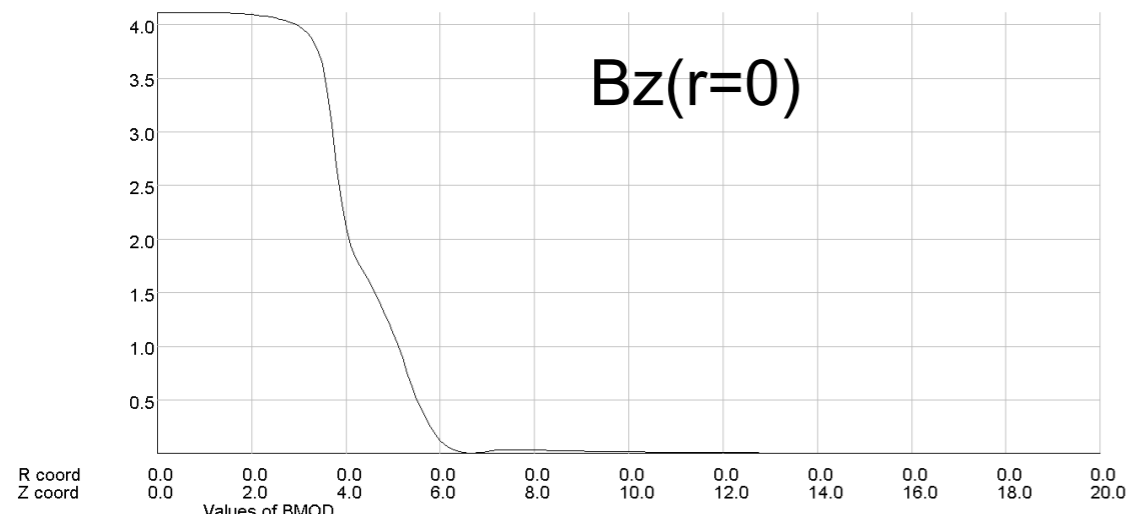
Iron : up to R=7m, up to Z=+/-7m (~3m thickness)  
 + 100 mm FSP (Field Shaping Plate)  
 Coil : 4 layers ,7.35 m length subdivided in 5 parts



UNITS

Length	: m
Flux density	: T
Field strength	: A m <sup>-1</sup>
Potential	: Wb m <sup>-1</sup>
Conductivity	: S m <sup>-1</sup>
Source density	: A m <sup>-2</sup>
Power	: W
Force	: N
Energy	: J
Mass	: kg

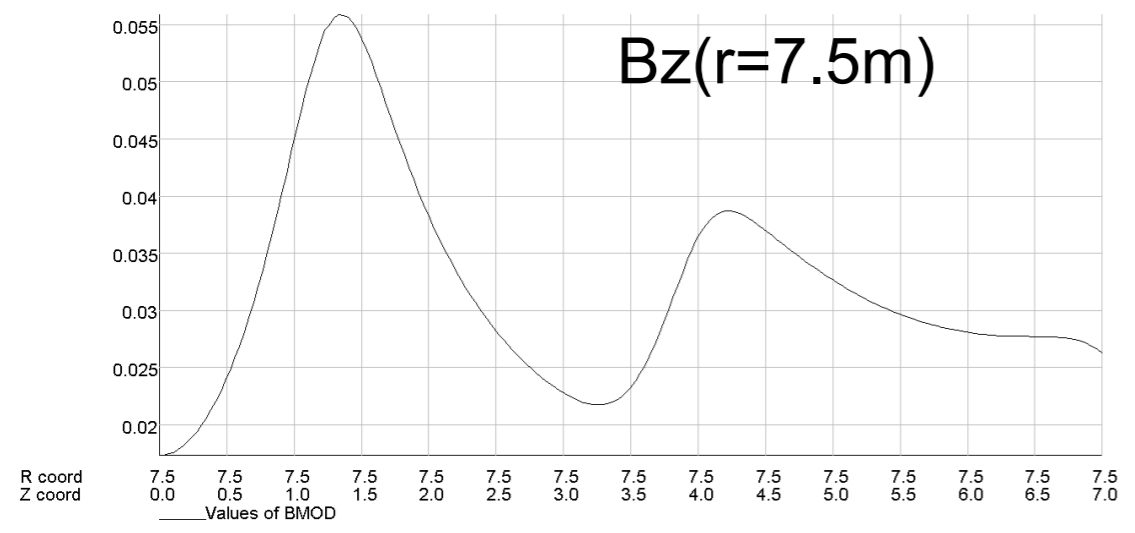
PROBLEM DATA  
 D:\Users\delfem\VF\OP  
 ERA-V12\ILD2\ILD-V1.  
 ST  
 Linear elements  
 Axi-symmetry  
 Modified R<sup>2</sup>vec pot.  
 Magnetic fields  
 Static solution  
 Scale factor: 1.0  
 267061 elements  
 134124 nodes  
 363 regions



UNITS

Length	: m
Flux density	: T
Field strength	: A m <sup>-1</sup>
Potential	: Wb m <sup>-1</sup>
Conductivity	: S m <sup>-1</sup>
Source density	: A m <sup>-2</sup>
Power	: W
Force	: N
Energy	: J
Mass	: kg

PROBLEM DATA  
 D:\Users\delfem\VF\OP  
 ERA-V12\ILD2\ILD-V1.  
 ST  
 Linear elements  
 Axi-symmetry  
 Modified R<sup>2</sup>vec pot.  
 Magnetic fields  
 Static solution  
 Scale factor: 1.0  
 267061 elements  
 134124 nodes  
 363 regions

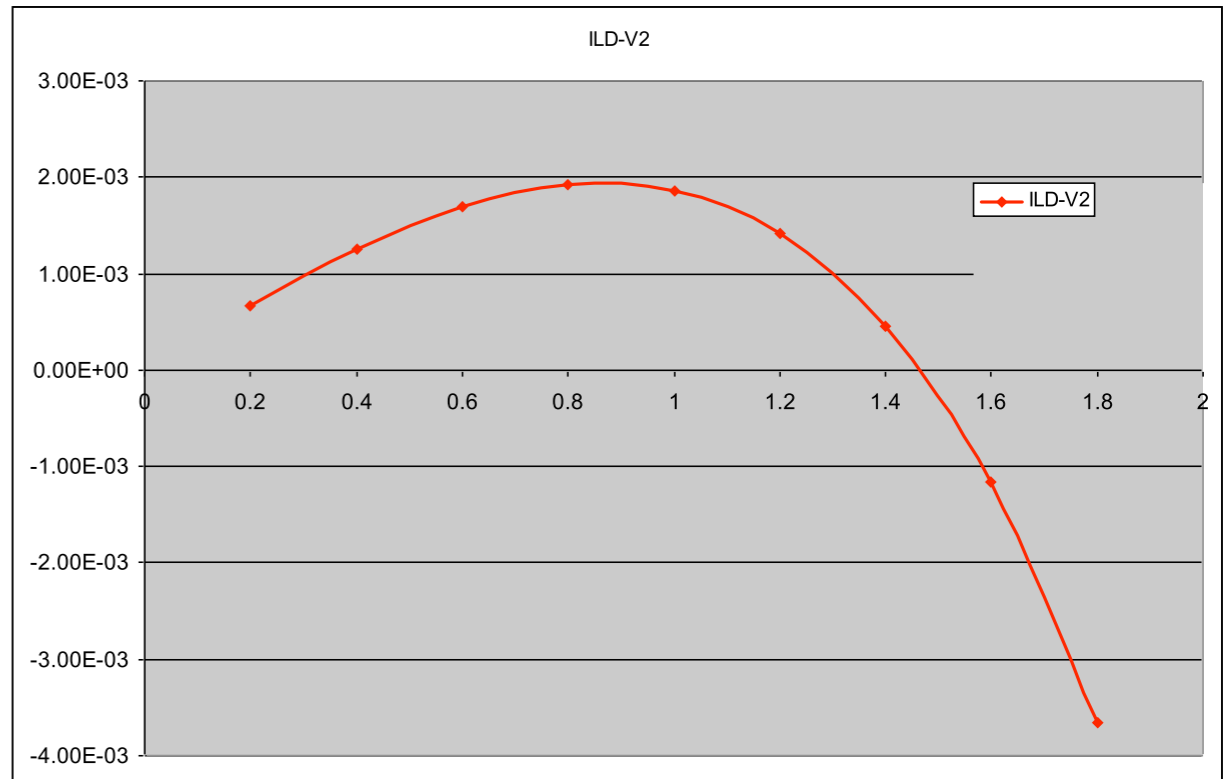


UNITS

Length	: m
Flux density	: T
Field strength	: A m <sup>-1</sup>
Potential	: Wb m <sup>-1</sup>
Conductivity	: S m <sup>-1</sup>
Source density	: A m <sup>-2</sup>
Power	: W
Force	: N
Energy	: J
Mass	: kg

PROBLEM DATA  
 D:\Users\delfem\VF\OP  
 ERA-V12\ILD2\ILD-V1.  
 ST  
 Linear elements  
 Axi-symmetry  
 Modified R<sup>2</sup>vec pot.  
 Magnetic fields  
 Static solution  
 Scale factor: 1.0  
 267061 elements  
 134124 nodes  
 363 regions

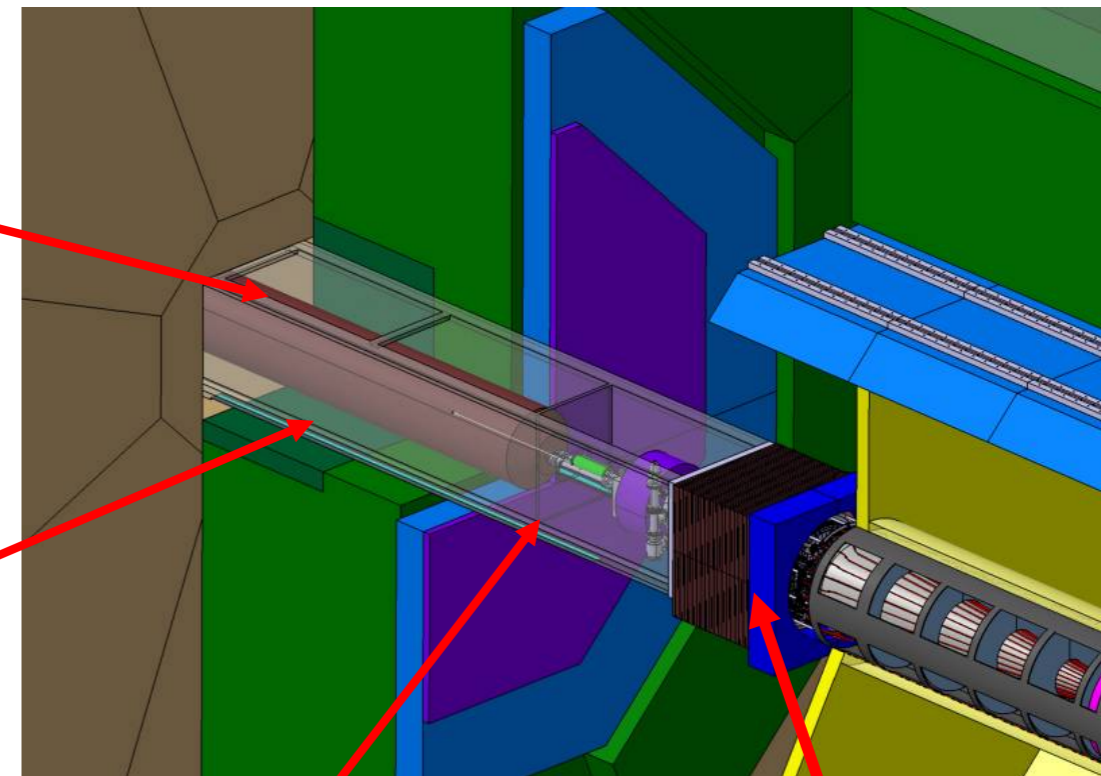
## f(Br/Bz) vs r (z=0 to 2.25 m)



- Description

QD0  
*(superconducting magnet)*

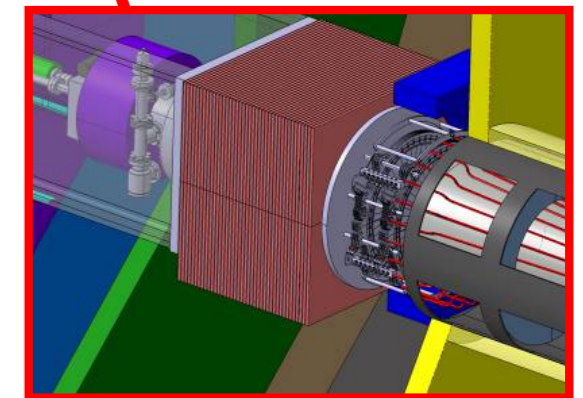
Support tube



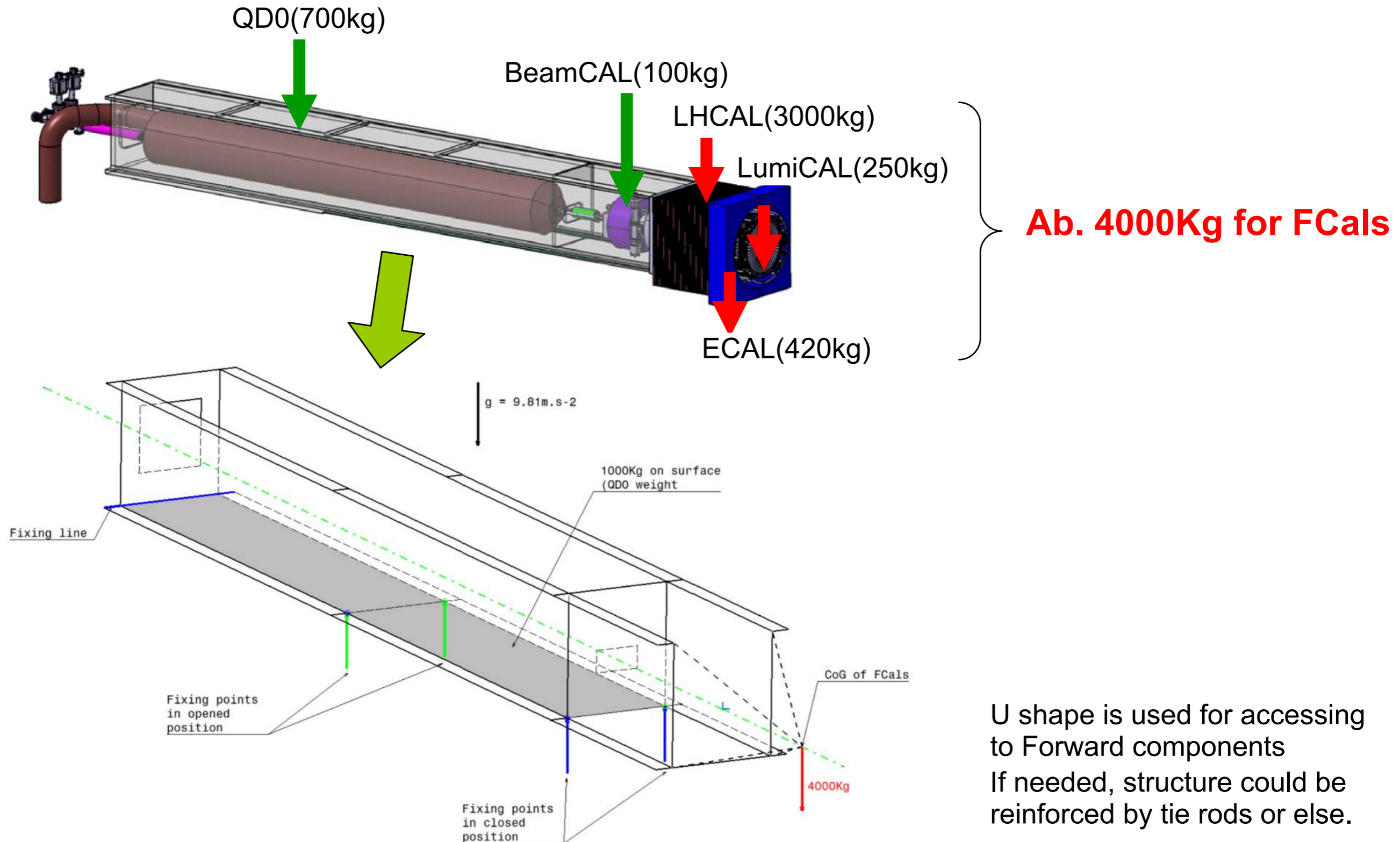
Beam line components

- Requirements on support tube

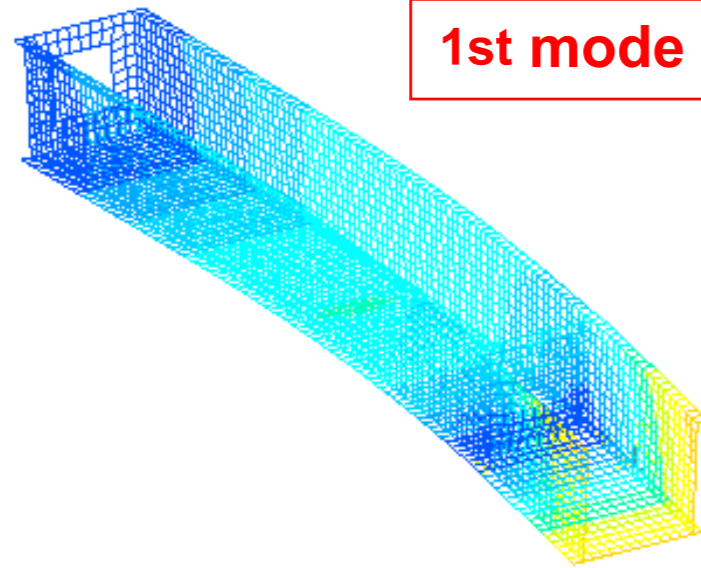
- **Support all the forward components**
- **Good vibration performance (QD0 stability)**
- **Allowable amplitude**
  - Few mm in static load
  - About 50nm for ground motion (IR interface document)
- **Alignment system is needed (in a mm range)**



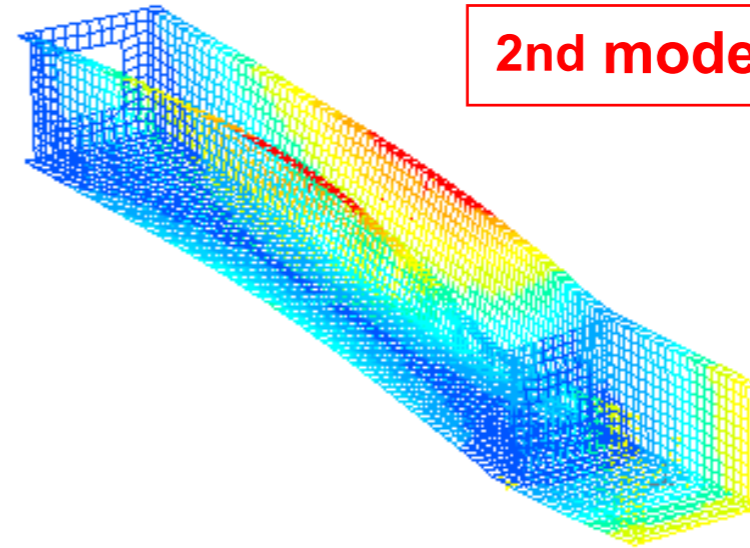
*Forward Cals*



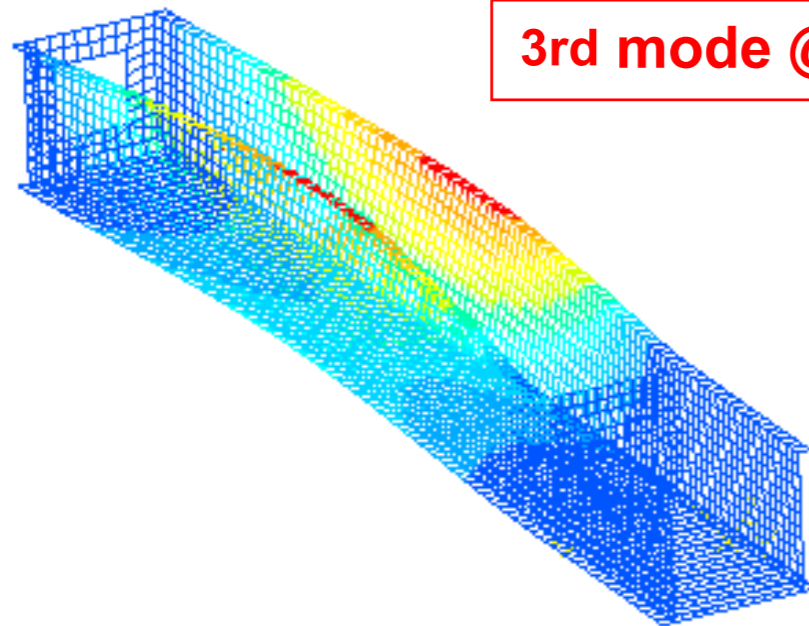
- For 50mm thick and Endcap closed



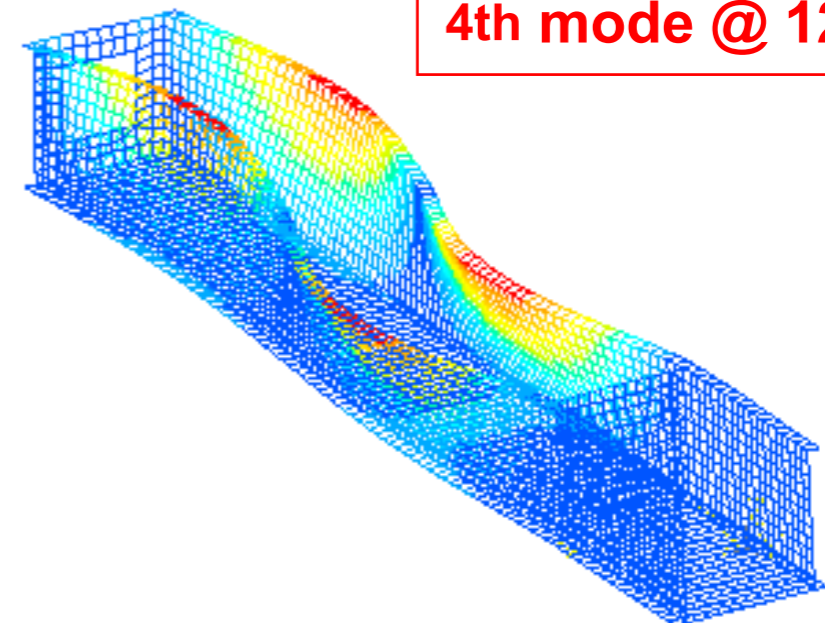
1st mode @ 44Hz



2nd mode @ 60Hz

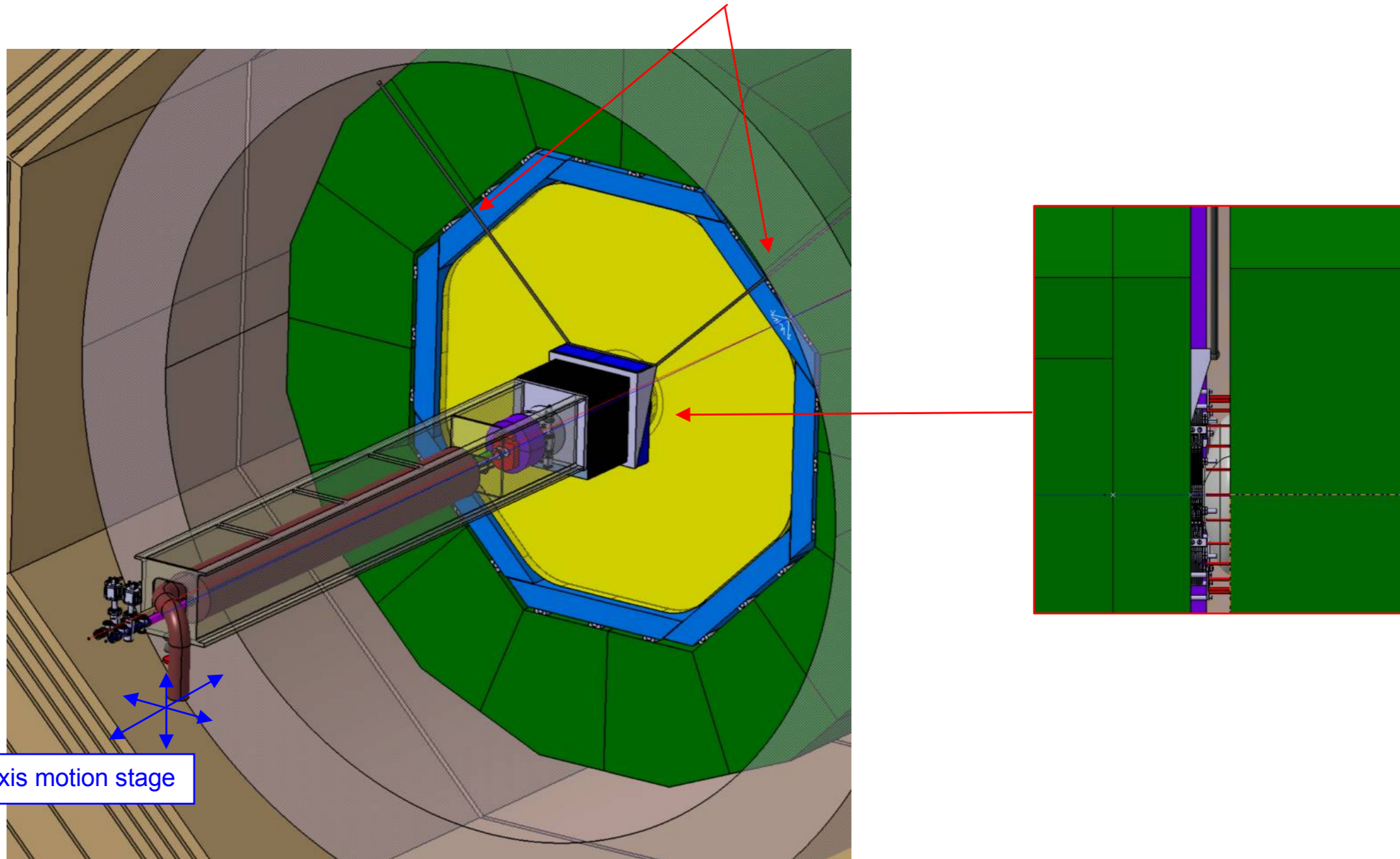


3rd mode @ 71Hz

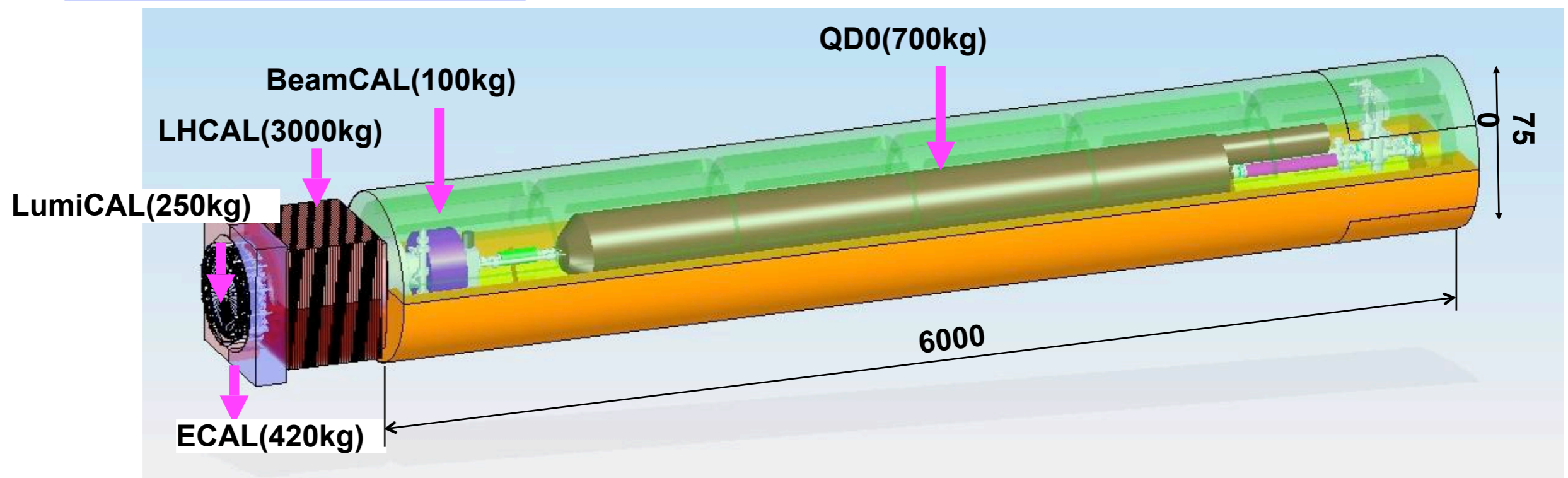


4th mode @ 125Hz

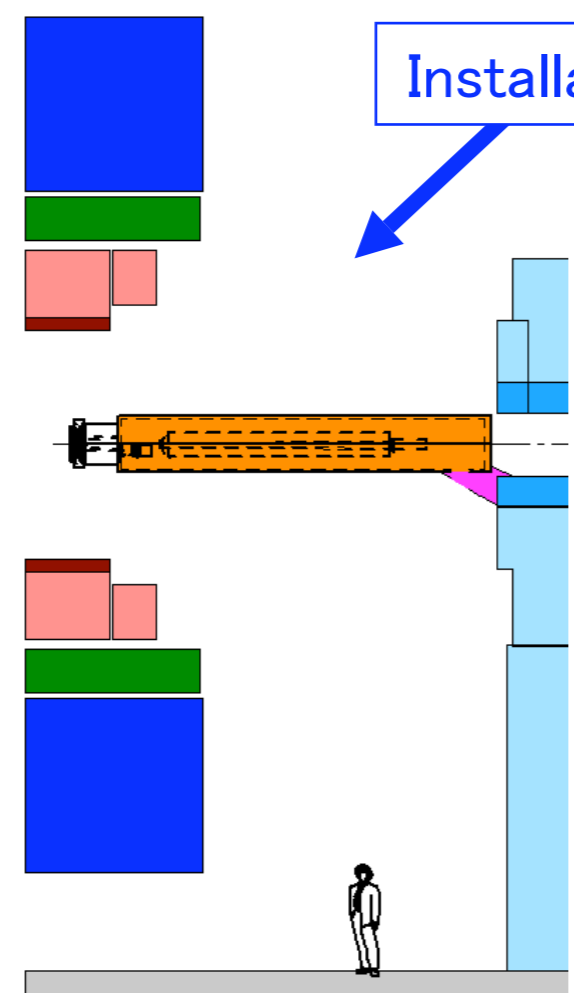
Adjustable tie rods



# Cylindrical Support Tube



## Installation method



H.Yamaoka will present the details at LCWS2008.

Progress since Warsaw, even after Cambridge ?

1. Engineering model of ILD

3D CAD

Opening scenario