

# RF Waveguide Distribution



#### RF Power Waveguide Distribution (1)

- Distribution of klystron output power to the superconducting cavities
- Protection of the klystron from reflected power
- Control of phase and Q<sub>ext</sub>



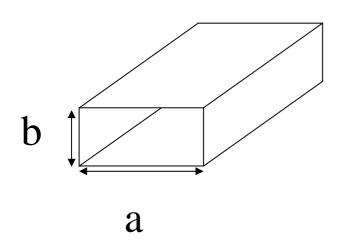
# RF Power Waveguide Distribution (2)

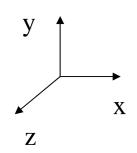
#### Distribution of RF power is done by:

- Waveguides: high power possible, low loss up to certain frequencies Other devices which are not used:
- Coaxial lines: power loss is high, heating of the inner conductor or the dielectric material
- Parallel wires: radiation into the environment
- Striplines: breakdown limit at high power is low, in use for low power applications e.g. integrated circuits



#### Rectangular Waveguide





# Which electromagnetic waves (frequencies, modes) can propagate?

- Start with Maxwell Equation
- Solve wave equation with boundary conditions:

#### Two types of solutions:

- TE (H-Wave):  $E_z=0$   $H_zK0$
- TM (E-Wave):  $E_z KO H_z = 0$
- The TE and TM waves can be classified due to the number of field maxima in the x and y direction:

 $TE_{nm}(H_{nm})$  and  $TM_{nm}(E_{nm})$ 

### Cut off wavelength

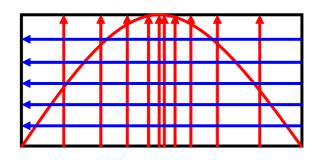
• In a rectangular waveguide only nm- modes below (above) a certain wavelength  $l_{cnm}$  (frequency  $n_{cnm}$ ) can propagate.

$$\lambda_{cnm} = \frac{2}{\sqrt{\left(\frac{n}{a}\right)^2 + \left(\frac{m}{b}\right)^2}} \qquad \nu_{cnm} = c \frac{\sqrt{\left(\frac{n}{a}\right)^2 + \left(\frac{m}{b}\right)^2}}{2}$$



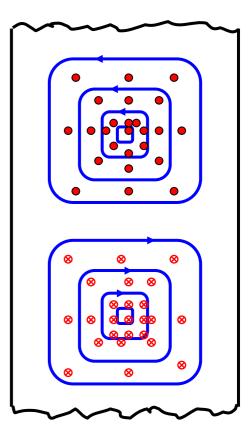
#### Rectangular Waveguides

• The mode with lowest frequency propagating in the waveguide is the  $TE_{10}$  ( $H_{10}$ ) mode.



Cutoff Frequency:  $n_{c10}$ =c/2a

E-Field H-Field





#### Waveguide Size for 1.3GHz

- Most common are 2:1 waveguides a=2b, for 1.3GHz the following waveguides would be appropriate
- WR650 (proposed for ILC) a=6.5inch b=3.25inch  $n_{c10}=908$ MHz
- WR770 a=7.7inch b=3.85inch  $n_{c10}$ =767MHz



### Attenuation of TE<sub>10</sub>

- Due to losses in the walls of the waveguides the wave is attenuated.
- The attenuation constant is:

$$\alpha[dB/m] = 0.2026 k_1 \frac{1}{b[cm]\sqrt{\lambda [cm]}} \frac{\frac{1}{2} + \frac{b}{a} \left(\frac{\lambda}{2a}\right)^2}{\sqrt{1 - \left(\frac{\lambda}{2a}\right)^2}}$$

 $k_1 = 1.00 \text{ Ag}, 1.03 \text{ Cu}, 1.17 \text{ Au}, 1.37 \text{ Al}, 2.2 \text{ Brass}$ 



# Phase constant and Impedance of TE<sub>10</sub>

$$\beta_g = \sqrt{k^2 - (\pi/a)^2}$$
 with  $k = 2\pi/\lambda$ 

• b<sub>g</sub> phase constant of the waveguide wave and k phase constant in free space

$$\lambda_g = 2\pi / \beta_g$$

- l<sub>g</sub> is the distance between two equal phase planes along the waveguide and is longer than l
- The impedance Z of the waveguide is

$$Z = \frac{377\Omega}{\sqrt{1 - \left(\frac{\lambda}{\lambda_{c10}}\right)^2}}$$

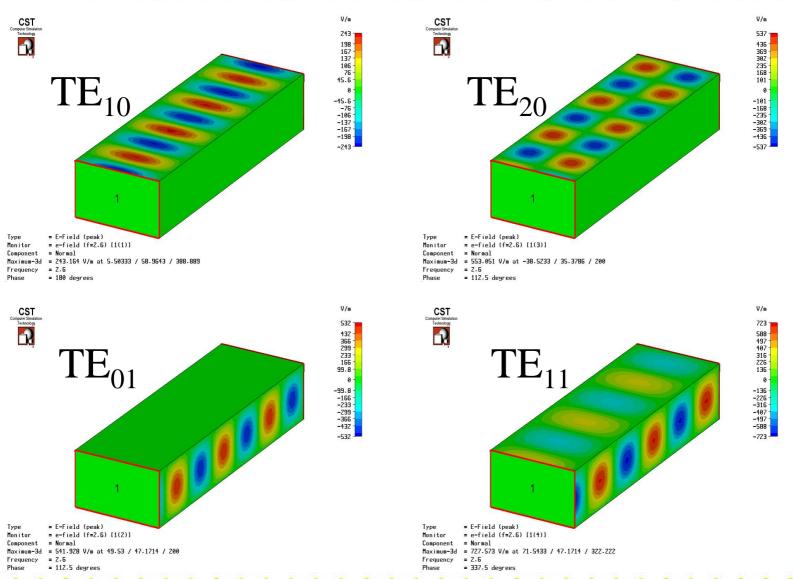
### Power in TE<sub>10</sub>

$$P_{RF} = 6.63 \times 10^{-4} a \left[ cm \right] b \left[ cm \right]^{\lambda} / \lambda_g E \left[ V / cm \right]^2$$

- The maximum power which can be transmitted theoretically in a waveguide of certain size a, b and wavelength l is determined by the breakdown limit  $E_{\text{max}}$ .
- In air it is  $E_{max}$ =32kV/cm and in SF6 it is  $E_{max}$ =89kV/cm (1bar, 20°C). Problem with SF6 is that although it is chemically very stable (1) it is a green house gas and (2) if cracked in sparcs products can form HF which is a very aggressive acid.
- The practical power limit is lower, typically 5-10 times lower, because of surface effects (roughness, steps at flanges etc.), dust in waveguides, huminity, reflections (VSWR) or because of higher order modes TE<sub>nm</sub>/TM<sub>nm</sub>. These HOMs are also generated by the power source. If these modes are not damped, they can be excited resonantly and reach very high field strength above the breakdown limit.

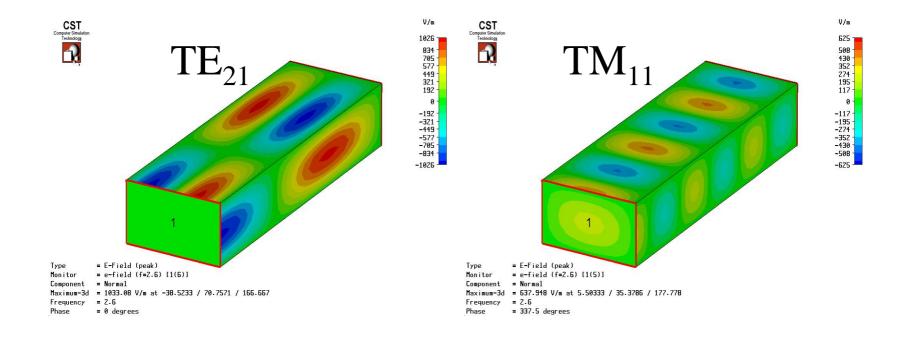


## Straight Waveguide (1)



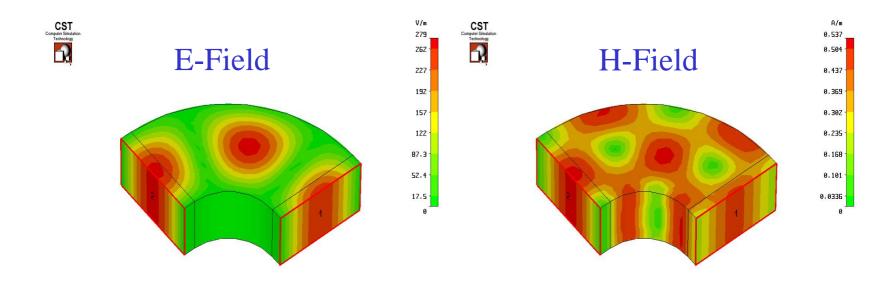


### Straight Waveguide (2)





#### **H-Bends**



= E-Field (peak) Туре Monitor = e-field (f=1.3) [1]

Component = Abs

Maximum-3d = 282.118 V/m at -55.9724 / 82.55 / 98.9501

Frequency = 1.3

= 157.5 degrees

= H-Field (peak) Туре Monitor = h-field (f=1.3) [1] Component = Abs

Maximum-3d = 0.552589 A/m at 66 / 61.9125 / 77

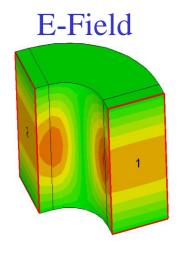
Frequency = 1.3

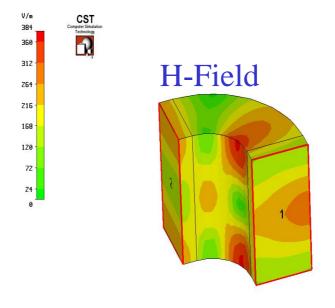
= 157.5 degrees

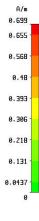


#### E-Bends









= E-Field (peak) Туре Monitor = e-field (f=1.3) [1]

Component = Abs

Maximum-3d = 386.366 V/m at 8.42857 / 82.55 / 25.2857

Frequency = 1.3

= 202.5 degrees

= H-Field (peak) Туре Monitor = h-field (f=1.3) [1] Component = Abs

Maximum-3d = 0.74572 A/m at 8.42857 / 148.59 / 33.7143

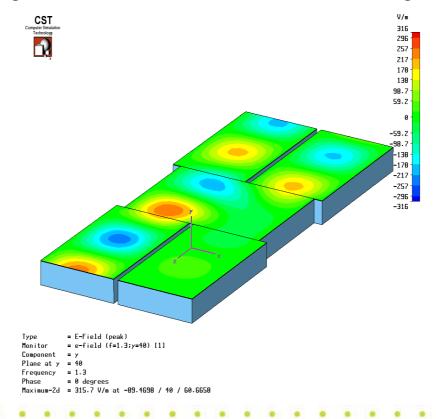
Frequency = 1.3

= 157.5 degrees



#### **Power Coupler**

- Power Coupler are used to couple out a certain amount of power from a main waveguide arm
- Hybrids, Magic Tees, Shunt Tees, Series Tees might be used



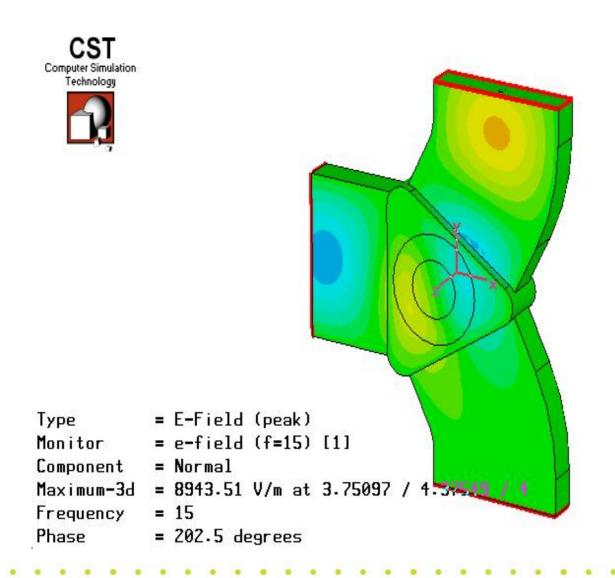


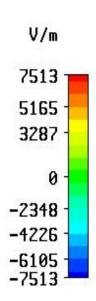
#### Circulator (1)

- A circulator is a device, which has an input port (1), output port (2) and load port (3). If power is entering (1) it is transferred to port (2), but if power is entering (2) it is transferred to (3) and than absorbed in a load.
- The ciculator protects the RF source from reflected power.
- Circulators make use of ferrite material in the waveguide which is premagnetized by an external magnetic field.
- The interaction of the H-vector of the RF field with the permanent magnets of the ferrites are responsible for the directive properties of a ciculator.
- The height in a circulator is reduced due to the ferrite plates. Therefore the breakdown limit and thus the power capability is reduced. In a WR650 waveguide and air it is ~500kW.



### Circulator (2)







#### Loads

- Loads absorb the power generated by an RF source
- Absorbing material can be ferrite, SiC or water.
- The amount of power reflected by a load is described by the VSWR defined as

$$VSWR = \frac{\left|E_f\right| + \left|E_r\right|}{\left|E_f\right| - \left|E_r\right|} = \frac{1 + \rho}{1 - \rho} \quad \text{and} \quad$$

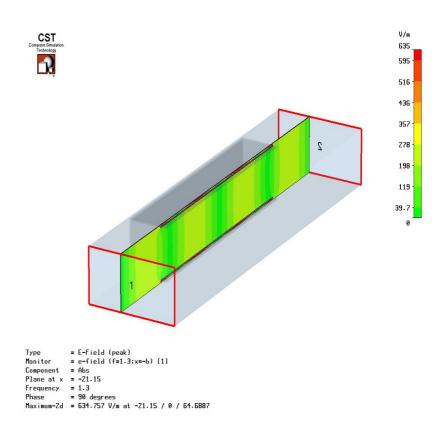
$$\rho = \frac{Z_L - Z}{Z_L + Z}$$
 With Z waveguide impedance of the waveguide and  $Z_L$  load impedance



### Phase Shifter

• By adjusting the dimensions of the waveguide e.g. the width a changes and therefore the phase constant changes.

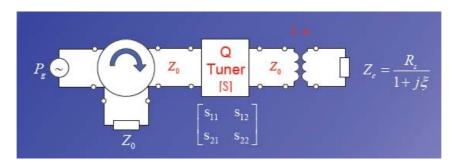
$$\beta_g = \sqrt{k^2 - (\pi/a)^2}$$





# Adjustment of $Q_{ext}(1)$

- The RF power required for a certain gradient of a superconducting cavity depends on the beam current and coupling between the cavity and waveguide.
- The coupling with the cavity may be changed by variation of  $Q_{ext}$ .
- The  $Q_L$  seen by the cavity is determined by the  $Q_{unloaded}$  and  $Q_{ext}$ .  $Q_{ext}$  is given by the load impedance  $Z_0$  plus variable coupling to this load.
- The Q<sub>ext</sub> can be adjusted by tuners like stub tuners, iris tuners, E-H tuners etc.





# Adjustment of $Q_{ext}(2)$

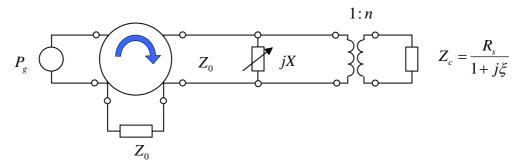


Figure 1: Equivalent circuit of cavity powered through a circulator with the variable obstacle (no moving along waveguide)

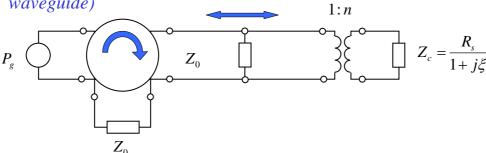


Figure 2: Equivalent circuit of cavity powered through a circulator with the fixed obstacle moving along waveguide

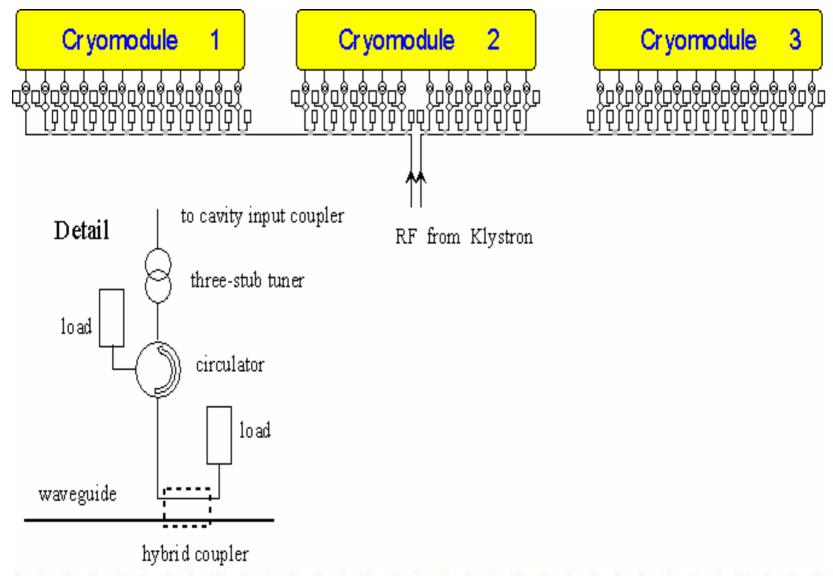


### Linear Distribution System (1)

- For TESLA a linear distribution system has been proposed
- Equal amounts of power are branched off from the main RF power waveguide
- Circulators in each branch protect the klystron from reflected power
- Stub tuners allow adjustment of phase and  $Q_{\text{ext}}$ , for the XFEL inductive iris tuners are proposed
- Alternative schemes have been proposed

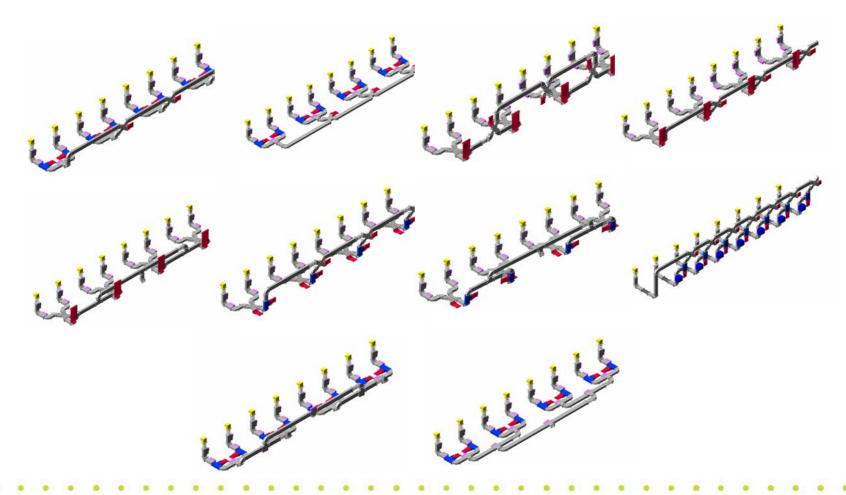


### Linear Distribution System (2)





# Alternative waveguide distribution schemes





## RF Waveguide Components

#### 3 Stub Tuner (IHEP, Bejing, China)



Changing phase, degree Impedance matching range Max power, MW

\* Zw - waveguide impedance

E and H Bends (Spinner)





0.4 Average power, kW 8 Min isolation at 1.3 GHz, dB >30 Max insertion loss at 1.3 GHz, dB ≤0.08 Input SWR at 1.3 GHz 1.1

WFHI 3-4

Circulator (Ferrite)

#### Hybrid Coupler (RFT, Spinner)

1/3Z<sub>w</sub> @3Z<sub>w</sub>



Directivity, dB Return loss, dB Coupling factor, dB 12.5; 12.0; 11.4; (due to tolerance overlapping only 13 different 10.7; 10.1; 9.6; coupling factors instead 18 are nessesary) 9.1; 8.5; 7.8; 7.0; 6.0; 4.8; 3.0 Accuracy of coupling factor, dB

RF Load (Ferrite)



WFHLL 3-1 Type Peak input power, MW 1.0 0.2 Average power, kW Min return loss at 1.3GHz, dB 32®40 Max VSWR at 1.3 GHz ■1.05 Max surface temperature, ∜T € 50 (for full average power)

#### RF Load (Ferrite)



Type	WFHL 3-1	WFHL 3-5
Peak input power, MW	2.0	5.0
Average power, kW	10	100
Min return loss at 1.3 GHz, dB	32÷40	32÷40
Max VSWR at 1.3 GHz	<1.05	<1.05
Max surface temperature, ΔT °C  (for full average power)	20	30
Physical length, mm	385	850



#### RF Waveguide Distribution Status

- New high power waveguide components for 1.3GHz have been developed in cooperation with industry or are standard of the shelves components
- Operation experience of 10 years from TTF
- Development of integrated components has been started (e.g. circulator with integrated load) to allow faster and more reliable installation