



# Undulator R & D

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**BAW-2 SLAC Jan 2011**

# Reminder

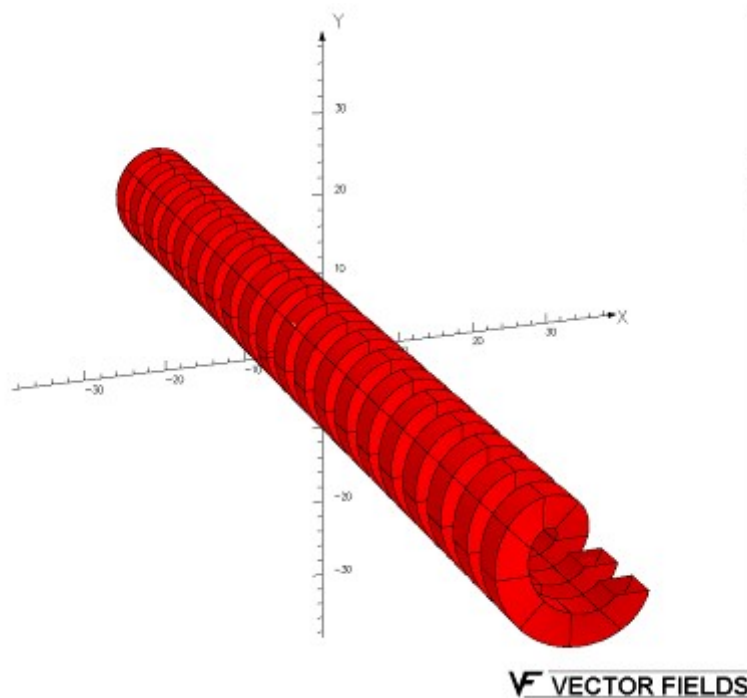
- A helical undulator is a core element of the positron source
- The parameters required by the ILC had never been demonstrated before
- Cornell and STFC (Daresbury and RAL) both built short superconducting prototypes
- The results of these short prototypes defined the (RDR) current undulator parameters (11.5mm period, 0.86T)
- **STFC have since built a 4m undulator module that meets the ILC specification**



# Basic Magnet Design Features

- **Bifilar Helix with iron poles**
- **NbTi wire**
- **Non-magnetic vacuum vessel**

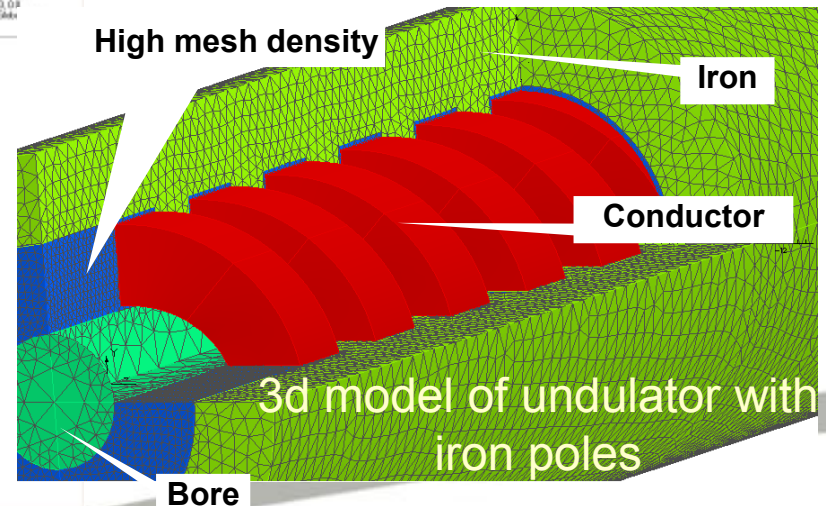
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| UNITS              |                  |
|--------------------|------------------|
| Length             | m                |
| Magn Flux Density  | T                |
| Magn Field         | A/m              |
| Magn Vector Pot    | A                |
| Magn Vector Pot    | V/m              |
| Elect Flux Density | C/m <sup>2</sup> |
| Elect Field        | V/m              |
| Conductivity       | S/m              |
| Current Density    | A/m <sup>2</sup> |
| Power              | W                |
| Force              | N                |
| Energy             | J                |

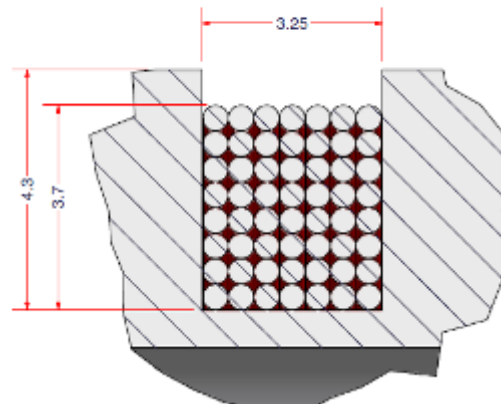
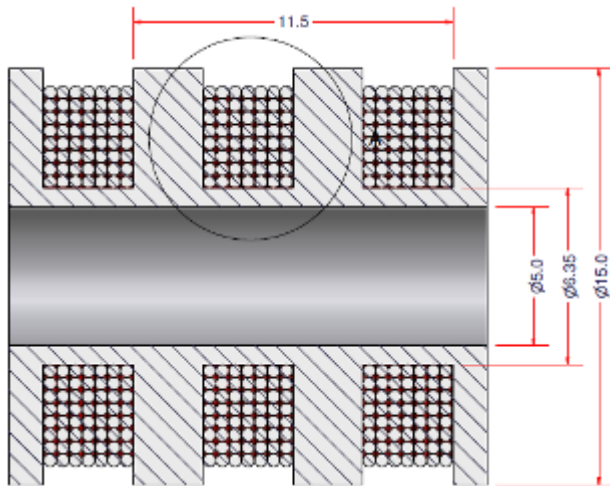
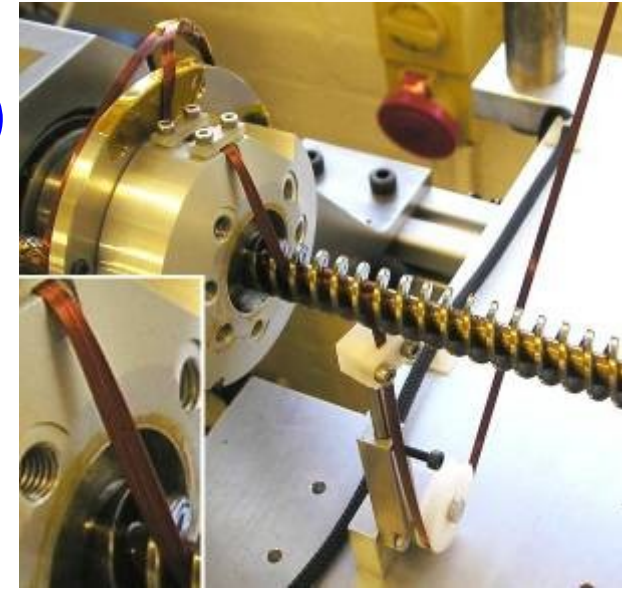
  

| FIDELITY DATA         |  |
|-----------------------|--|
| 100 conductors        |  |
| Local Coordinates     |  |
| Origin: 0.0, 0.0, 0.0 |  |
| Local P12: 0.000      |  |

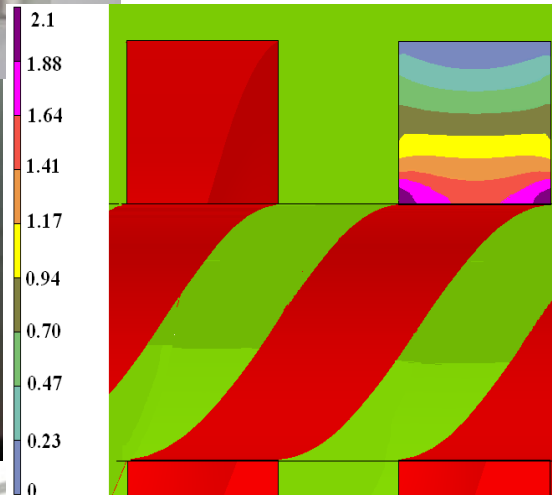


# NbTi Winding

- Wound with **7 wire ribbon**, 8 layers
- Ø0.4 mm NbTi wire, with 25 µm enamel (Ø0.45 mm when insulated)
- 3.25 mm wide winding for 11.5mm period
- Packing factor of 62%



# NbTi Prototypes



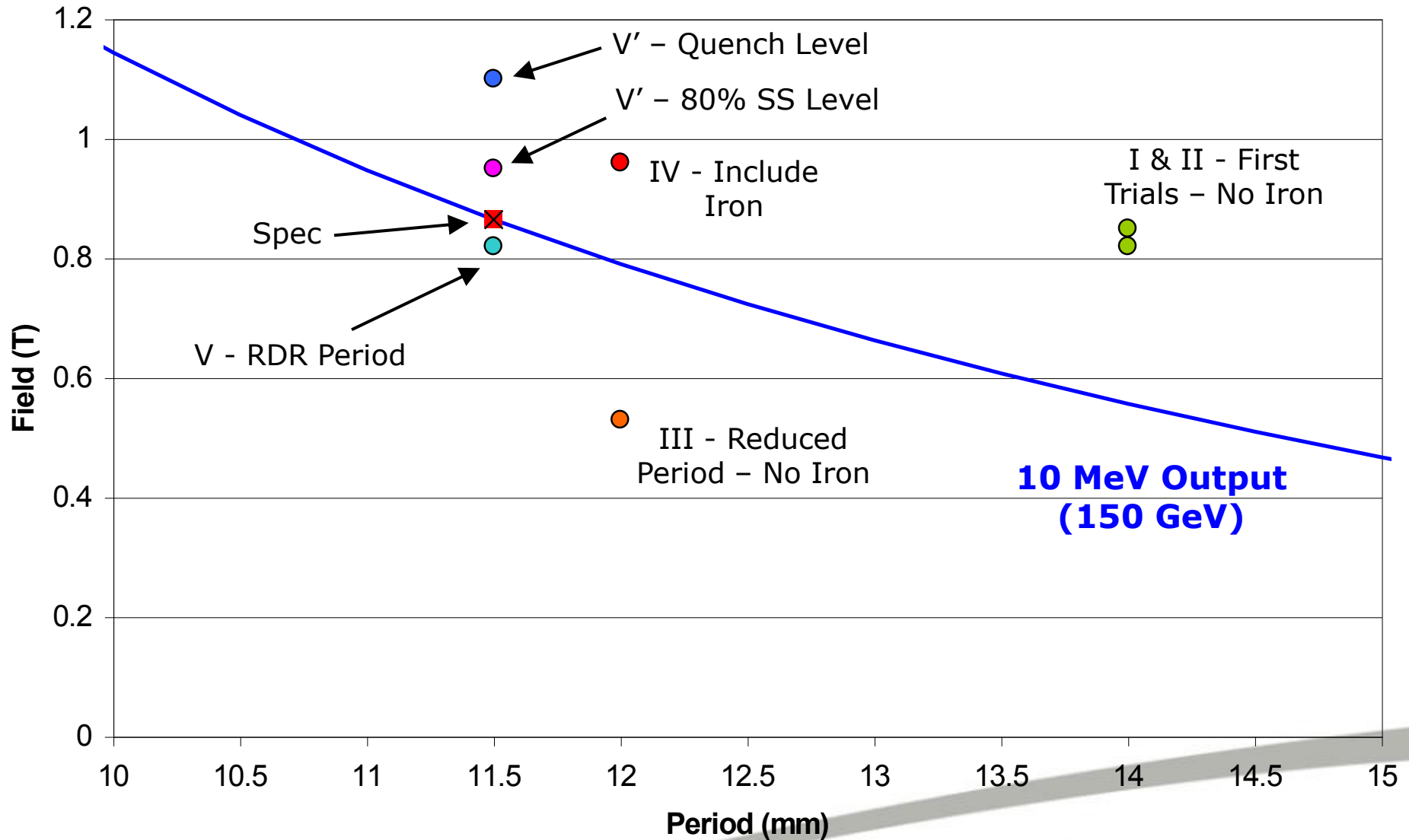


# Prototypes Summary

| Parameter       | Prototype 1                | Prototype 2                  | Prototype 3                | Prototype 4                 | Prototype 5                | Prototype 5'                       |
|-----------------|----------------------------|------------------------------|----------------------------|-----------------------------|----------------------------|------------------------------------|
| Prototype goal  | <b>Winding Technique</b>   | <b>Mechanical tolerances</b> | <b>Reduced period</b>      | <b>Check effect of iron</b> | <b>Increased period</b>    | <b>improved impregnation</b>       |
| Length          | 300 mm                     | 300 mm                       | 300 mm                     | 300 mm                      | 500 mm                     | <b>500 mm</b>                      |
| Former material | Aluminium                  | Aluminium                    | Aluminium                  | Iron                        | Iron                       | <b>Iron</b>                        |
| Bore tube       | Integral                   | integral                     | integral                   | integral                    | copper                     | <b>copper</b>                      |
| Winding period  | 14 mm                      | 14 mm                        | 12 mm                      | 12 mm                       | 11.5 mm                    | <b>11.5 mm</b>                     |
| Winding bore    | 6 mm                       | 6 mm                         | 6 mm                       | 6 mm                        | 6.35 mm                    | <b>6.35 mm</b>                     |
| Magnet bore     | 4 mm                       | 4 mm                         | 4 mm                       | 4.5 mm                      | 5.23 mm                    | <b>5.23 mm</b>                     |
| SC wire         | Cu:SC<br>1.35:1            | Cu:SC<br>1.35:1              | Cu:SC<br>1.35:1            | Cu:SC<br>1.35:1             | Cu:SC<br>0.9:1             | <b>Cu:SC<br/>0.9:1</b>             |
| Winding         | 8-wire ribbon,<br>8 layers | 9-wire ribbon,<br>8 layers   | 7-wire ribbon,<br>8 layers | 7-wire ribbon,<br>8 layers  | 7-wire ribbon,<br>8 layers | <b>7-wire ribbon,<br/>8 layers</b> |



# Prototypes Summary



# Full Undulator Parameters (RDR)

| Undulator Parameters                            | Symbol     | Value   | Units |
|---|------------|---------|-------|
| Undulator period                                | $\lambda$  | 1.15    | cm    |
| Undulator strength                              | K          | 0.92    |       |
| Undulator type                                  |            | helical |       |
| Active undulator length                         | $L_u$      | 147     | m     |
| Field on axis                                   | B          | 0.86    | T     |
| Beam aperture                                   |            | 5.85    | mm    |
| Photon energy (1 <sup>st</sup> harmonic cutoff) | $E_{c10}$  | 10.06   | MeV   |
| Photon beam power                               | $P_\gamma$ | 131     | kW    |

Undulator to be made of 4m long modules

Only the total length has been changed since the RDR

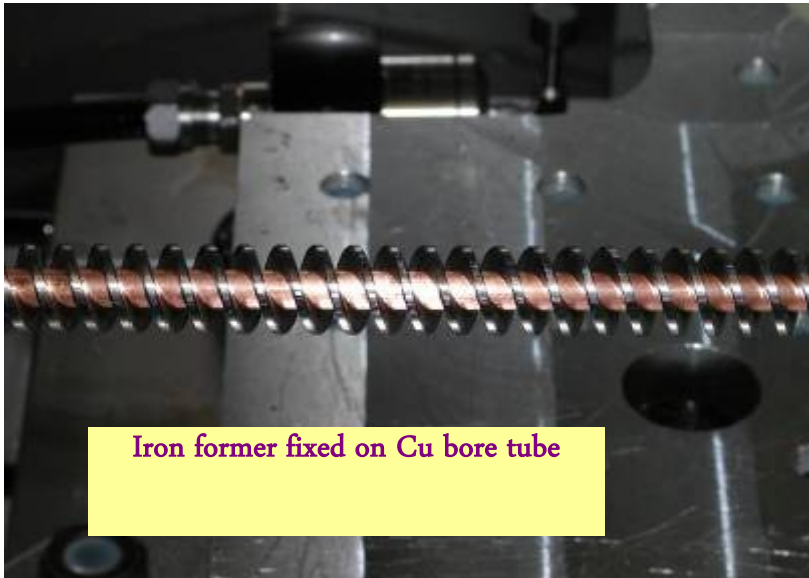




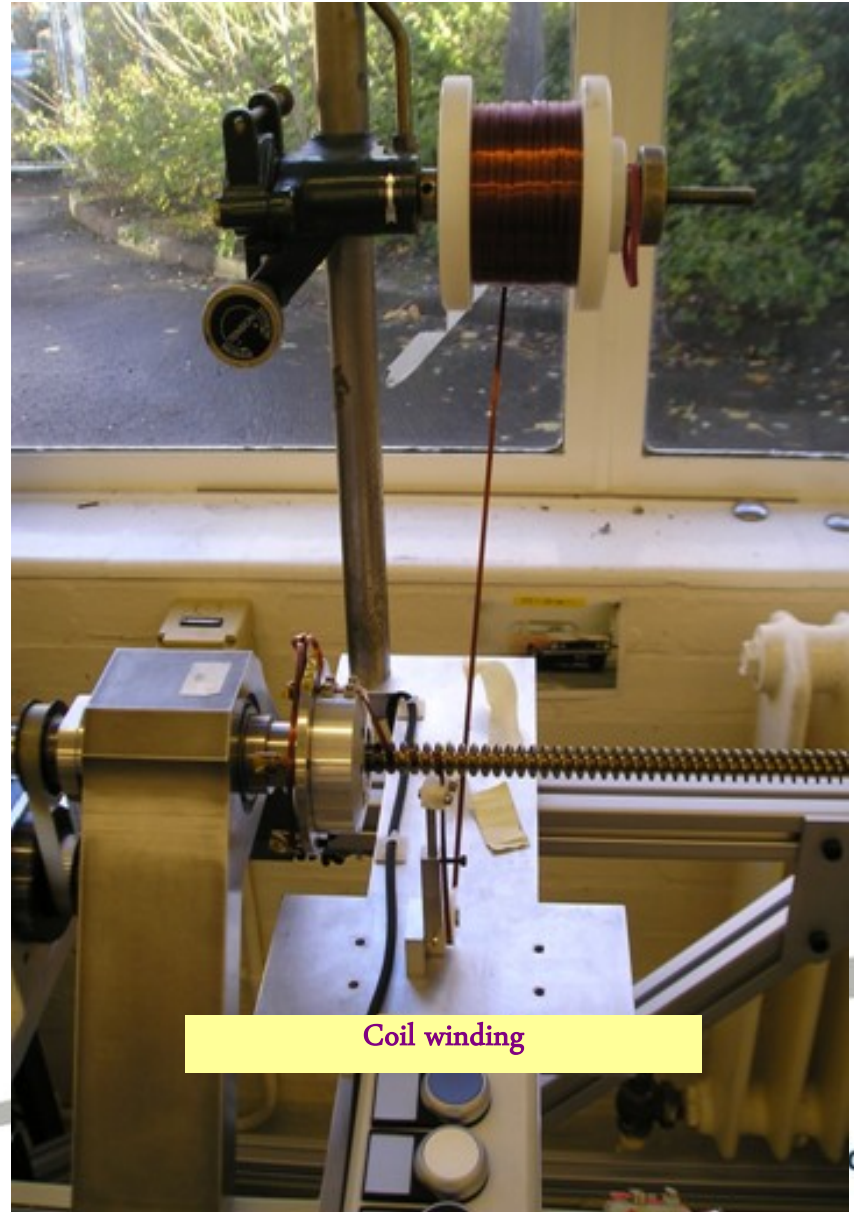
# 4m Prototype manufacture



4 axis machining

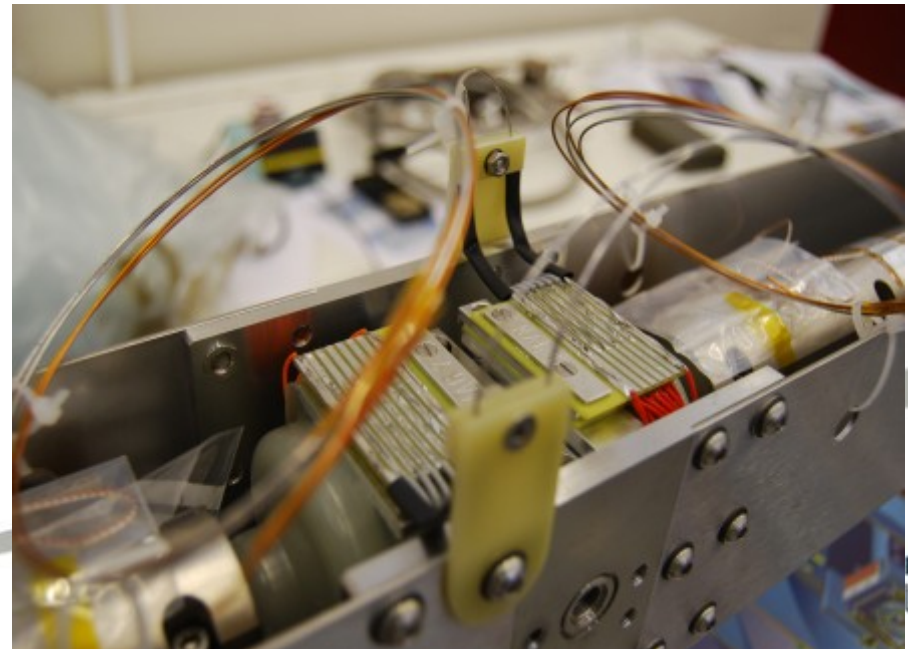
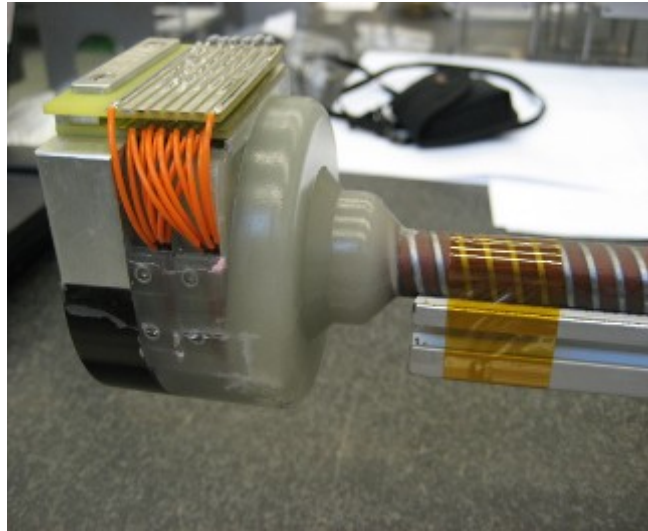


Iron former fixed on Cu bore tube



Coil winding

# 4m Prototype manufacture

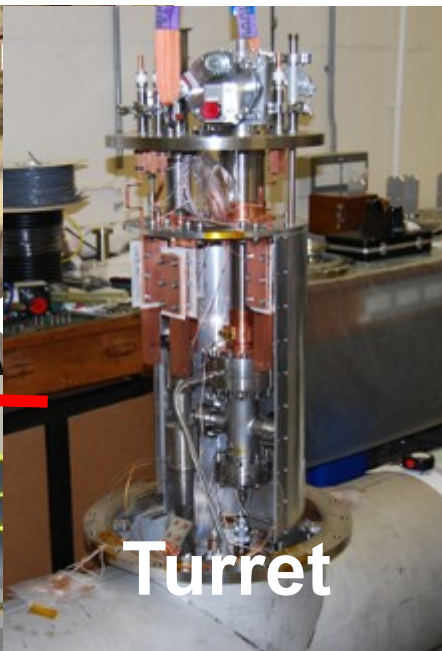




# 4m Cryomodule Fabrication



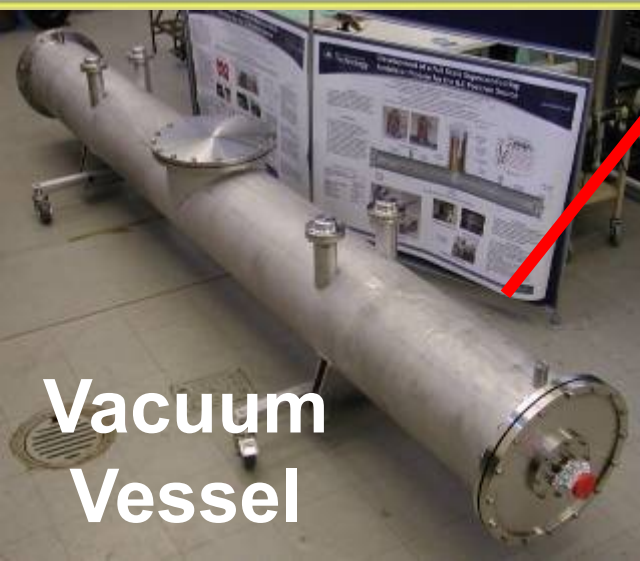
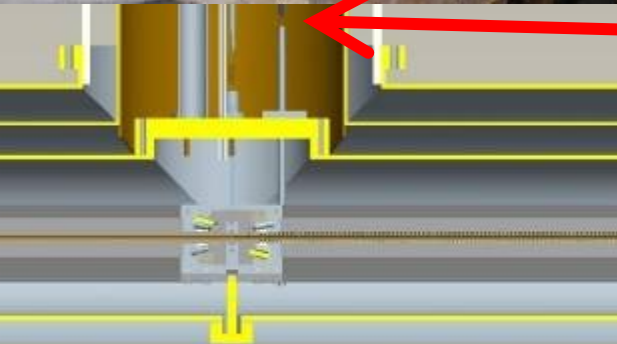
Heat Shield



Turret



U Beam



Vacuum Vessel



He Vessel

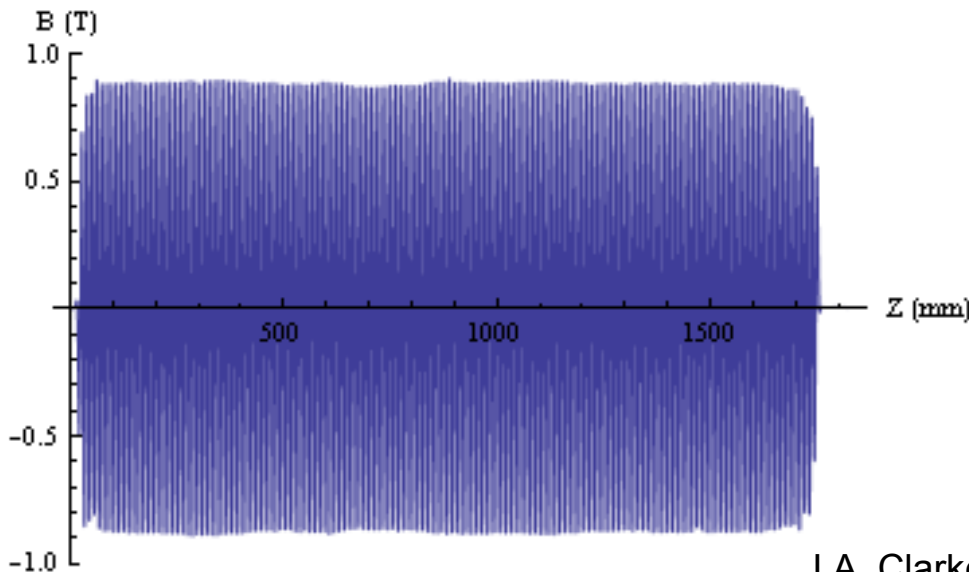
# Cryomodule

- A 4m module containing 2 x 1.75m helical undulators (11.5 mm period) was constructed at RAL
- Closed loop cryo system with cryocooler

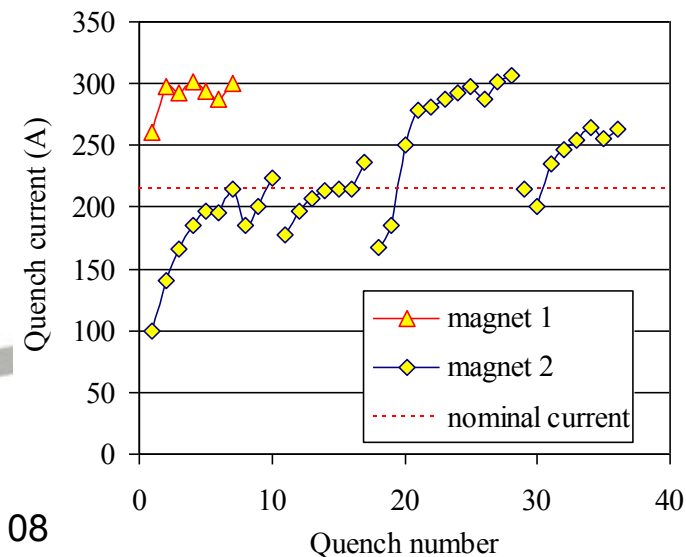


# Vertical Tests

- The quench test results show different behaviour between the two identical magnets
- Both do actually reach the same final quench current which agreed well with expectations
- **300A = 1.15T (spec is 0.86T, 215A)**

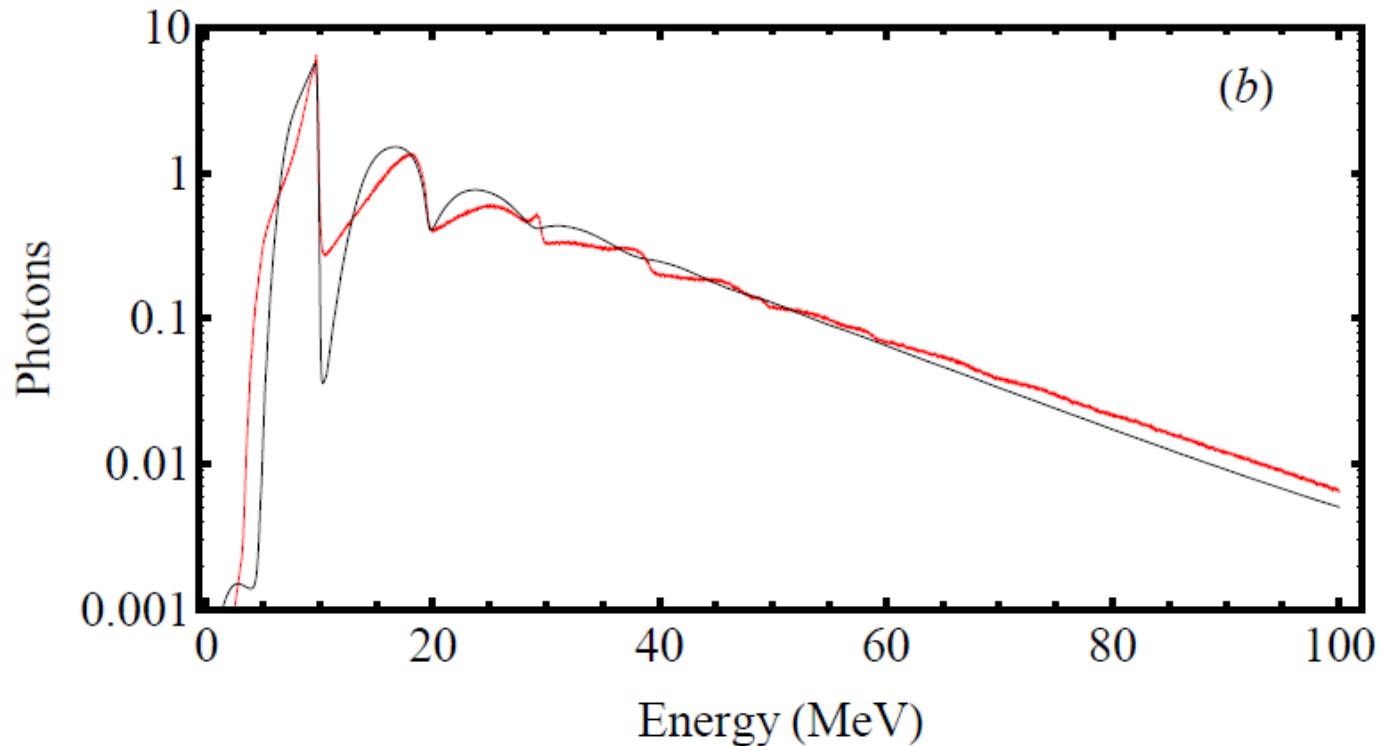


J.A. Clarke et al, EPAC 08



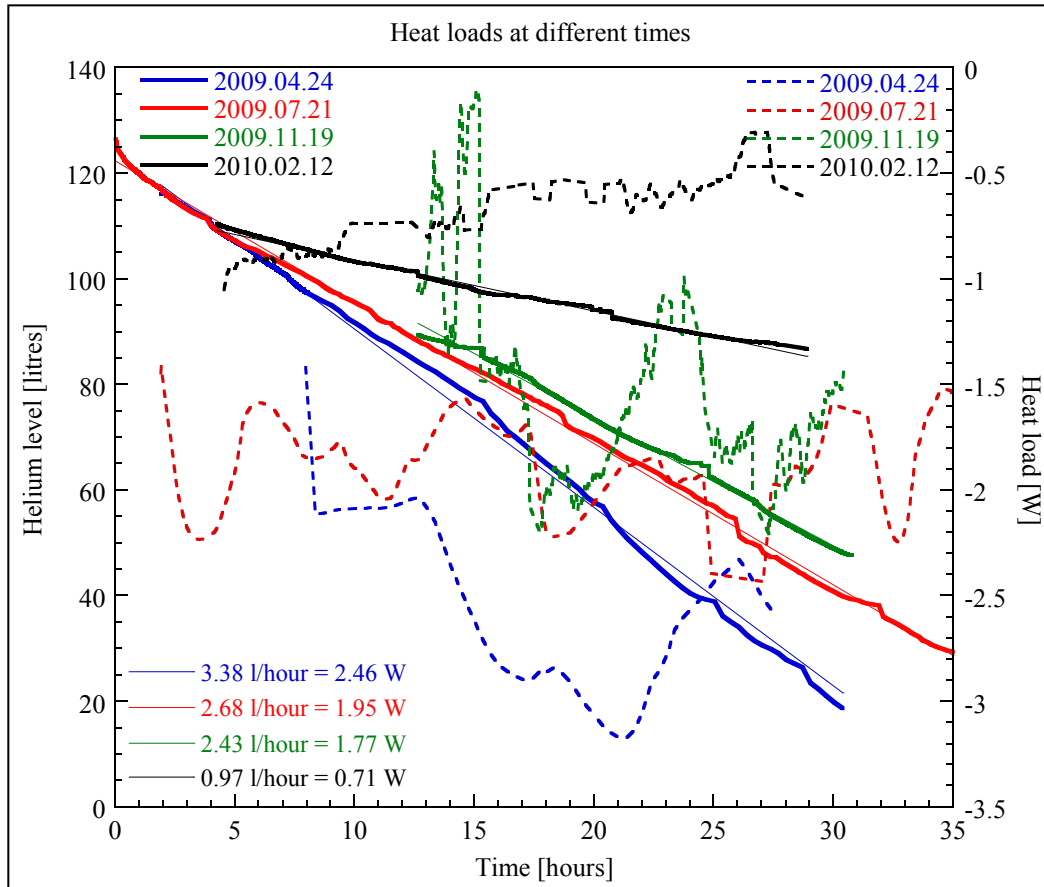
# Photon Output

- Photon Flux per 150 GeV electron per unit relative energy bandwidth for the two undulators in series (red) and an ideal undulator with the same average parameters (black)





# Module Heat Load Problem



- Heat load higher than anticipated
  - System not recondensing
- Incremental improvements were made slowly with time
  - Main issue was top plate not at 4K

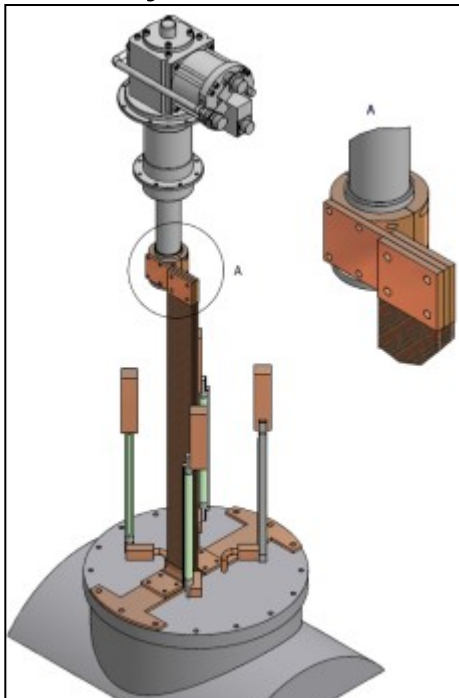


# Undulator Cryomodule

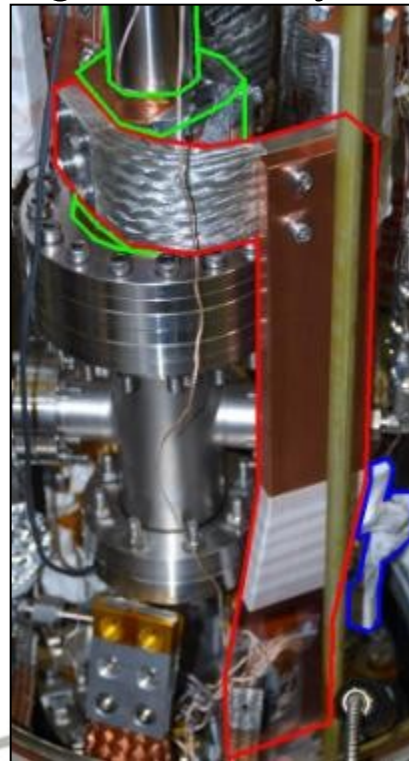
## July 2010 – Top plate cooled by cryocooler

It was seen that it did not take much heat input to change temperature of top plate and HTS/LTS join.

Large copper bars have been inserted to cool top plate and HTS/LTS join directly from the 2<sup>nd</sup> stage of the cryocooler.

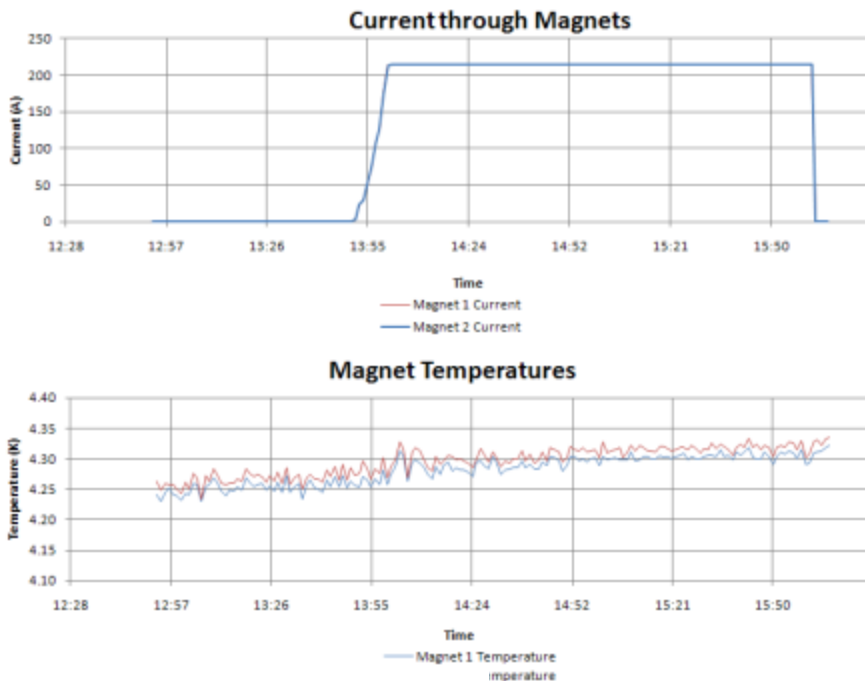


Owen Taylor, STFC



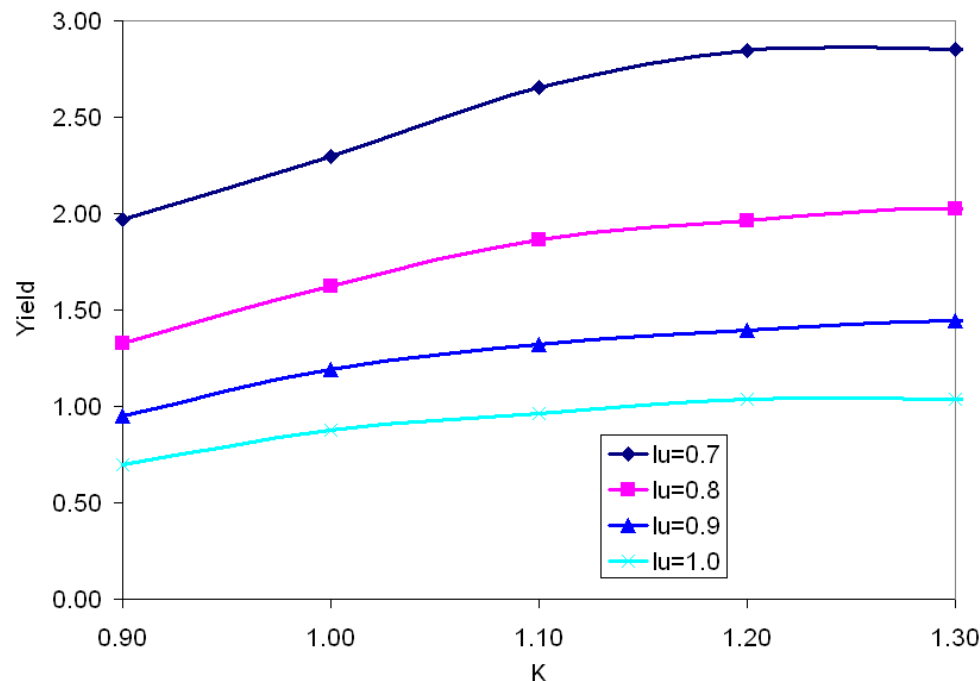
# Undulator Cryomodule

- Both undulators now powered individually and together at 215 A (0.86T) – stable operation (during 2 hour test)
- Both also powered at 252A for > 1hour but then lead quenched above top plate
  - Not enough margin on top plate temperature at high current?
  - No magnet quenches so far



# Use Different Undulator Parameters?

- Yield shown for:
  - 231 m long undulator
  - 100 GeV drive beam energy
  - Flux Concentrator
- Shorter period required!



# Application of Nb<sub>3</sub>Sn

- To generate higher fields or to be able to reduce the period we need to use Nb<sub>3</sub>Sn
- Goal would be to reduce period to ~9mm
- **Concerns**
  - Packing factor reduced as insulation is thicker
  - Performance of wire at <5T
  - Insulation of former
  - Can no longer wind with ribbon
  - More difficult material to work with (heat treatment)
- Need Nb<sub>3</sub>Sn wire to have small diameter for similar filling factor
- Have purchased 1 km of Ø0.5 mm (Ø0.63 mm with glass braid) wire from OST.

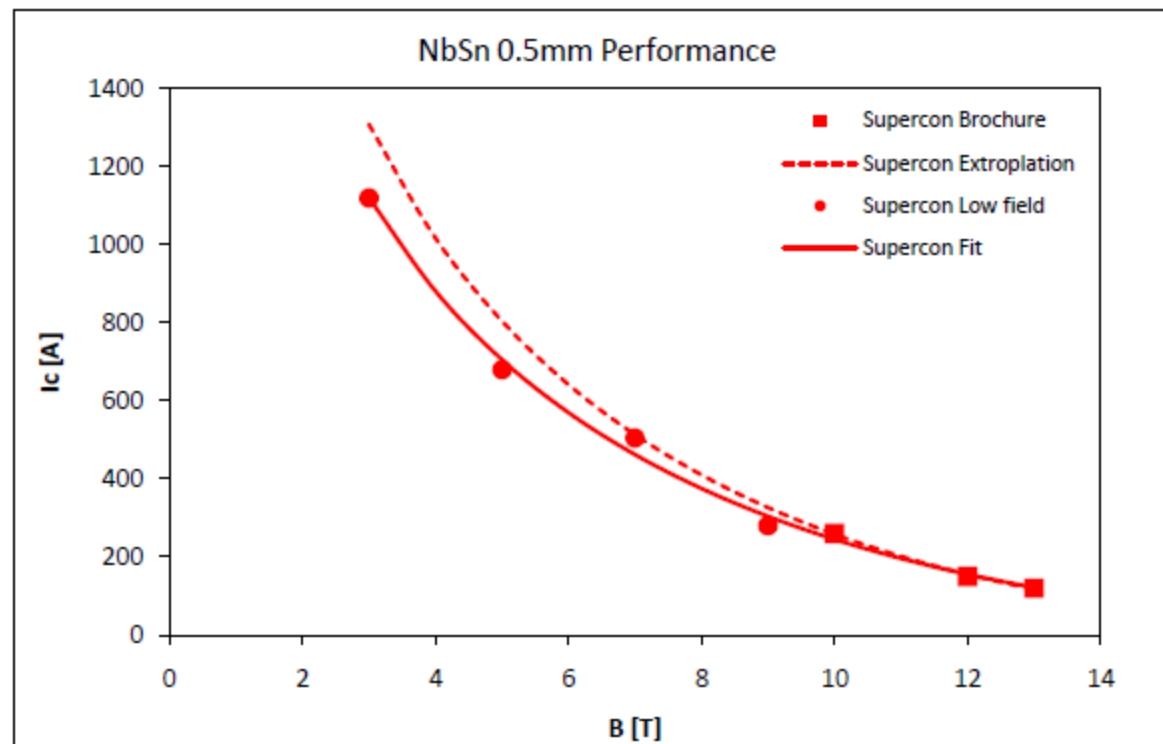


# Nb<sub>3</sub>Sn Performance

- Nb<sub>3</sub>Sn Availability
  - EAS Bruker do not make Nb<sub>3</sub>Sn smaller than Ø0.7 mm
  - Supercon Inc. and Oxford Instruments Superconducting Technology (OST) make Ø0.4 mm and Ø0.5 mm respectively
- Nb<sub>3</sub>Sn Performance
  - Due to small winding area, need large currents to achieve ~1 T on axis
  - Need to know critical current in winding at ~4 T
  - No companies have data for performance below 9 T
  - Large extrapolation needed – no confidence
  - Supercon Inc. made measurements from 3 T for us

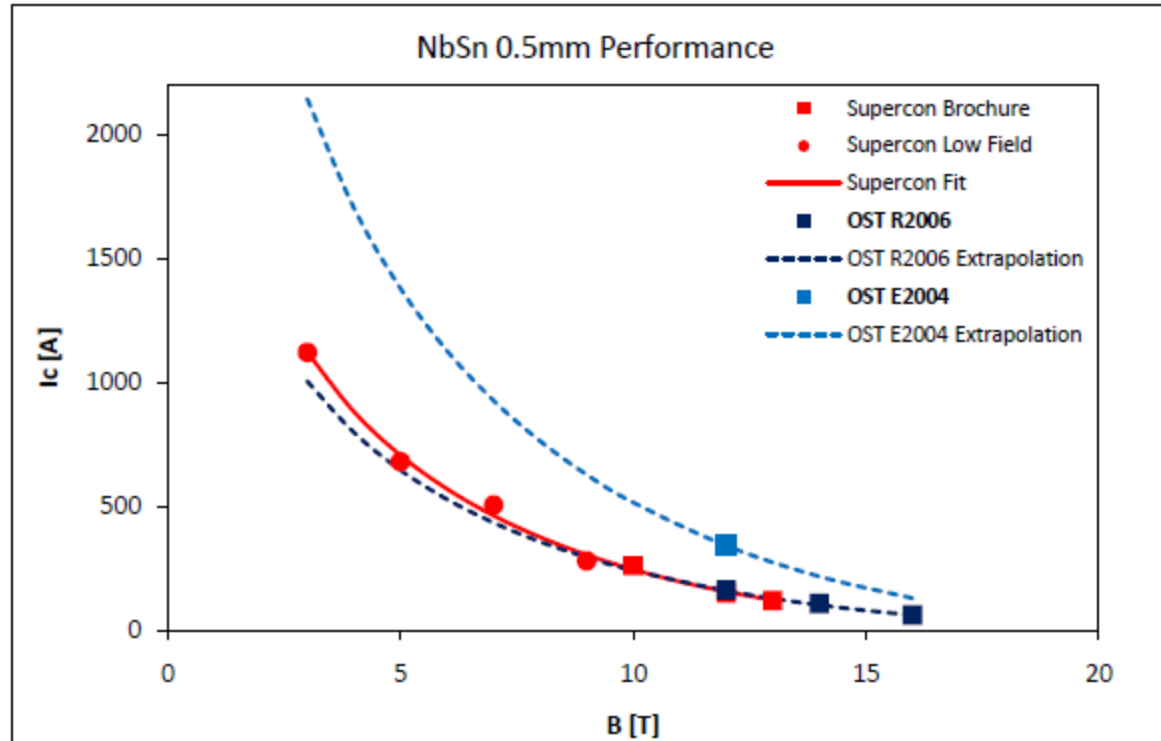


# Supercon 0.5mm Internal Tin wire performance



- Solid line shows Kramer fit to all data
- $I_c = 1120$  A at 3 T, 4.2 K

# OST 0.5 mm Nb<sub>3</sub>Sn Performance, two grades of wire



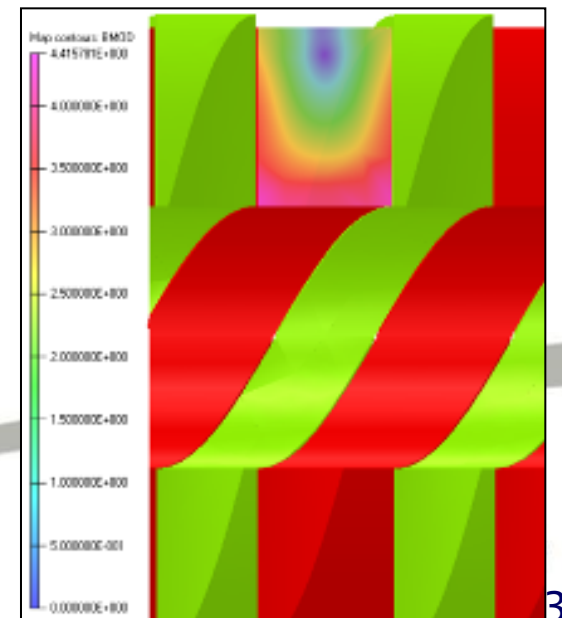
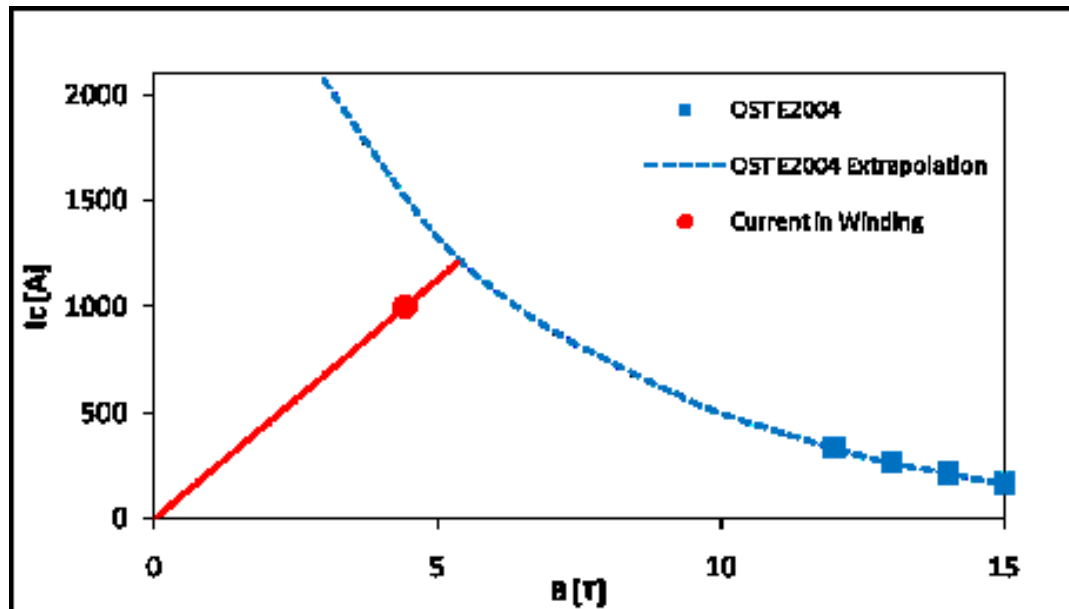
Large extrapolation to available data

OST R2006:  $I_c \sim 1000$  A at 3 T, 4.2 K ( $J_c \approx 1600$  A/mm<sup>2</sup>, 4.2 K 12 T)

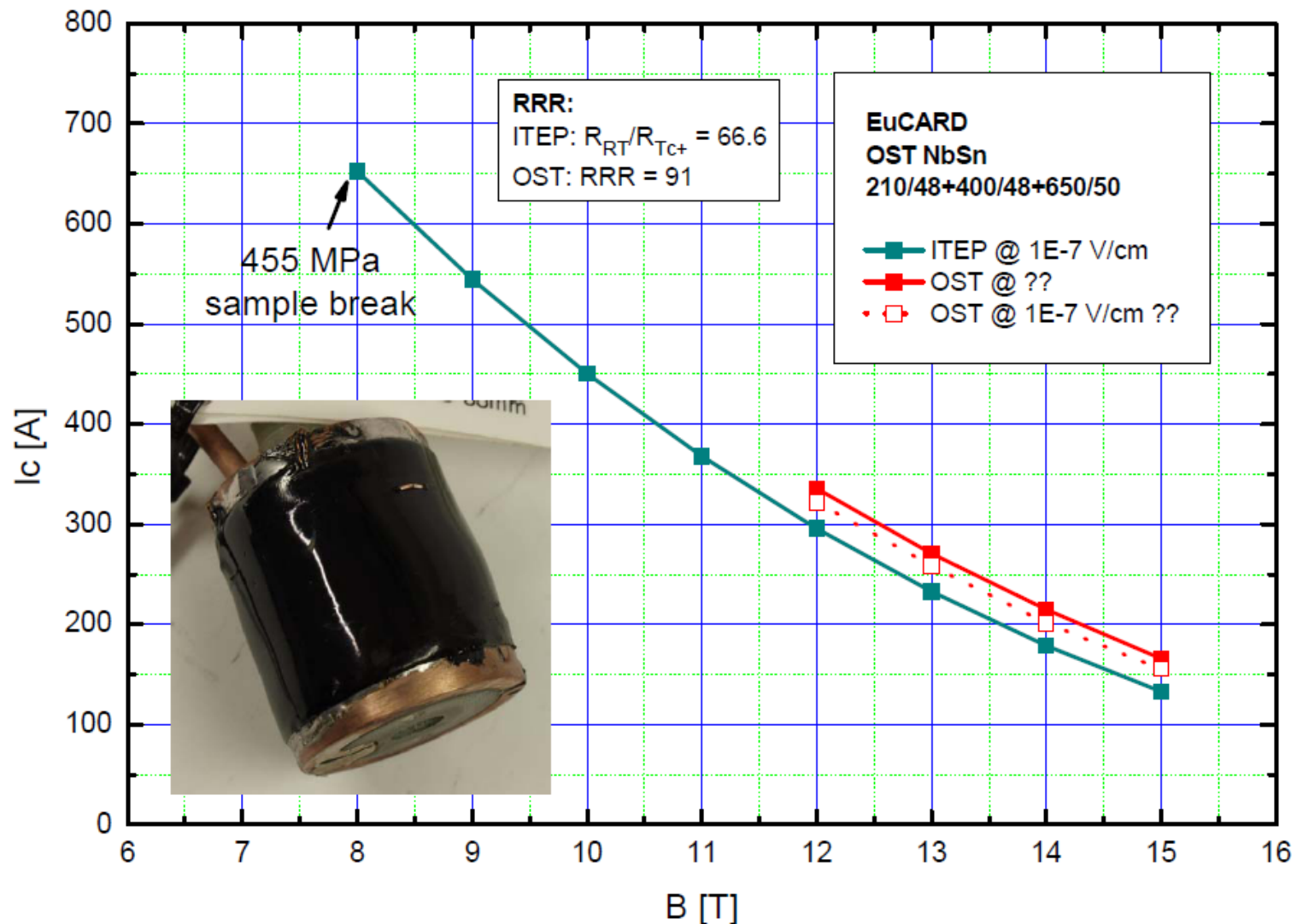
OST E2004:  $I_c \sim 2000$  A at 3 T, 4.2 K ( $J_c \approx 2900$  A/mm<sup>2</sup>, 4.2 K 12 T)

# FEA Modelling

- Winding ID: Ø6.35 mm as before
- Field on axis: 1.54 T for 11.5mm period (cf 0.86T)
- Peak field in conductor: 4.4 T
- Operating at 82% of  $I_c$
- Wire performance measurements have started at KIT

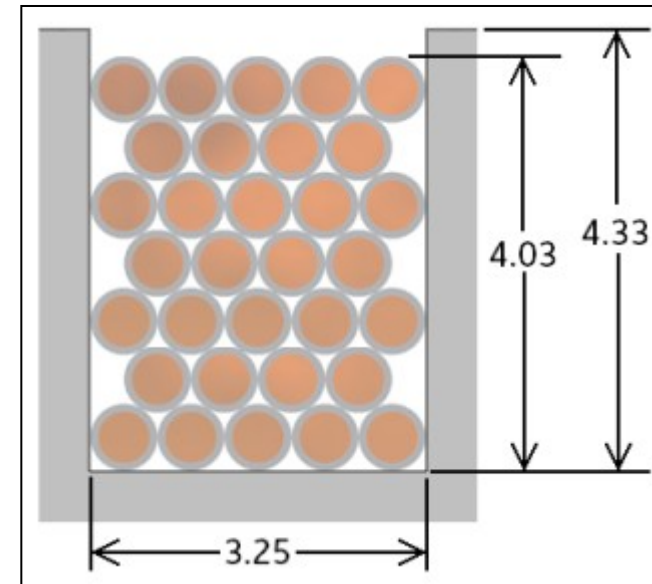


# Results: Comparison to OST-data (HT “A”)

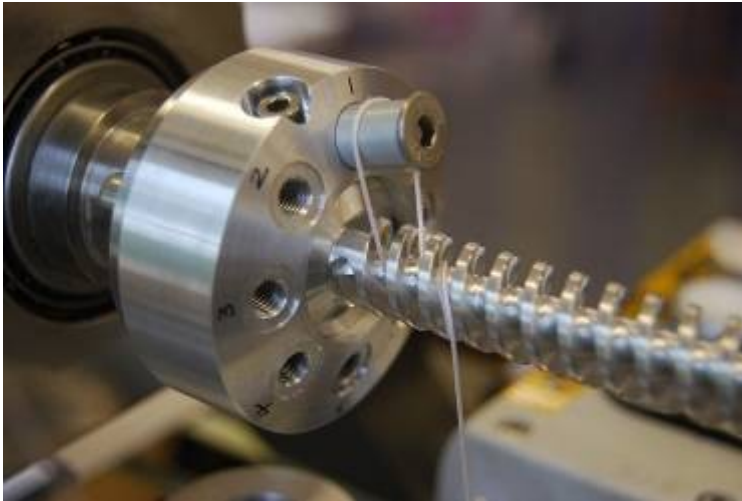


# Trial Winding

- Need to do a trial winding to confirm groove dimensions
- Aluminium former has been made with the dimensions shown
- Will be 32 wires in winding
- 11.5 mm period
- Will be wound, potted and sectioned to check groove width etc




# Trial Winding Started





# Summary

- A SC Helical Undulator Cryomodule with the current ILC parameters has been constructed and tested successfully using NbTi wire at RAL
- A project to develop Nb<sub>3</sub>Sn short prototypes with enhanced parameters has now started in the UK 
- The wire has been procured and is being tested at low field by KIT
- The benefit to the ILC of a reduced period undulator using Nb<sub>3</sub>Sn could be significant at low energies (<150 GeV)