



# ILC Helical Undulator Development Update

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On behalf of Helical team

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## Collaboration members

### ASTECC:

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### DESY :

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(Moved on)

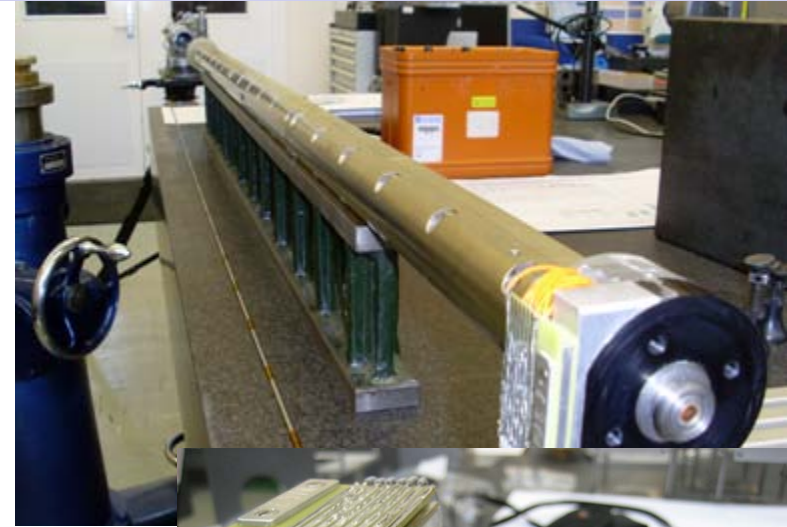


- Brief overview of the construction of the undulator
- Main parameters
- Testing in 4m cryomodule
- Work (EuCARD) on the use of Nb<sub>3</sub>Sn
- Nb<sub>3</sub>Sn magnet insulation issues
- Summary

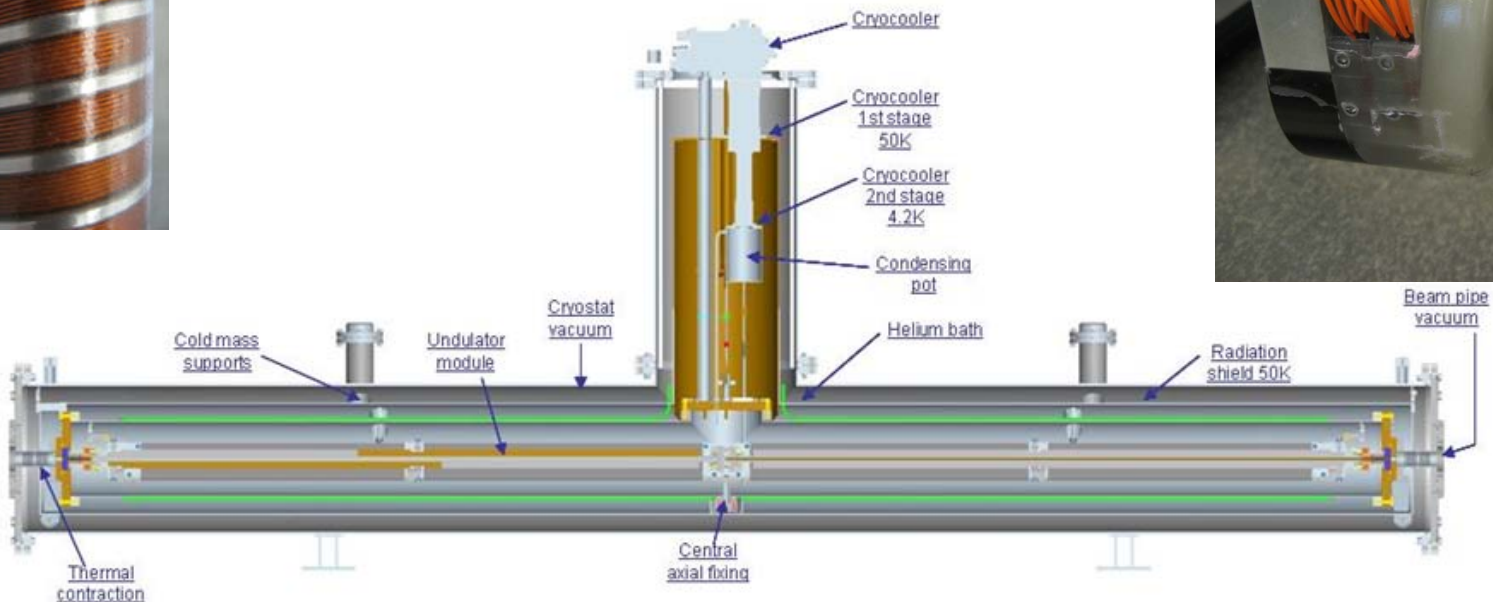


# 4 metre Cryomodule

- Two 1.7 metre helical undulator magnets have been successfully made using NbTi.
- Magnets positioned back to back in cryostat.
- Cryostat has been assembled and tested – was designed to be zero-loss



View of windings



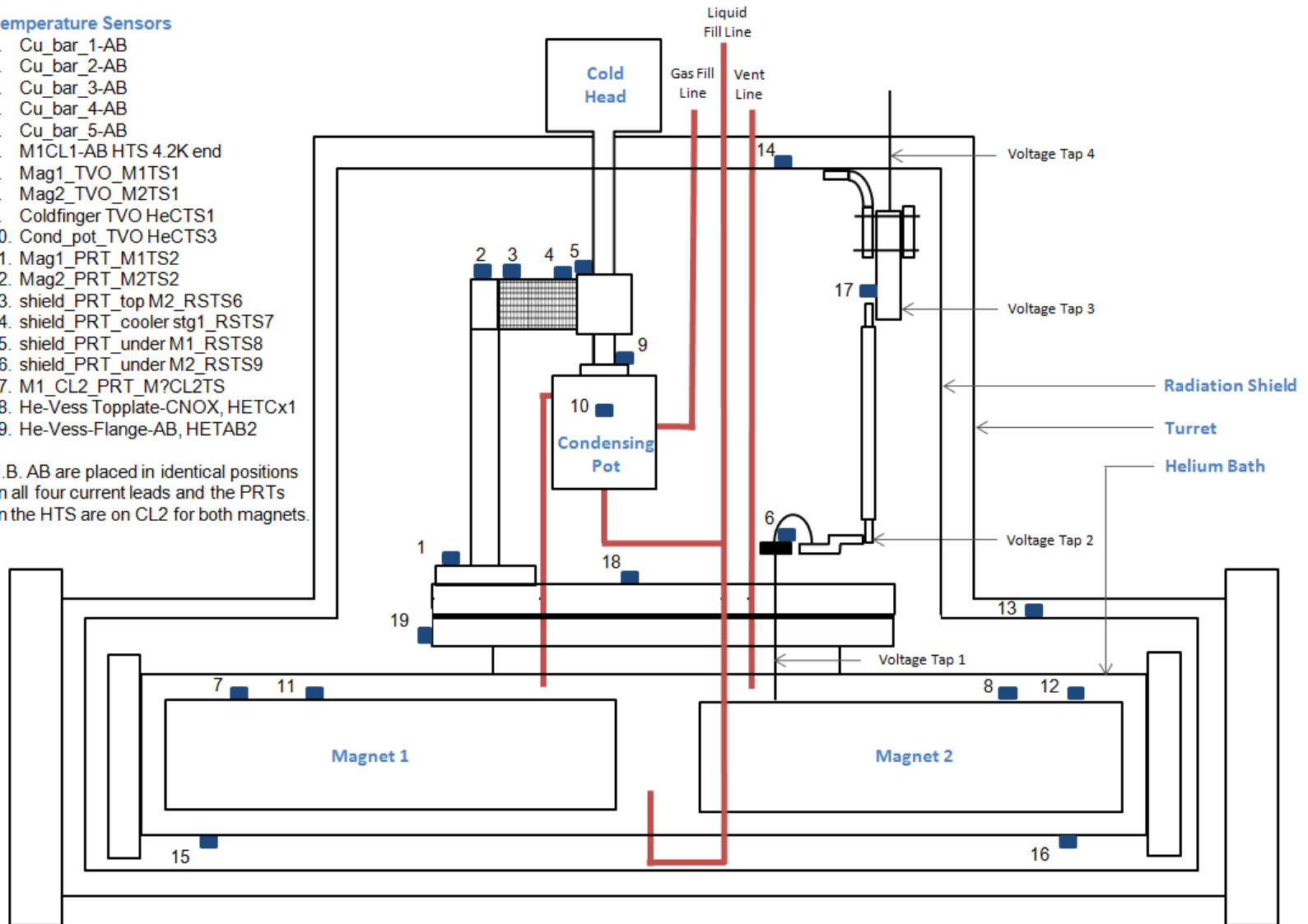


# Cryostat configuration

## Temperature Sensors

1. Cu\_bar\_1-AB
2. Cu\_bar\_2-AB
3. Cu\_bar\_3-AB
4. Cu\_bar\_4-AB
5. Cu\_bar\_5-AB
6. M1CL1-AB HTS 4.2K end
7. Mag1\_TVO\_M1TS1
8. Mag2\_TVO\_M2TS1
9. Coldfinger TVO HeCTS1
10. Cond\_pot\_TVO HeCTS3
11. Mag1\_PRT\_M1TS2
12. Mag2\_PRT\_M2TS2
13. shield\_PRT\_top M2\_RSTS6
14. shield\_PRT\_cooler stg1\_RSTS7
15. shield\_PRT\_under M1\_RSTS8
16. shield\_PRT\_under M2\_RSTS9
17. M1\_CL2\_PRT\_M?CL2TS
18. He-Vess Topplate-CNOX, HETCx1
19. He-Vess-Flange-AB, HETAB2

N.B. AB are placed in identical positions on all four current leads and the PRTs on the HTS are on CL2 for both magnets.





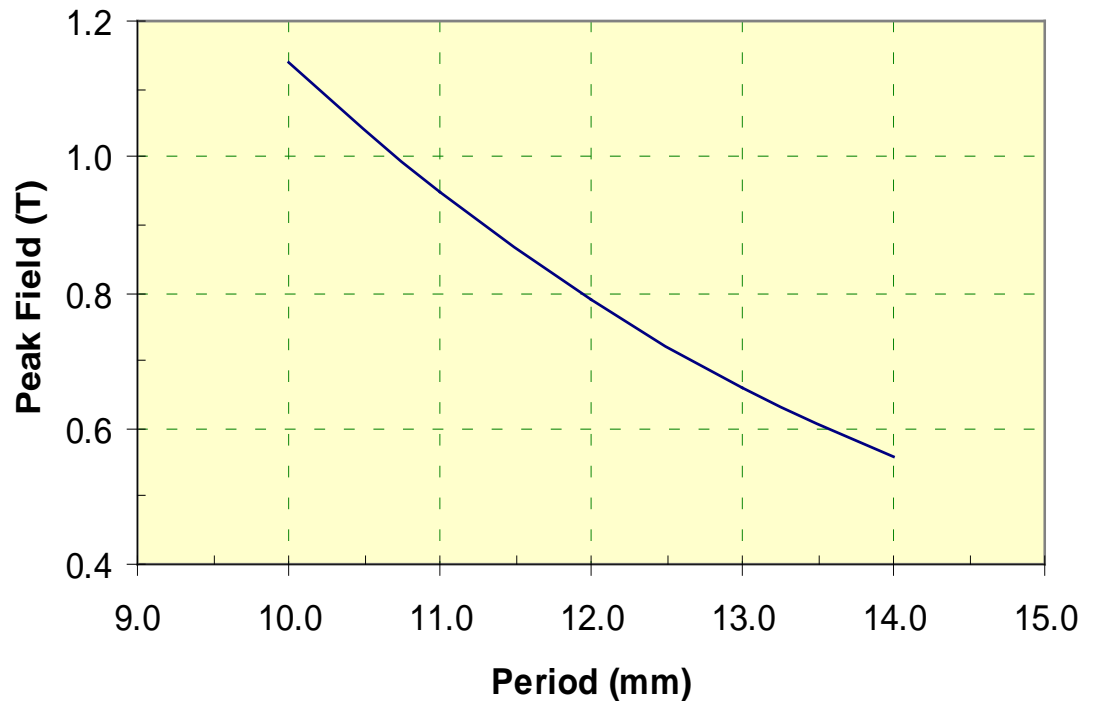
## Powering tests

- Magnet has achieved 215A (0.88T) and was stable
- Achieved 252 A but there was a problem with a burn-out of the current lead just below the top plate
- This is being repaired and the thermal issues are being addressed



## Initial specification

- Electron Drive Beam Energy 150 GeV
- Photon Energy (*1st harmonic*) 10.06 MeV
- Photon Beam Power 131 kW
- Total undulator length 100-200m
- Undulator Period 11.6mm
- Field on Axis 0.84 T
- Beam Stay clear 4.5mm dia





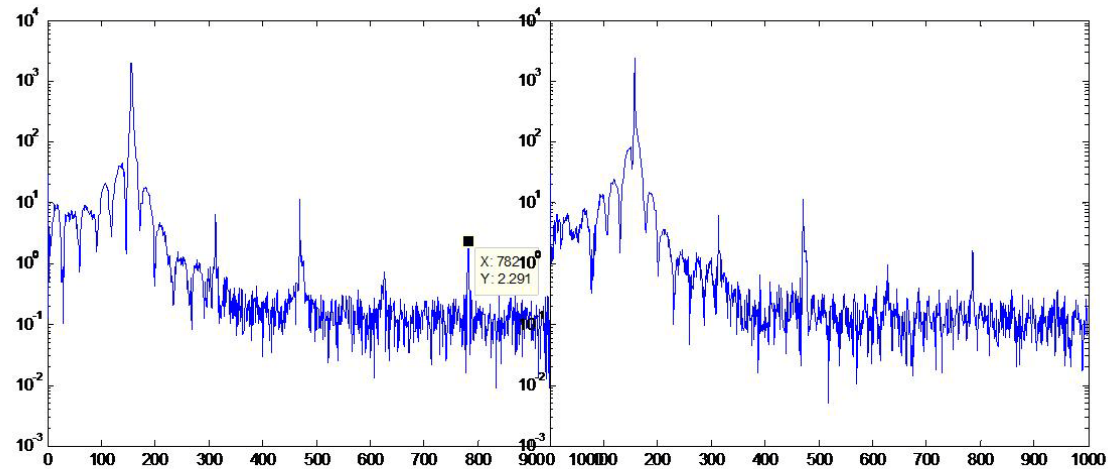
<b>Undulator Period</b>	<b>11.5 mm</b>
<b>Field on Axis</b>	<b>0.86 T</b>
<b>Peak field homogeneity</b>	<b>&lt;1%</b>
<b>Winding bore</b>	<b>&gt;6mm</b>
<b>Undulator Length</b>	<b>147 m</b>
<b>Nominal current</b>	<b>215A</b>
<b>Critical current</b>	<b>~270A</b>
<b>Magnetic bore</b>	<b>6.35mm</b>
<b>K</b>	<b>0.92</b>
<b>Manufacturing tolerances</b>	
winding concentricity	<b>+/-20um</b>
winding periodicity	<b>+/-50um</b>
Axial straightness	<b>+/-50um</b>
<b>NbTi wire Cu:Sc ratio</b>	<b>0.9</b>
<b>Winding block</b>	<b>9 layers</b>
	<b>7 wire ribbon</b>



# Helical beam purity

Field profile Fourier analysed and plotted on a semi-logarithmic scale – sinewave is very pure – these are the same magnet with data taken on two different runs.

Peak corresponds to 11.5mm period

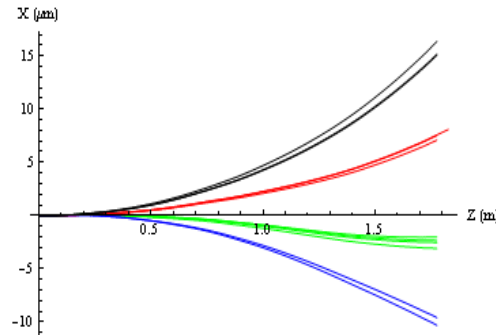


7<sup>th</sup> February

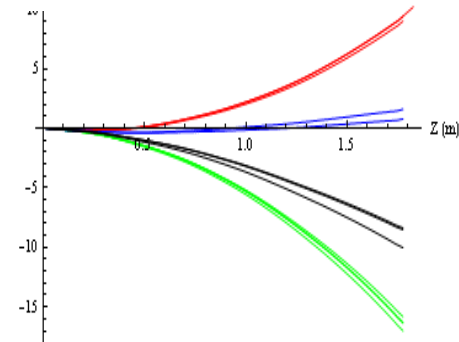
14<sup>th</sup> February

Particle trajectories using measured beam profile as calculated by SPECTRA as expected

R(um)



R(um)







## Power deposited from resistive wall heating

We need to know this for thermal reasons as we don't want the beam to quench the magnet

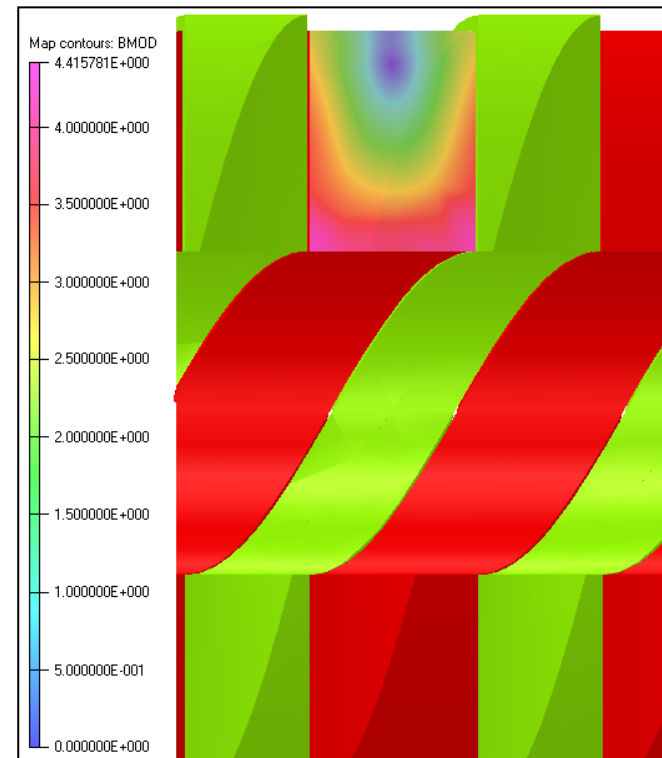
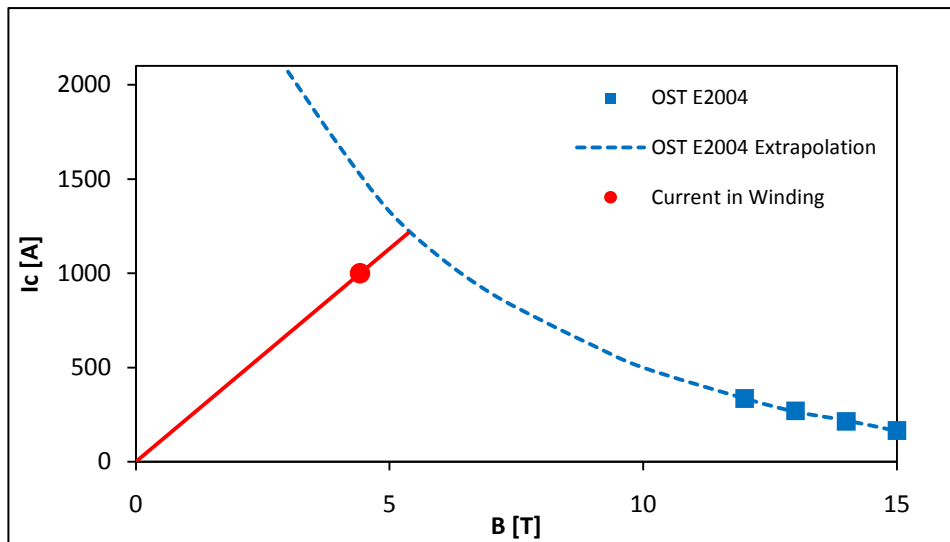
Parameter	Unit	1	2	3
Repetition rate	Hz	5	5	5
Bunch spacing	ns	150	300	500
Bunch length	$\mu\text{m}$	150	300	500
Particles/bunch	$10^{10}$	1	2	2
Peak Bunch Frequency	MHz	6.66	3.33	2
Bunches/pulse		5640	2820	2820
Fill factor	$\times 10^{-3}$	14.1	4.23	7.05
Power/metre	W/m	0.081	0.052	0.022

**We will be simulating this in the tests with a resistor chain in the bore to assess influence on magnet**



Wire in the undulator will see fields of around 4T – this is quite low for Nb<sub>3</sub>Sn and there was some concern that there may be stability problems due to flux jumping.

Stability can be improved by good stabilisation of the wire.



Field strength and  $I_c$  at 1 kA.  
Winding ID: Ø6.35 mm.  
Field on axis: 1.54 T.  
Peak field in conductor: 4.42 T.  
Operating at 82% of  $I_c$ .



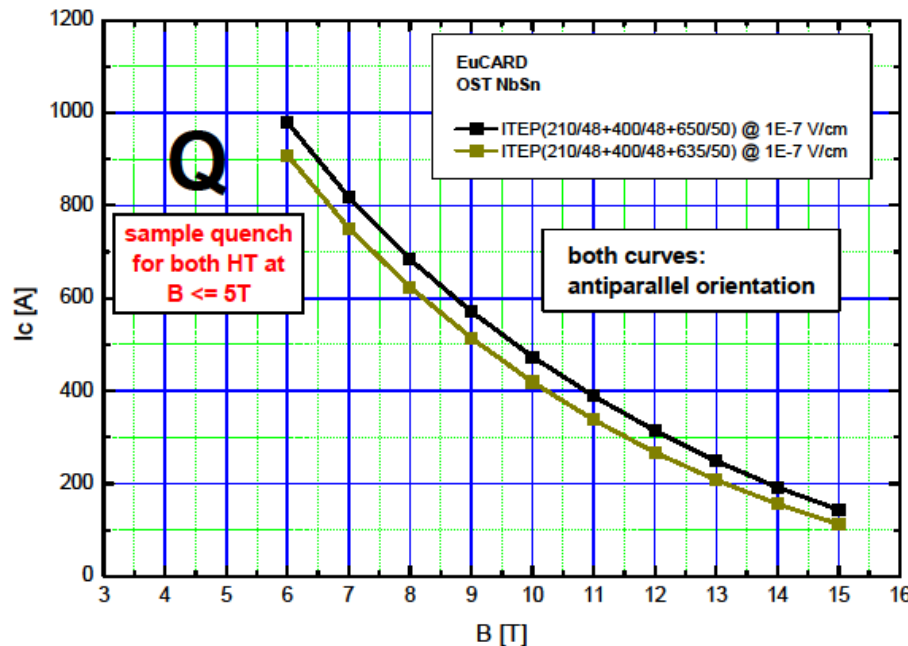
- The helical undulator design has a small winding groove due to the small repeat period.
- For large magnetic field, need maximum current density in winding, but many wires within winding to limit current in each wire (better for Cryogenics).
- Need Nb<sub>3</sub>Sn wire to have maximum performance commercially available with as small diameter as possible – there is a worry over low field stability (see later)
- Have purchased 1 km of Ø0.5 mm (Ø0.63 mm with glass braid) E2004 RRP wire from OST.
  - Recommended heat treatment:  
210°C/48hr + 400°C/48hr +  
650°C/50hr
  - Heat treatment can be modified to improve RRR of copper and hence the low field stability (tried 635/50).





We have had the superconducting wire tested at Karlsruhe Institute of Technology and found (as we feared) that it is unstable at low fields:

Results: Comparison HT "A" & "B" (ap-config)



We have two samples tested which have undergone different heat treatment to assess influence of stabilising copper RRR



Stability parameter gives an indication of how the wire will behave \*:

$$B = \frac{\mu_0 J_c^2 d^2}{4C(T_{bath} - T)} < 3$$

Still investigating this and struggling with some parameters but it looks as though the effective filament diameter is too large for use in a helical undulator. Looking for wire technology advances

Where

- J<sub>c</sub> is the critical current at T
- T is the transition temperature
- T<sub>bath</sub> is the bath temperature
- C is the volumetric heat capacity of the superconductor
- d is the filament diameter.

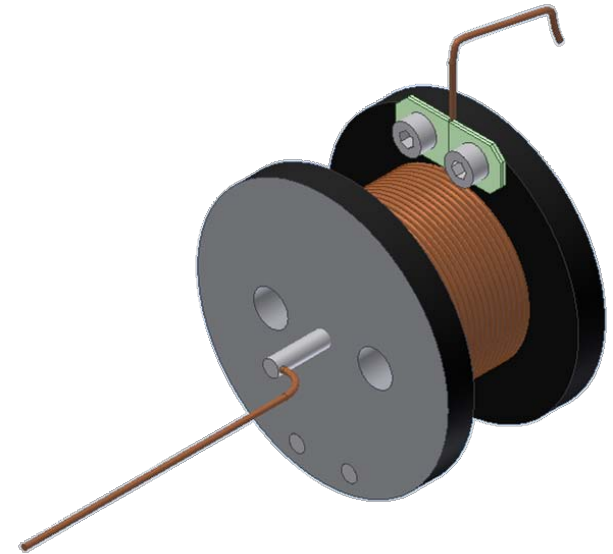
This parameter should be less than 3 for stability.



Ground plane insulation tests using a small bobbin and constant tension.

This type of test has several advantages:

- Known constant force between wire and specimen.
- Coil has much greater contact area than a single point so has more chance of finding pinholes or other weaknesses in coating.
- Build up of coating will be evident in corners.
- Abrasion between wire and specimen will demonstrate wear resistance of coating
- Relatively simple and cheap to make specimens.
- The geometry will show if there are any directional or shadow affects from coating processes.





Plasma Sprayed Alumina – this is a directional spray process that requires several sprays from different angles to get full coverage, this leads to a non-uniform coating build up (1.5mm ~ 10x specified thickness in places) and high stress within the Alumina causing it to fracture easily.

This is refractory paint basically Zirconia + a binder – a lot less of the build up problems but very little wear resistance and comes off in critical places during winding



Diamond Like Carbon – good locally but seemed to have pinholes (maybe due to poor surface preparation) so that globally it was shorting.

Development programme is continuing.....



Where we are:

- Results from the tests on the 4m helical look good
- Working to address minor issues to achieve zero loss in cryostat
- Planning tests to look at influence of wakefield heating on the magnet
  
- Nb<sub>3</sub>Sn development not looking too promising because of low field stability issues
- Insulation system development continuing – important for a number of projects
- Vital that it is thin for the use of Nb<sub>3</sub>Sn in the helical otherwise advantage over NbTi is quickly lost





**END**