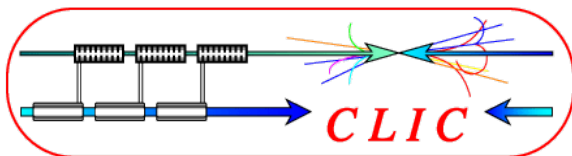
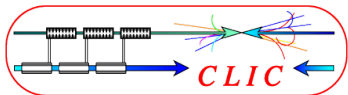


# Comparison of W and Fe HCal at Multi-TeV-Energies

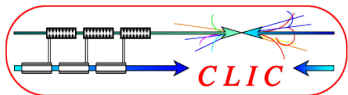
ALCPG, Albuquerque  
October 2, 2009

Angela Lucaci-Timoce (DESY)  
Peter Speckmayer (CERN)  
Christian Grefe (CERN)





- Motivation
- HCal stack simulation studies
- Simulations with CALICE AHCal module
- Particle Flow Performance
- Future Plans



- SiD (LoI version)

- HCAL

- $R_{\min} = 141 \text{ cm}$ ,  $R_{\max} = 253 \text{ cm}$
    - 40 layers of Steel/Gas (2.0 cm + 0.8 cm)
    - $\lambda = 5.1$  ,  $X_0 = 46.5$
    - Readout: 1.0 cm x 1.0 cm digital
    - 12 fold

- Coil

- $R_{\min} = 255 \text{ cm}$ ,  $R_{\max} = 338 \text{ cm}$
    - $B = 5.0 \text{ T}$

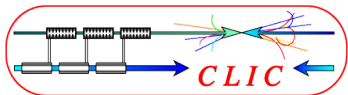
- ILD (LoI version)

- HCAL

- $R_{\min} = 206 \text{ cm}$ ,  $R_{\max} = 333 \text{ cm}$
    - 48 layers of Fe/Scint (2.0 cm + 0.5 cm)
    - $\lambda = 6.0$  ,  $X_0 = 55.3$
    - Readout: 3.0 cm x 3.0 cm analog
    - 16 fold (outside), 8 fold (inside)

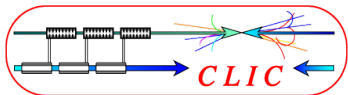
- Coil

- $R_{\min} = 344 \text{ cm}$ ,  $R_{\max} = 419 \text{ cm}$
    - $B = 3.5 \text{ T}$

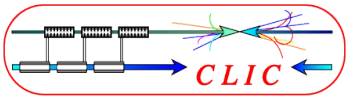


## Why Tungsten?

- Need shorter longitudinal shower size
  - High energetic jets require more HCal material in terms of interaction lengths – to achieve better containment
  - Strong constraints by coil – cost and feasibility
- Need smaller lateral shower size
  - High energetic jets are more boosted
  - PFA performance is decreasing because of overlapping showers
- Tungsten might solve both problems
- We consider tungsten only for the HCal barrel since space constraints for the endcaps are not severe

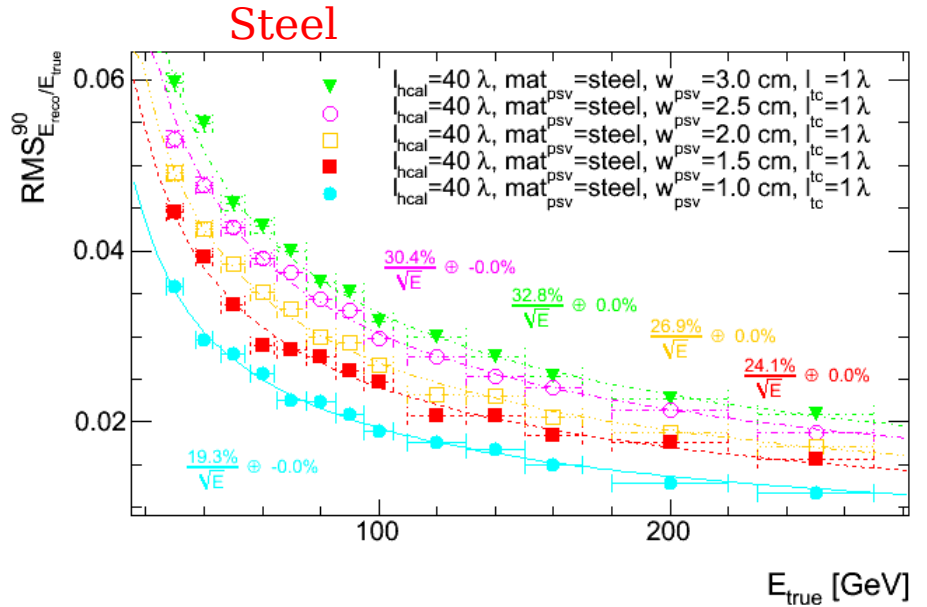
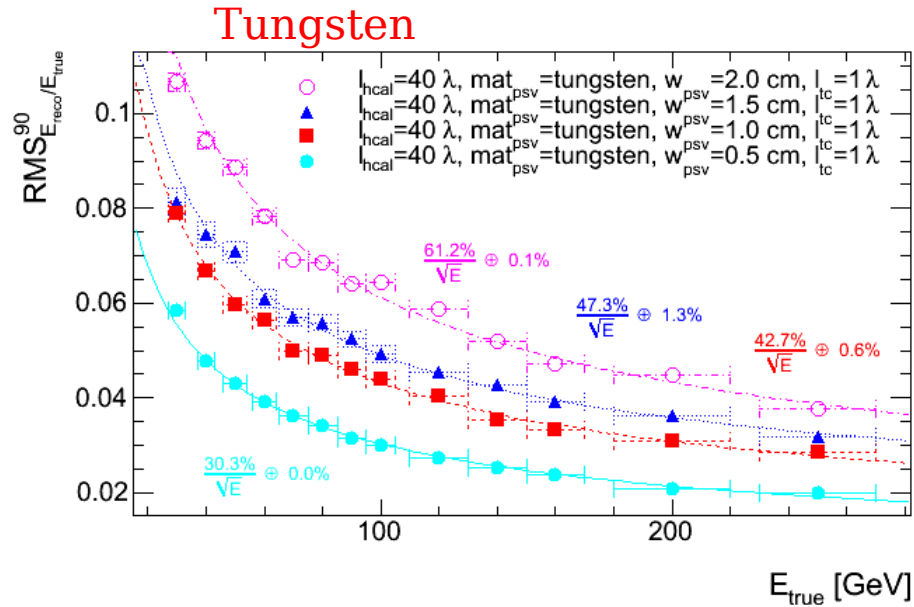


- Simple HCal geometry to investigate materials and sampling ratios
- Materials: tungsten, steel, steel-tungsten-sandwich (various thicknesses)
- Constant gap size: 5.0 mm Scint + 2.5 mm G10
- Dimensions: 5x5m and more than  $25 \lambda$  in depths to guarantee shower containment
- Simulated 100k  $\pi^+$  between 1 GeV and 300 GeV for each geometry
  - This should cover the energy range of jet main constituents of events with  $\#jets \geq 4 @ 3 \text{ TeV}$
- Defined active and dead layers during reconstruction – corresponding to different HCal, coil and tailcatcher sizes
- Reconstruction with a neural network (TMVA)
- Using simple shower variables: width, length, center, energy density, etc.

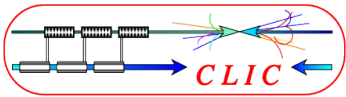


# HCal-Stack Simulations

- “extremely deep”-HCal performance

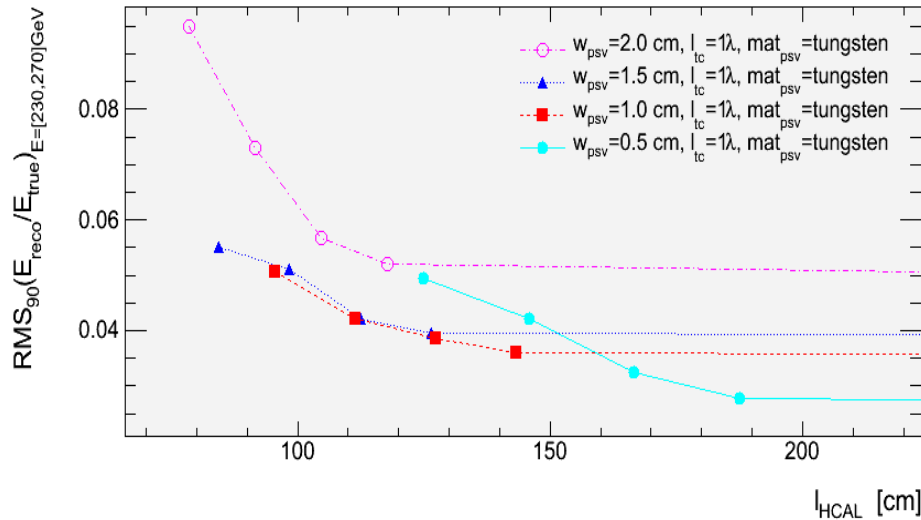


- Linearity is better than 2% (not shown)
- “extremely deep”-case:
  - Finer passive layers are better
  - Steel performs better than tungsten

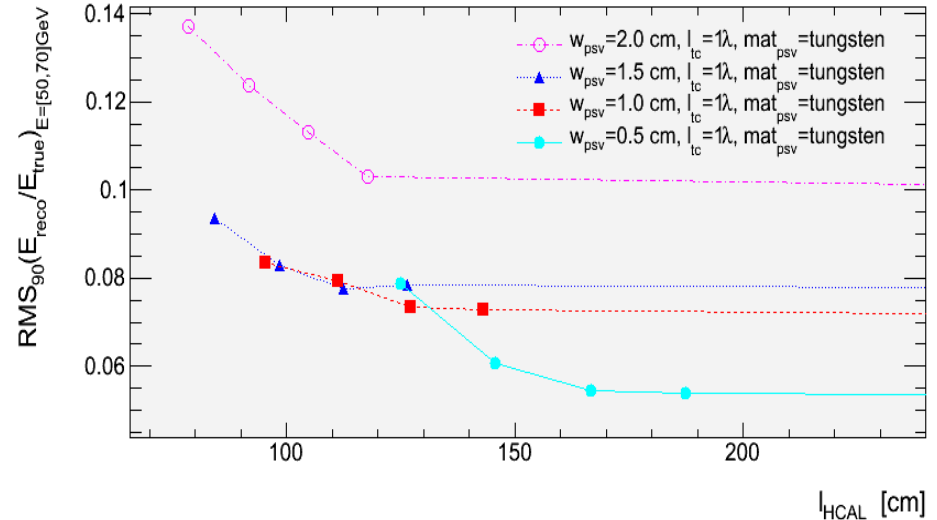


- Performance vs HCal depth (tungsten)

$E_{MC} \sim 250 \text{ GeV}$

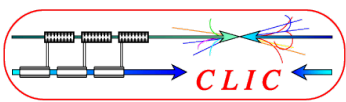


$E_{MC} \sim 60 \text{ GeV}$



The 4 points of each graph correspond to 6, 7, 8 and 9  $\lambda$  total calorimeter material

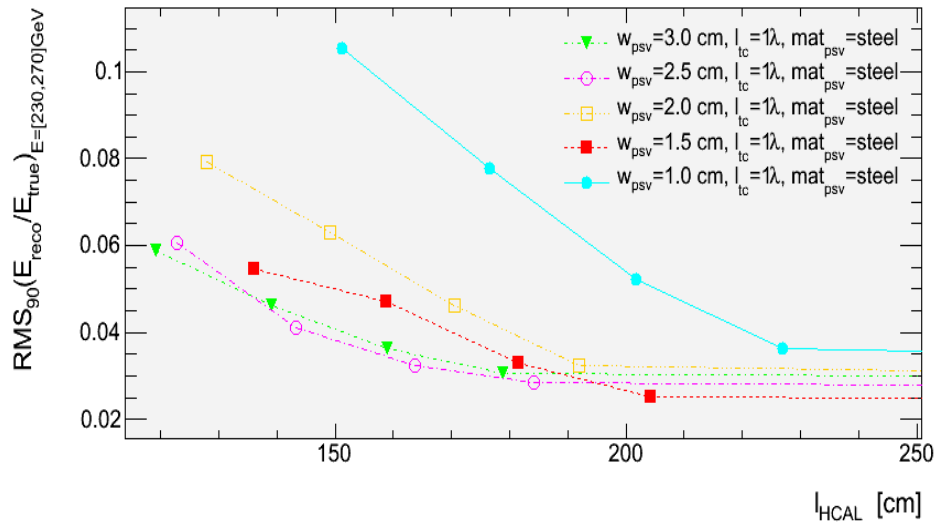
- For an HCal depth of around  $\sim 140 \text{ cm}$  an absorber thickness of  $\sim 1 \text{ cm}$  tungsten seems optimal
- This corresponds to  $\sim 8 \lambda$ ; taking into account  $1 \lambda$  of ECal, a  $7 \lambda$  HCal appears to be sufficient for CLIC energies
- Stay away from the steep areas where leakage becomes the dominating factor



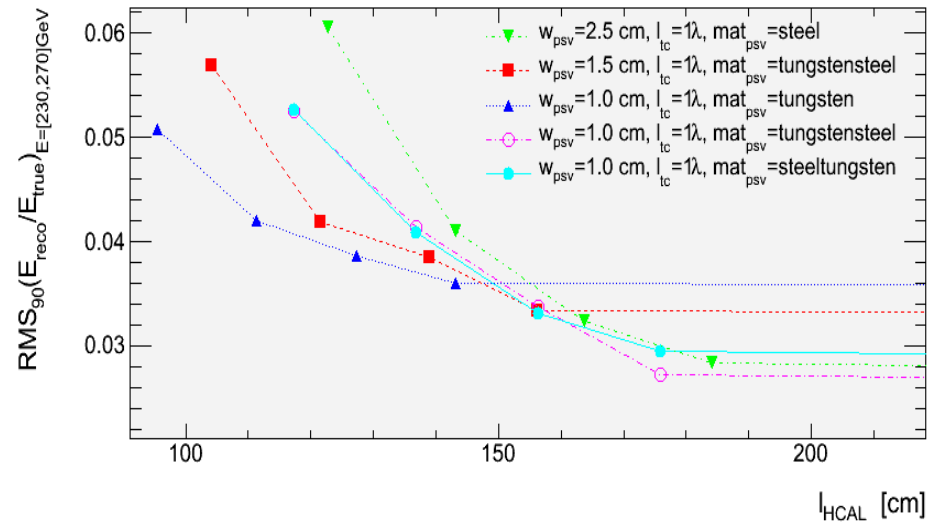
# HCal-Stack Simulations

- Performance vs HCal depth (tungsten vs steel)

Steel

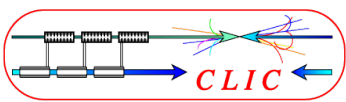


Steel, Tungsten, Steel & Tungsten



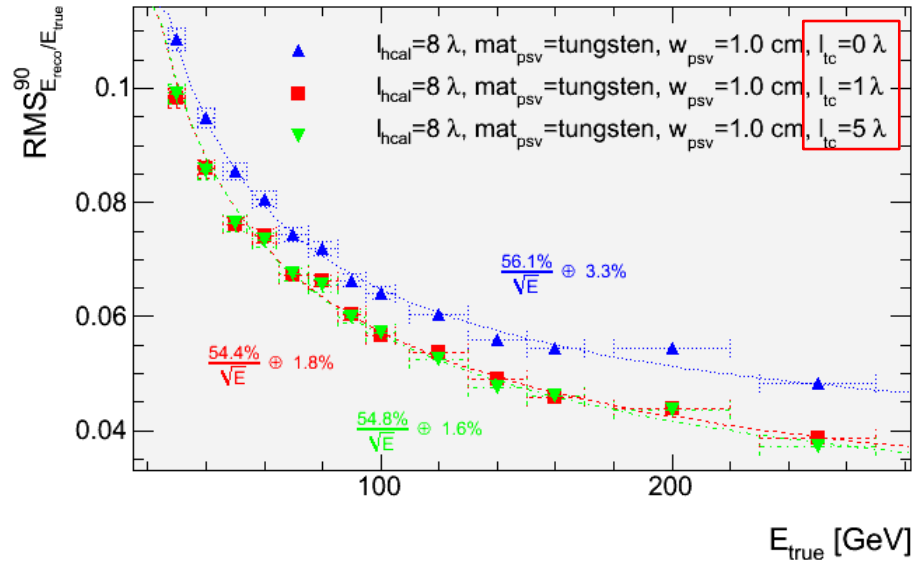
- Steel can perform better than tungsten, but only at a significantly bigger HCal size



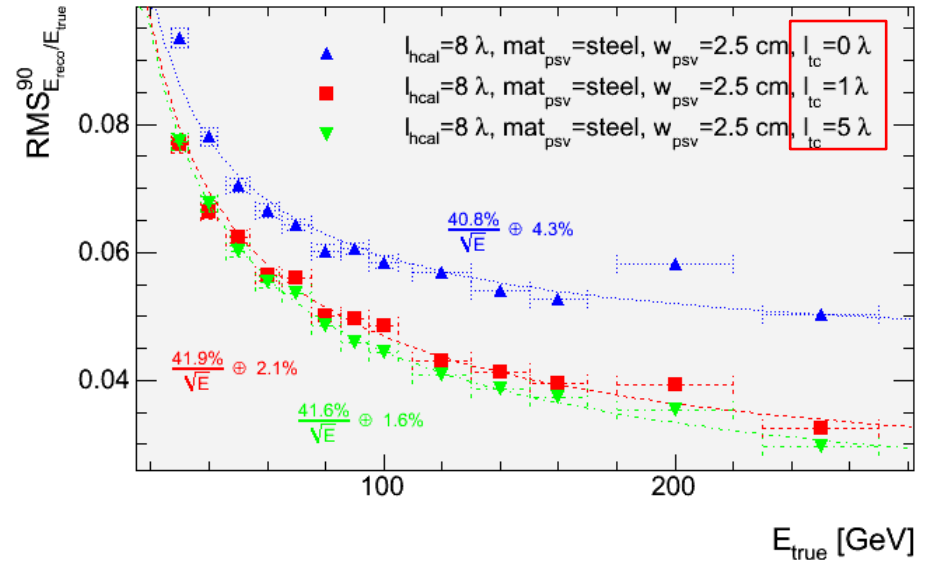


## Impact of a Tailcatcher

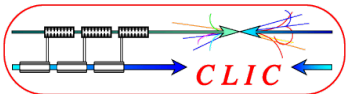
### Tungsten



### Steel

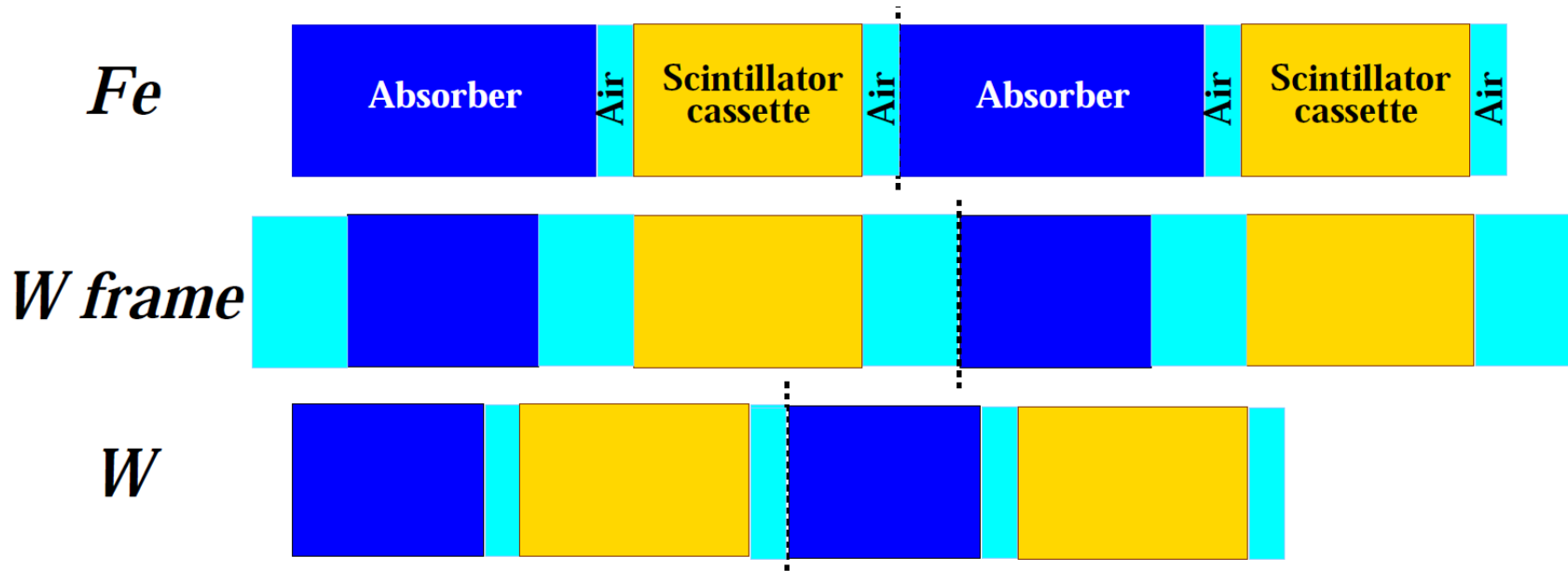
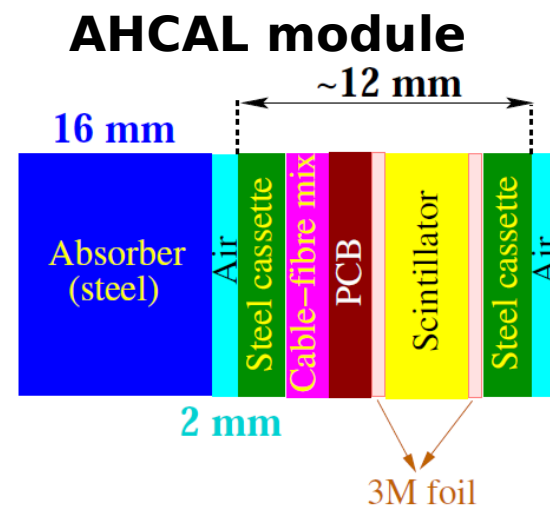


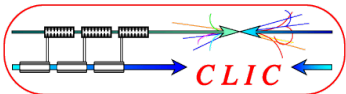
- Resolution is improved by adding a tailcatcher of  $\sim 1 \lambda$
- The effect of a bigger tailcatcher is negligible
- In this case:  $0 \lambda$  implies no active material after the coil



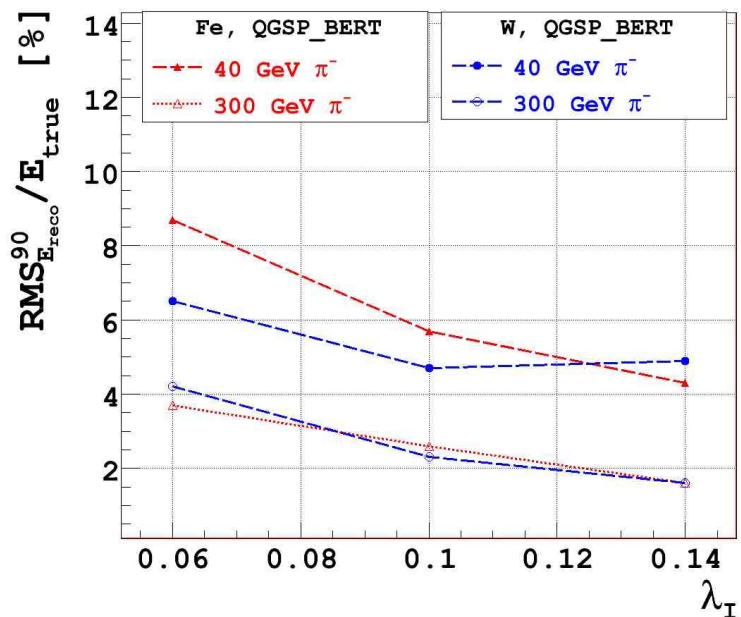
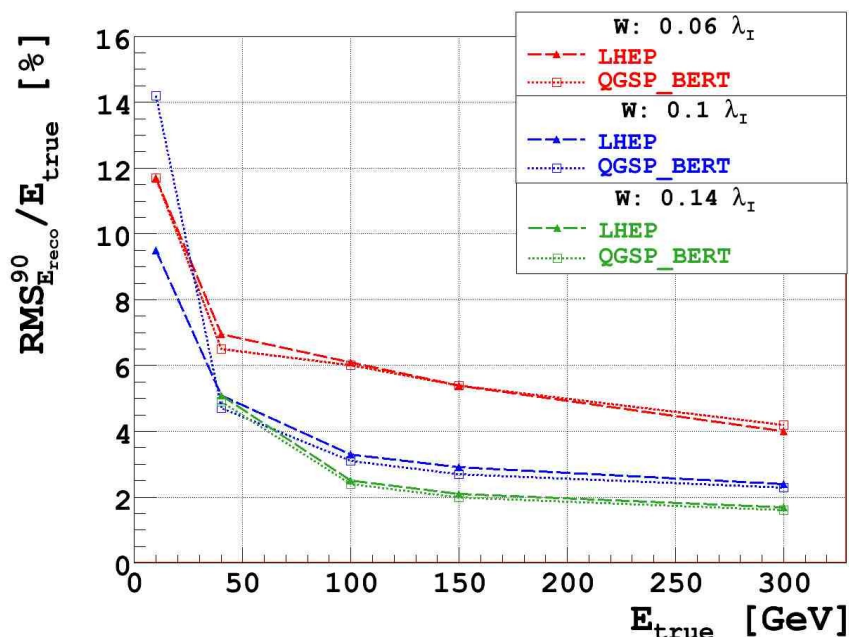
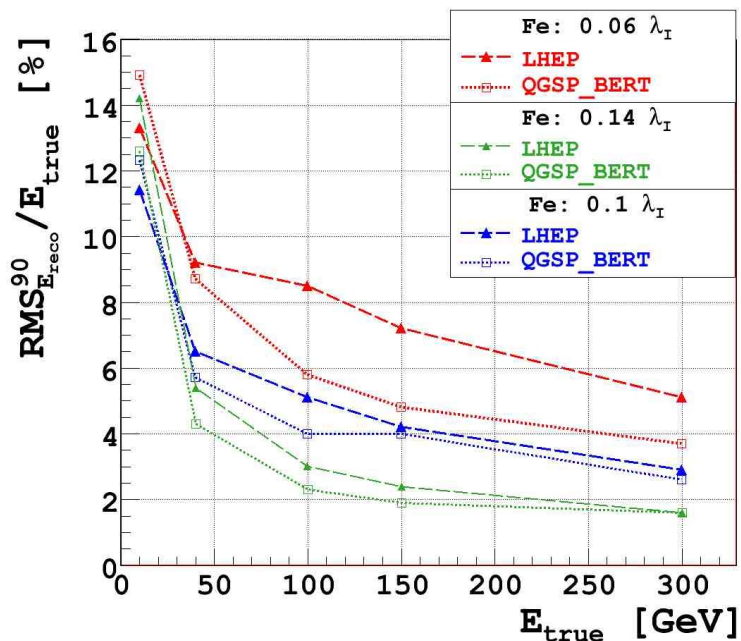
# Simulations with CALICE AHCal Module

- In a possible tungsten HCal prototype the existing active modules would be re-used
- Current electronics require the full 30mm pitch
- Additional air gaps in the HCal

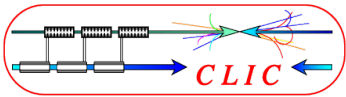




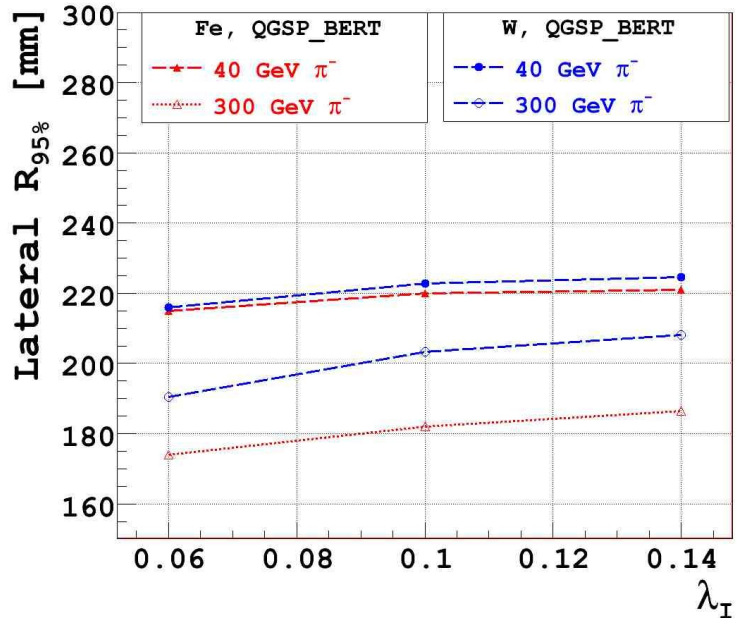
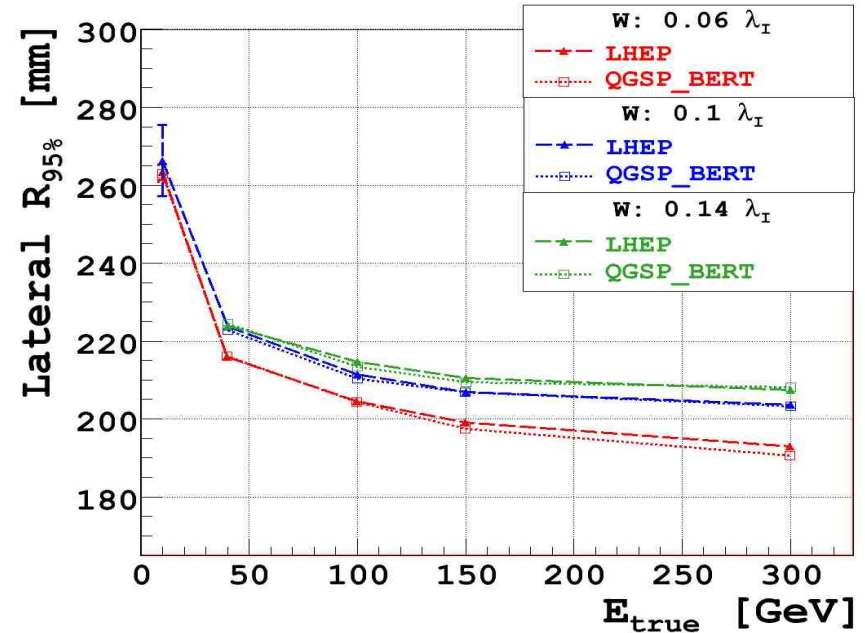
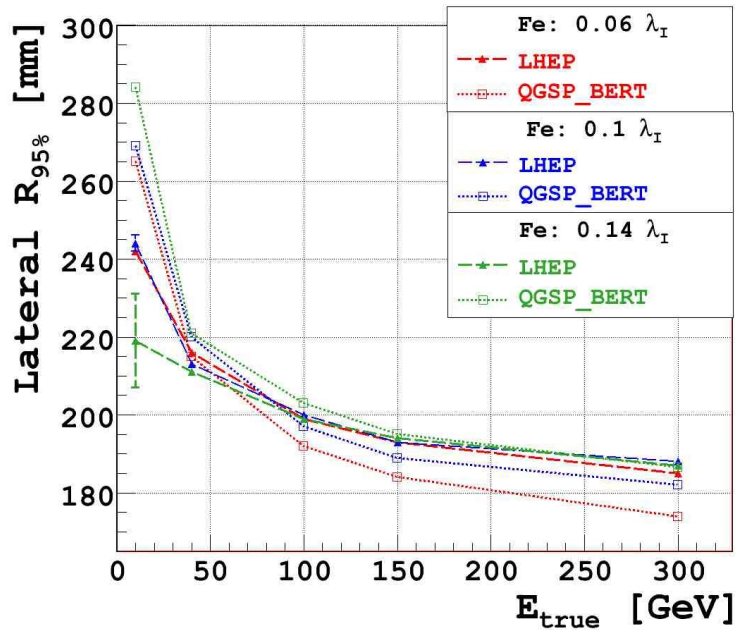
# Energy Resolution



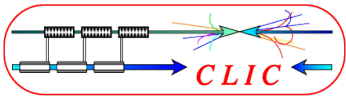
- 40 GeV  $\pi^-$  : better resolution with W
- 300 GeV  $\pi^-$  : comparable results for both



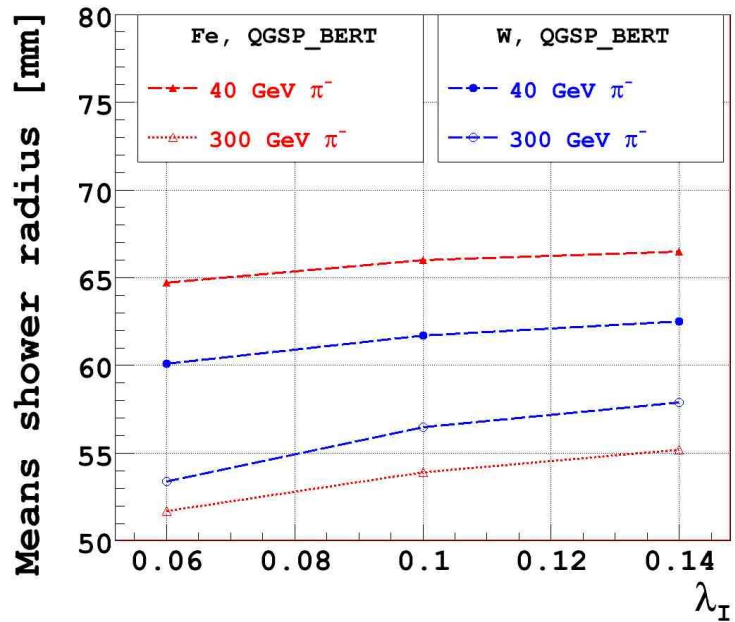
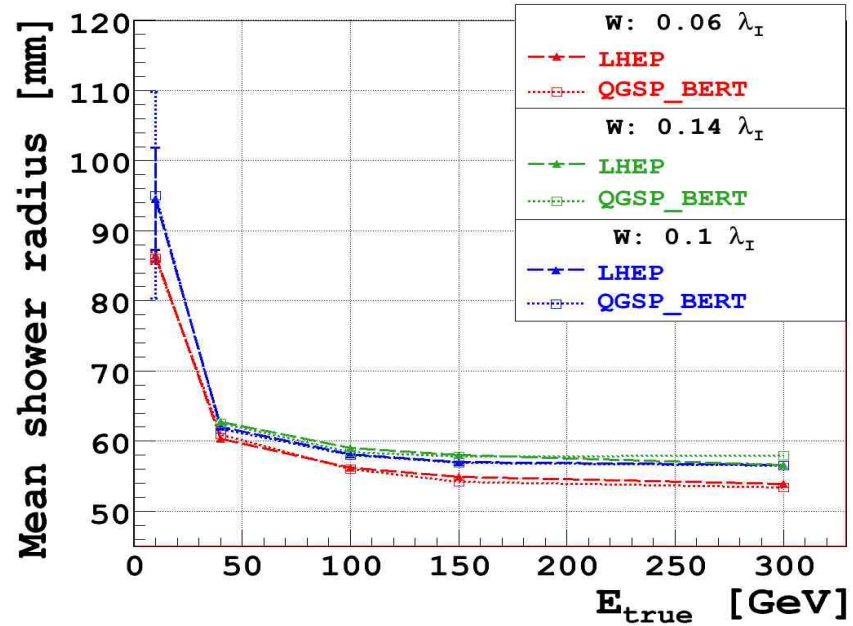
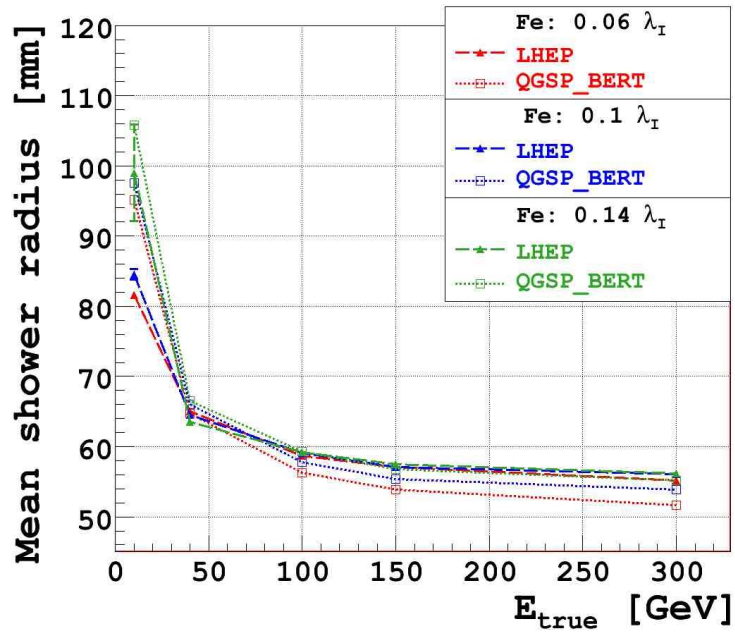
# Lateral Shower Containment



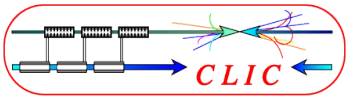
- 40 GeV  $\pi^-$  :  $R_{95\%} \approx 22\text{cm}$  for W and Fe
- 300 GeV  $\pi^-$  : 95% containment at smaller radius for Fe



# Mean Shower Radius

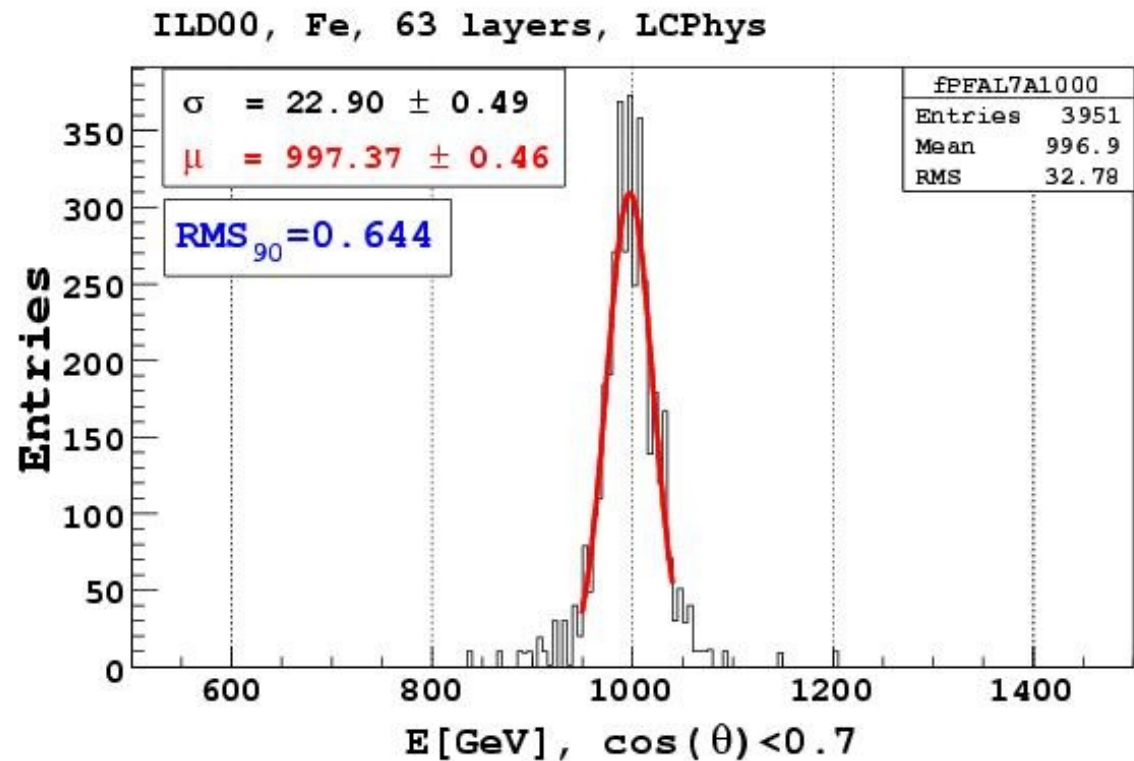


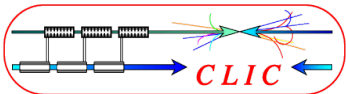
- 40 GeV  $\pi^-$  : smaller radius for W
- 300 GeV  $\pi^-$  : smaller radius for Fe



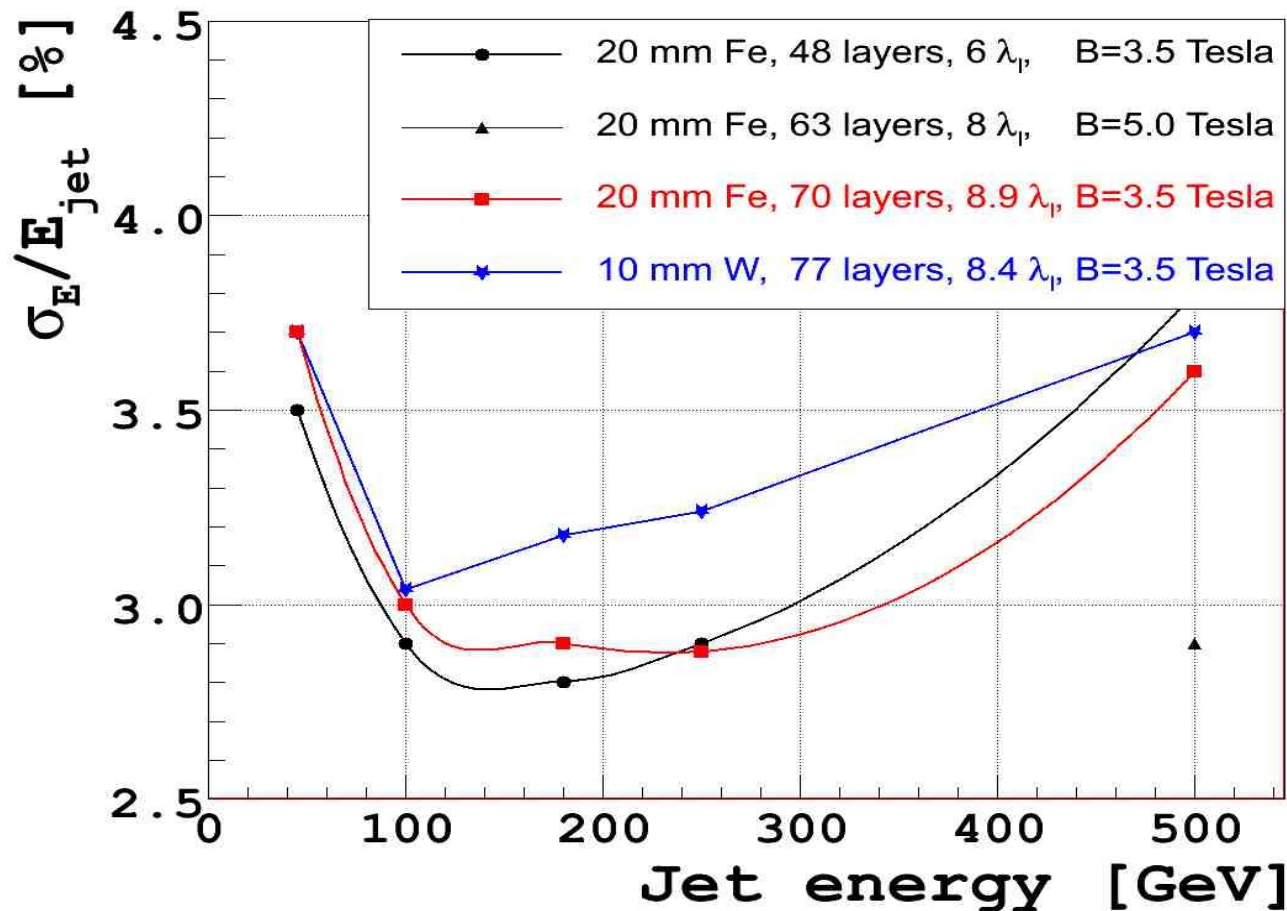
# Particle Flow Performance

- Modified ILD detector
  - 77 layers of 10mm W + 5mm Scint  $\approx 8.4 \lambda$
  - 70 layers of 20mm Fe + 5mm Scint  $\approx 8.9 \lambda$
- Use Pandora PFA (without special tuning)
- Example for  $8.0 \lambda$  HCal, Fe absorber,  $B = 5 \text{ T}$  :  
 $\sigma_E/E \approx 64\%/\sqrt{E/\text{GeV}}$
- Consistent with M. Thomsons results

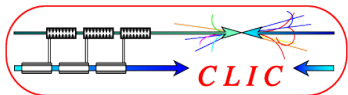




## Particle Flow Performance



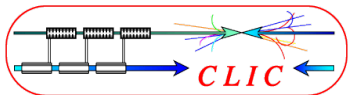
- Jet energy resolution comparable for W and Fe for low energies
- W performance degrades for higher energies
- No tuning of Pandora PFA



## Plans for W HCal Prototype

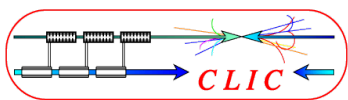
- Verify simulation results with a tungsten HCal prototype
- Re-use existing active modules (scintillator, micromegas, ...)
- Re-use existing mechanical support structure
- Very productive workshop on September 24 at LAPP
  - <http://indico.cern.ch/conferenceDisplay.py?confId=68025>
- Possible dimensions:
  - 40 layers
  - Between 60x60 cm<sup>2</sup> and 80x80 cm<sup>2</sup> W plates in Fe or Al frame
- Possible timeline
  - 2010 – start of W plate production
  - 2011 – first beam tests



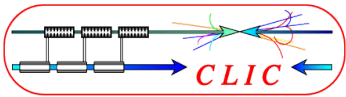


- W HCal is a viable option at CLIC energies because of the strong constraints imposed by the coil radius
- Further simulation studies are needed, especially for PFA performance
- A prototype is needed to verify simulations
- Construction of a W HCal prototype is planned within CALICE

# Thank You

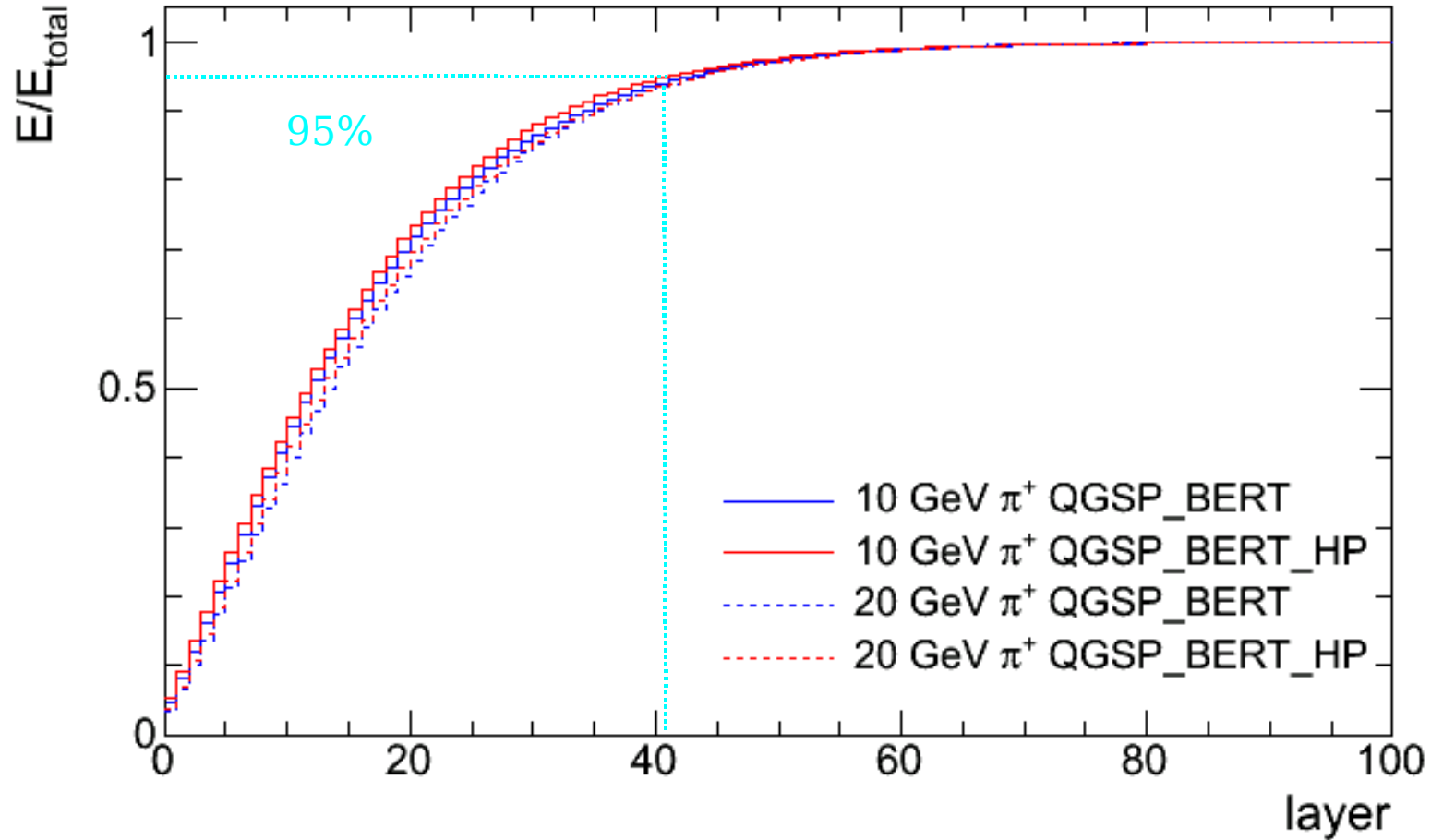


# Backup Slides

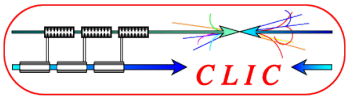


# Longitudinal Shower Size

## longitudinal shower containment

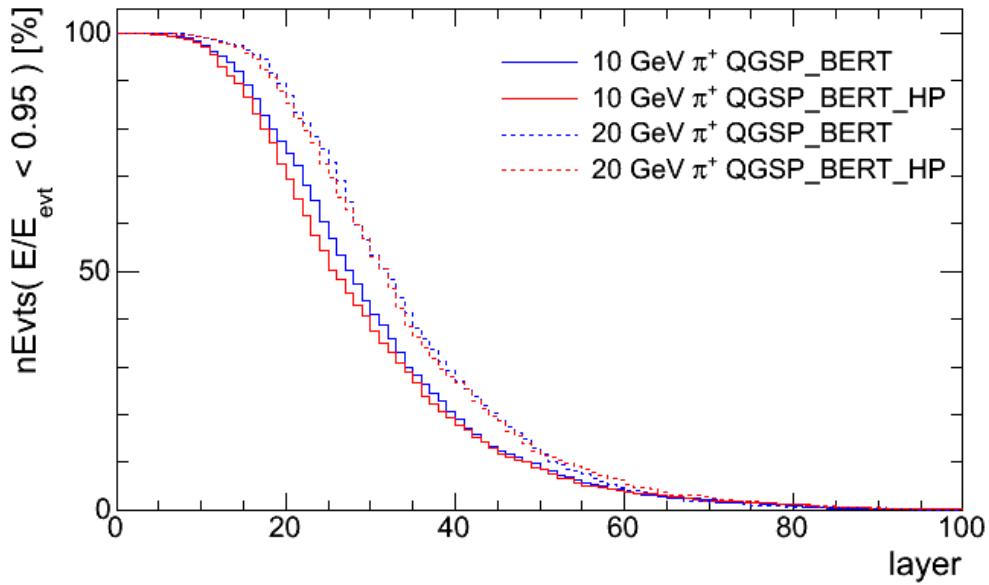


**12 mm tungsten + scint**

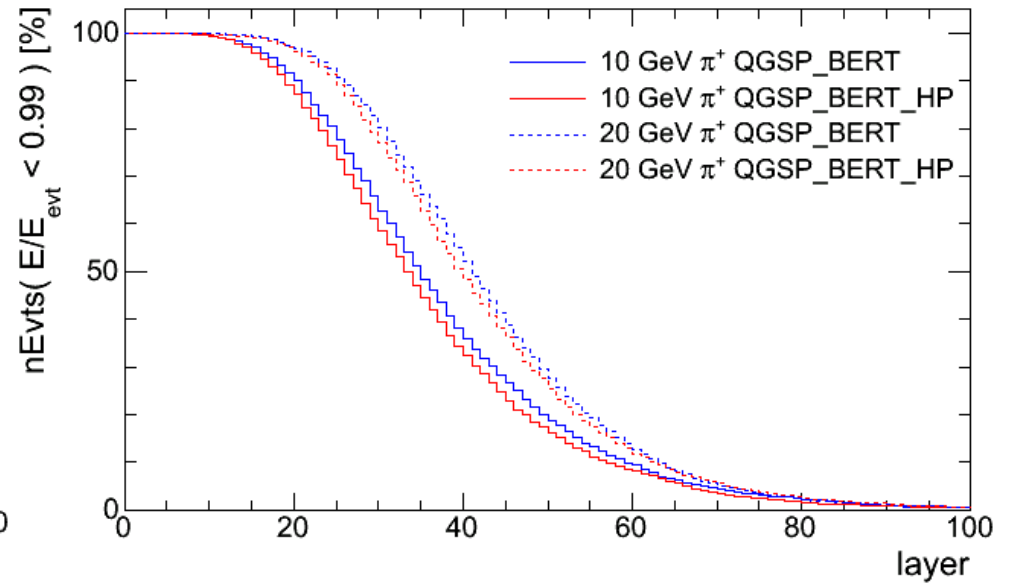


# Longitudinal Containment Efficiency

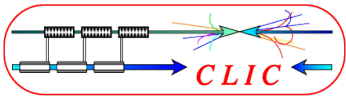
longitudinal shower containment efficiency



longitudinal shower containment efficiency

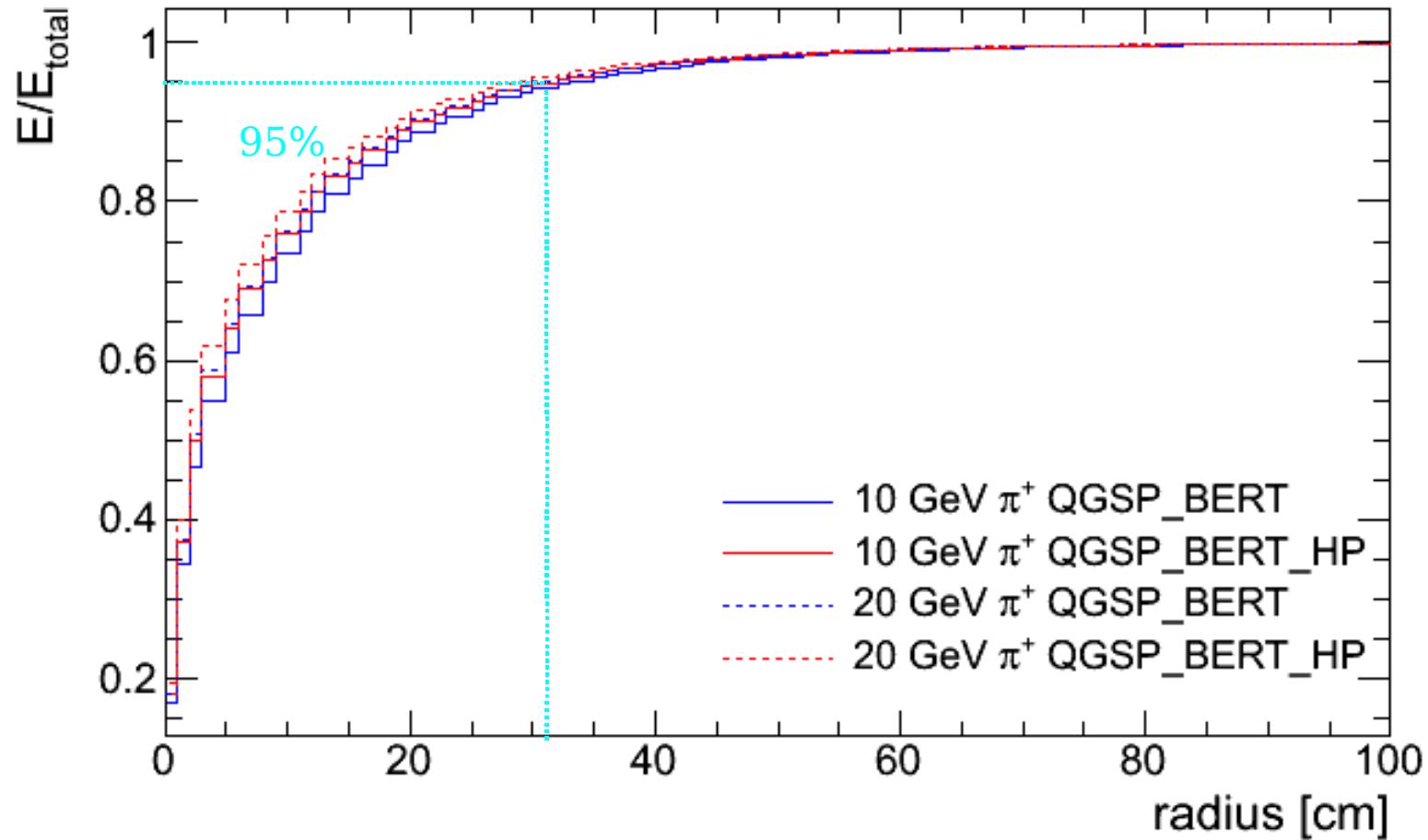


**12 mm tungsten + scint**

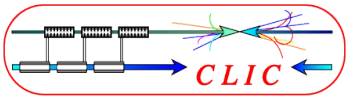


# Lateral Shower Size

## lateral shower containment

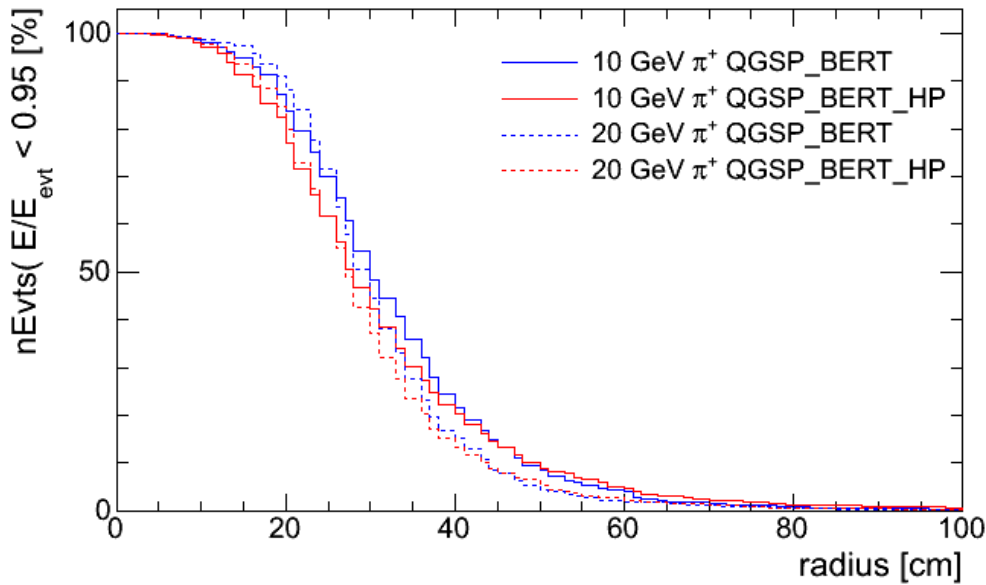


**12 mm tungsten + scint**

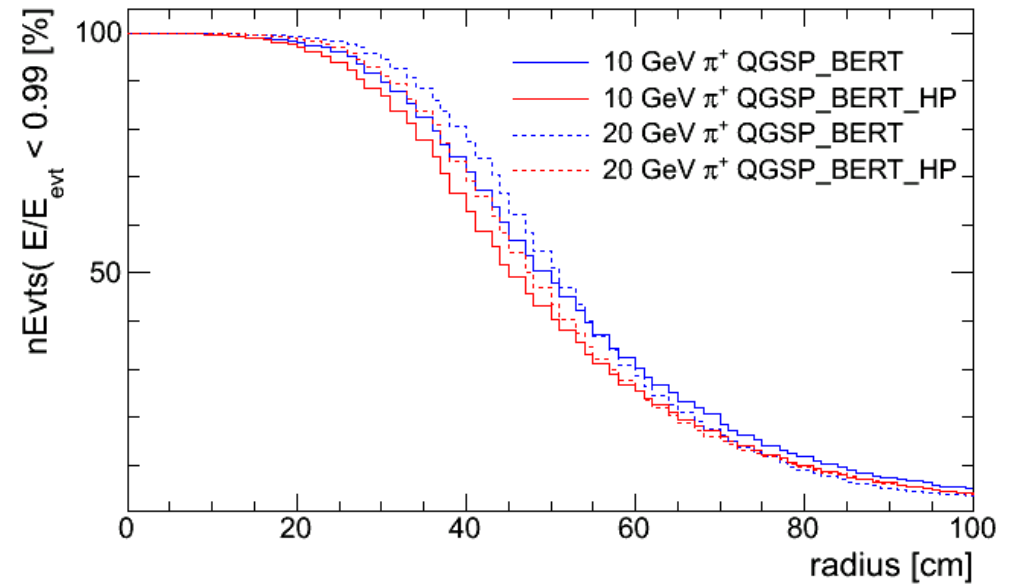


# Lateral Containment Efficiency

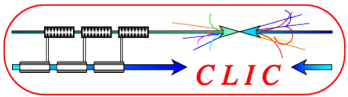
lateral shower containment efficiency



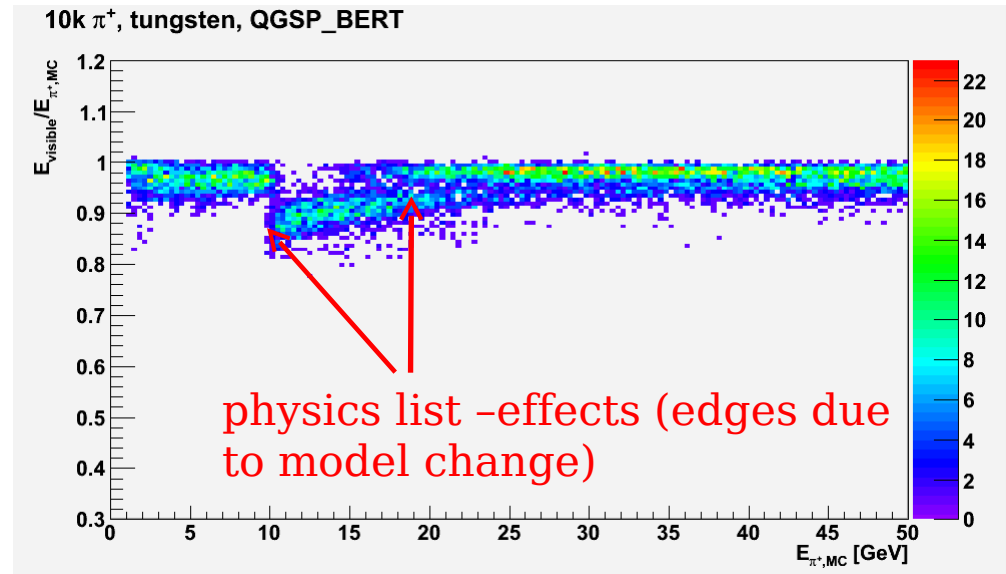
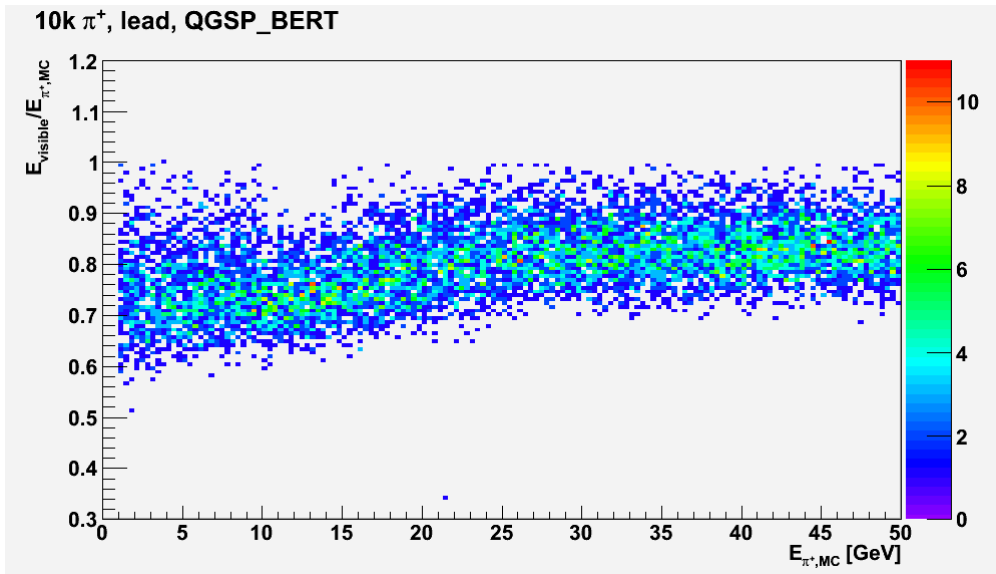
lateral shower containment efficiency



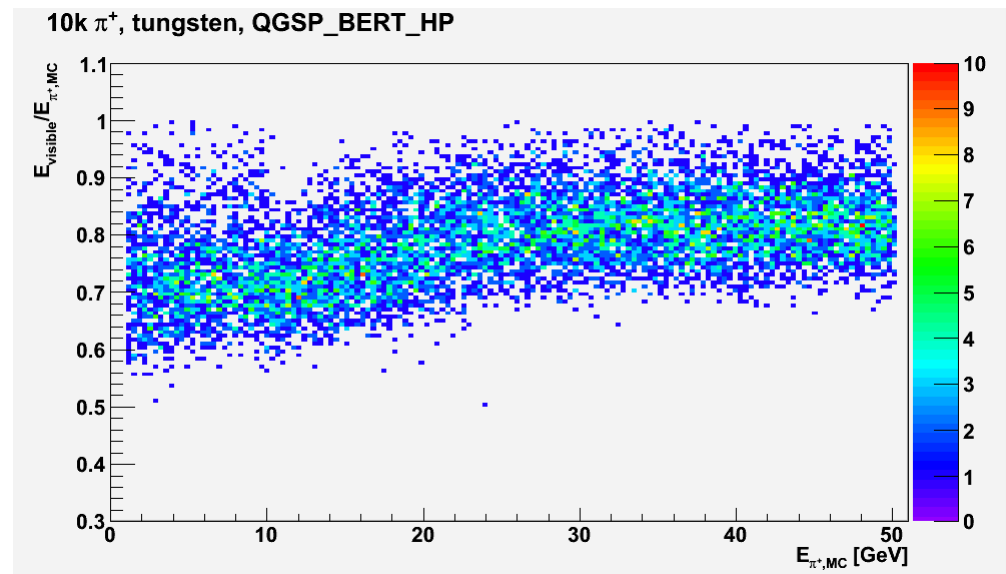
**12 mm tungsten + scint**

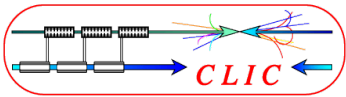


- GEANT4 treatment of neutrons spoils visible energy simulation

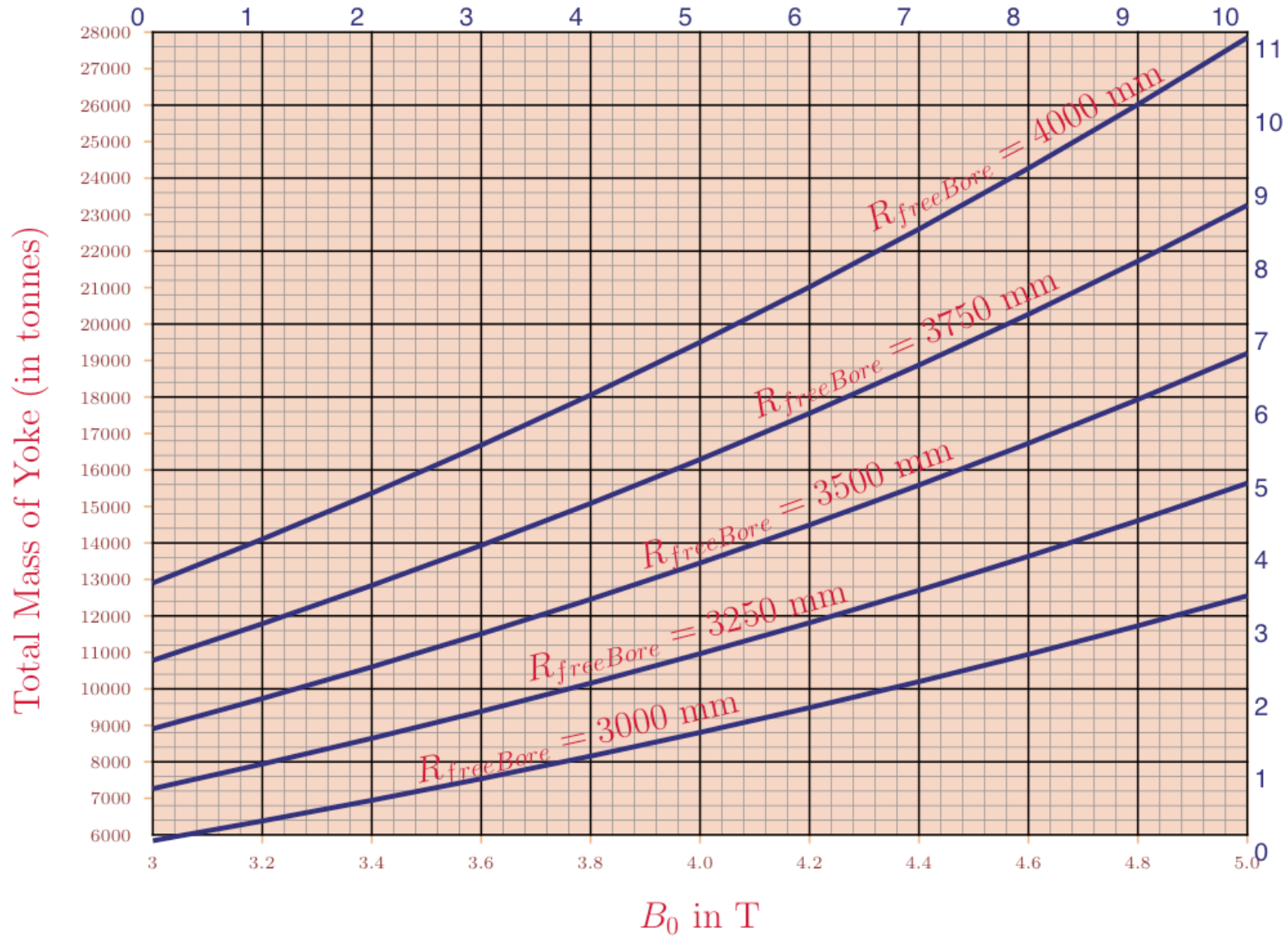


- QGSP\_BERT\_HP seems to solve the problem
- Need to investigate impact on shower shapes and resolution

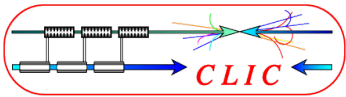




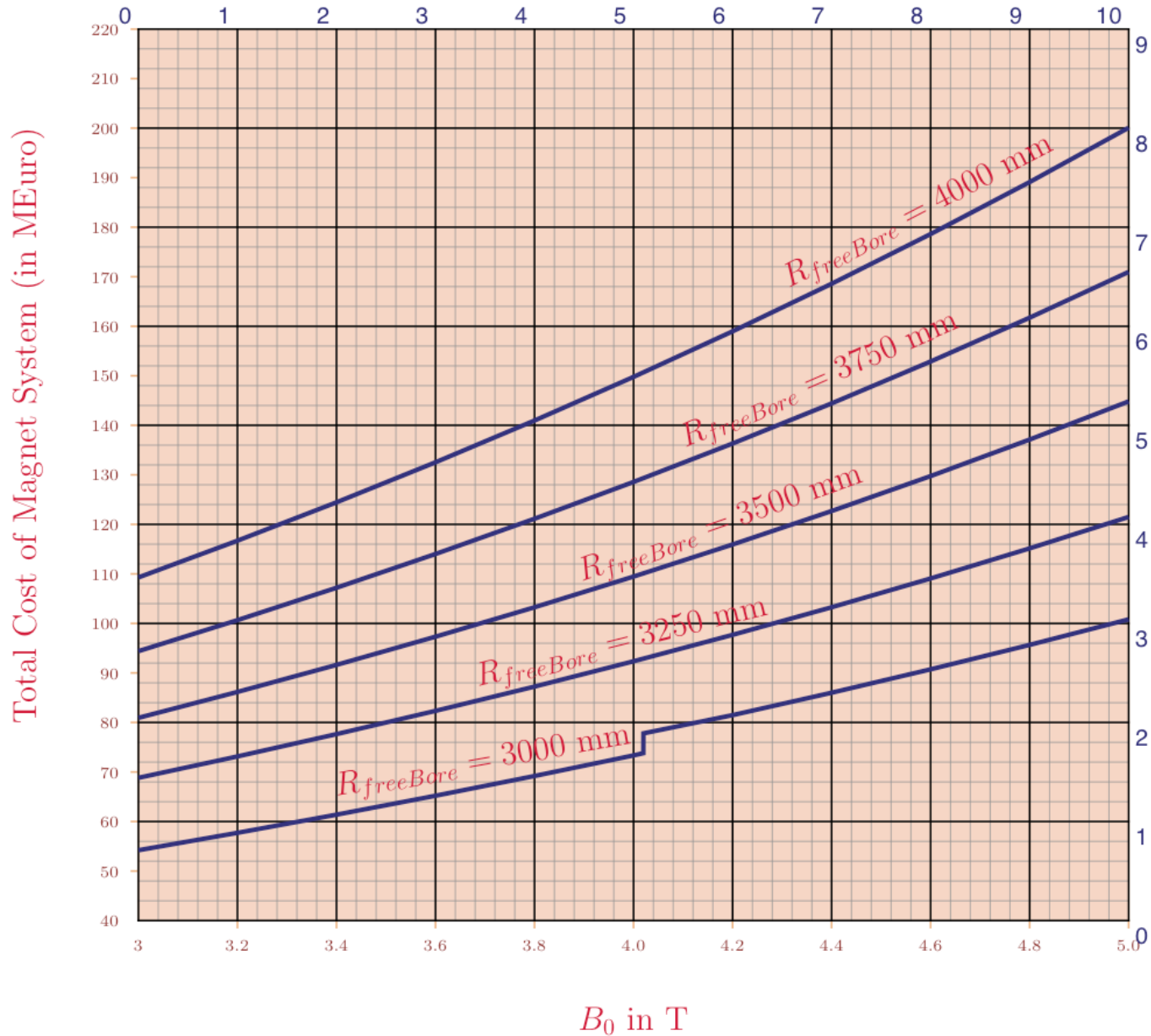
# Coil Parametrization



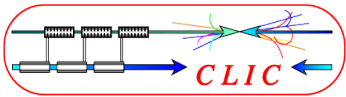




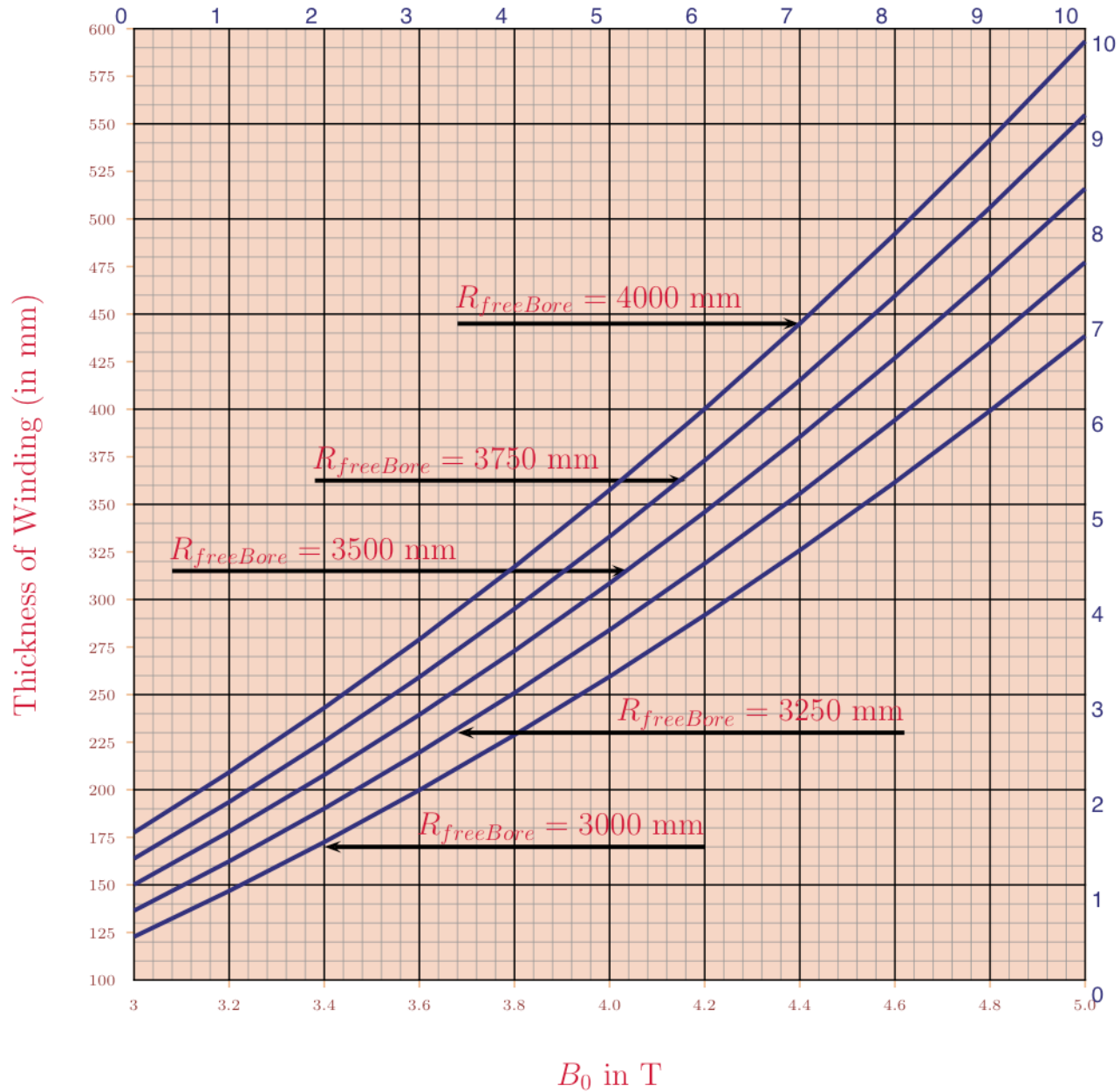
# Coil Parametrization

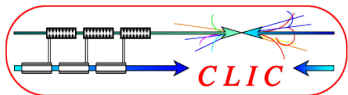


Alain Hervé

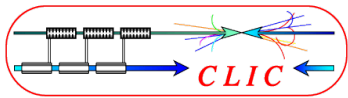


# Coil Parametrization



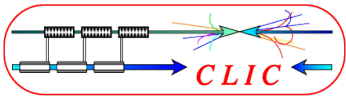


- Pure tungsten
  - $\rho = 19.3 \text{ g/cm}^3$
  - $\lambda = 9.94 \text{ cm}$ ,  $X_0 = 0.35 \text{ cm}$
  - brittle and hard to machine
  
- Tungsten alloys with  $W > 90\%$  + Cu / Ni / Fe
  - $\rho = 17 - 19 \text{ g/cm}^3$
  - $\lambda \approx 10 \text{ cm}$ ,  $X_0 \approx 0.4 \text{ cm}$
  - Well established production procedure
  - Easy to machine
  - Price  $\sim 70 \text{ Euro/kg}$  (without machining)



- Tungsten is usually used in alloys for better mechanical properties and machinability
- Several ferromagnetic (W,Ni,Fe) or paramagnetic (W,Ni,Cu) alloys are available

Werkstoff Material	Abkürzung Abbreviation	Chemische Zusammensetzung [%]		Nominelle Dichte Nominal density	AMS-T-21014 Class
		Chemical composition [%]			
		W	Rest		
Schwach ferromagnetisch / Weakly ferromagnetic					
DENSIMET® 170	D170	90,5	Ni, Fe	17,0	1
DENSIMET® 176 / W	D176 / DW	92,5	Ni,Fe	17,6	2
DENSIMET® 180	D180	95	Ni, Fe	18,0	3
DENSIMET® 185	D185	97	Ni, Fe	18,5	4
DENSIMET® 188	D188	98,5	Ni, Fe	18,8	-
DENSIMET® D2M	D2M	90	Ni, Mo, Fe	17,2	-
Paramagnetisch / Paramagnetic					
INERMET® 170	IT170	90,2	Ni, Cu	17,0	1
INERMET® 176	IT176	92,5	Ni, Cu	17,6	2
INERMET® 180	IT180	95	Ni, Cu	18,0	3



# Tungsten Alloys

	D170	IT170	D176 / W	IT176	D180	IT180	D185
Elastizitätsmodul E [GPa]	340	330	360	350	380	360	385
Young's modulus E [GPa]	340	330	360	350	380	360	385
Schubmodul G [GPa]	140	125	145	135	150	140	160
Modulus of rigidity G [GPa]	140	125	145	135	150	140	160

