



Notes for ILD Beam Pipe (Technical Aspect)

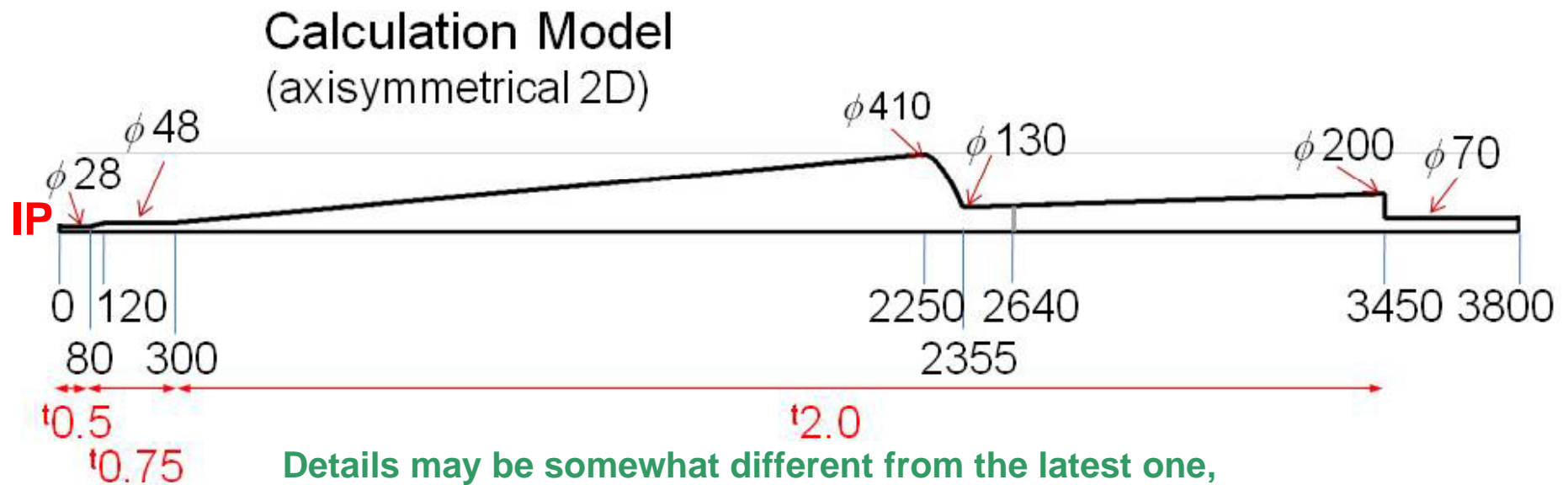
Y. Suetsugu, KEK

- Parasitic loss
- Vacuum pressure profile
- Some comments for beam pipe



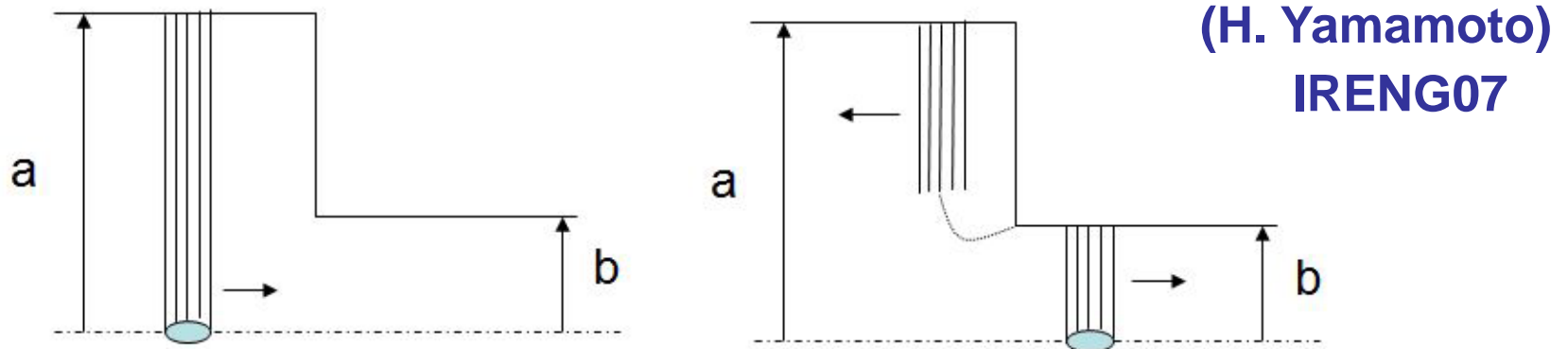
Introduction

- Here presented are some calculations and brief notes on
 - **Parasitic loss**
 - **Vacuum pressure profile**for the beryllium ILD beam pipe.



1. Parasitic loss

- Any steps in a beam pipe result in the energy loss of passing bunches.



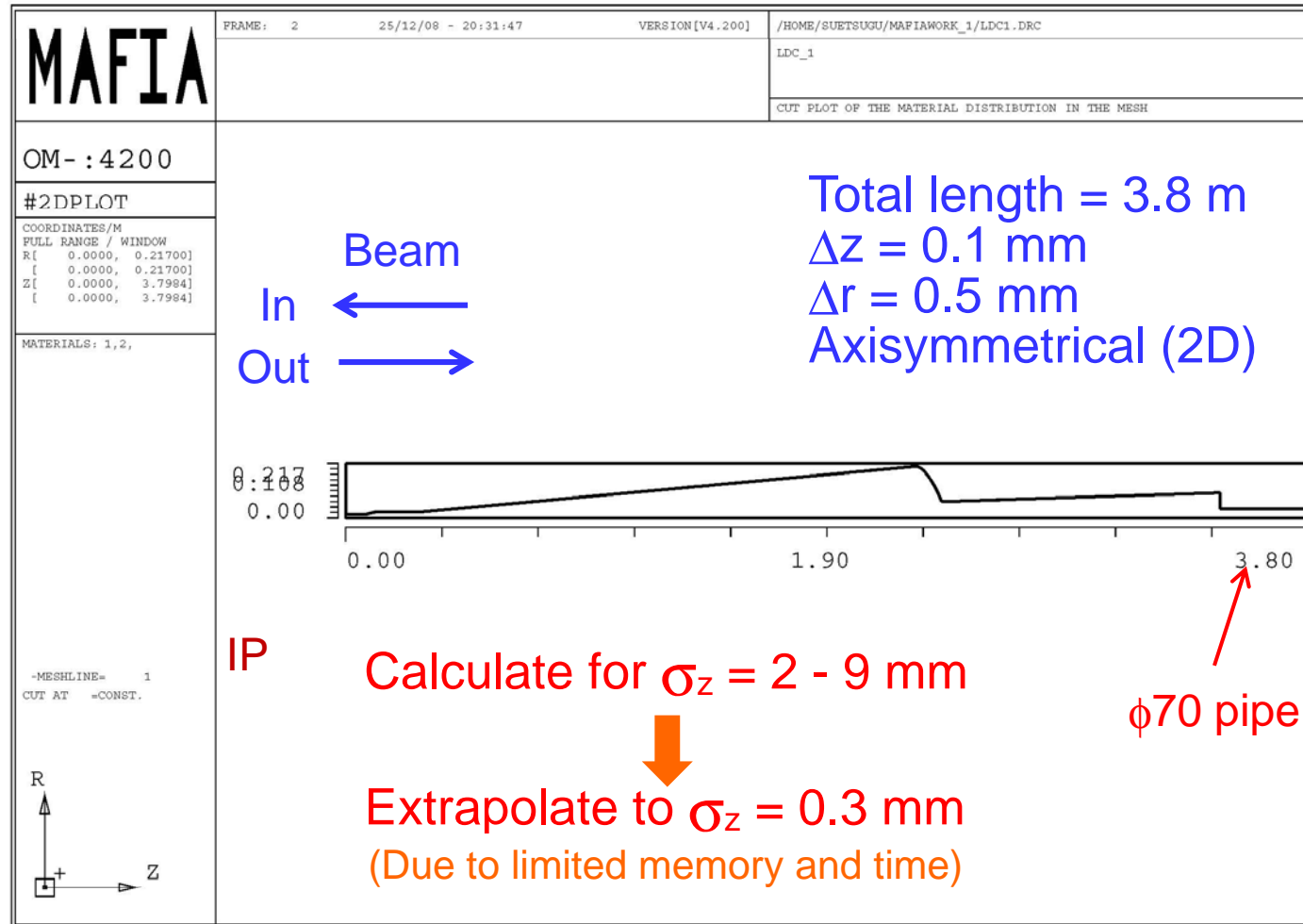
Ex. EM energy bounced back = HOM loss (Parasitic loss)

- Parasitic loss: P
 - $P = k \times q \times I$
 - k : loss factor, q : charge and I : beam current



1. Parasitic loss

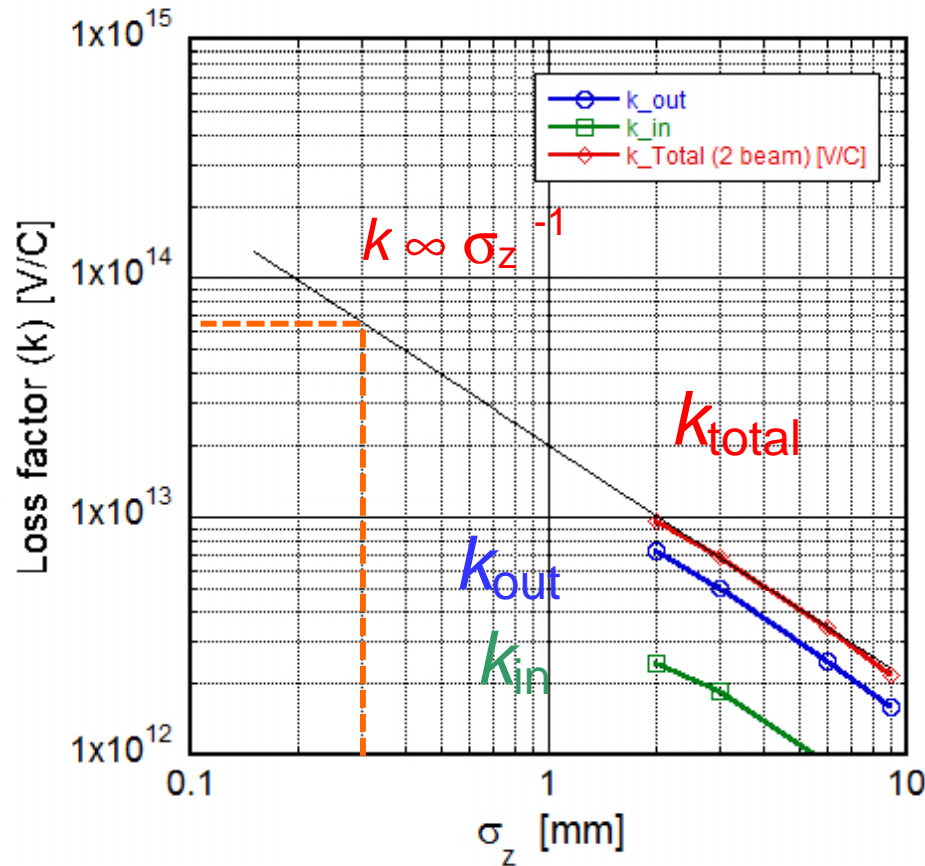
- Calculation of the loss factor (k) using MAFIA





1. Parasitic loss

- Results



k_{total} (two beams) $6 \sim 7 \times 10^{13}$ V/C
@ $\sigma_z = 0.3$ mm

If $q = 3.2$ nC, $N_b = 6600$ bunch,
and $f_r = 5$ Hz : $I = 8.6 \times 10^{-5}$ A
(Low P option)

$\therefore P = kql = 20 \sim 24$ W (one side)

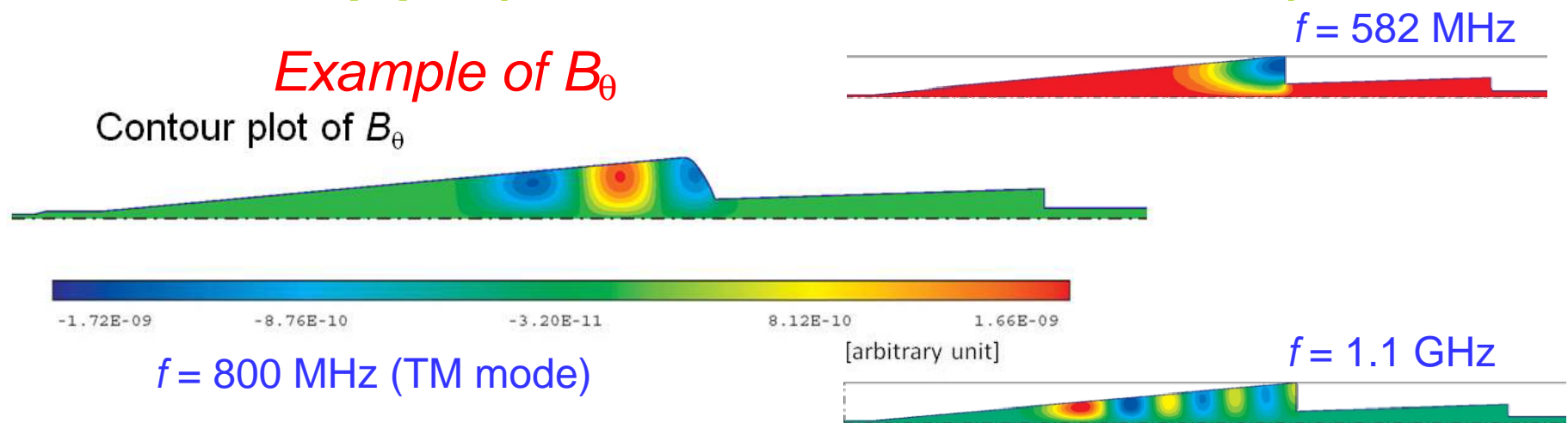
Same to that presented
in TILC08

k_{in} and k_{out} is different, since the
apertures at both ends are different.



1. Parasitic loss

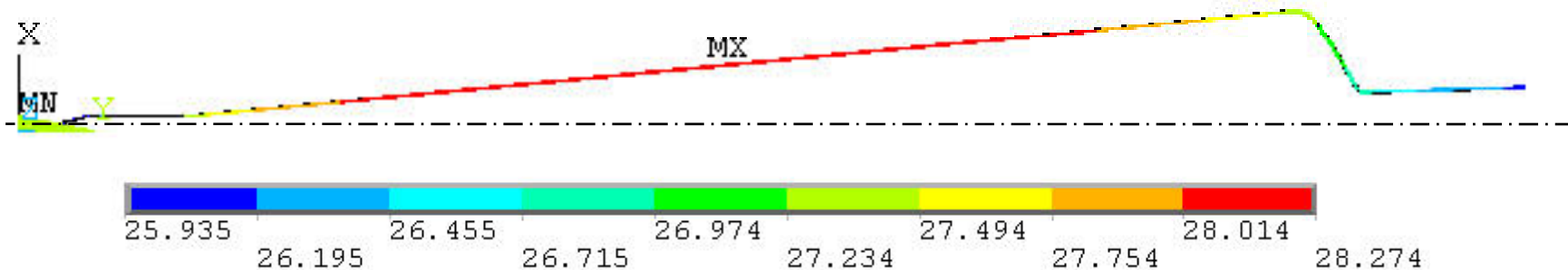
- Dissipation of power
 - **ILD Beam Pipe** : a cavity structure
 - **Some low frequency modes are trapped in the beam pipe.** (~10 %?, S. Pei et al., IRENG07)



The power will be dissipated at the big cone section.

1. Parasitic loss

- Expected temperature
 - Assumption: Cooling by natural laminar air flow
 - $\alpha = 5 \text{ Wm}^{-2}\text{K}^{-1}$, λ (beryllium) = $210 \text{ Wm}^{-1}\text{K}^{-1}$, $25 \text{ }^\circ\text{C}$
 - All Power is dissipated in the big cone part, $P = 17 \text{ Wm}^{-2}$
(Area = 1.4 m^2)



Temperature rise $\sim 3 \text{ }^\circ\text{C}$.
 No cooling water. Air blow will be sufficient.



2. Vacuum pressure profile

- In order to evaluate the vacuum pressure profile,
 - **Gas desorption rate of beryllium**
 - **Pumping speed**
 - **Required pressure**are required.

- For the gas desorption rate, however, we have no value for beryllium at present.
 - **The values without baking, since a baking (150~200 °C) is hardly possible.**
 - **After a proper surface cleaning.**



2. Vacuum pressure profile

- Here used are the data for **aluminum**, as the first approximation.

- **Thermal gas desorption rate without baking:**

- After **10 hours** evacuation:

CO: $2 \times 10^{-7} \text{ Pa m}^3\text{s}^{-1}\text{m}^{-2}$ ($\sim 2 \times 10^{-10} \text{ Torr / s}^{-1}\text{cm}^{-2}$)

H₂: $2 \times 10^{-6} \text{ Pa m}^3\text{s}^{-1}\text{m}^{-2}$ ($\sim 2 \times 10^{-9} \text{ Torr / s}^{-1}\text{cm}^{-2}$)

- After **100 hours** evacuation (after 4 days)

CO: $2 \times 10^{-8} \text{ Pa m}^3\text{s}^{-1}\text{m}^{-2}$ ($\sim 2 \times 10^{-11} \text{ Torr / s}^{-1}\text{cm}^{-2}$)

H₂: $2 \times 10^{-7} \text{ Pa m}^3\text{s}^{-1}\text{m}^{-2}$ ($\sim 2 \times 10^{-10} \text{ Torr / s}^{-1}\text{cm}^{-2}$)

- About 20 times larger than those after baking (O. Malyshev, IRENG07)

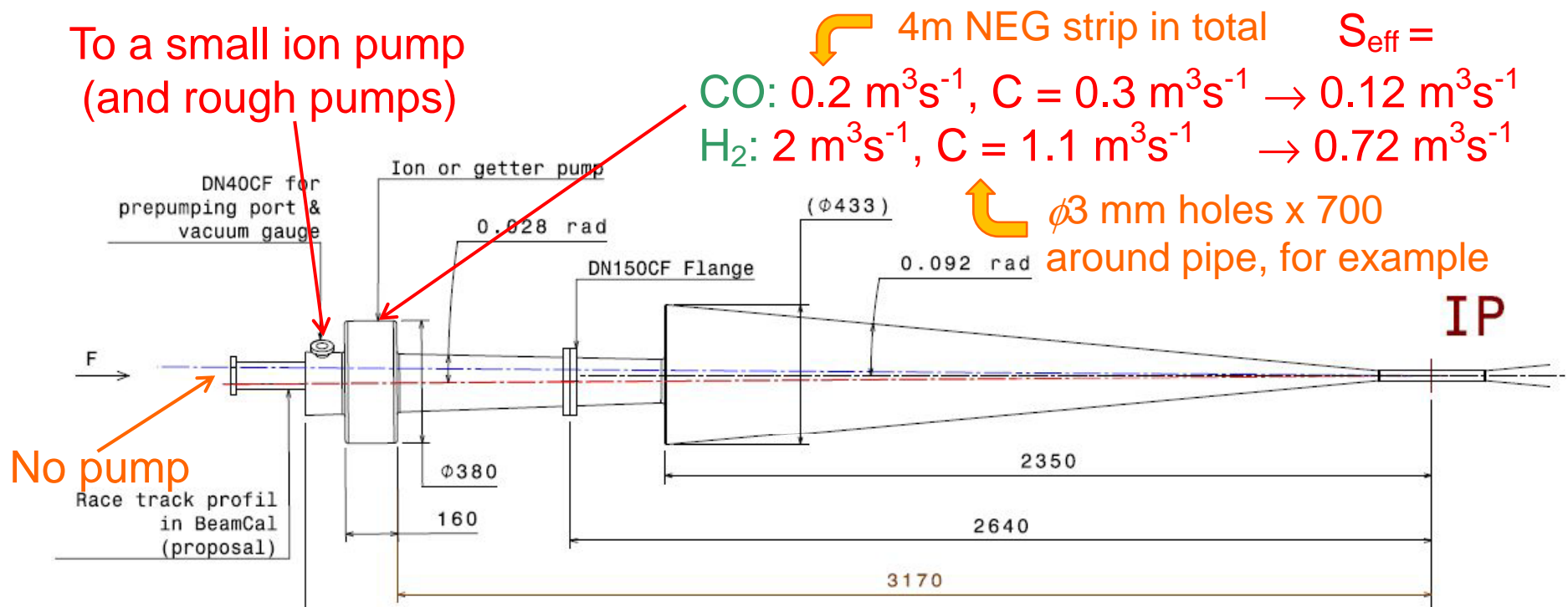
- **Uniform gas desorption in the beam pipe**



2. Vacuum pressure profile

- Pumps

- **NEG strip (ST707[SAES Getters]), or Cylindrical sputter ion pump**
- **Aligned at the circumference of pipe**





2. Vacuum pressure profile

- Required pressure (in IRENG07)

Conclusions

1. At 10 nTorr within the IP region there are 0.02–0.04 hits/bunch (3-6 hits TPC) at an average energy of about 100 GeV/hit originating inside 200 m from the IP. Some of these cause intolerable background in the vertex detector, so to reduce this background to less than 1% per bunch crossing, the pressure specification inside 200 m from the IP is 1 nTorr.
2. At 10 nTorr, on the FD protection collimator 13 m from the IP, there are 0.21 charged hits (33 hits TPC) at an average charged energy of about 240 GeV/hit and 0.06 photon hits/bunch (9 hits TPC) at an average photon energy of about 50 GeV/hit originating inside 800 m from the IP. This leads to a conservative pressure specification of 10 nTorr in the BDS from 200 to 800 m.
3. From a particle background standpoint, within the IP region between the QD0 quadrupoles, the pressure can be greater than 1 nTorr since luminosity backgrounds will be dominant in this region.

$P \geq 1 \times 10^{-7}$ Pa is OK.

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But, what is the upper limit?

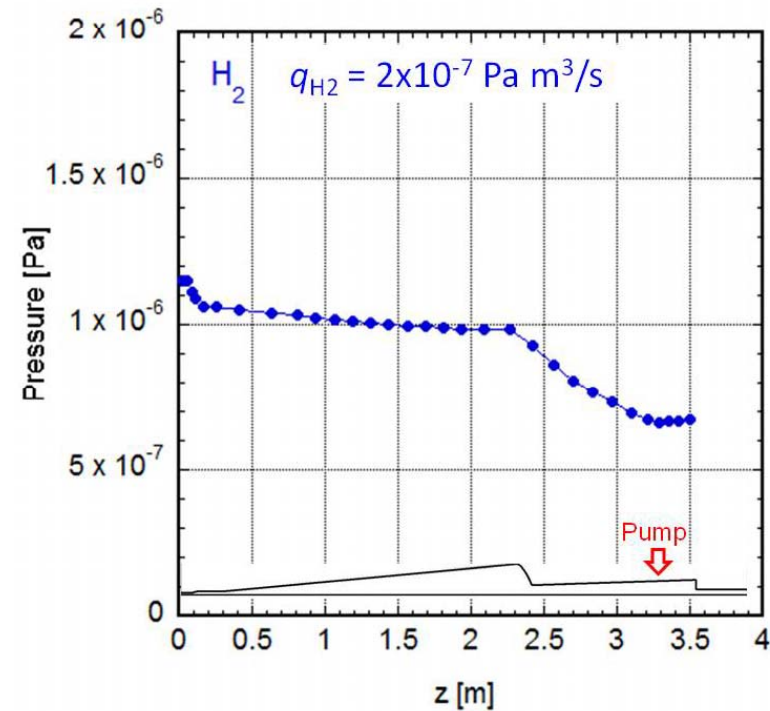
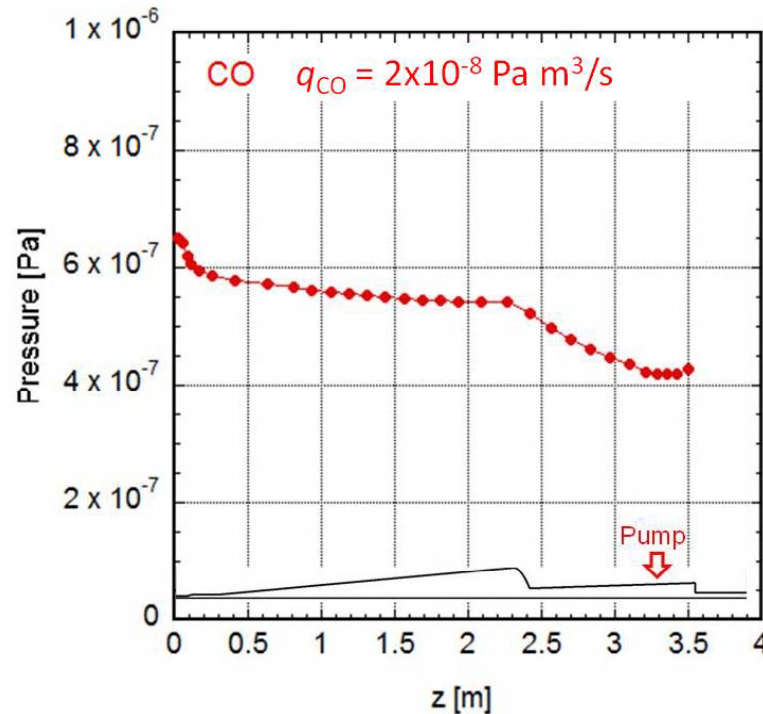
(L. Keller)

(1 nTorr = 1×10^{-7} Pa)



2. Vacuum pressure profile

- Results



$P \sim 1 \times 10^{-6}$ Pa for H₂. Is it OK?

To achieve $P \sim 10^{-7}$ Pa, lower gas desorption rate and/or higher pumping speed are required.



3. Notes on beryllium beam pipe

- Vacuum pressure:
 - In order to evaluate the vacuum pressure more practically, a measurement of thermal gas desorption rate from beryllium is required.
 - Experiments to measure it using a test chamber is necessary.
 - Residual gas
 - How about a baking with low temperature?.
 - Surface treatment
 - New pumping port should be prepared at the big cone region depending on the result.
 - It also depends on the upper limit of the pressure.
 - Checking of other sources of the gas desorption, such as photons, electrons and ions may be necessary



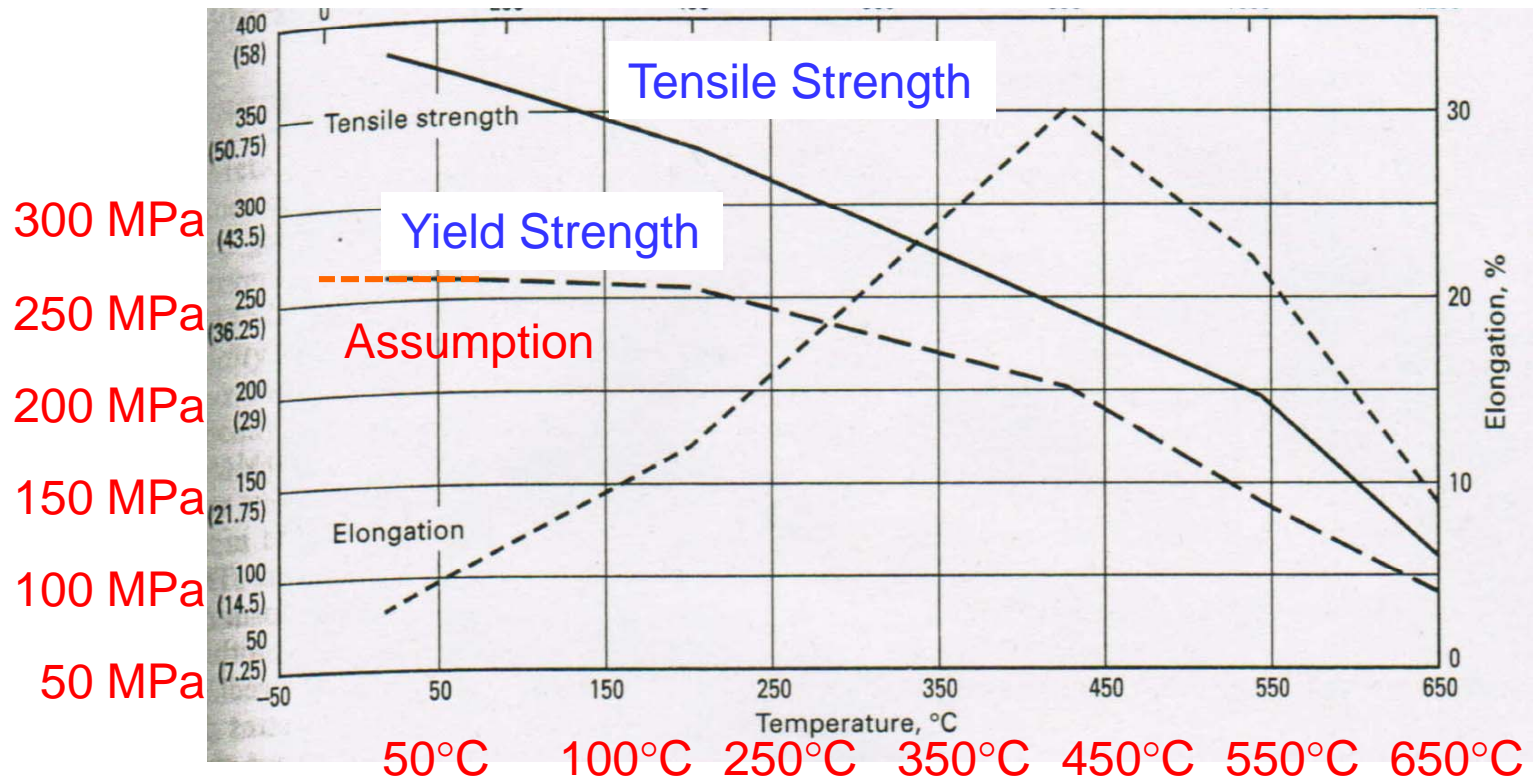
3. Notes on beryllium beam pipe

- Mechanical properties
 - Beryllium may be the best material for IP pipe.
 - However, note that beryllium oxide has a high toxicity, especially to the lung, as is well known.
 - Welding of beryllium by TiG or electron beam (EB) is usually avoided, and the vacuum brazing has been widely used.
 - Even if TiG or EB was used, the thermal conductivity of beryllium is high, only a half of Cu, and the melting point is high, 1280°C. So, **some portion of beryllium will be heated up during the welding.**
 - Thus the beam pipe is likely to experience a high temperature, 800–900 °C, during the brazing or welding process (although restricted range).



3. Notes on beryllium beam pipe

- Beryllium pipe can be annealed, and the mechanical strength will weaken.
- **Structural analysis should take it into account.**





3. Notes on beryllium beam pipe

- Manufacturing of beryllium pipe
 - **The method of joining beryllium should be considered carefully.**
 - Any measures to enforce the structural strength will be required if vacuum brazing is adopted.
 - **The cutting and welding of beryllium requires careful consideration. The manufacturer that can treat beryllium should be limited. → Cost.**
 - **Don't we need bellows near to the collision point?**
 - Small bellows is enough to avoid mechanical shock to IP



Summary

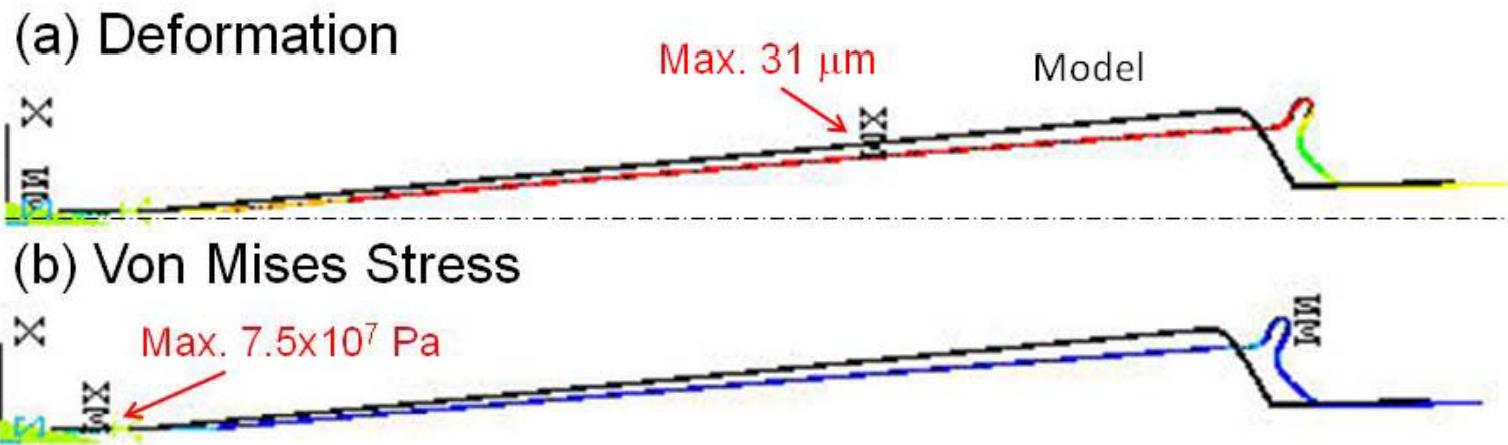
- Parasitic loss and vacuum pressure profile was estimated for the present beryllium beam pipe.
- Power loss is 20-24 W, and not so large.
- Many ambiguity are in the vacuum pressure evaluation.
- Measurement using a test chamber is highly required.
- Structural strength should be evaluated considering the thermal history and welding methods.



Ref: Structural strength

- Deformation and stress: only for double check
 - Studied in detail by M. Anduze et al., including buckling.
 - Material: **Beryllium**
 - Load: Atmospheric pressure (1.013×10^5 Pa)

Total length = 3.8 m
 $E = 7.056 \times 10^{10}$ N/m²
 $\nu = 0.3$
Axisymmetrical (2D)



Similar results were obtained for the deformation and stress.
Reinforcement by discs seems good if more thin wall is required.