

Comparison of Tuner Performance in S1-G Cryomodule

Rocco Paparella,
on behalf of S1-Global team

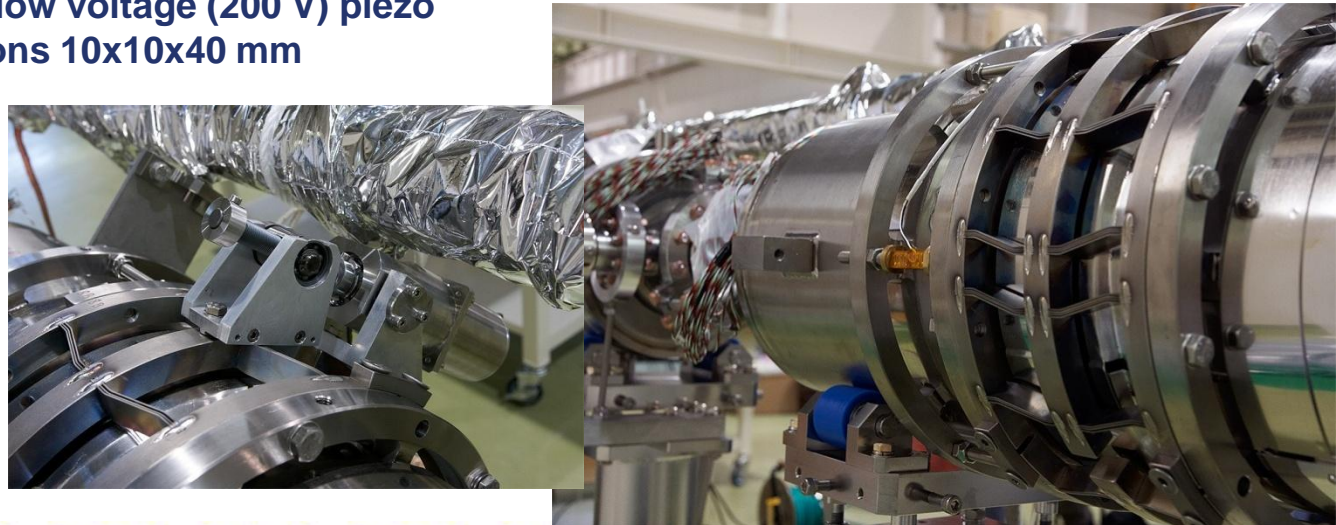
Outline of the talk

- Tuning systems installed in S1-Global:
 - **Rationales and details**
- Low power CW cold tests:
 - **Static tuning capabilities**
 - **Dynamic tuning capabilities**
 - **Spectral analyses**
- Pulsed high power cold test:
 - **Measurement of dynamic LFD**
 - **LFD compensation with FNAL Piezo Control System**
 - **LFD compensation with KEK Piezo Control System**
- **Conclusions**



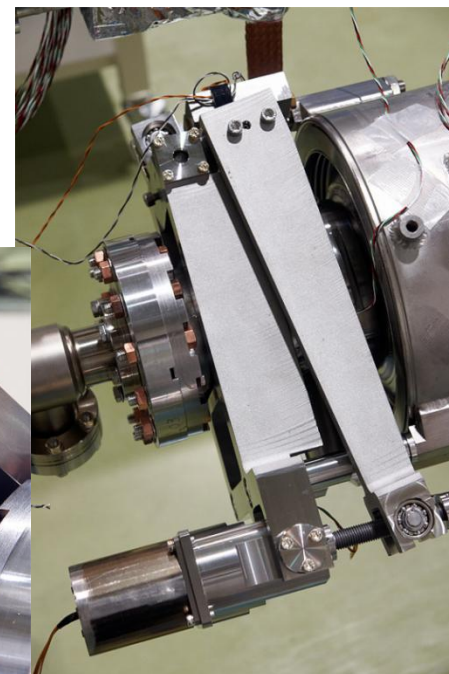
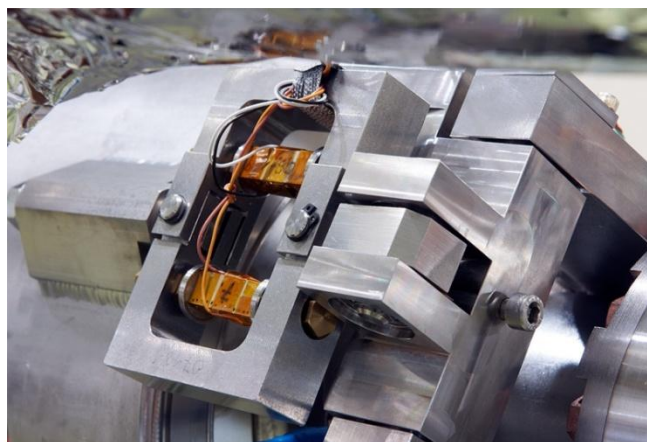
Tuning systems in details: FNAL/INFN cavity units

- Blade Tuner rationales:
 - Designed to be as light and as compact as possible
 - Coaxial to the cavity, tuning action is transmitted to cavity through deformation of thin blades to minimize backlash or free play in the system.
 - Piezo action is in series to the tuner one, designed to achieve the highest possible efficiency in transferring the stroke to the cavity
- FNAL/INFN S1-Global cavity units:
 - AES004 (C1) and ACC011 (C2) TESLA cavities
 - Helium tank from FNAL with specific design for coaxial tuner developed for CM2 at ILC-TA
 - Blade Tuner coaxial unit from INFN
 - Phytron stepper motor drive unit and Harmonic Drive gear from FNAL
 - 2 Noliac multilayer low voltage (200 V) piezo actuators, dimensions 10x10x40 mm



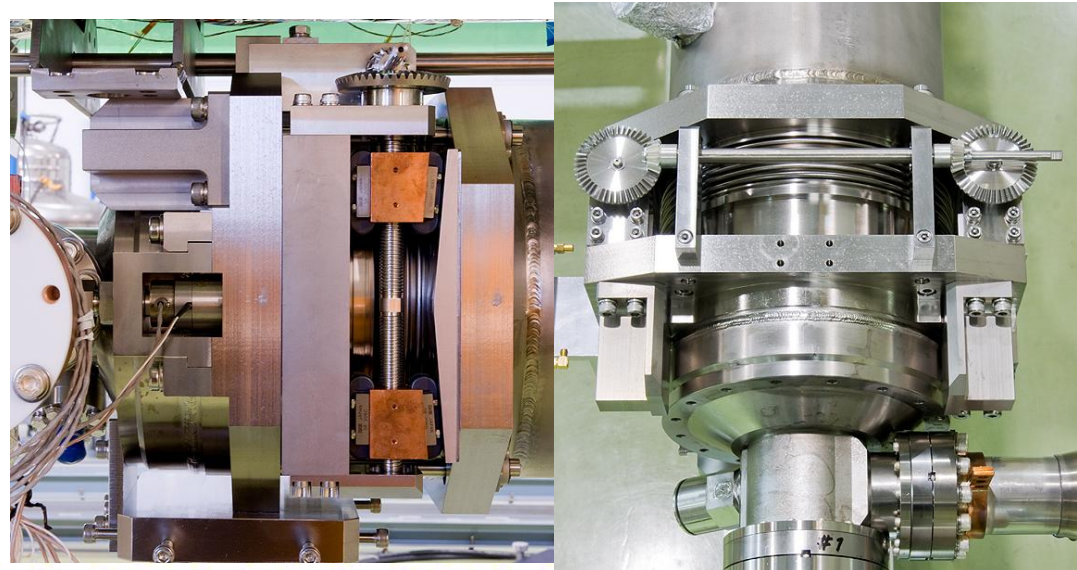
Tuning systems in details: DESY cavity units

- DESY/Saclay tuner rationales:
 - Affordable and well-known, basically in use since TTF. Originally designed at Saclay and then developed at DESY.
 - Installed at the cavity side opposite to coupler, tuning action is transferred to cavity through a compact double leverage system.
 - Piezo are installed in a preloading frame on one side, their action is transferred through the leverage mechanics.
- DESY S1-Global cavity units:
 - Z108 (C3) and Z109 (C4) TESLA cavities, with standard DESY/FLASH helium tank
 - Lateral DESY/Saclay tuner, latest XFEL-like model
 - Phytron stepper motor drive unit and Harmonic Drive gear from DESY
 - 2 Noliac low voltage (200 V) multilayer actuators



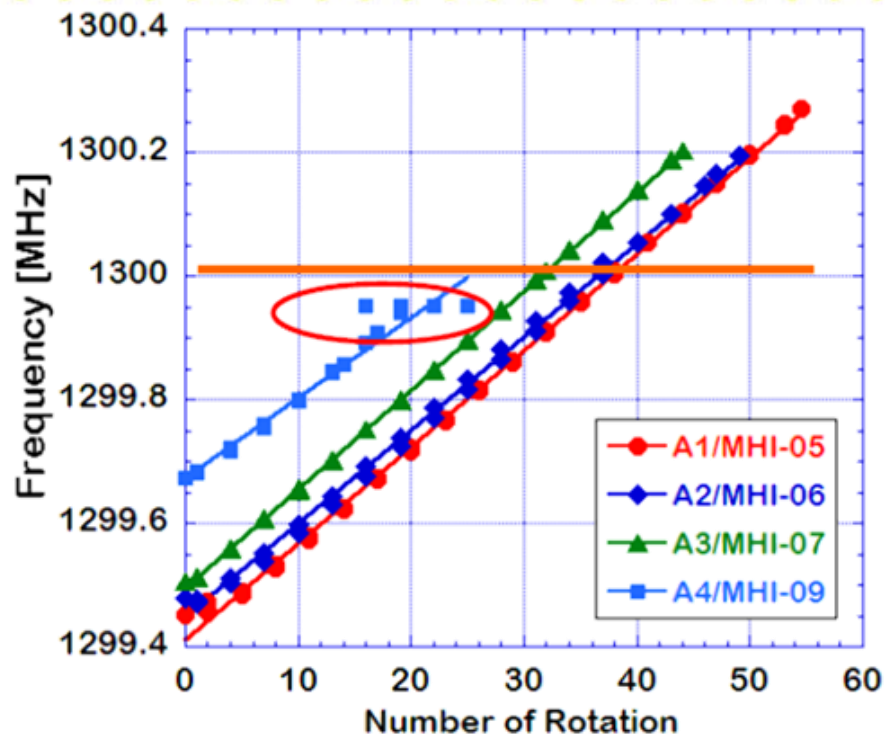
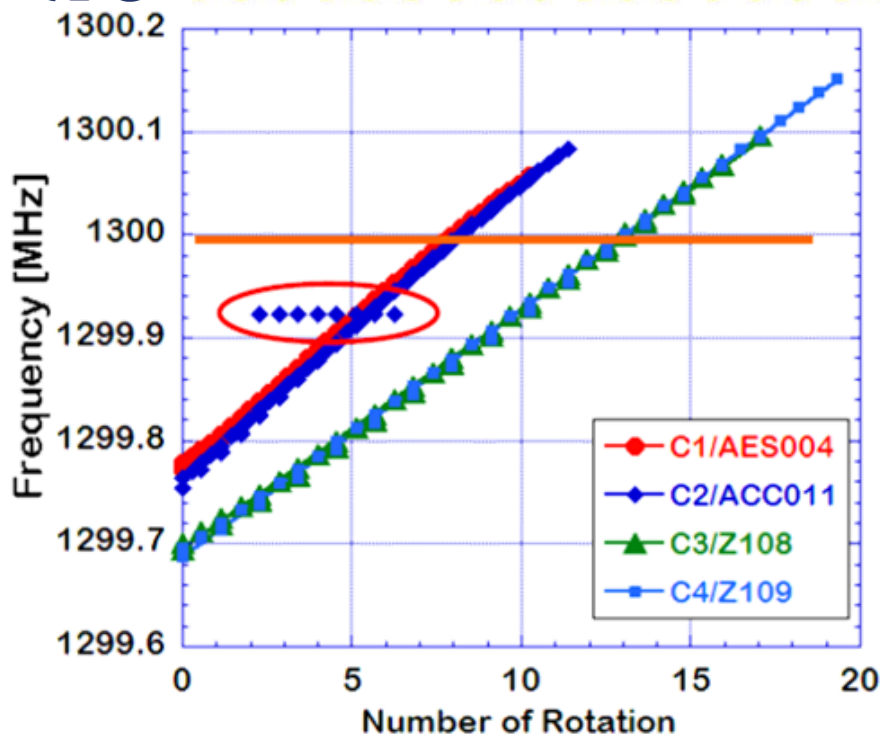
Tuning systems in details: KEK cavity units

- KEK Slide-Jack Tuner rationales:
 - Stiff design specifically developed for KEK TESLA-like cavities
 - The tuning driving action is generated outside the vessel and transferred to a feed-trough shaft: no motor units is required to be install inside the module.
 - The longitudinal strain is generated through rolling elements sliding on a sloping surface
 - One single piezo acts in series to the tuner and is installed on the fixed side
- KEK S1-Global cavity units:
 - KEK TESLA-like cavities: MHI05 (A1), MHI06 (A2), MHI07 (A3) and MHI09 (A4)
 - For A1 and A2, helium tank with bellow between pads and Slide-Jack Tuner installed as middle tuner
 - For A3 and A4, helium tank with bellow at coupler side and Slide-Jack Tuner installed as lateral tuner outside pads.
 - Tuner is driven by a stepping motor drive unit through a drive shaft.
 - One high voltage (1000 V limited to 500 V), few-layer piezo stack from PiezoMechanik.
Dimensions: 35 mm diameter and 50 mm length.





Static tuning range at cold

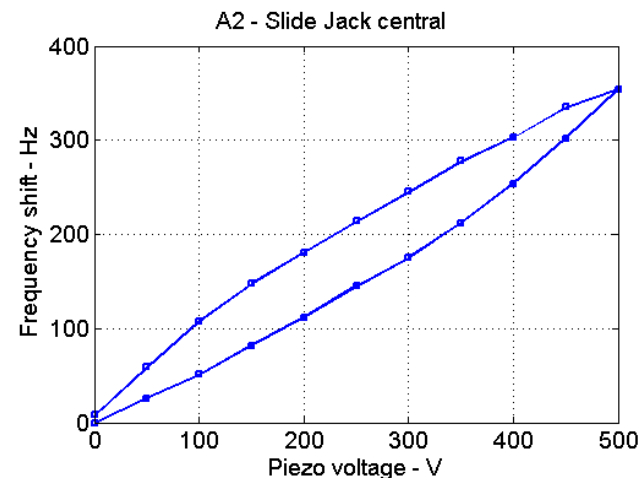
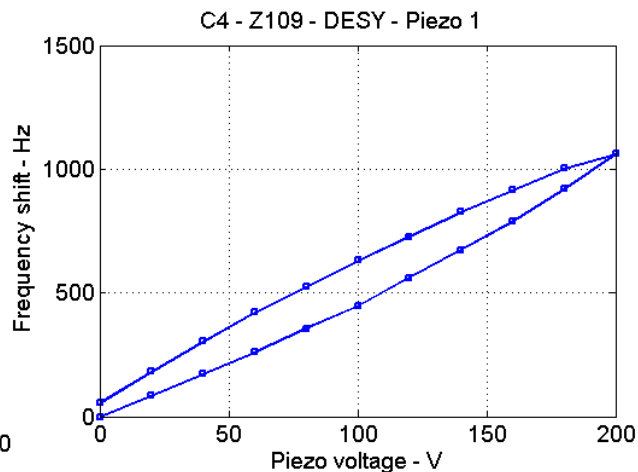
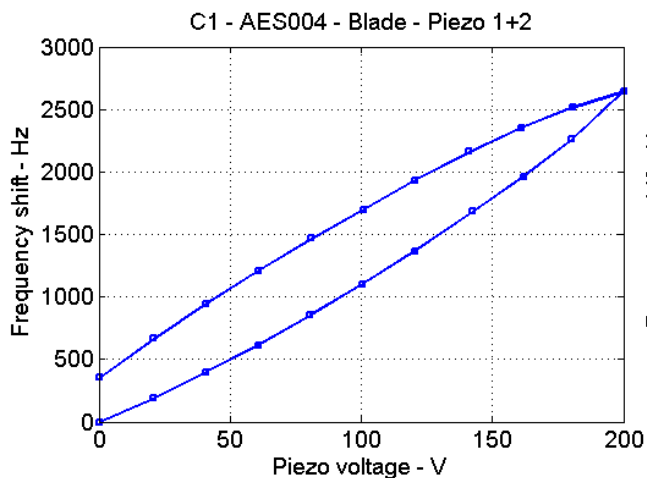


	Blade Tuner (C2)	DESY tuner (C4)	Slide-Jack tuner (A1)
Coarse tuning range measured (expected value)	330 kHz 12/22 turns (600 kHz)	450 kHz 19/23 turns (500 kHz)	800 kHz 54/60 turns (900 kHz)
Tuning sensitivity at 1.3 GHz (expected value)	25 kHz/spindle turn 1.4 Hz/step (1.5 Hz/step)	20 kHz/spindle turn 1.1 Hz/step (1 Hz/step)	15 kHz/spindle turn 3 Hz/step (3 Hz/step)

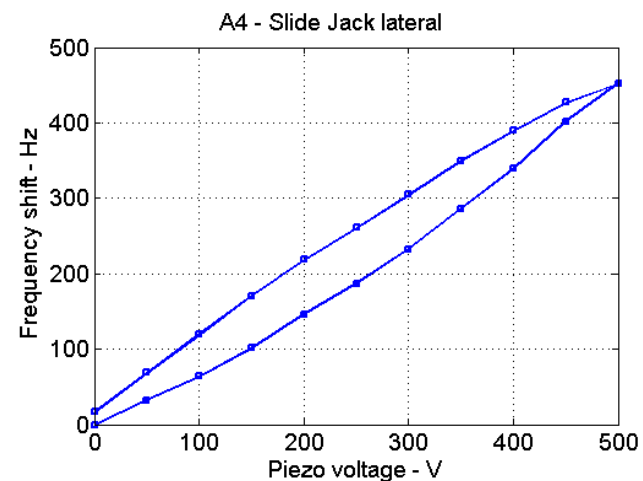
- Issue with Blade Tuner in cavity C2:
 - during the second cycle the frequency resulted to be stacked at 1299.92 MHz.
- Issue with Slide-Jack Tuner in A4:
 - Failure in the driving shaft joint and frequency stacked at 1299.95 MHz.
- Under investigation ...



Selection of piezo DC response curves



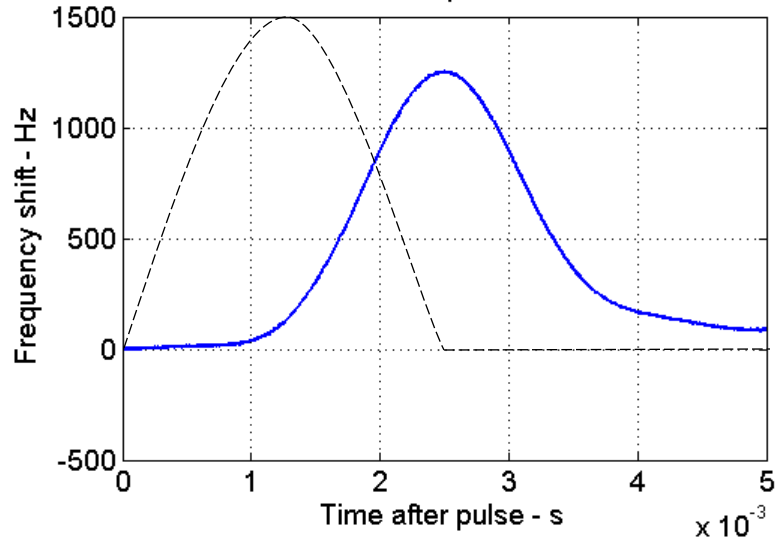
Cavity	Maximum nominal piezo voltage [V]	Piezo configuration	Maximum applied voltage [V]	Frequency shift [Hz]
C1-Blade	200	1+2	200	2650
C2-Blade	200	1	200	610
C3-DESY	200	2	200	1010
C4-DESY	200	1	200	1060
A1-S.J cent.	1000	-	500	190
A2-S.J cent.	1000	-	500	350
A3-S.J lat.	1000	-	500	210
A4-S.J lat.	1000	-	500	450



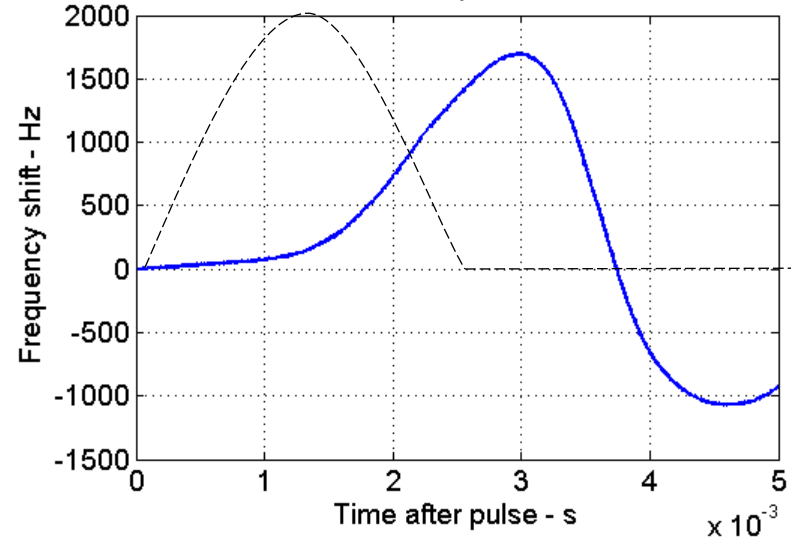


Selection of SIN pulse responses

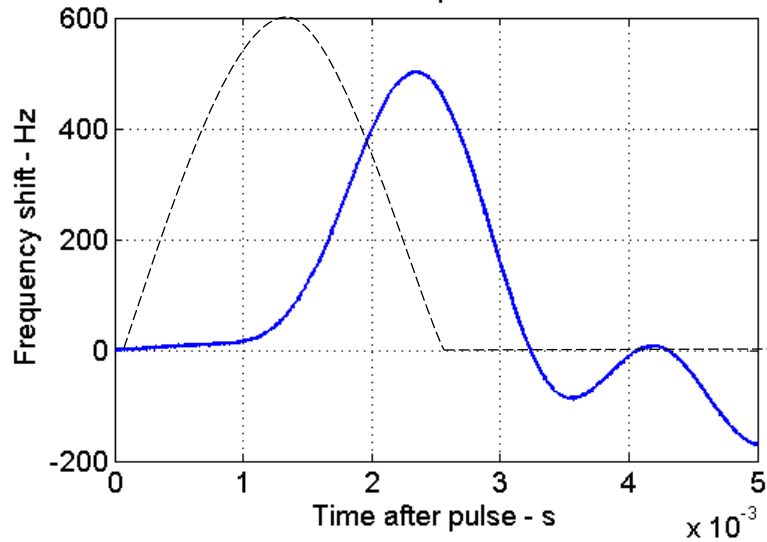
C1 - AES004 - Blade - Piezo 1+2
135V pulse



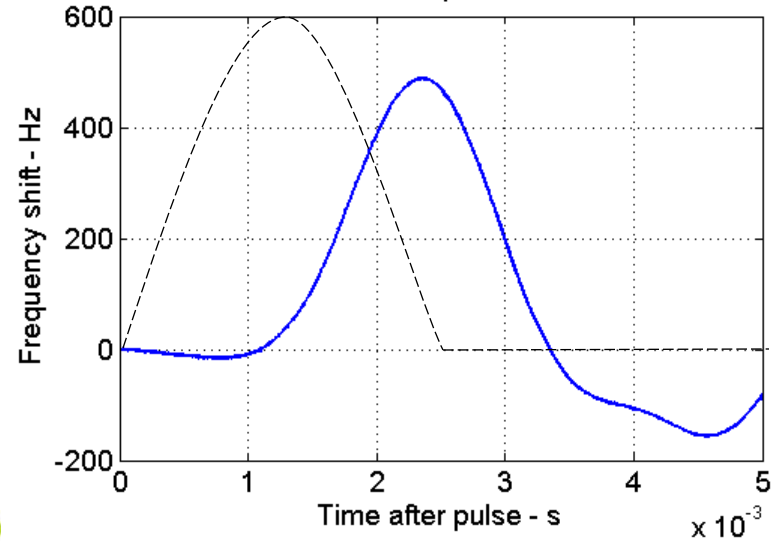
C4 - Z109 - DESY - Piezo 1
170V pulse



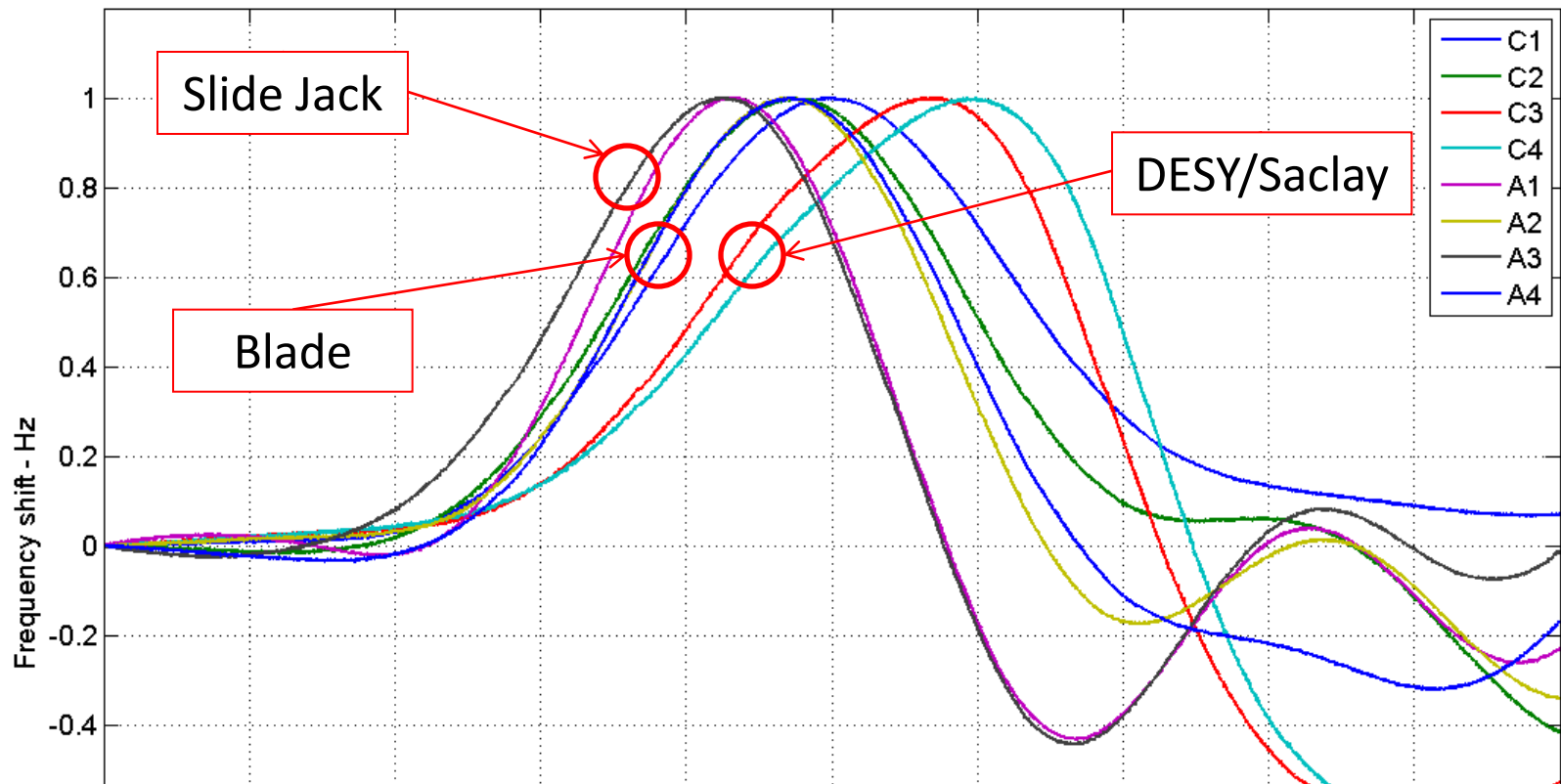
A2 - Slide Jack central
470V pulse



A4 - Slide Jack lateral
470V pulse



SIN pulse response - All tuners with scaling factor

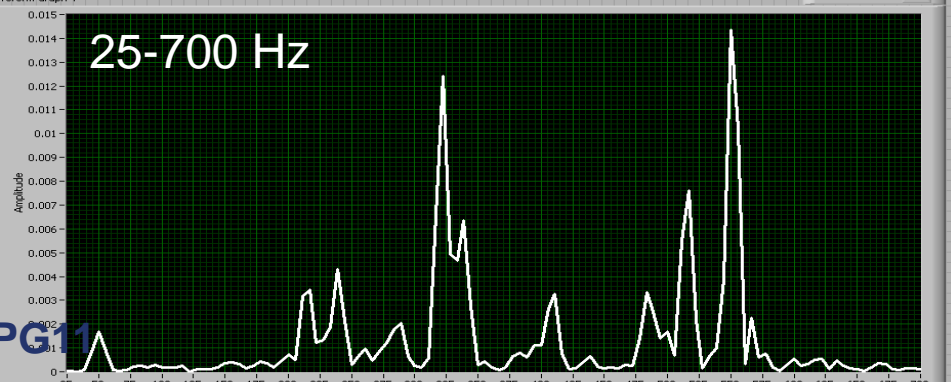
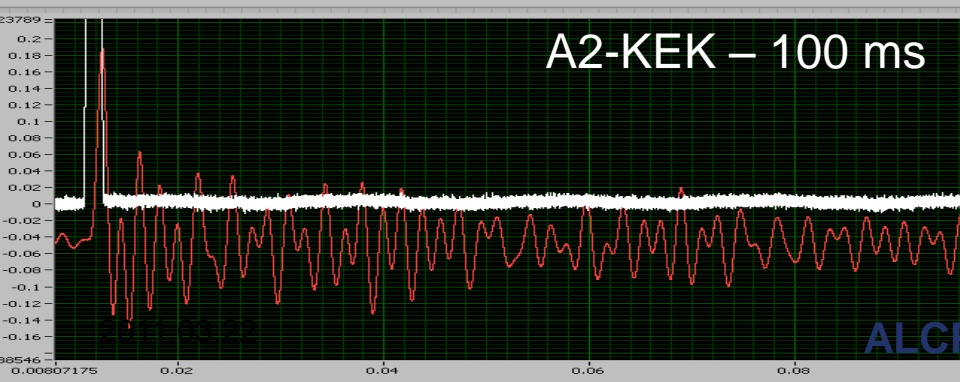
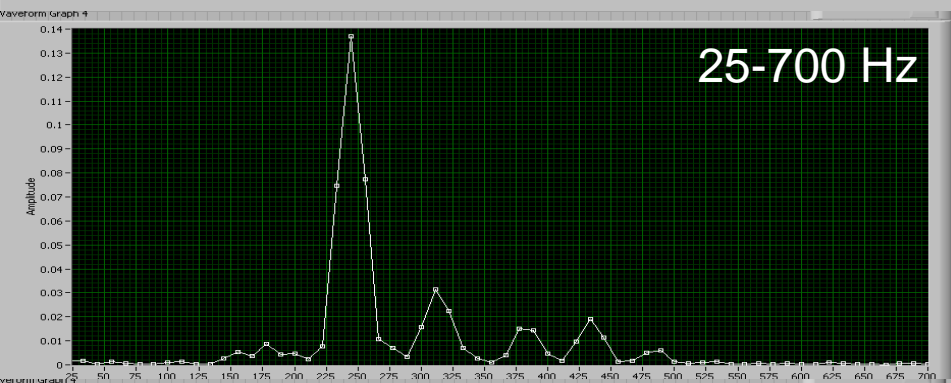
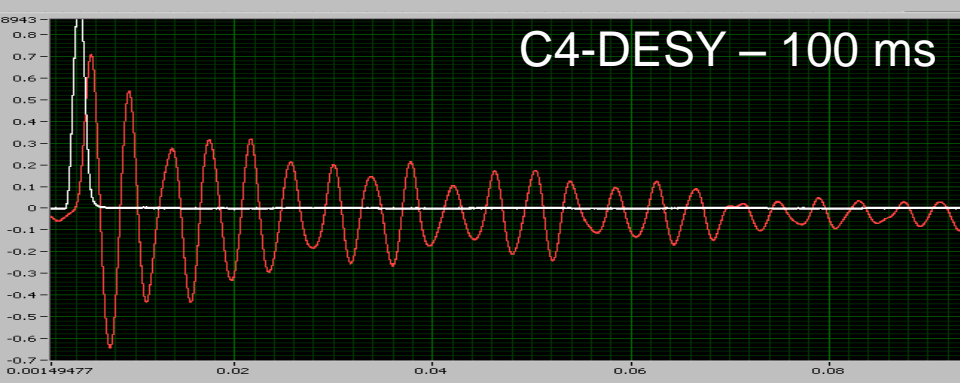
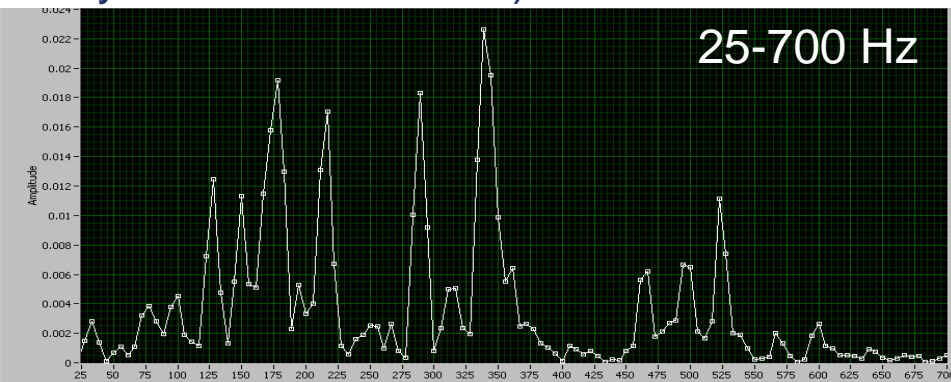
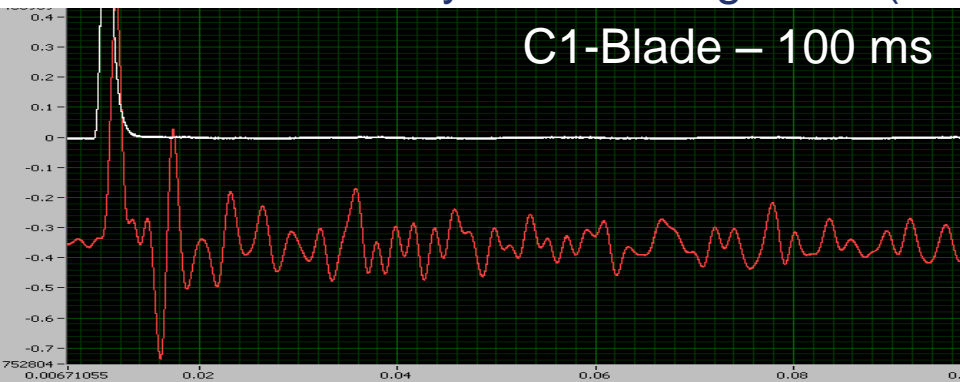


Cavity-Tuner	Max. piezo voltage [V]	Load C at 2 K [μ F]	Piezo Config.	SIN pulse amp. [V]	Max. Freq. shift in 1 ms [Hz]	Best lead from pulse start [ms]	Dyn. over Static detuning ratio
C1-Blade	200	4.1	1+2	135	1040	1.31	0.6
C2-Blade	200	3.9	1+2	100	590	1.24	1
C3-DESY	200	2.0	2	180	1100	1.58	1.2
C4-DESY	200	1.9	1	170	1170	1.64	1.3
A1-S.J cent.	1000	0.19	-	470	270	1.10	1.5
A2-S.J cent.	1000	0.21	-	470	450	1.26	1.4
A3-S.J lat.	1000	0.20	-	470	270	1.03	1.3
A4-S.J lat.	1000	0.21	-	470	450	1.22	1.1



Spectral analyses

On a larger time scale, piezo response analyses reveal dynamics of different cavity systems through FFT (courtesy of Y. Pischalnikov):





Comments on low power CW tests

- Piezo issues in C2:
 - Severe lack of mechanical coupling on both piezo
 - Piezo 2 discharging at lower voltage, not seen at RT.
 - Puzzling scenario: possibly correlated to static tuning failure? To be investigated.
- Assuming DESY design as a reference, the other two rely on different design concepts:
 - **“Small external stiffness guideline” for the Blade Tuner:**
 - Simple and light cavity constraints (i.e. end cones), and therefore the same for the tuner
 - achieve a large LFD compensation capability as required
 - **“High external stiffness guideline” for the Slide-Jack Tuner:**
 - Strong and stiff cavity constraints, and therefore the same for the tuner
 - Minimize the amount of LFD to be compensated
- Collected data set is fully consistent with the scenario previously described:
 - **“Soft” Blade (and DESY actually) units systems act as low-bandwidth systems, with dominant modes placed at lower frequency and therefore longer rise-time.**
 - **“Stiff” KEK units act as high-bandwidth systems, with dominant modes at higher frequency and shorter rise-time.**
 - **Very large DC stroke for the Blade Tuner piezo system (C1). This does not lead to equivalently high dynamic tuning capabilities. Lower static-to-dynamic detuning ratio is due to the very small overshooting.**



Resuming all LFD measurements

- RF setup:
 - 0.54 ms rise-time (QL=2.4E+6)
 - 1.0 ms flat-top
 - 5 Hz repetition rate
- The K_{LFD} parameters:
 - K_{LFD} computed along the full pulse
 - K_{LFD}^{RS} computed along the rise-time
 - K_{LFD}^{FT} computed along the flat-top

$$\Delta f = (f_{t1} - f_{t0}) = -k \cdot E_{acc}^2$$

$$[K] = \left[\frac{Hz}{\left(\frac{MV}{m}\right)^2} \right]$$

	FNAL tests			KEK tests		
	K_{LFD}	K_{LFD}^{RS}	K_{LFD}^{FT}	K_{LFD}	K_{LFD}^{RS}	K_{LFD}^{FT}
C1-Blade	0.95	0.54	0.41	0.90	0.46	0.43
C2-Blade	0.75	0.38	0.37	0.83	0.31	0.51
C3-DESY	1.12	0.50	0.62	1.22	0.49	0.73
C4-DESY	1.14	0.50	0.64	1.00	0.41	0.59
A1-S.J cent.				0.70	0.56	0.14
A2-S.J cent.	0.72	0.50	0.22	0.66	0.49	0.17
A3-S.J lat.	0.70	0.60	0.10	0.69	0.55	0.14
A4-S.J lat.				0.79	0.50	0.29

Comments:

- Data are correctly correlated and coherent
- The same sharp harmonic response observed during CW test in DESY systems is affecting also now its behavior: higher K_{LFD} due to large overshooting!
- The very low K_{LFD}^{FT} for KEK cavity is clear a proof of the higher system stiffness
- The K_{LFD}^{RS} is remarkably similar over different tuners. This is possibly the results of two opposite effects: Slide-Jack tuner has lower detuning but shorter rise time so the response is stronger at the beginning of the pulse.



FNAL's Piezo Control System

FNAL built and deliver to KEK LFD Compensation system:

Hardware:

1,3GHz → 13MHz receivers (for cavities RF signals),

100MHz ADC for cavities RF signals,

PXI DAQ system (Processor & FPGA),

HV Piezo Drivers.

Software:

Matlab, LabView, FPGA codes.

Algorithm:

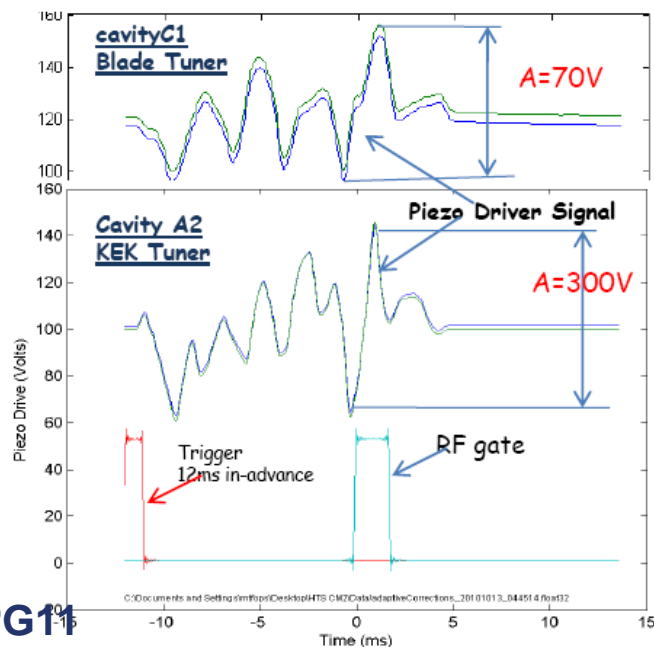
FNAL's Adaptive LS LFD Compensation Algorithm
(developed by Warren Schappert)

FNAL Adaptive LS LFD Compensation

Algorithm:

- Able to maintain flat cavity phase during both part of part of RF pulse "fill" and "flattop";
- An adaptive version of the LS procedure implemented on the FNAL HTS Piezo Control System for routine Cavity/Tuner testing (and will be part of NML -CM1 piezo control instrumentation);
- During operation LS algorithm able to automatically compensate LFD as cavity was ramped up from 15 MV/m to 32 MV/m and back up again;

Piezo Impulse Calculated by LS LFD algorithm





FNAL Piezo Control System

Selected material from a review of system and results from Yuriy Pischalnikov (FNAL)

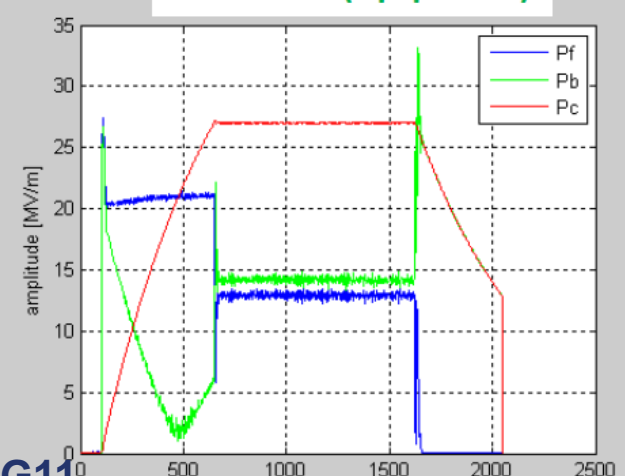
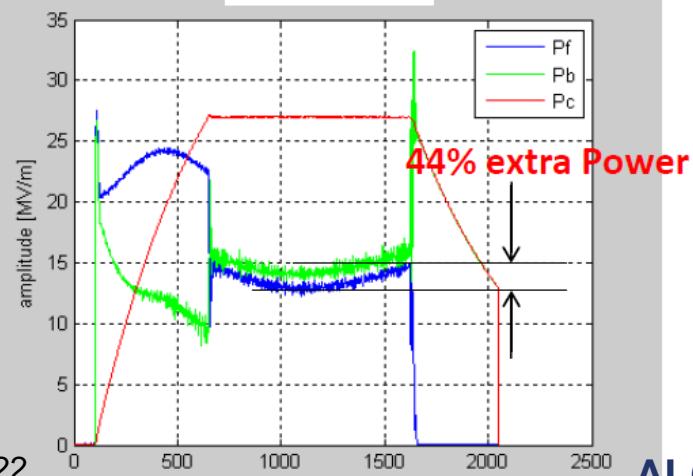
C1(AES04)- FNAL/Blade Tuner Cavity
Eacc=27MV/m, RF feedback ON
by FNAL Piezo Control System



PIEZO OFF



PIEZO ON (Vp-p=90V)





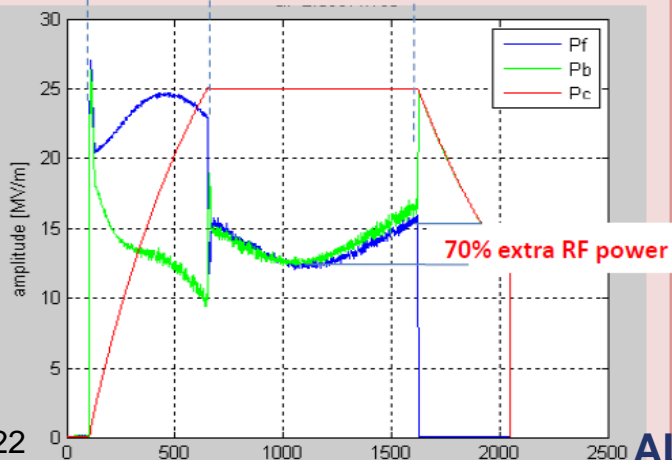
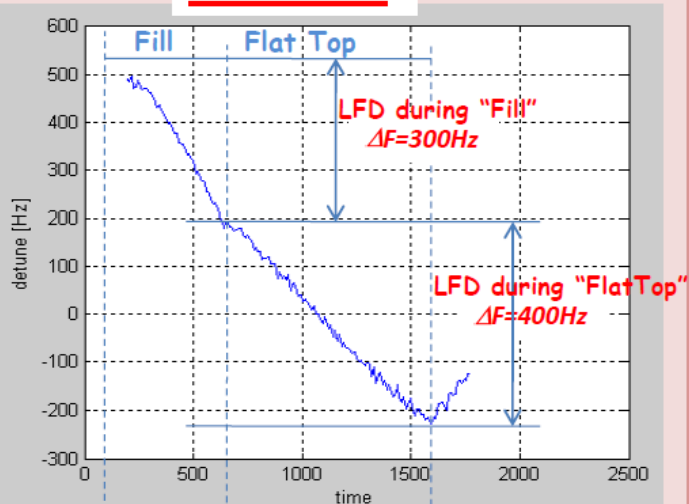
FNAL Piezo Control System

Selected material from a review of system and results from Yuriy Pischalnikov (FNAL)

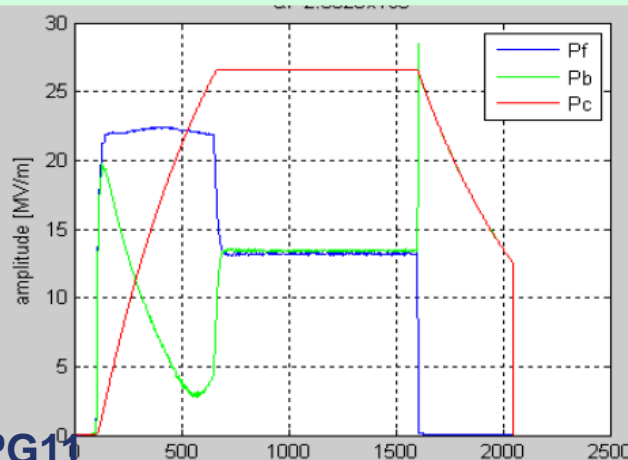
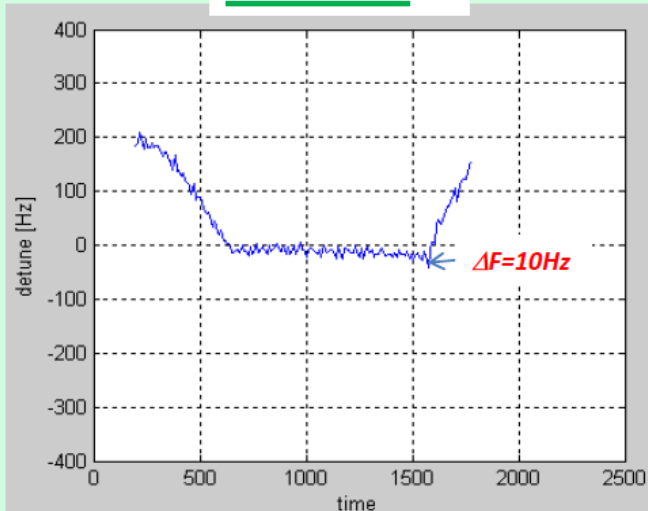
C4-DESY Cavity/Tuner System LFD at $E_{acc}=25\text{MV/m}$

RF feedback ON; LFD Compensation "FlatTop" only

Piezo OFF



Piezo ON

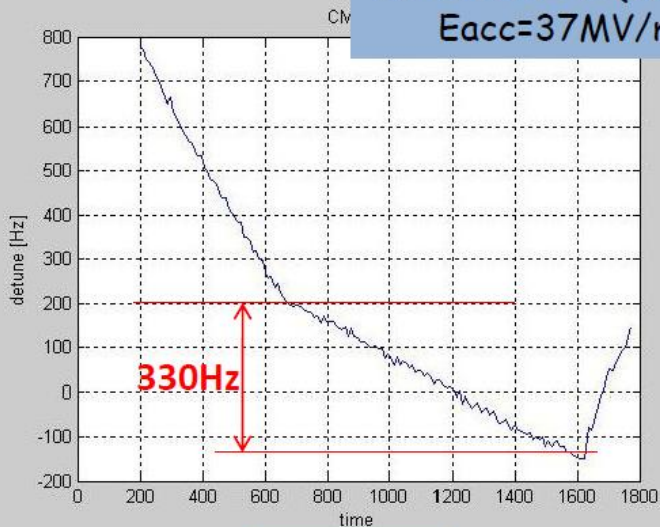




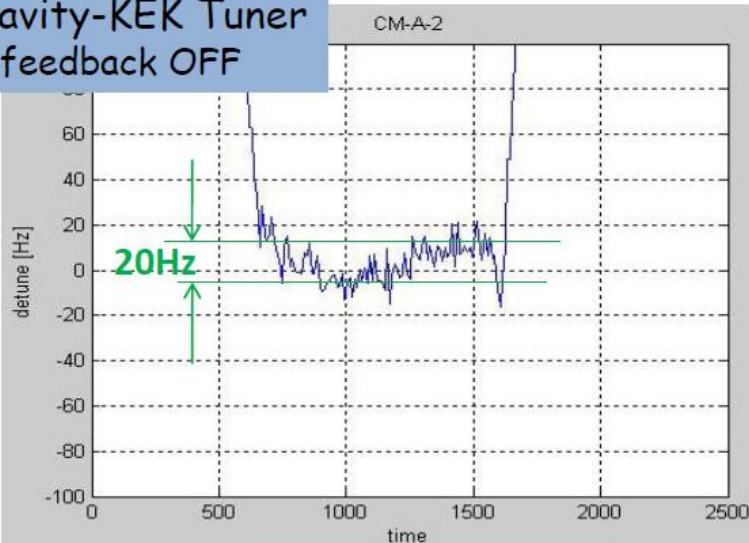
FNAL Piezo Control System

Selected material from a review of system and results from Yuriy Pischalnikov (FNAL)

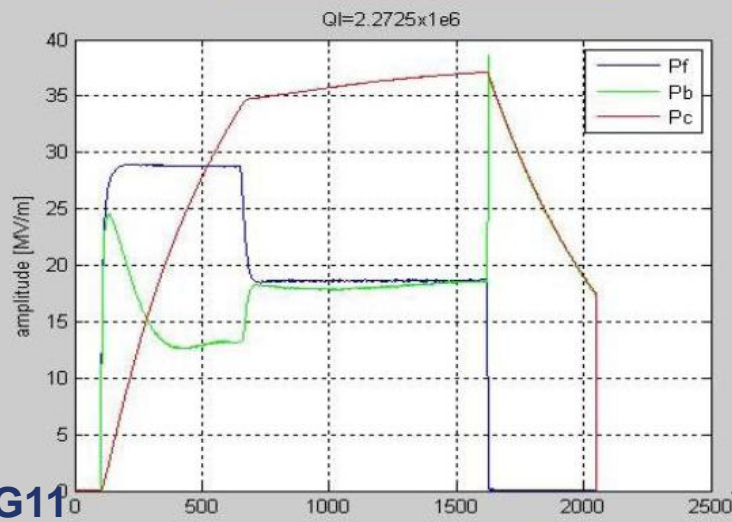
S1 Global A2(KEK) Cavity-KEK Tuner
Eacc=37MV/m, RF feedback OFF



Piezo OFF



Piezo ON; $V_{p-p}=300V$

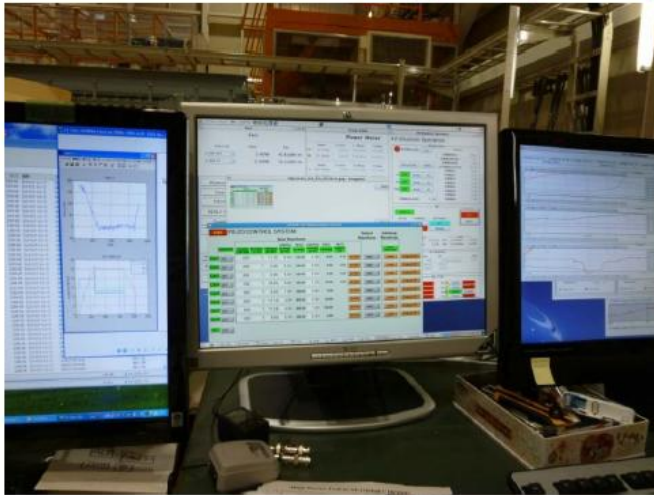


KEK Piezo Control System

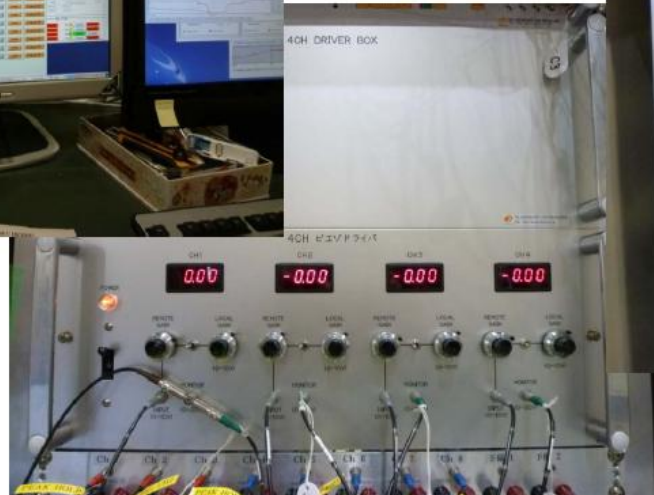
Selected material from a review of system and results from Eiji Kako (KEK)

KEK Control system of Piezo Tuner

Piezo control by PC
Monitor of detuning frequency



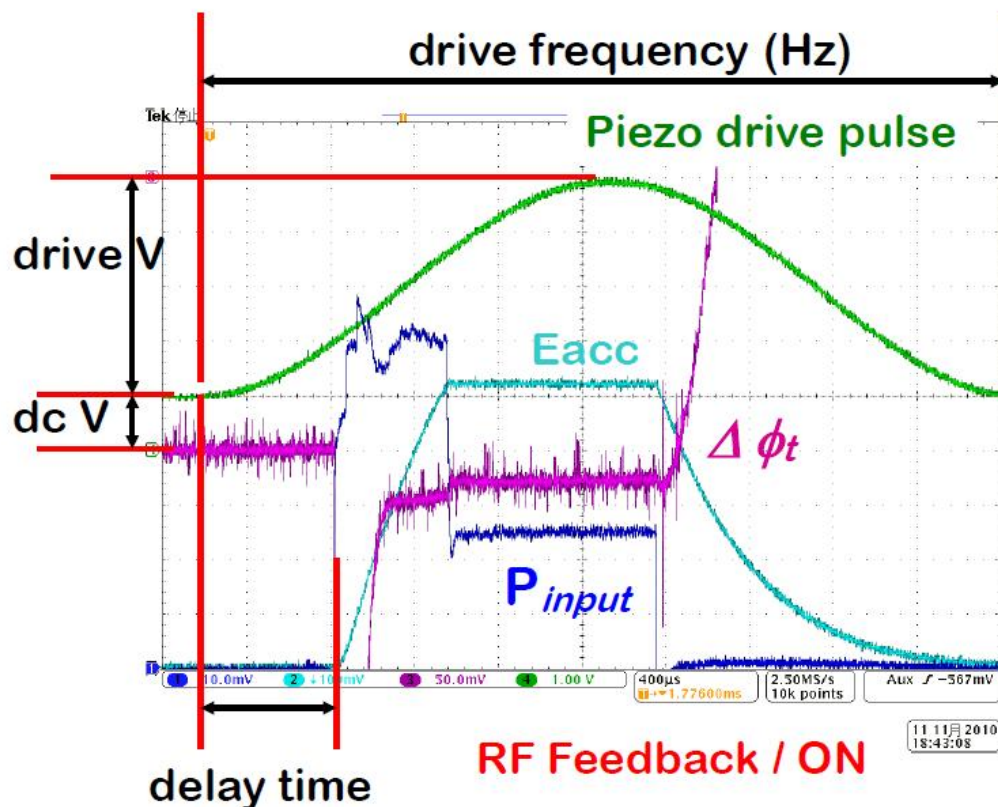
Piezo driver for
KEK cavities (+1000V)



Piezo driver for DESY/FNAL cavities (+200V)

Parameters of Piezo drive pulse

Pre-detuning by motor tuner



control panel

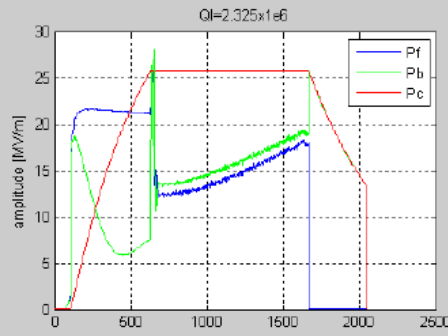
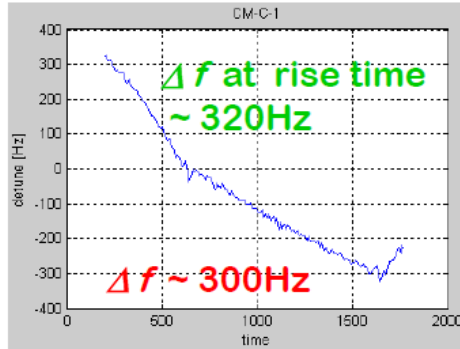
Single pulse of inverse cosine waveform

Compensation of Lorentz detuning (C1)

C1/AES004

25.6 MV/m

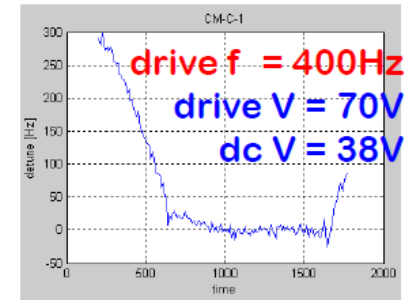
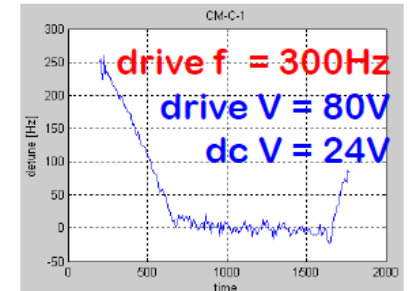
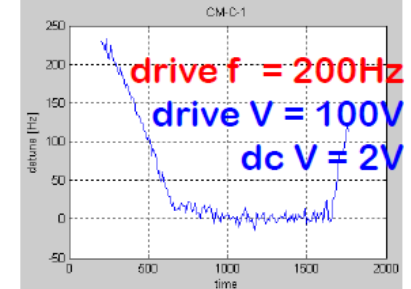
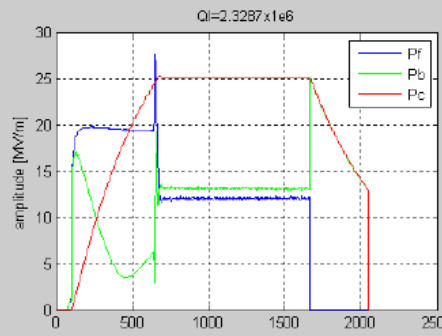
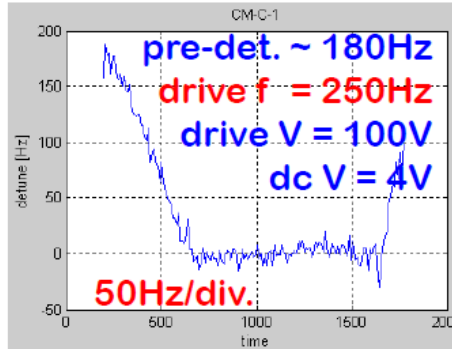
FB/on, Piezo/off



C1/AES004 (Blade Tuner)

25.6 MV/m

FB/on, Piezo/on

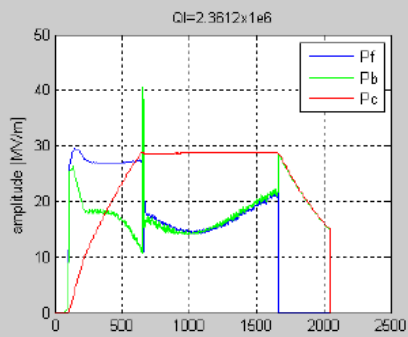
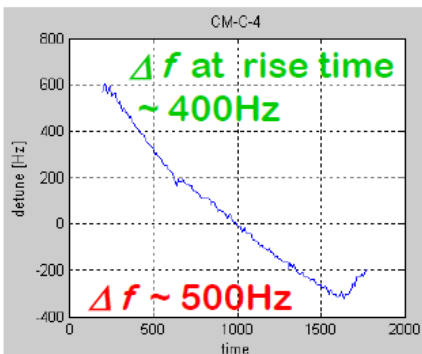


Compensation of Lorentz detuning (C4)

C4/Z109

29 MV/m

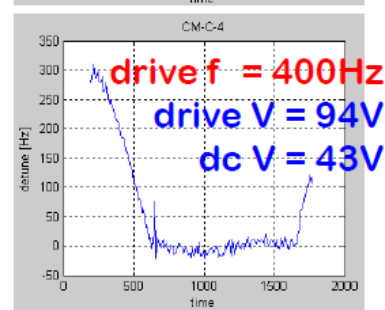
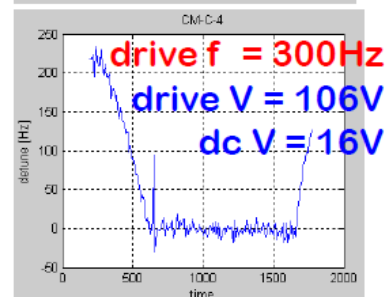
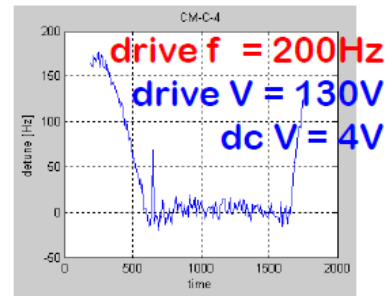
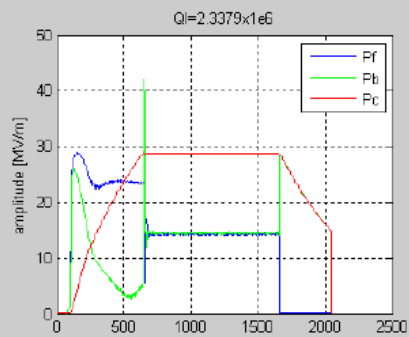
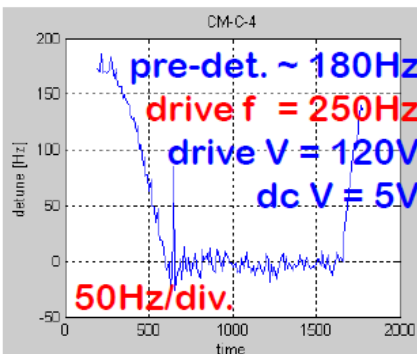
FB/on, Piezo/off



C4/Z109 (Saclay Tuner)

29 MV/m

FB/on, Piezo/on

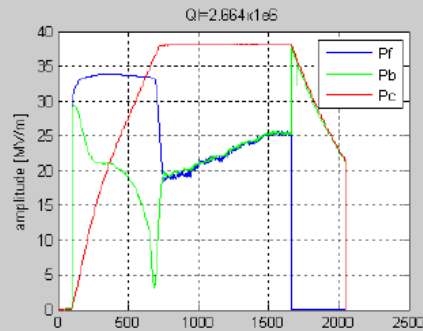
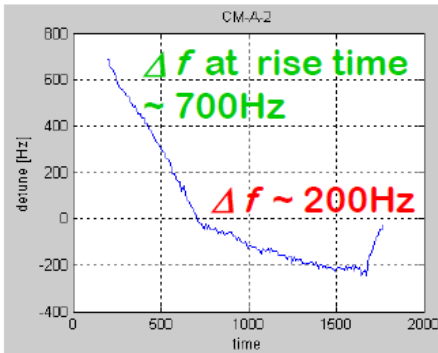


Compensation of Lorentz detuning (A2)

A2/MHI-06

38 MV/m

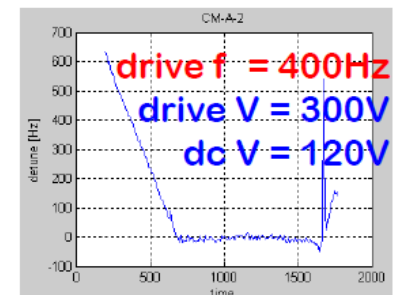
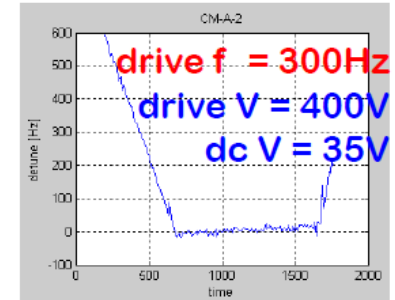
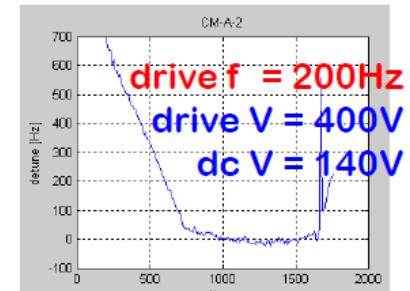
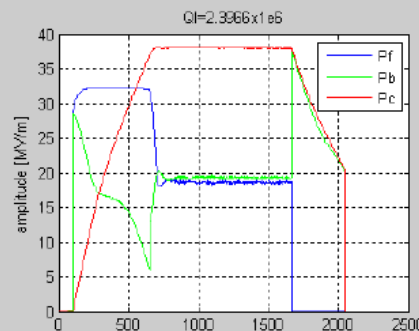
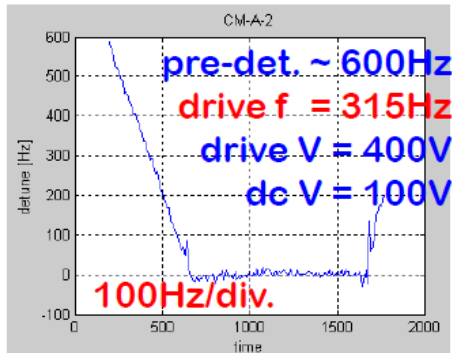
FB/on, Piezo/off



A2/MHI-06 (Slide Jack)

38 MV/m

FB/on, Piezo/on



Conclusions

- Globally, each of the different models of tuning systems installed at S1-Global proved to be capable to accomplish its main goals:
 - **Statically tune the cavity with proper resolution to the target frequency**
 - **Achieve pulsed operation at maximum gradient with an active compensation of the LFD up to tens of Hz-level residual detuning.**
 - **Demonstrate to grant enough performance margin in LFD compensation in view of ILC-level target gradients.**
- Failures emerged in some key components:
 - **Details have still to be investigated but ...**
 - **Stepper motors, mechanical gears or piezo actuators are well-known and substantially affordable: we don't expect observed issues to be intrinsic problems.**
 - **More likely, for S1-Global both the technical novelties present in some elements and the lack of experience on a module string could have played a major role (both INFN/FNAL and KEK systems are installed on a string here for the first time).**
- The overall S1-Global experience:
 - **Has been an outstanding possibility to operate different tuners simultaneously**
 - **The investigation of failures in tuning systems will provide a remarkable experience to improve reliability in future installations.**