

The ATF Damping Ring BPM Upgrade

- Overview and Status -

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for the ATF DR BPM Upgrade Collaboration

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- **Motivation**
- **The ATF Damping Ring**
- **Details of the BPM read-out electronics upgrade**
- **Beam studies and performance measurements**
- **Conclusions**

- ILC damping ring R&D at KEK's Accelerator Test Facility (ATF):
 - Investigation of the beam damping process (damping wiggler, minimization of the damping time, etc.)
 - Goal: generation and extraction of a low **emittance beam** ($\epsilon_{\text{vert}} < 2 \text{ pm}$) at the nominal ILC bunch charge
- A major tool for low emittance corrections:
a high resolution BPM system
 - Optimization of the closed-orbit, beam-based alignment (BBA) studies to investigate BPM offsets and calibration.
 - Correction of non-linear field effects, i.e. coupling, chromaticity,...
 - Fast global orbit feedback(?)
 - **Necessary: a state-of-the-art BPM system, utilizing**
 - a broadband turn-by-turn mode ($< 10 \text{ }\mu\text{m}$ resolution)
 - a narrowband mode with high resolution ($\sim 100 \text{ nm}$ range)

- **ATF Damping Ring Beam Position Monitor System**
 - Button style BPM pickup stations
 - Original read-out electronics:
Analog signal processing, no TBT, intensity dependence
- **2006: M. Ross & SLAC team**
 - Analog downconverter & digital receiver (*Echotek*) read-out system, prototype achieves 1-2 μm resolution
- **2007/8: KEK/SLAC/Fermilab collaboration**
 - 20 BPMs in both arcs equipped with new read-out system
 - EPICS & LabVIEW software
 - Few μm resolution in TBT, ~ 200 nm narrowband
 - First test of an integrated automatic calibration system
- **2009: KEK/Fermilab**
 - Improvements on the downconverter

Machine and Beam Parameters

beam energy $E = 1.28 \text{ GeV}$

beam intensity, single bunch $\approx \sim 1.6 \text{ nC} \equiv 10^{10} \text{ e}^- (\equiv I_{\text{bunch}} \approx 3.46 \text{ mA})$

beam intensity, multibunch (20) $\approx \sim 22.4 \text{ nC} \equiv 20 \times 0.7 \times 10^{10} \text{ e}^- (\equiv I_{\text{beam}} \approx 48.5 \text{ mA})$

accelerating frequency $f_{\text{RF}} = 714 \text{ MHz}$

revolution frequency $f_{\text{rev}} = f_{\text{RF}} / 330 = 2.1636 \text{ MHz} (\equiv t_{\text{rev}} = 462.18 \text{ ns})$

bunch spacing $t_{\text{bunch}} = t_{\text{RF}} / 2 = 2.8011 \text{ ns}$

batch spacing $t_{\text{batch}} = t_{\text{rev}} / 3 = 154.06 \text{ ns}$

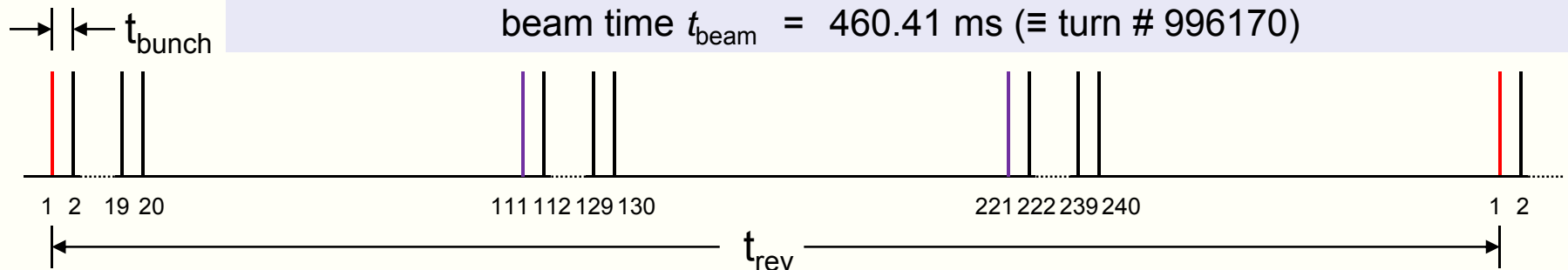
horizontal betatron tune $\approx 15.204 (\equiv f_h \approx 441 \text{ kHz})$

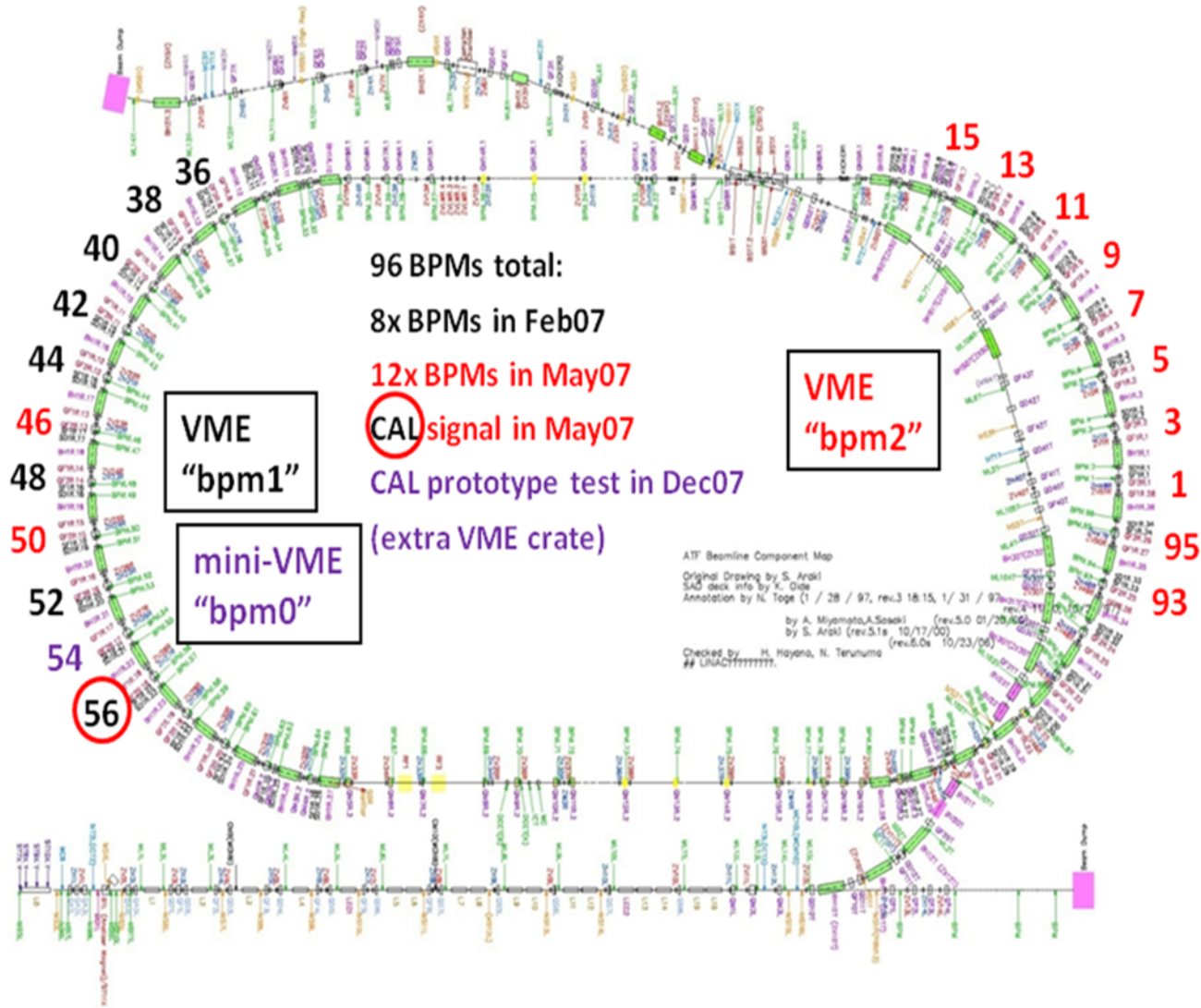
vertical betatron tune $\approx 8.462 (\equiv f_v \approx 1000 \text{ kHz})$

synchrotron tune $\approx 0.0045 (\equiv f_s \approx 9.7 \text{ kHz})$

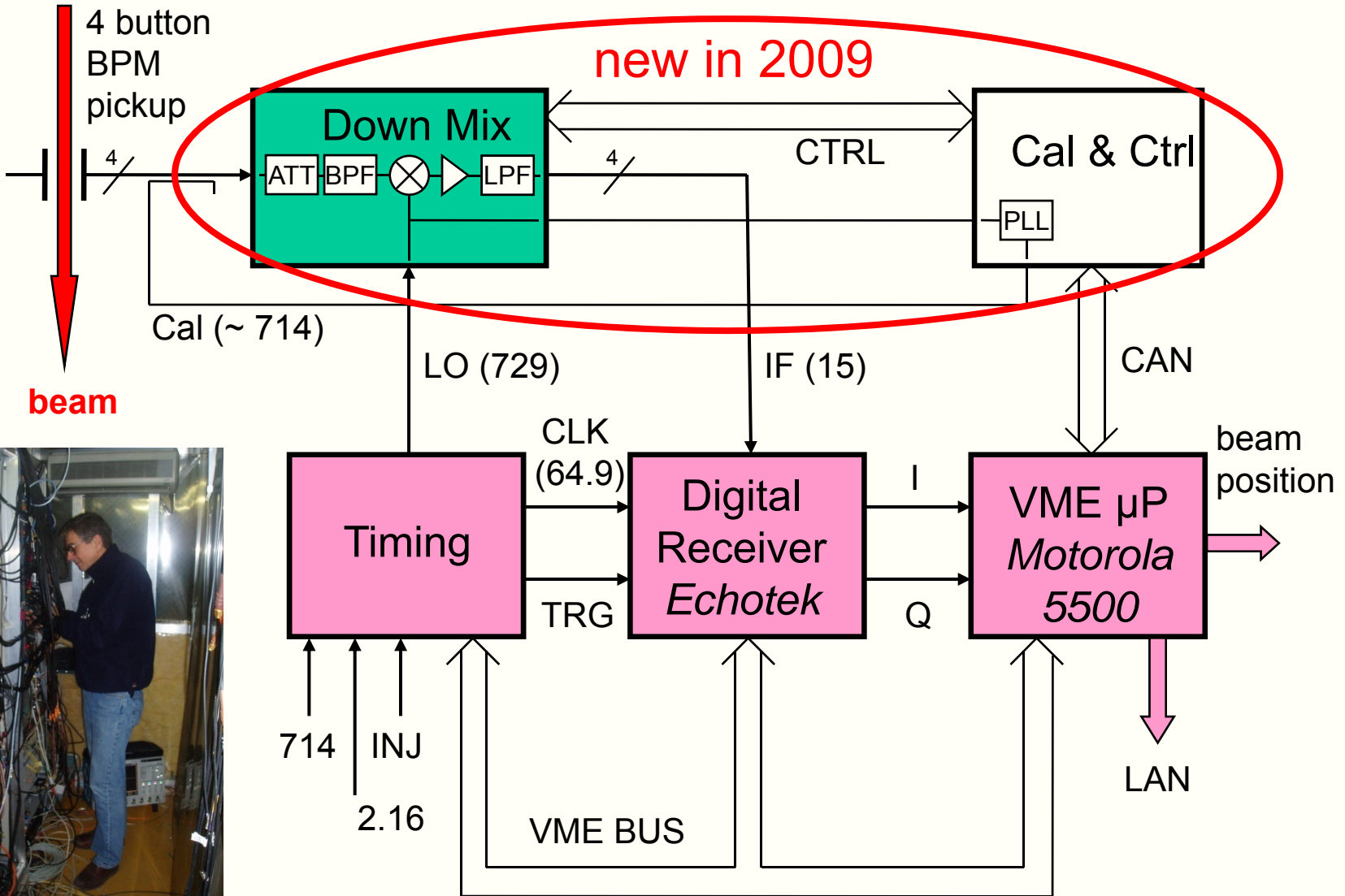
repetition frequency $f_{\text{rep}} = 1.56 \text{ Hz} (\equiv t_{\text{rep}} = 640 \text{ ms})$

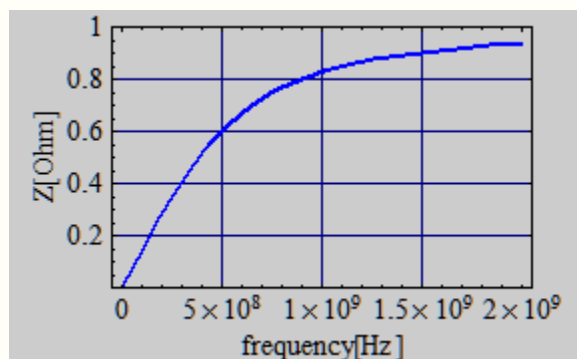
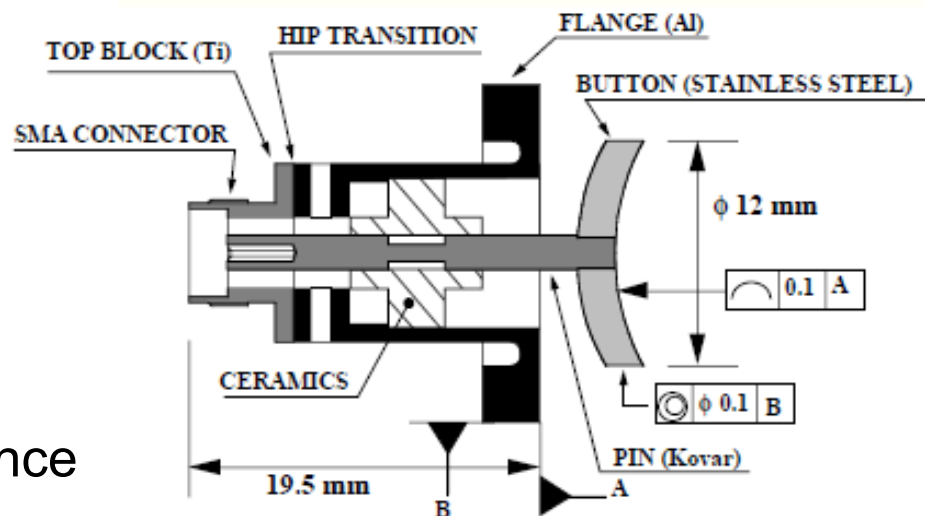
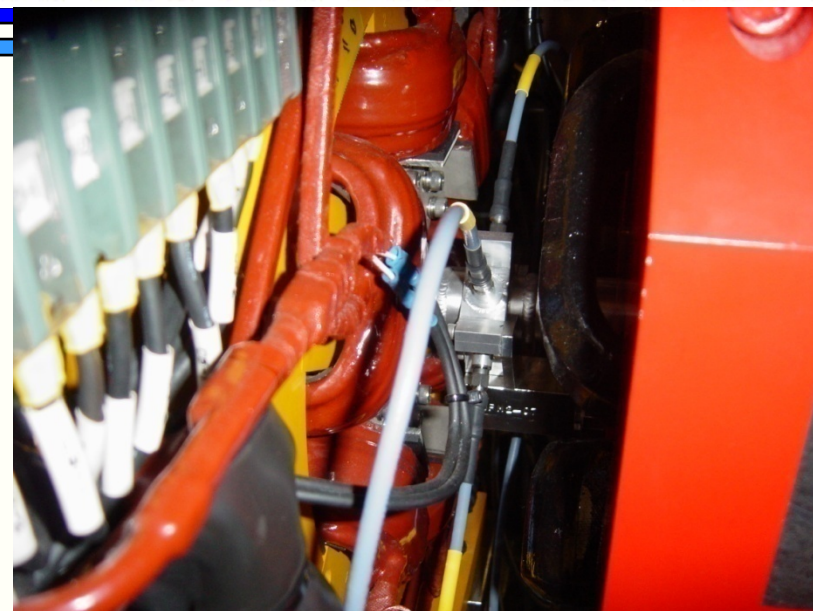
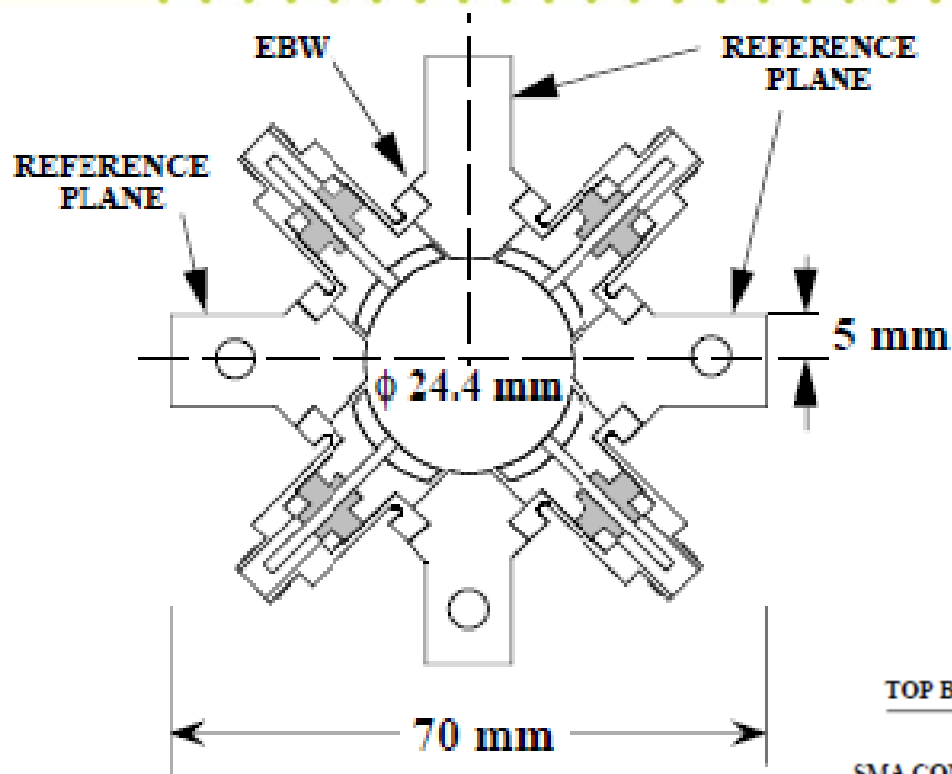
beam time $t_{\text{beam}} = 460.41 \text{ ms} (\equiv \text{turn \# 996170})$



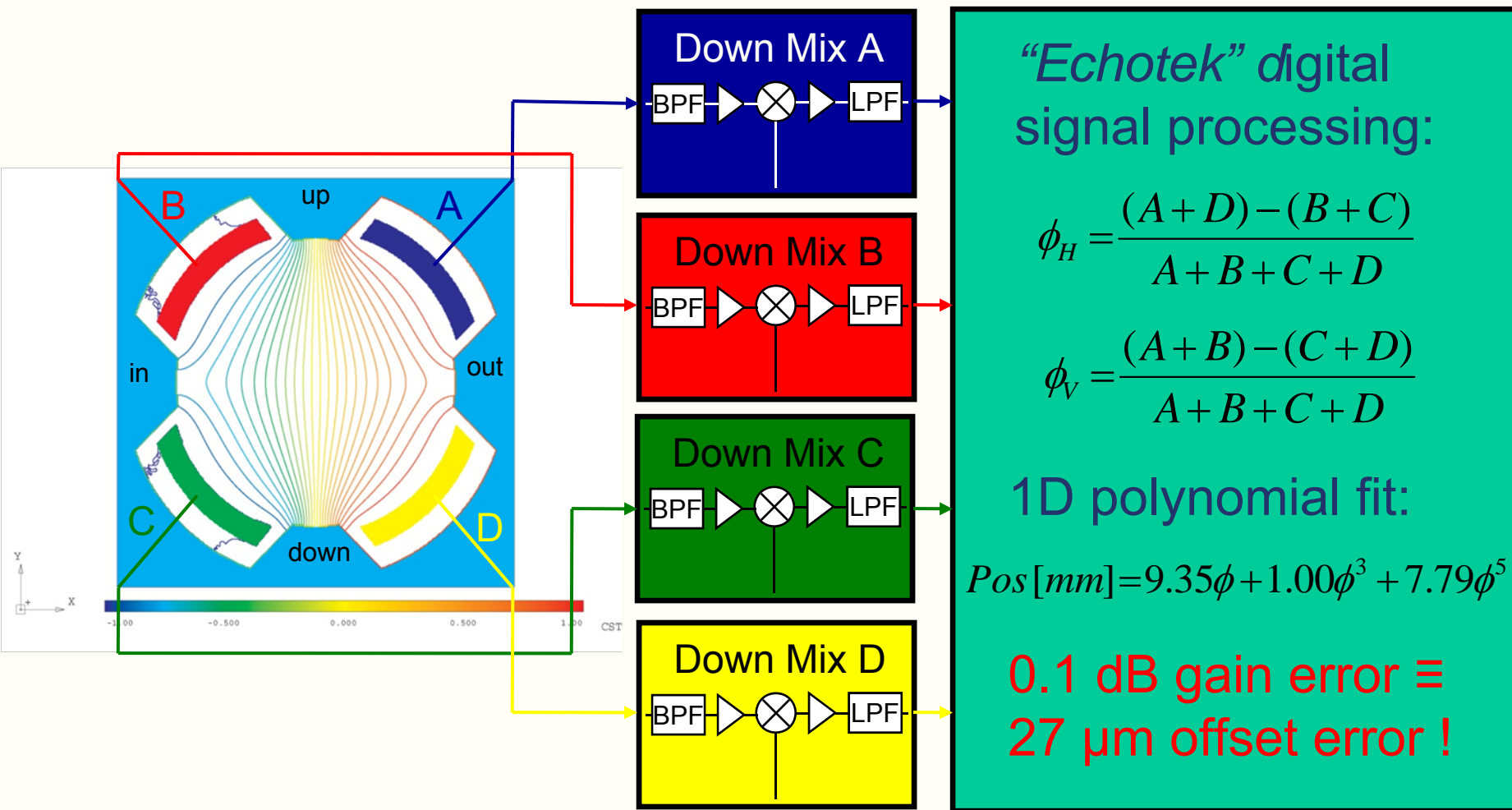


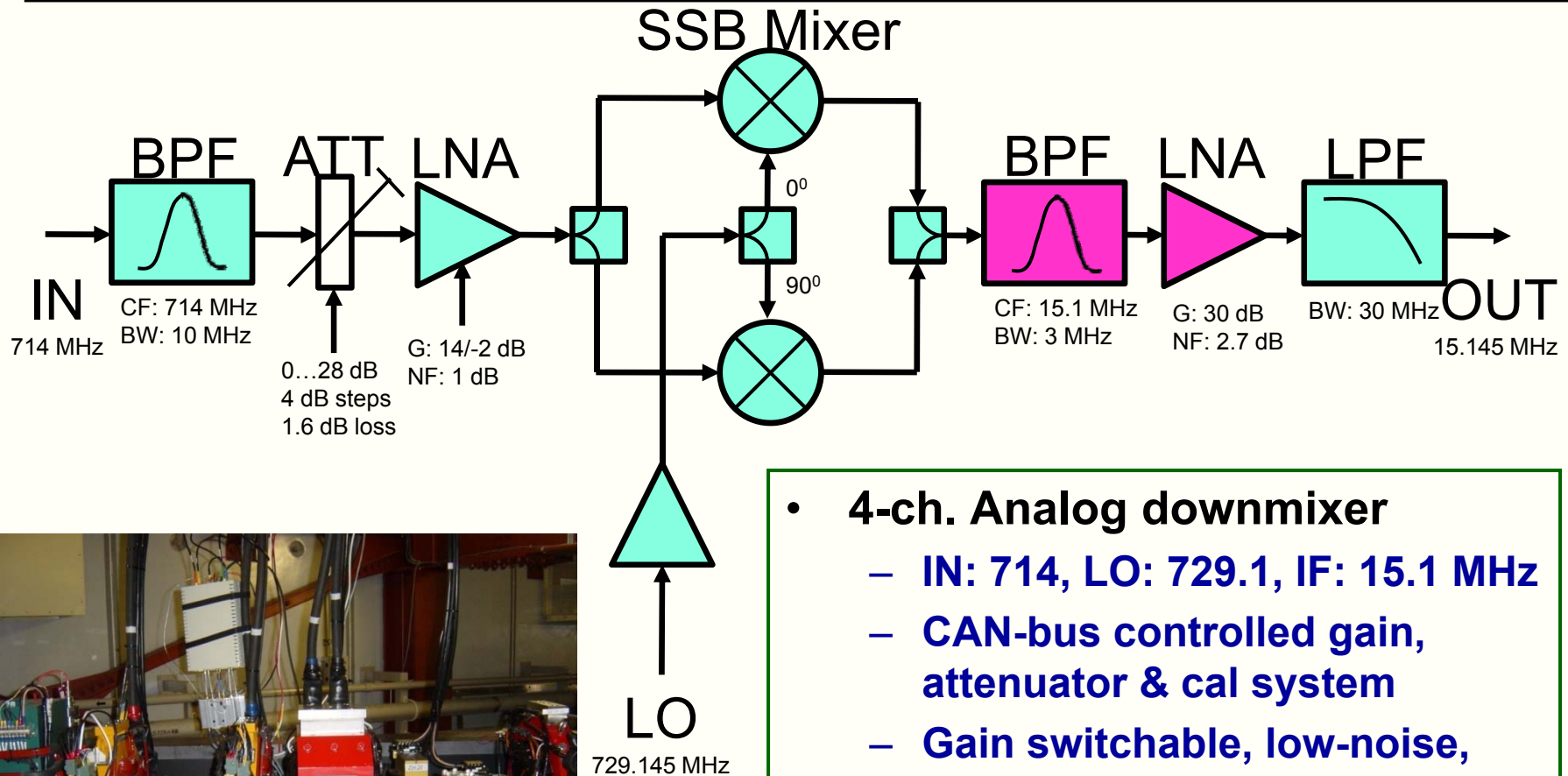
- New read-out hard-, firm- and software, BPM pickups (button-style) stay unchanged.
- Mixed analog/digital signal processing, based on spare *Echotek* digital receiver boards (pragmatic, cost efficient R&D approach):
 - Still modern, but not of latest technology digital downconverters (DDC)
 - Long term experience at Fermilab (p/pbar), spare units available for a cost effective proof of principle. **We may switch to VME digitizers?!**
- BPM system components:
 - 714-to-15.1 MHz analog downmixer (SLAC), with high dynamic range (located in the tunnel), plus remote-control & calibration prototype unit (Fermilab). **Pre-series of improved downmix/cal unit ready for testing!**
 - VME hard- & software:
 - 8-ch. *Echotek* digital receiver (105 Ms/s, 14-bit ADC, 4 ch. *Graychip* DDC)
 - VME timing generator (Fermilab).
 - Motorola 5500 VME controller, running VxWorks & EPICS software





Button:
transfer
impedance



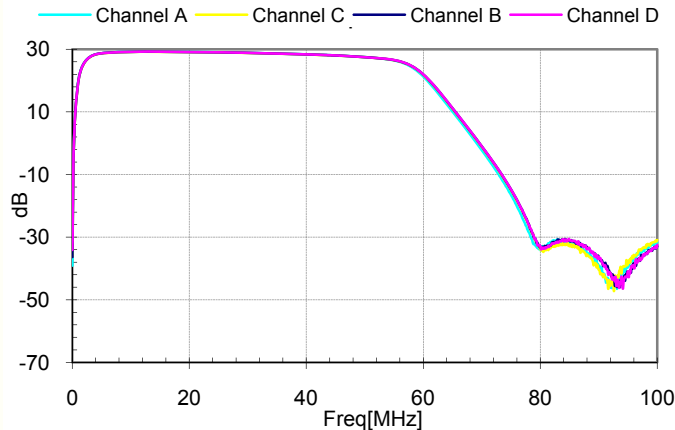


• 4-ch. Analog downmixer

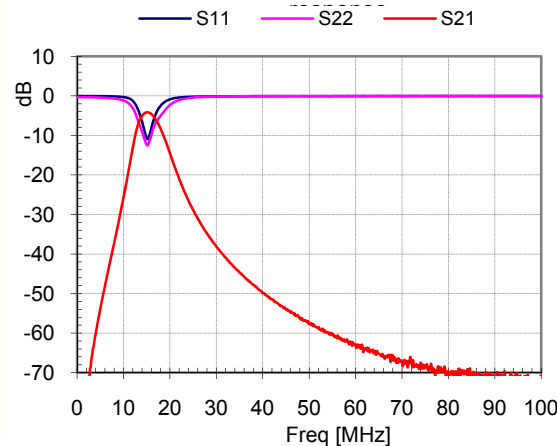
- IN: 714, LO: 729.1, IF: 15.1 MHz
- CAN-bus controlled gain, attenuator & cal system
- Gain switchable, low-noise, high IP3 input gain stage
- Image rejection (SSB) mixer
- 27dB gain, ultralinear IF stage



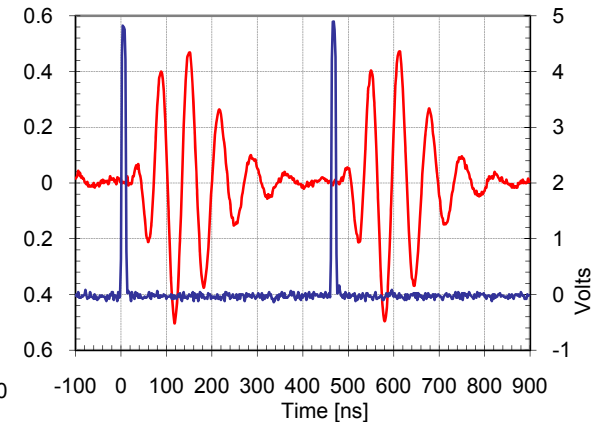
KEK-ATF-09 Downconverter BD IF section



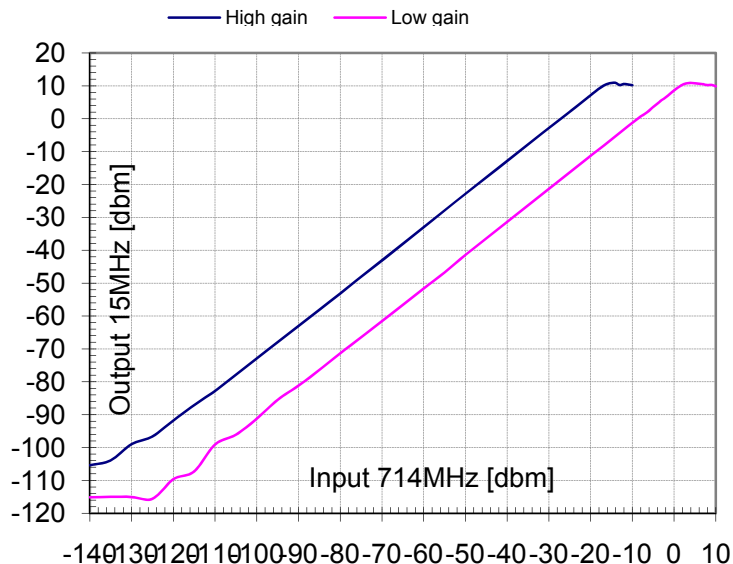
KEK-ATF 15MHz BPF frequency



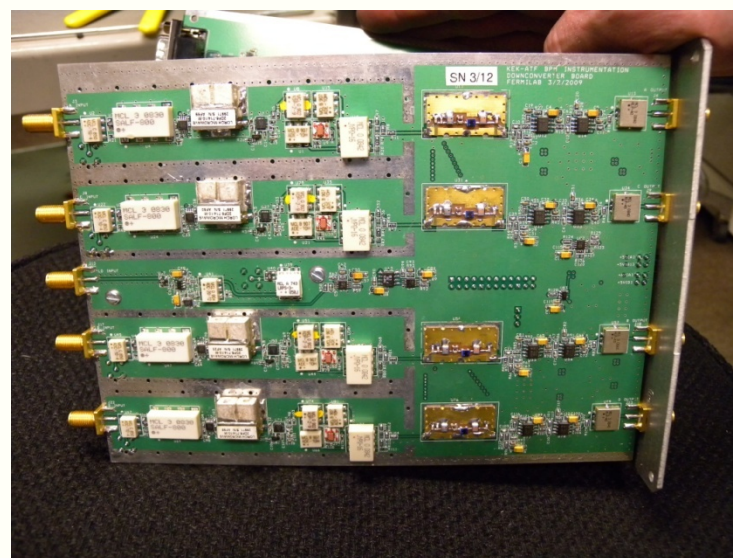
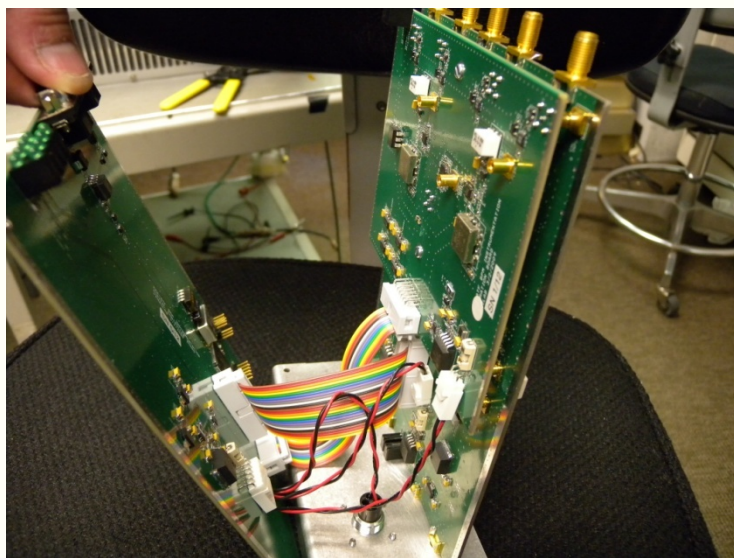
15MHz BPF time response



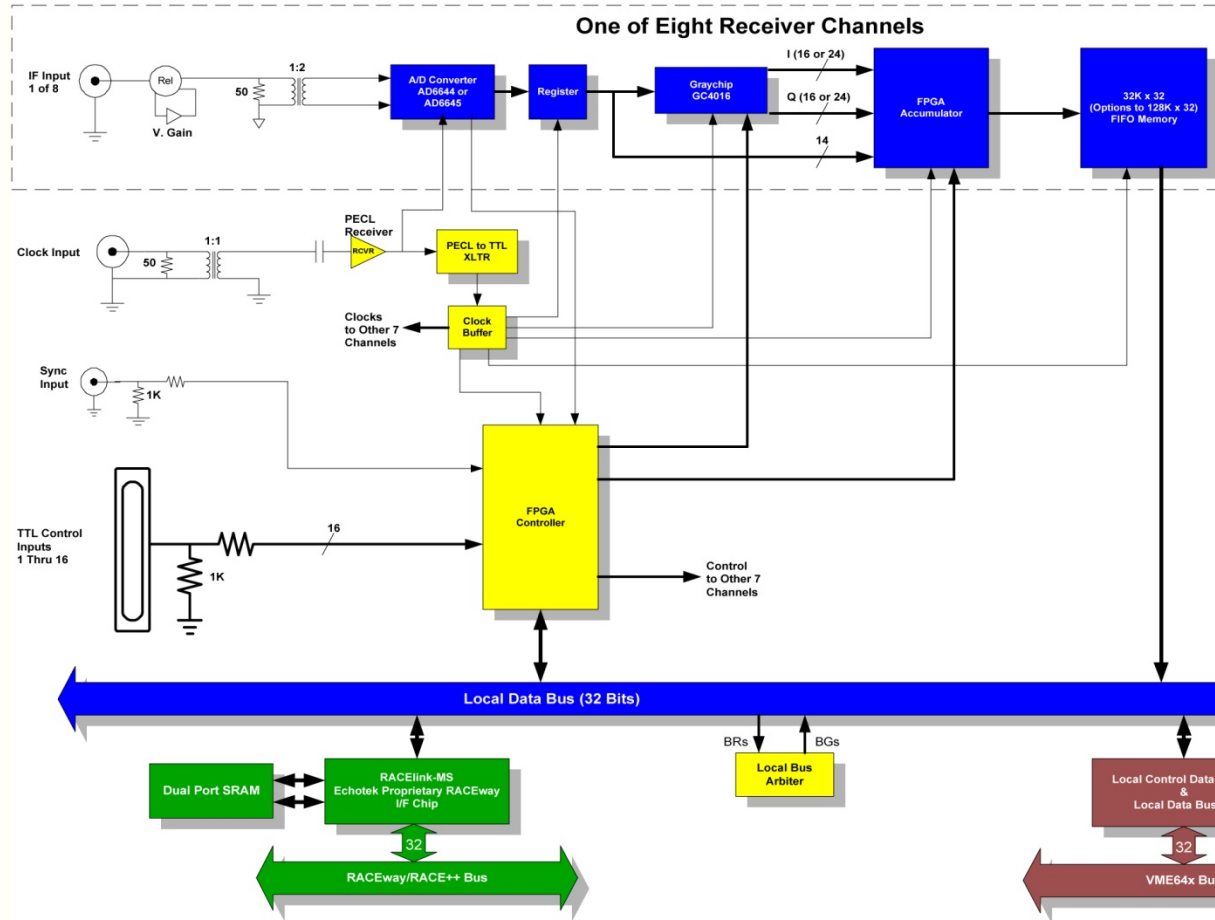
ATF_KEK Downconverter dynamic range test



- **Modified IF section**
 - Low-noise gain stage
 - 15.1 ± 1.5 MHz BPF, ~ 400 ns ring-time
- **Improved NF & dynamic range**
 - NF = 17 dB (?)
 - >90 dB dynamic range

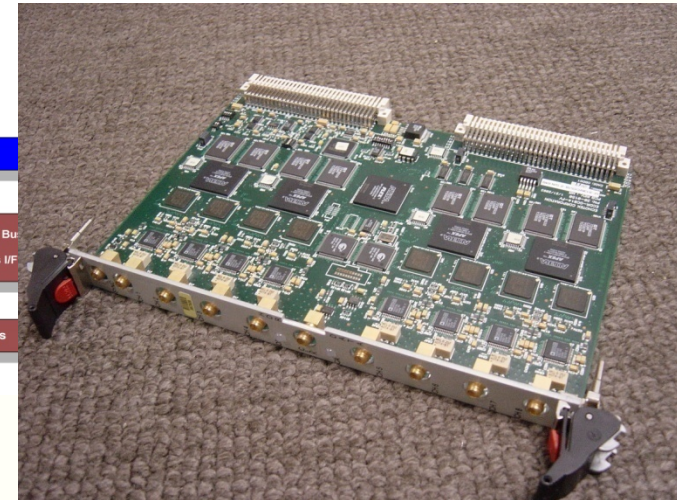


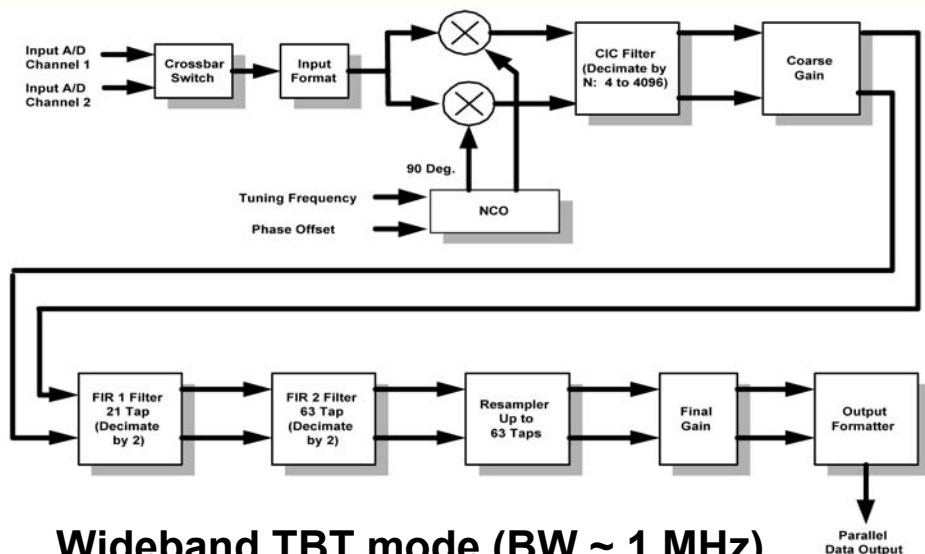
ECDR-GC814 BLOCK DIAGRAM



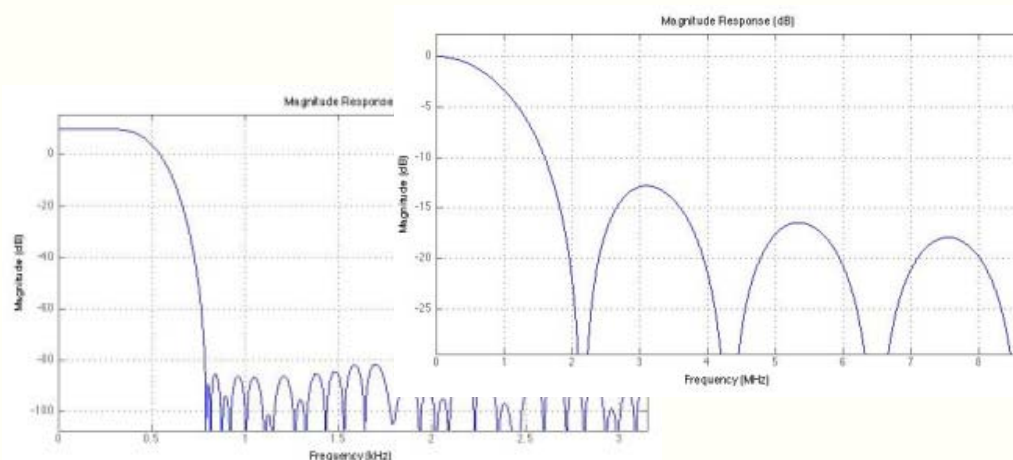
• Echotek digital receiver

- 8-ch VME64x module
- *Analog Devices* 14-bit 105 MS/s AD6645
- Each ADC channel: *Texas Instruments* 4-ch GC4016 “Graychip” digital downconverter
- 128 kWord FIFO





- **Graychip digital downconverter**
 - 4 independent channels per ADC
 - NCO set to $f_{IF} = 15.145$ MHz (downconvert to DC baseband)
 - ADC clock set to 32 samples per revolution: $f_{CLK} = 32 \times f_{rev} = 69.2$ MHz
 - Decimation and filtering for wide- and narrowband mode using CIC and FIR digital filters
 - Simultaneous DDC operation of beam and calibration signals!



NB mode PFIR response

WB CFIR response

- **Wideband TBT mode (BW ~ 1 MHz)**

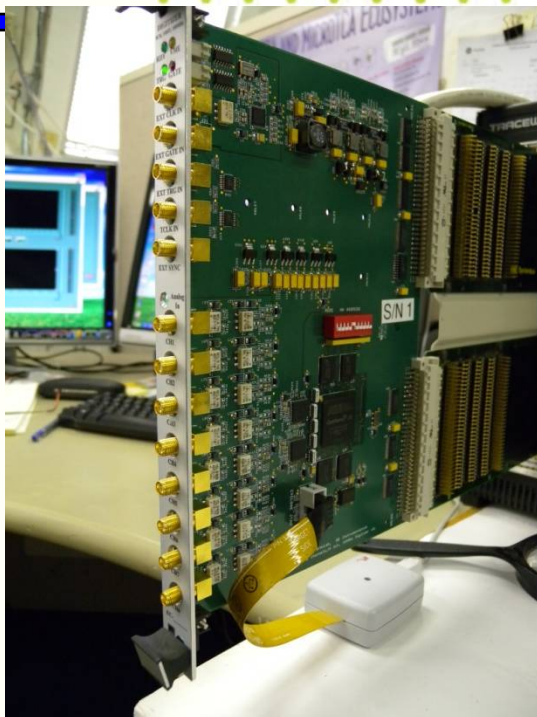
- 5 stage CIC: decimate by 4
- CFIR: 7-tap boxcar, decimate by 2
- PFIR 1-tap, no decimation

- **Narrowband mode (BW ~ 500 Hz),**

$t_{dec} = 158.7 \mu s, 1280$ pt (~200 ms)

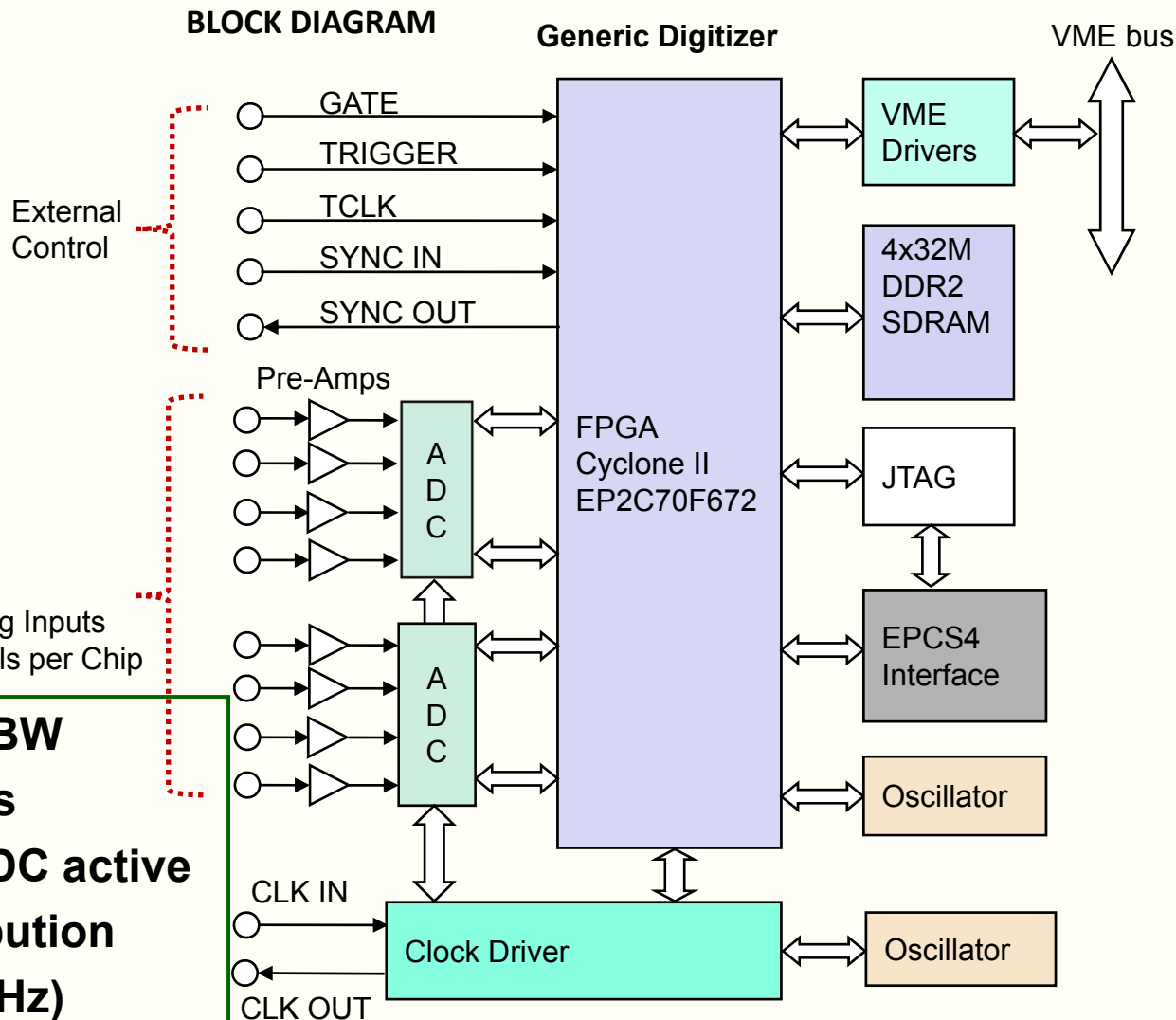
- 5 stage CIC: decimate by 2746
- CFIR: 21-tap RRC, decimate by 2
- PFIR: 63-tap RRC, decimate by 2

iLC 8-Ch, 14-bit, 125 MS/s VME Digitizer

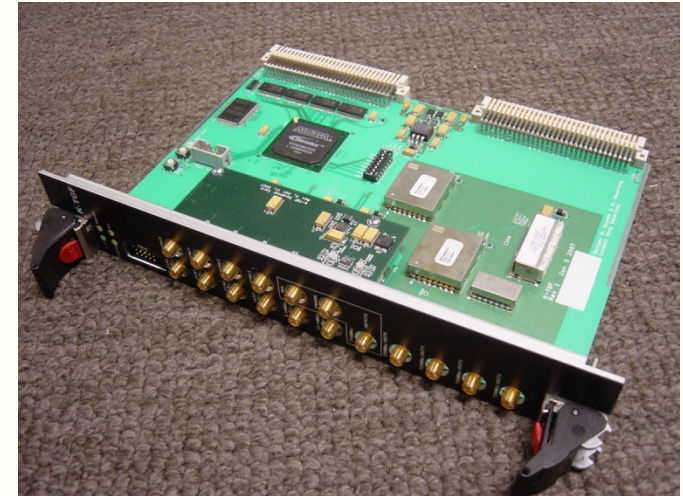


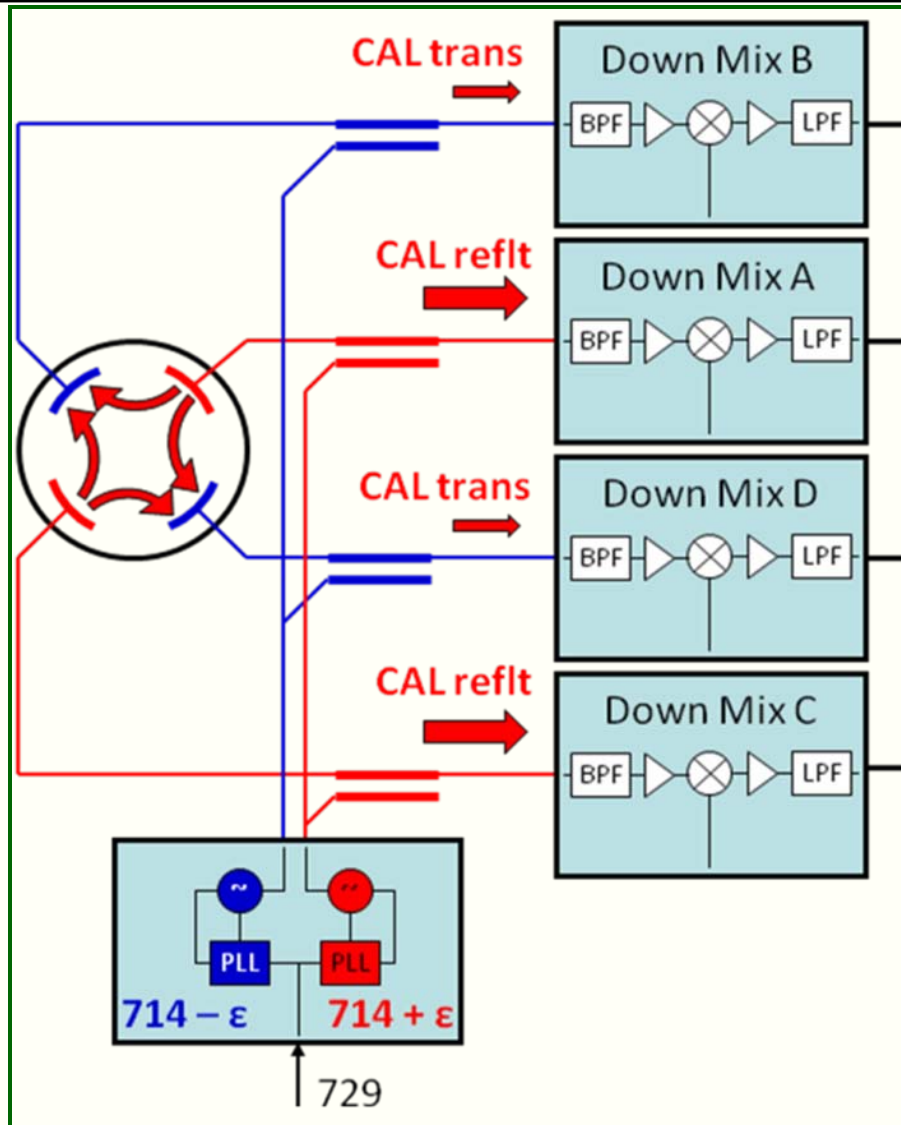
8 Analog Inputs
4 Channels per Chip

- 125 MSPS, 500 MHz BW
- 4-ch serial ADC chips
- 8-ch, AC passive or DC active
- PLL/VCO CLK distribution
- SNR > 72 dB (@50 MHz)



- **VME Timing module:**
 - $f_{\text{CLK}} = f_{\text{RF}} * 32/330 = 69.236$ MHz clock signals (4x)
 - $t_{\text{rev}} = 462.2$ ns turn marker signals (4x), 0...115 double-buckets (2.8 ns) delayable
 - To f_{RF} phase-locked $f_{\text{LO}} = 729.145$ MHz
 - Auxiliary f_{rev} and f_{IF} signals
- **Motorola 5500 VME CPU:**
 - Data collection and normalization
 - Box-car post-processing filter (20 ms)
 - Local diagnostic and control software
 - EPICS control interface
- **Calibration & remote control unit (prototype):**
 - To f_{RF} phase-locked $f_{\text{CAL}} \approx 714$ MHz (*Analog Devices ADF4153*)
 - In-passband, through button-BPM, or reflected signal calibration
 - 2nd and 3rd *Graychip* channels for CAL signal downconversion
 - CAN-bus remote control functions (attenuation, gain, PLL freq., etc.)





- **2 calibration tones:**
 - **714 + ε MHz**
 - **714 - ε MHz**
 - In passband of the downconverter
 - Coupled through the button BPM
 - Alternative: Reflected CAL signal
- **On-line calibration**
 - In presents of beam signals
 - Available only in narrowband mode
 - Using separate *Graychip* channels

- **Calibration tone frequencies:**

- $f_{\text{CALx}} = 713.6 \text{ MHz}$

- $f_{\text{CALy}} = 714.4 \text{ MHz}$

- **Calibration procedure:**

- **Correction values:**

$$A_{\text{Corr}} = \frac{A_{\text{CAL}} + B_{\text{CAL}} + C_{\text{CAL}} + D_{\text{CAL}}}{4A_{\text{CAL}}}$$

$$B_{\text{Corr}} = \frac{A_{\text{CAL}} + B_{\text{CAL}} + C_{\text{CAL}} + D_{\text{CAL}}}{4B_{\text{CAL}}}$$

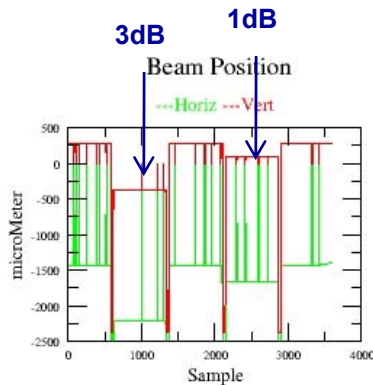
$$C_{\text{Corr}} = \frac{A_{\text{CAL}} + B_{\text{CAL}} + C_{\text{CAL}} + D_{\text{CAL}}}{4C_{\text{CAL}}}$$

$$D_{\text{Corr}} = \frac{A_{\text{CAL}} + B_{\text{CAL}} + C_{\text{CAL}} + D_{\text{CAL}}}{4D_{\text{CAL}}}$$

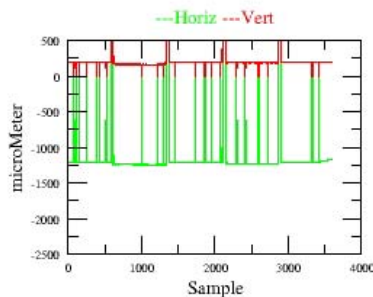
- **Corrected beam positions:**

$$\phi_{\text{Hcorr}} = \frac{(A A_{\text{Corr}} + D D_{\text{Corr}}) - (B B_{\text{Corr}} + C C_{\text{Corr}})}{A A_{\text{Corr}} + B B_{\text{Corr}} + C C_{\text{Corr}} + D D_{\text{Corr}}}$$

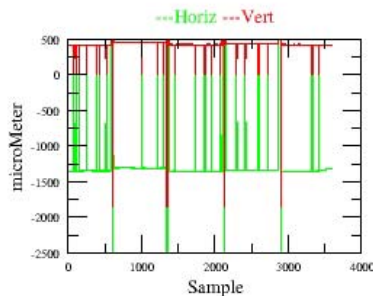
$$\phi_{\text{Vcorr}} = \frac{(A A_{\text{Corr}} + B B_{\text{Corr}}) - (C C_{\text{Corr}} + D D_{\text{Corr}})}{A A_{\text{Corr}} + B B_{\text{Corr}} + C C_{\text{Corr}} + D D_{\text{Corr}}}$$



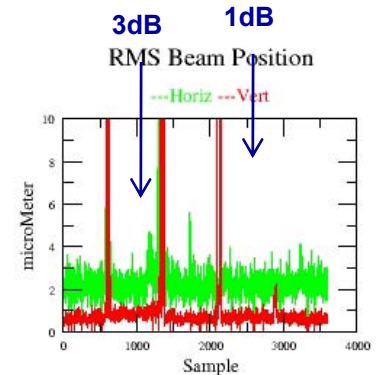
Coupled Position



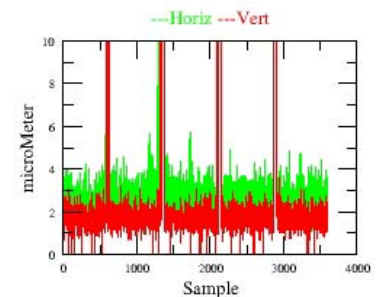
Reflected Position



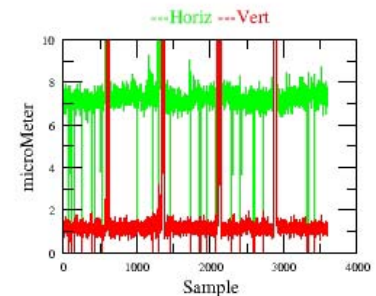
- Calibration on, datalogger on
- Comparing uncorrected, corrected (coupled-through), and corrected (reflected)
- Introduce large 3 & 1 dB gain errors.
- Automatic correction compensates the gain error almost completely!!
- Corrected beam position shows a slight increase of the RMS error (to be further studies!).



RMS Coupled Position

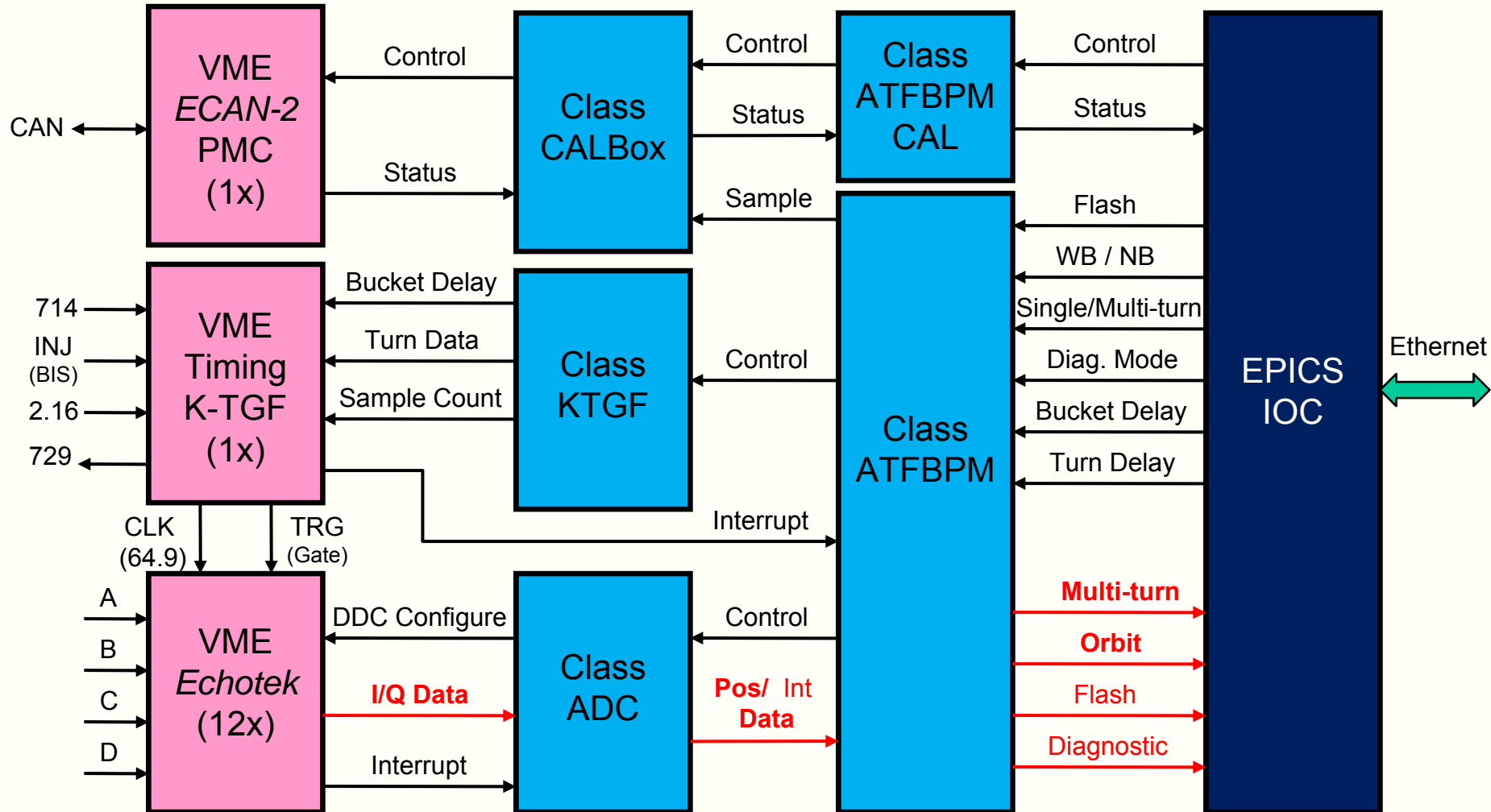


RMS Reflected Position

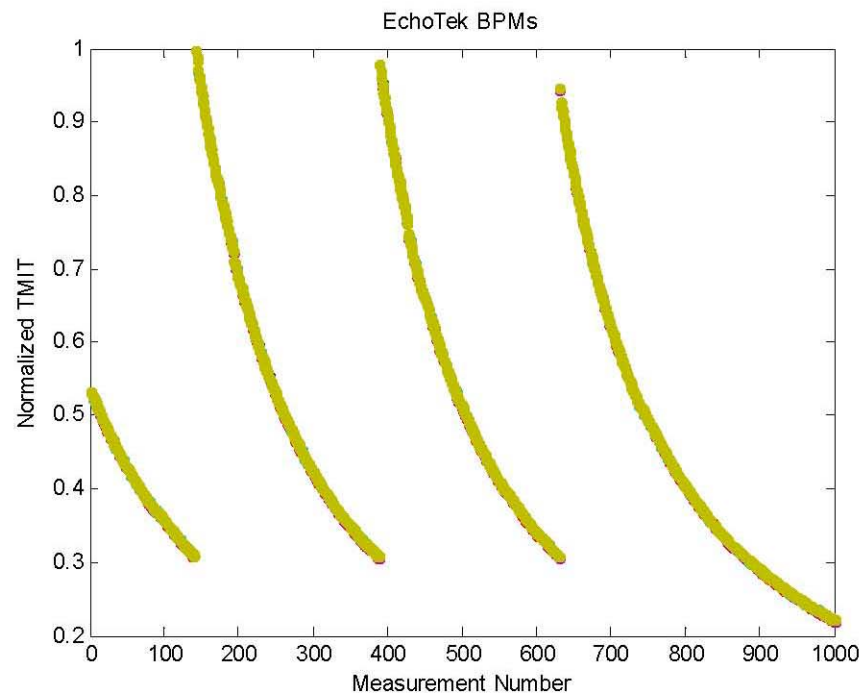
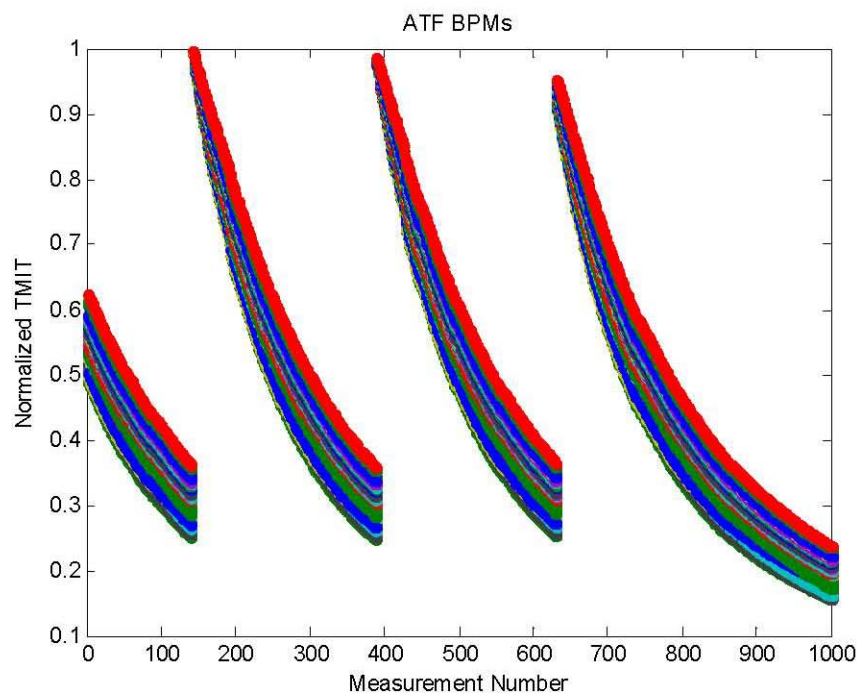


VME Hardware

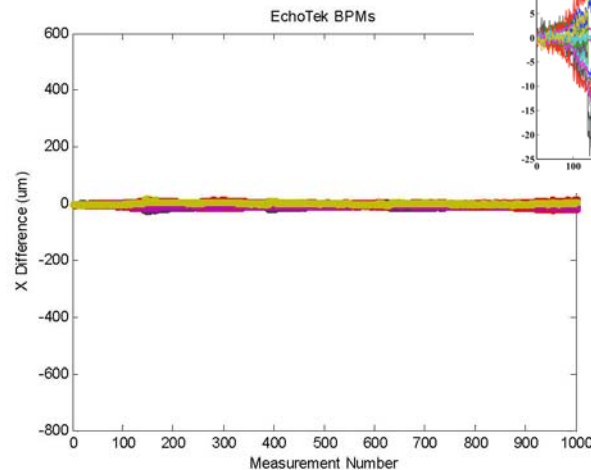
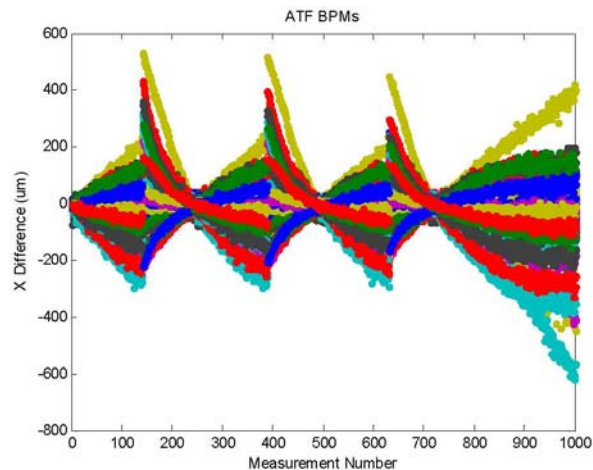
Motorola 5500 μ P Software (VxWorks)



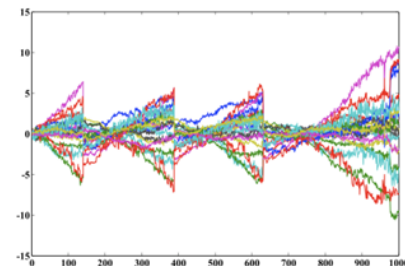
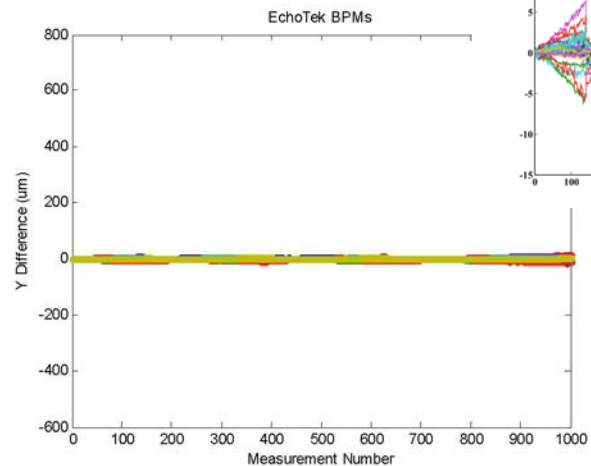
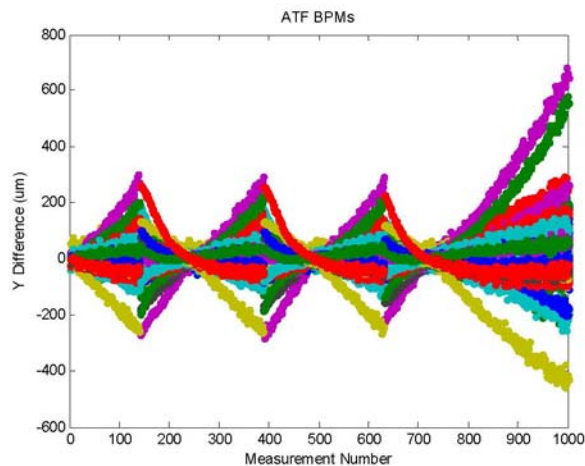
Normalized Intensities



Horizontal Position

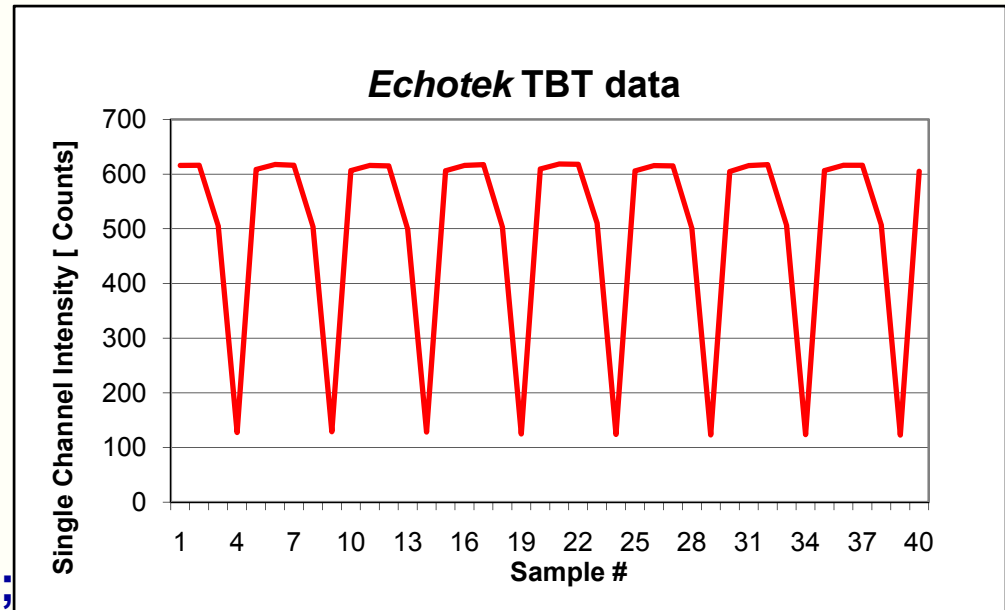
 $\pm 700 \text{ } \mu\text{m}$

 $\pm 25 \text{ } \mu\text{m}$

Vertical Position

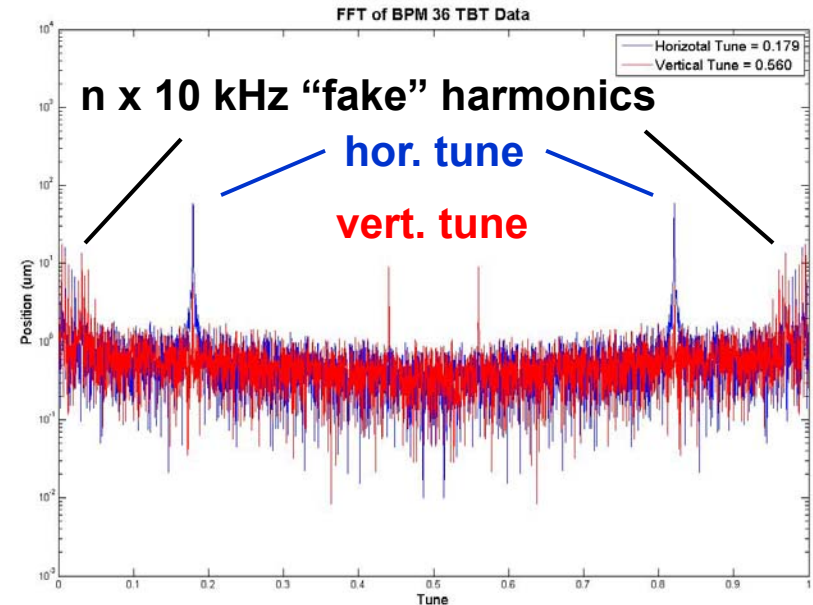
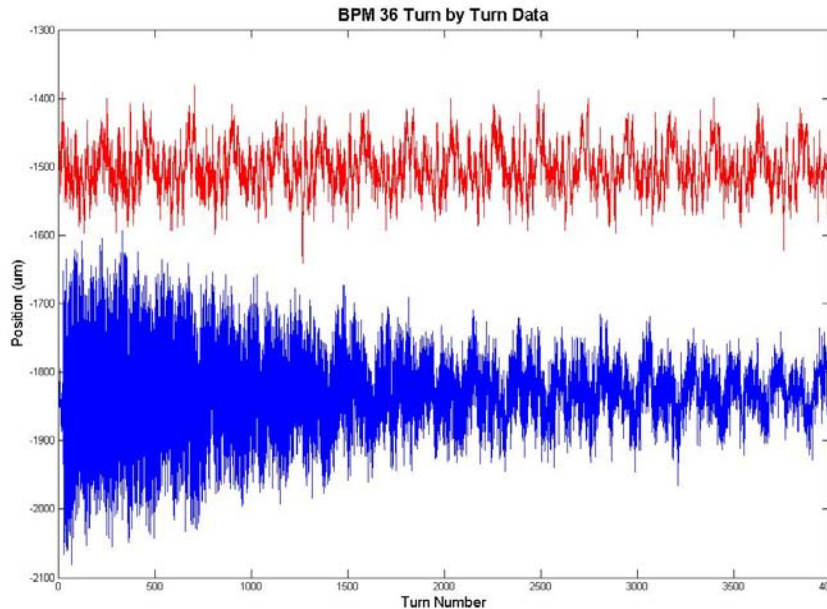
 $\pm 700 \text{ } \mu\text{m}$

 $\pm 15 \text{ } \mu\text{m}$

- Several “issues” had to be resolved:

- CIC & FIR digital filter impulse responses to resolve true turn-by-turn data (no “smearing”)
- Timing issues, e.g. channel-to-channel, as well as between BPMs and “houses” (VME crates); and of course the usual “seam” problem.



- In particular for the kicked beam TBT response tests:
 - Vertical beta at pinger is 0.5 m (12 times smaller than the horizontal one): we had to resort to injection oscillations -> lower resolution.



- Turn-by-Turn data BPM #36 (pinger: On)
- Identifying hor. and vert. tune lines (387 kHz, 1.212 MHz).
- Observed short time, broadband TBT resolution: few μm !
- **Observation of “fake” harmonics at $n \times 10$ kHz (not f_s), due to power supply EMI in the analog downconverter unit!**

- TBT data at the j^{th} BPM following a single kick in the z -plane ($z \equiv x, y$):

$$z_n^j = \frac{1}{2} \sqrt{\beta_z^j} e^{i\Phi_z^j} A_z e^{iQ_z(\theta_j + 2\pi n)} + c.c.$$

– with

$n \equiv$ turn number , $A_z = |A_z| e^{i\delta_z} \equiv$ constant of motion

$\Phi_z \equiv \mu_z - Q_z \theta$ (periodic phase function)

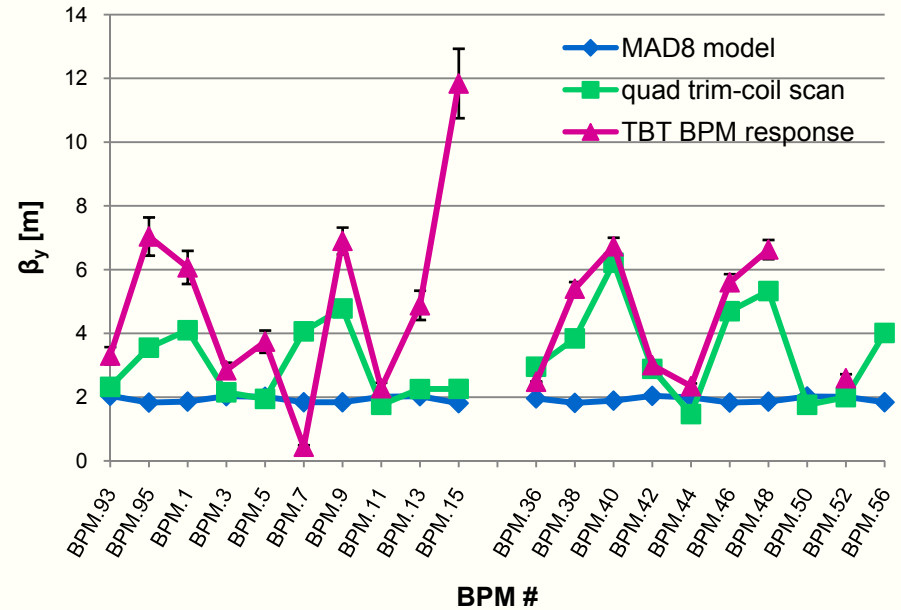
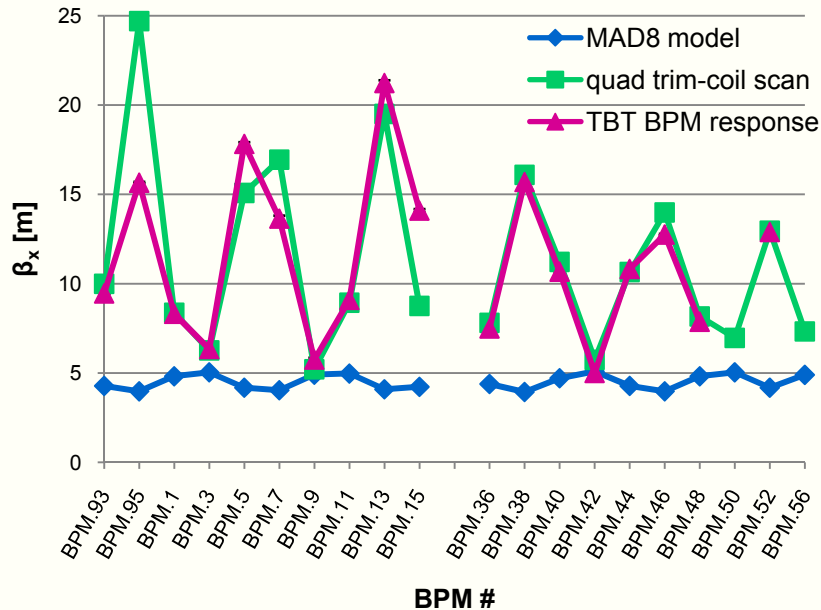
- Twiss functions:

$$\beta_z^j = |Z_j(Q_z)|^2 / |A_z|^2 \quad \mu_z^j = \arg(Z_j) - \delta_z$$

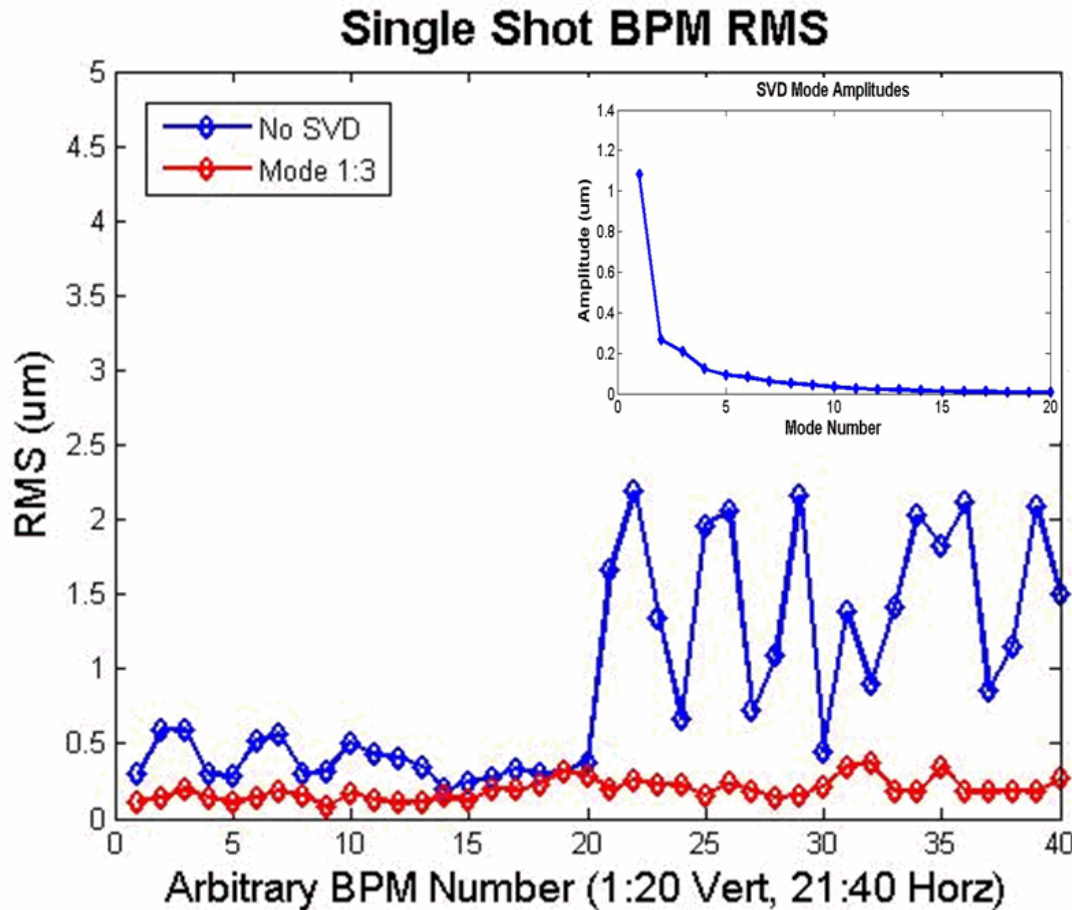
$Z_j(Q_z) \equiv$ Fourier component of z_j

- Amplitude fit:

$$|A_z|^2 = \frac{\sum_j 1/\beta_z^{0j}}{\sum_j 1/|Z_j(Q_z)|^2}$$



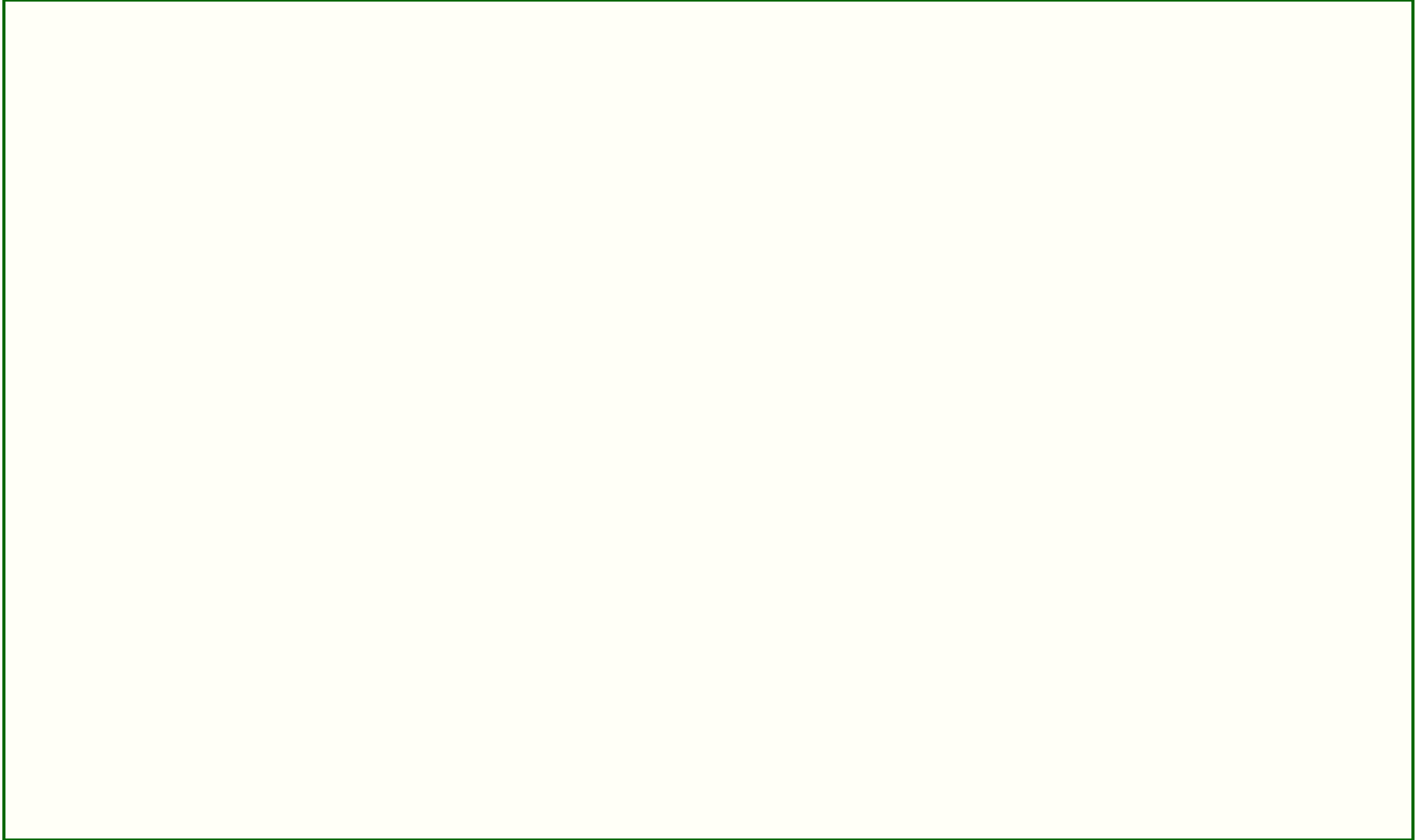
- MAD8 model (M. Woodley, marginal differences wrt. Kuroda SAD model).
- Nearby quadrupole trim coil scan (May 2008).
- TBT Fourier analysis, amplitude by fit to beta measured through trim coil scan (April 2008).



- Triggered at turn #500,000
- ~200 ms position data per shot (1280 narrowband mode BPM measurements).
- 126 tap box car filter to reject 50 Hz:
 - ~ 800 nm resolution
- SVD analysis, removing modes with hor./ vert. correlation:
 - ~200 nm resolution

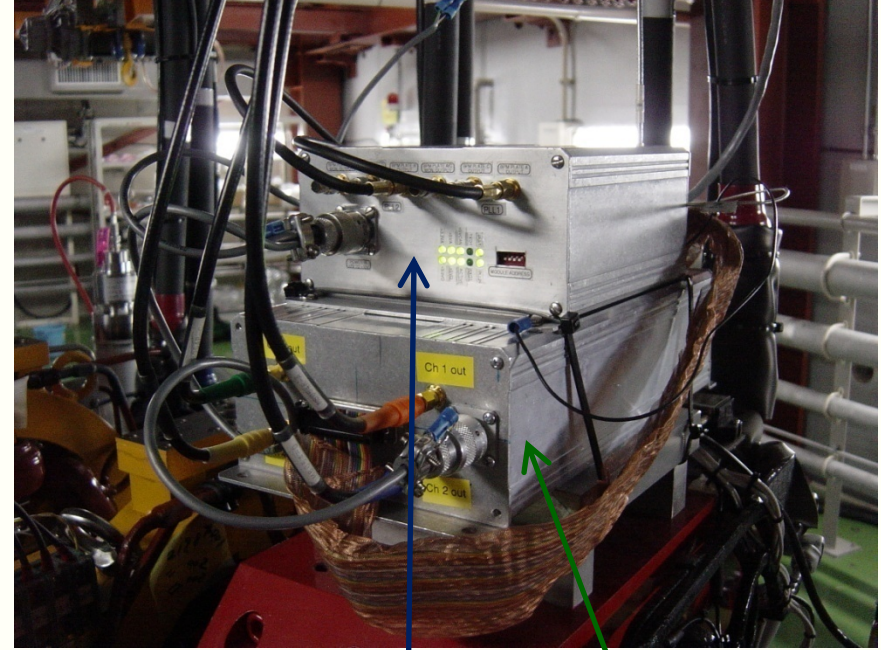
- **“Final” Analog Downmixer with integrated CAL system**
 - April 2009: perform beam tests on a pre-series (6 units)
 - Spring 2009: finalize layout
 - Summer 2009: production, test and burn-in of 110 units
- **VME System**
 - Spring 2009: finalize VME digitizer hardware
 - Summer 2009: establish downconverter & filter firmware
 - Fall 2009: Series production of 55 units
 - Fall 2009: Overhaul of the timing module(s), increase clock frequency to 40 samples / turn, increase # of CLK outputs
 - Winter 2009: finalize timing modules.
- **Software**
 - Integration of VME digitizer (drivers, EPICS interface, etc.)

- A DR BPM read-out system with high resolution in TBT (few μm), and narrowband mode ($<200\text{ nm}$) has been developed.
- An automatic calibration system for gain drift correction was tested. It operates in presence of the beam signal!
 - **Systematic long term studies using the automatic gain correction system need to be accomplished.**
- Soft-/firmware activities & beam studies at ATF could be realized through remote operation!
- TBT kicked beam response studies uncovered discrepancies between theoretical and measured ATF DR optics.
- A revised analog/calibration electronics has been prototyped to resolve problems and limitations of the first series (20-of-96).
 - **To be tested right now!**
- Echotek digital receivers may be replaced by in-house developed VME digitizer modules for the digital signal processing.



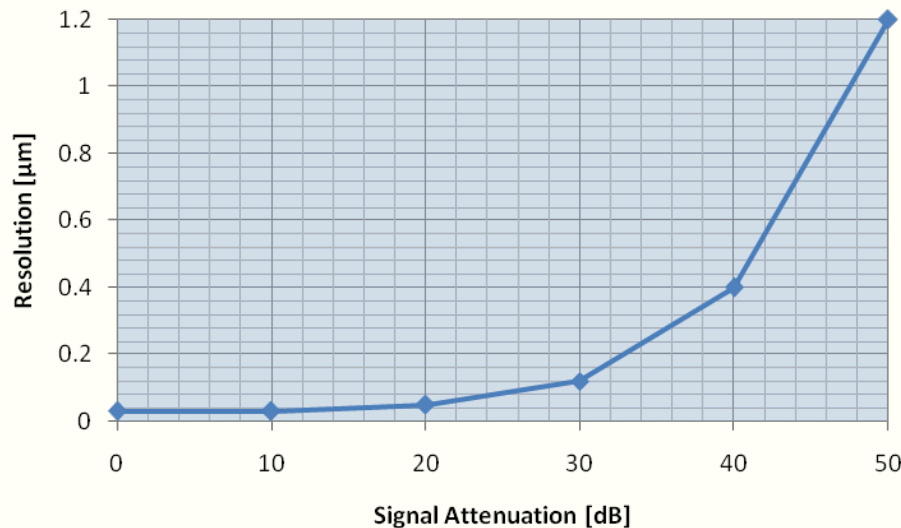


- Mini VME crate accommodating:
 - *Motorola 5500* CPU
 - PMC CAN bus interface *ECAN-2*
 - Timing module TGF
 - *Echotek* digital receiver module



- BPM #54 prototype installation (temporary):
 - CAN bus remote control & CAL signal PLL unit (Fermilab)
 - 4 ch. Downconverter unit (SLAC)

	Multi-turn	Orbit	Flash
Wide-Band	Samples: 4096 Samples/turn: 4 Turns: 1024 POSITION Intensity	Average Samples: 4096 Turns: 1024 POSITION (RMS & StdDev) Intensity (RMS & StdDev)	N th Sample (1) POSITION Intensity
Narrow-Band	Samples: 1280 μ sec/Sample: 158.73 Turns: 439600 POSITION Intensity	Average Samples: 126 (50 Hz Boxcar) Turns: 43273 POSITION (RMS & StdDev) Intensity (RMS & StdDev)	N th Sample (1) POSITION Intensity



Theoretical:

- ADC SNR: 75 dB
- Process gain: 40.4 dB
- NF 1st gain stage: ~ 1 dB
- CAL tone level: -10 dBm
- Splitter attenuation: 6 dB
- Effective gain: ~ 100 dB
- BPM sensitivity: 240 $\mu\text{m}/\text{dB}$
- Calculated equivalent resolution: ~ 20 nm

**CAL tone resolution measurement
on BPM #56: ~ 30 nm(!) equiv. resolution
(no beam operation at ATF!, magnets off)**