

Summary

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- . The magnet main parameters have been fixed during the Cambridge meeting last September

- . Since that time, the design of both the coil and the yoke has been refined to cope with these parameters, and with the integration of the magnet within the detector

- . As ILD magnet parameters are roughly the same as for CMS magnet, the ILD magnet concept is based on CMS magnet one, with two extra requests:

- . High integral field homogeneity in the TPC volume
- . Lower fringing field (push-pull operation)

- . The ILD-V5 version presented today is also that one for the Lol

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Cambridge meeting decisions

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- The main parameters for the ILD detector magnet have been fixed at the ILD Cambridge meeting of last September:

- . Central field = 3.5 T for operation
4.0 T for design

- . R_{int} cryostat = 3.44 m

- . L coil = 7.35 m

- . $B_{\text{ext}} \leq 50$ G @ $R=15$ m in the radial direction (push-pull operation)

- . Integral of field homogeneity within the TPC volume ≤ 10 mm

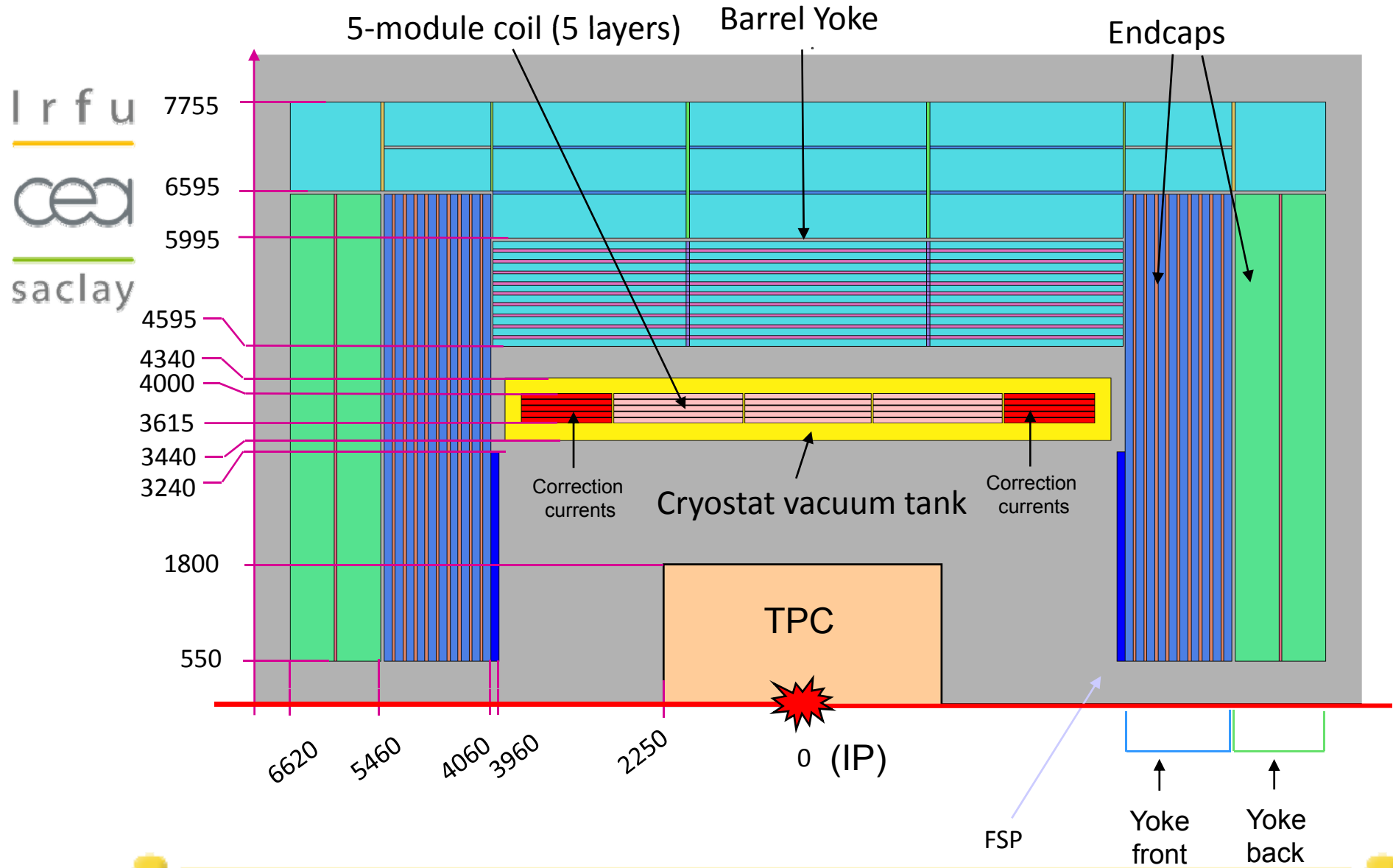
- . Addition of a anti-DiD (Dipole in Detector) within the magnet structure

Version ILD-V5 : generalities



- Magnet = Coil + iron yoke (barrel + end-caps)
- Coil
 - 5 modules (2 different lengths)
 - 5 layers in each module (one layer added from the previous versions)
 - correction current in some parts of the coil to adjust the field homogeneity
- Yoke configuration:
 - as described by Uwe in his previous talk
- For all cases: 2D calculations (cylindrical symmetry)

Version ILD-V5 : magnet design



Version ILD-V5: field homogeneity

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- homogeneous field in the volume of the TPC:

$$\Delta I(\mathbf{R}) = \int_0^{z_{\max}} (\mathbf{B}_r(\mathbf{R}) / \mathbf{B}_z(\mathbf{R})) dz \leq 10 \text{ mm}$$

within the TPC volume:

$$z_{\max} = 2.25 \text{ m}$$

$$\text{and } R = 0 \text{ to } R_{\max} = 1.8 \text{ m}$$

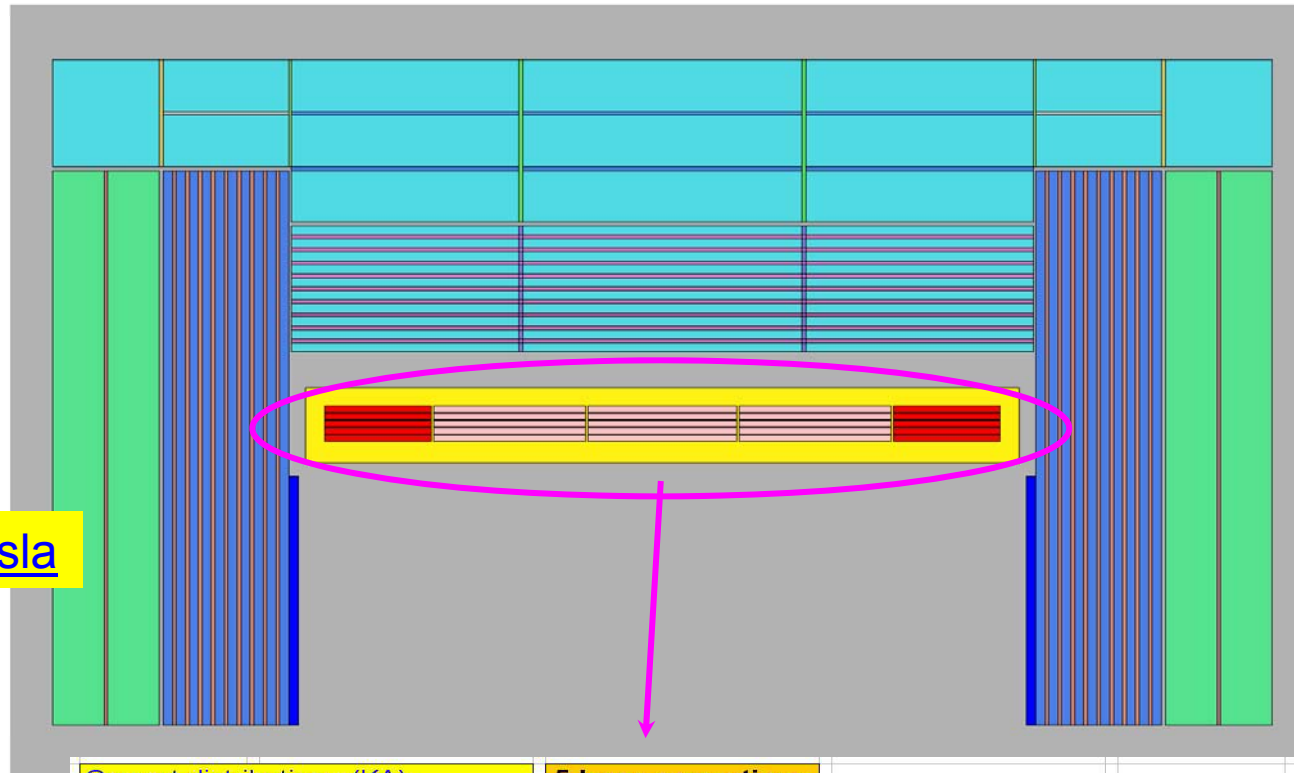
- the field homogeneity is adjusted with a FSP (Field Shaping Plate), located ahead of the end-cap yoke, and correction currents in some places of the coil.

Version ILD-V5: main outputs

| Parameter | Operation | Design |
|--|-----------|-----------|
| Central field (T) | 3.5 | 4 |
| Maximum field on conductor (T) | 4.82 | 5.50 |
| Inom (kA) | 15.8 | 18.4 |
| ΔI cor (kA) | 16.2 | 18.4 |
| Stored energy (GJ) | 2.07 | 2.73 |
| Density of stored energy in the cold mass(kJ/kg) | 9.0 | 11.9 |
| Integral homogeneity in TPC volume (mm) (without anti-DiD) | ≤ 5 | ≤ 10 |
| Stay field @ R = 15 m (G) | 35 | 38 |

Version ILD-V5: magnet configuration

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ILD-V5 @ 4 Tesla

| Current distribution : (KA) | 5 layer corrections | | | |
|-----------------------------|---------------------|-------|-------|-------|
| 36.80 | 18.40 | 18.40 | 18.40 | 36.80 |
| 36.80 | 18.40 | 18.40 | 18.40 | 36.80 |
| 36.80 | 18.40 | 18.40 | 18.40 | 36.80 |
| 36.80 | 18.40 | 18.40 | 18.40 | 36.80 |
| 36.80 | 18.40 | 18.40 | 18.40 | 36.80 |

Version ILD-V5: coil configuration

| | | | | |
|----|----|----|----|----|
| C2 | C1 | C1 | C1 | C2 |
| C2 | C1 | C1 | C1 | C2 |
| C2 | C1 | C1 | C1 | C2 |
| C2 | C1 | C1 | C1 | C2 |
| C2 | C1 | C1 | C1 | C2 |

3.5 T

| | NI (MA) | J (A/mm ²) | N (turns/layer) | I per turn (kA) | I correction (kA) | Length (m) |
|----|---------|------------------------|-----------------|-----------------|-------------------|------------|
| C1 | 0.87 | 7 | 55 | 15.8 | 0 | 1.65 |
| C2 | 1.28 | 14.8 | 40 | 32 | 16.2 | 1.2 |

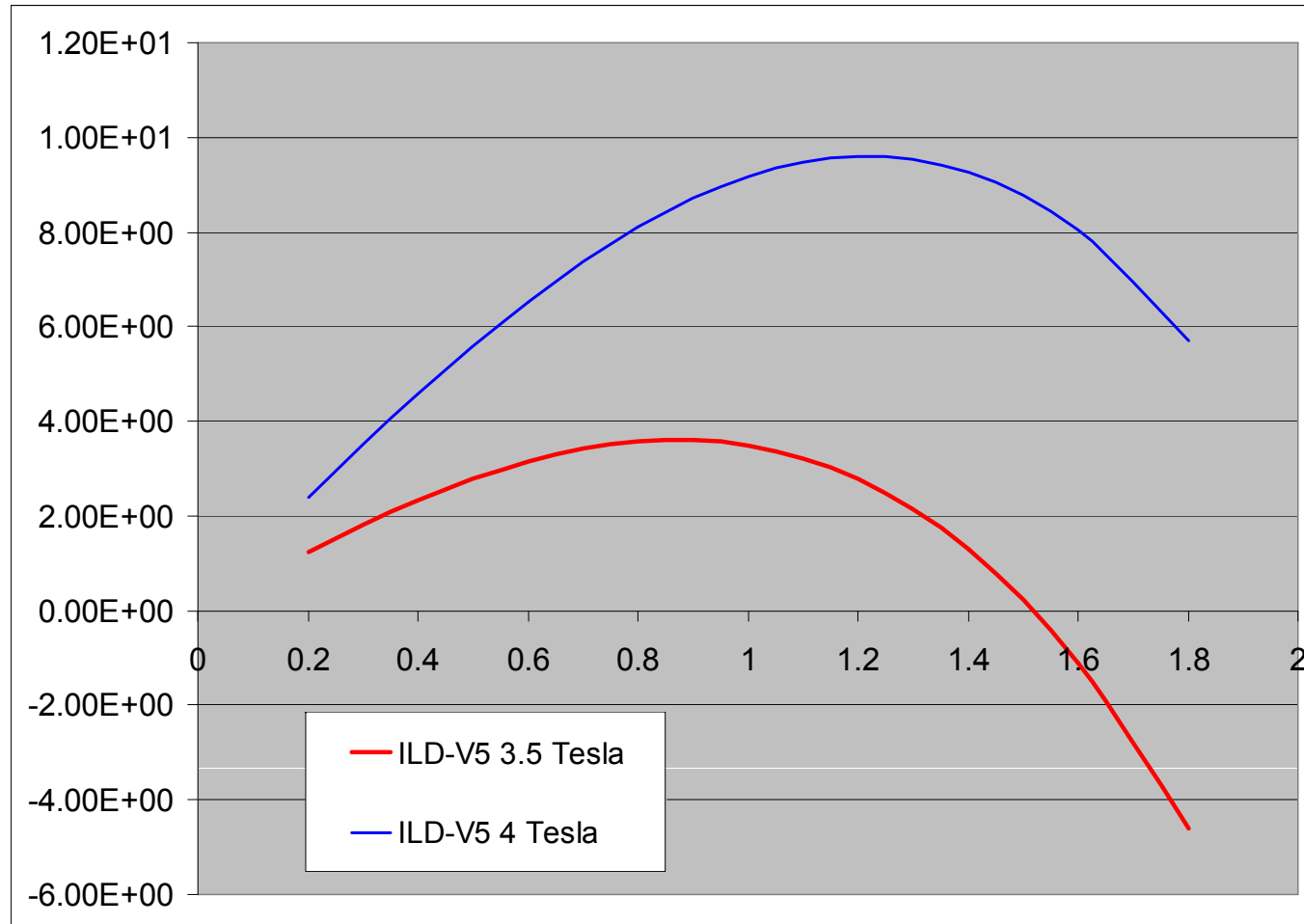
4. T

| | NI (MA) | J (A/mm ²) | N (turns/layer) | I per turn (kA) | I correction (kA) | Length (m) |
|----|---------|------------------------|-----------------|-----------------|-------------------|------------|
| C1 | 1.02 | 8.2 | 55 | 18.4 | 0 | 1.65 |
| C2 | 1.47 | 17 | 40 | 36.8 | 18.4 | 1.2 |

Version ILD-V5: field homogeneity

$\int (B_r/B_z) dz$ vs r ($z=0$ to 2.25 m)

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Comparison of ILD-V5 and CMS designs

| Parameter | CMS | ILD-V5 |
|----------------------------------|-----------------------------------|-----------------------------------|
| Useful aperture (m) | 6 | 6.9 |
| Length (m) | 12.5 | 7.35 |
| Design field (T) | 4 | 4 |
| Max. field (T) | 4.6 | 5.50 |
| Nominal current (kA) | 19.1 | 18.4 |
| Extra correction current (kA) | 0 | 18.4 |
| Coil configuration | 5 modules * 4 layers, same length | 5 modules * 5 layers, 2 ≠ lengths |
| Stored energy (GJ) | 2.6 | 2.73 |
| Density of stored energy (kJ/kg) | 11.6 | 11.9 |

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2. Some technical points
 - 2.1 Points similar to CMS
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 - 2.3 Anti DiD coil design

Technical points similar to CMS

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A lot of technical points will be similar to CMS:

- . Reinforced conductor, based on a superconducting cable
- . Inner winding of the five layers of each module
- . Mandrel also acting as mechanical support and quench-back tube
- . Indirect cooling by saturated liquid helium at 4.5 K, with thermo-siphon
- . Cold mass supported in the vacuum tank by several sets of tie-rods
- . Vacuum tank supported in a cantilever way by the central barrel yoke
- . Inner sub-detectors supported on rails inside the vacuum tank

The experience gained by CMS will be (and already has been) of a great interest for ILD.

Modules with correction current

This is one of the main novelty from CMS.



Basic concepts:

- the conductor with the extra correction current has:
 - . the same overall dimension as the conductor with the main current, typically $73 \times 22 \text{ mm}^2$ without insulation
 - . but a higher current transport capacity to work with about the same safety margin with respect to the critical current
 - . a stronger mechanical support: at least for the conductor with the extra correction current, the ratio of structural material is close to 1 (cf conductor for the ATLAS Central Solenoid developed by Akira Yamamoto et al.), vs 0.6 for CMS

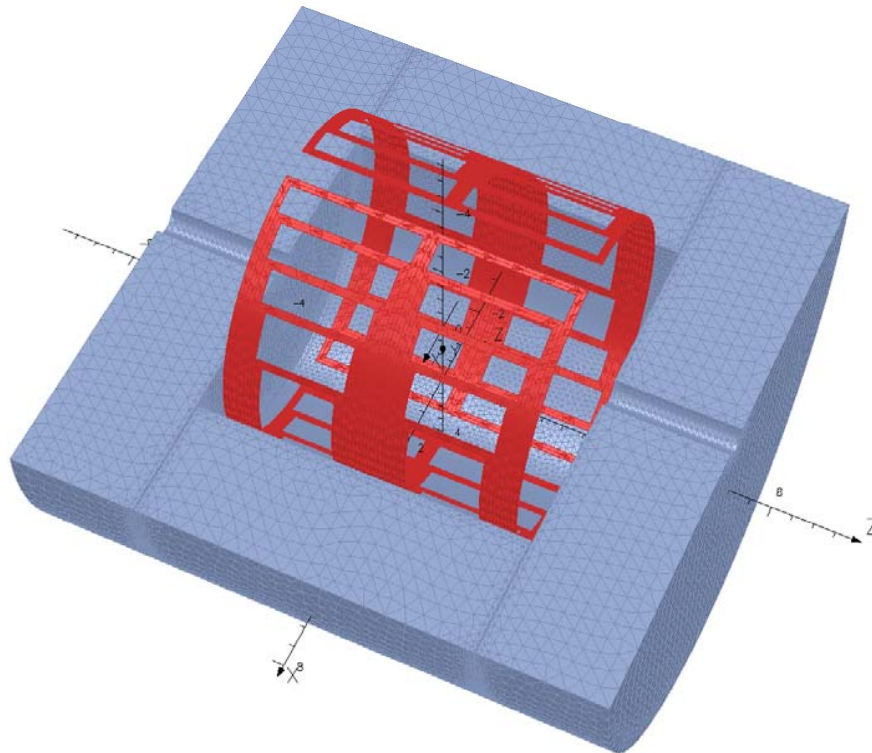
- in case of quench, the extra local Joule heating is absorbed by the quench-back phenomenon, much quicker than the increase of temperature of the coil, and which diffuses the uniformly the heat

Anti-DID coil design

The anti-DiD allows to zero the crossing angle for the outgoing beam (and pairs) behind the I.P.

Brett Parker has started some conceptual design study

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- . Two dipole coils, anti-symmetric with respect to the I.P.
- . Proposal to wind the anti-DID coil outside the main solenoid coil (reduced field region)
- . Field maps (3D) do not yet include the ILD solenoid
- . $B_{\text{anti-DID}} \sim 0.065 \text{ T}$

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- Magnetic calculations have been done with the Lol parameters. Solutions which meet the specifications have been found
- Most of the CMS concepts can still be used for ILD. Some R&D on a conductor with a ratio of structural material close to 1 would strengthen the mechanical design of the most mechanically solicited modules
- Conceptual design of the anti-DID has started, and must continue with the present detector magnet configuration
- Even if some points can still evolve and/or need some more studies, the present design is at an acceptable level of study for the Lol