CAVITY FABRICATION

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Center for Accelerator Science
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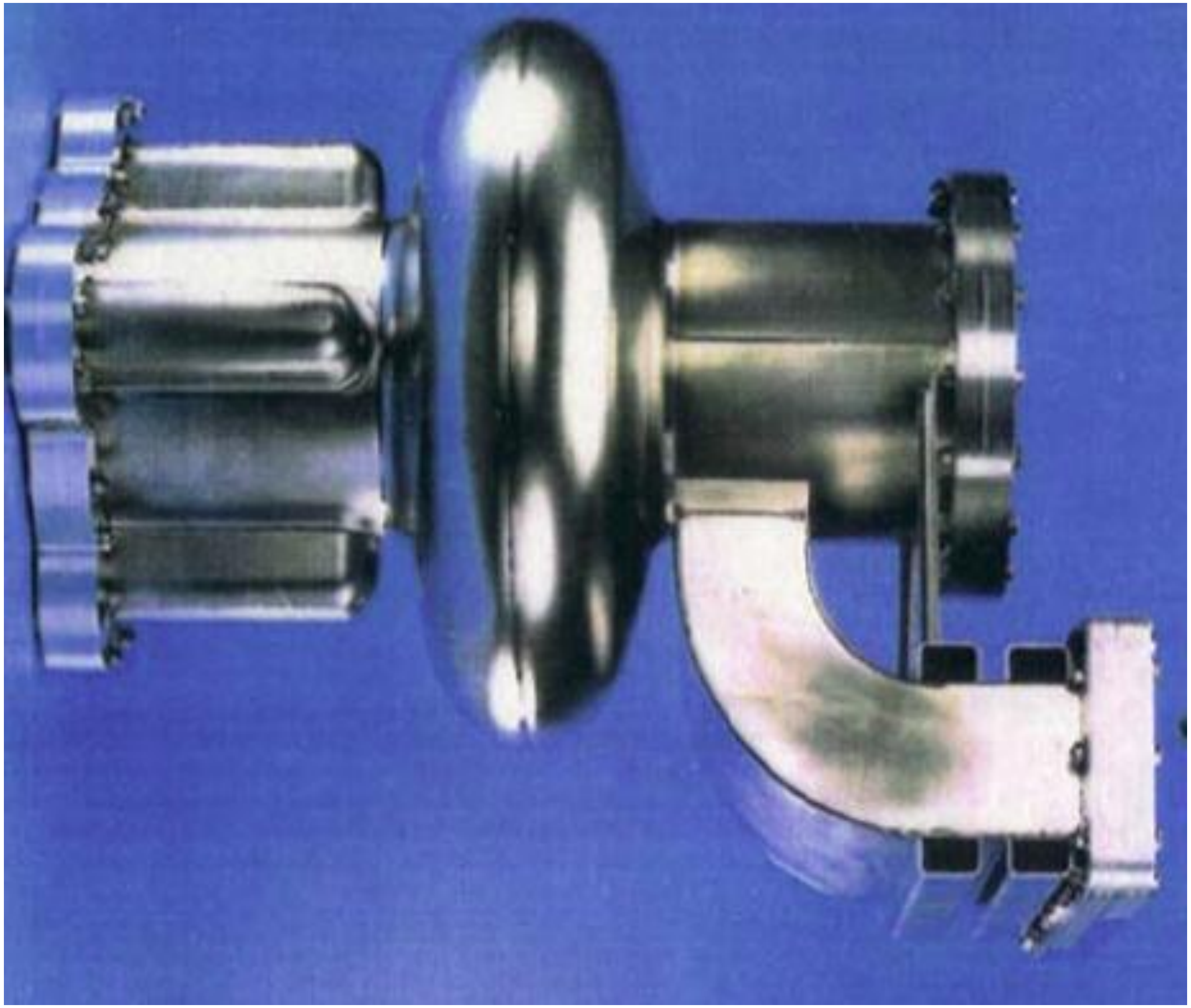
and
Thomas Jefferson National Accelerator Facility

500 MHz, Single-cell



350 MHz, 4-cell, Nb on Cu

1500 MHz, 5-cell

1300 MHz 9-cell

Nb = SRF

- Niobium is the material of choice to fabricate SRF cavities:
  - High critical temperature (T_c = 9.25K)
  - High critical field (H_c(0K) ≅ 200mT)
  - Chemically inert (surface covered by oxide layer)
  - Easily machined and deep drawn
  - Available as bulk and sheet material in any size

Niobium, Brief History

- Named after *Niobe* (daughter of Tantalus, Greek mythology)

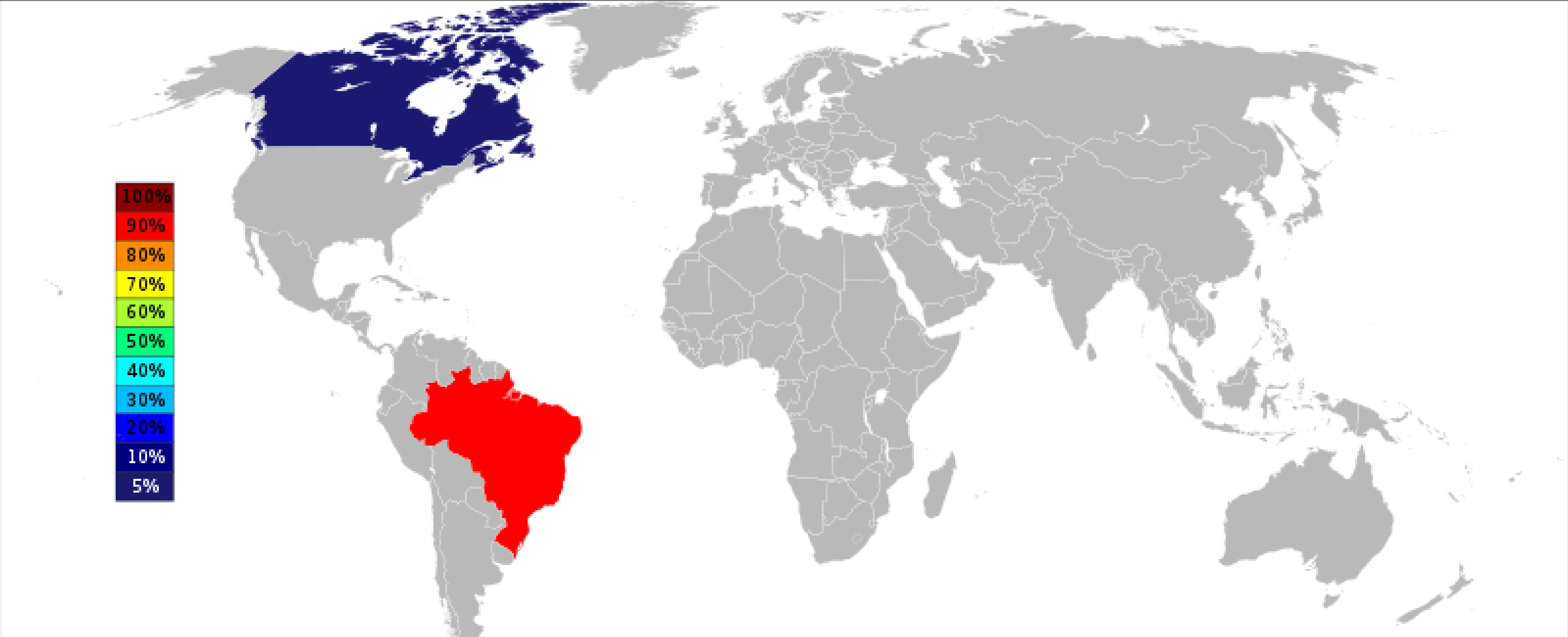
- Discovered in 1801 by Charles Hatchett in England from a columbite ore from Connecticut. He called it *Columbium*

Niobium, Brief History

- It was confused with tantalum until 1846, when it was re-discovered by Heinrich Rose and Jean Charles Galissard de Marignac, who called it *Niobium*
- "Niobium" was officially adopted as the name for the element 41 in 1950

- It was found to be a superconductor (zero electrical resistance) in the 1920s

Niobium Production



World Niobium Production in 2006 based on the Comodity Report of the United States Geological Survey 2006

Niobium is mostly obtained from mineral known as pyrochlore ($NaCaNb_2O_6F$). The pyrochlore mineral is processed to give a concentrate ranging from 55 to about 60% niobium oxide (Brazil, CBMM).
Columbite ($(Fe, Mn)(Nb,Ta)_2O_6$), a mineral with a ratio of Nb_2O_5:Ta_2O_5 ranging from 10:1 to 13:1, occurs in Brazil, Nigeria, and Australia, also other countries in central Africa. Niobium is recovered when the ores are processed for tantalum.

Niobium mines

The world's largest niobium deposits are located in Araxá, Brazil owned by Companhia Brasileira de Metalurgia e Mineração (CBMM). The reserves are enough to supply current world demand for about 500 years, about 460 million tons. The mining of weathered ore, running between 2.5 and 3.0% Nb_2O_5, is carried out by open pit mining without the need for drilling and explosives. Approximately 85 to 90% of the niobium industry obtains its niobium ores.

Niobium Processing Plant

- CBMM Plant
- CBMM hosted the International Workshop on Single Crystal Niobium Technology in 2006

Nb Production (CBMM)

- Niobium Ore in Araxa mine (open air pit) is pyrochlor with 2.5% Nb_2O_5
- The ore is crushed and magnetite is magnetically separated from the pyrochlor.
- By chemical processes the ore is concentrated in Nb contents (50 –60 % of Nb_2O_5)
- A mixture of Nb_2O_5 and aluminum powder is being reacted to reduce the oxide to Nb
- This Nb is the feedstock for the EBM processes

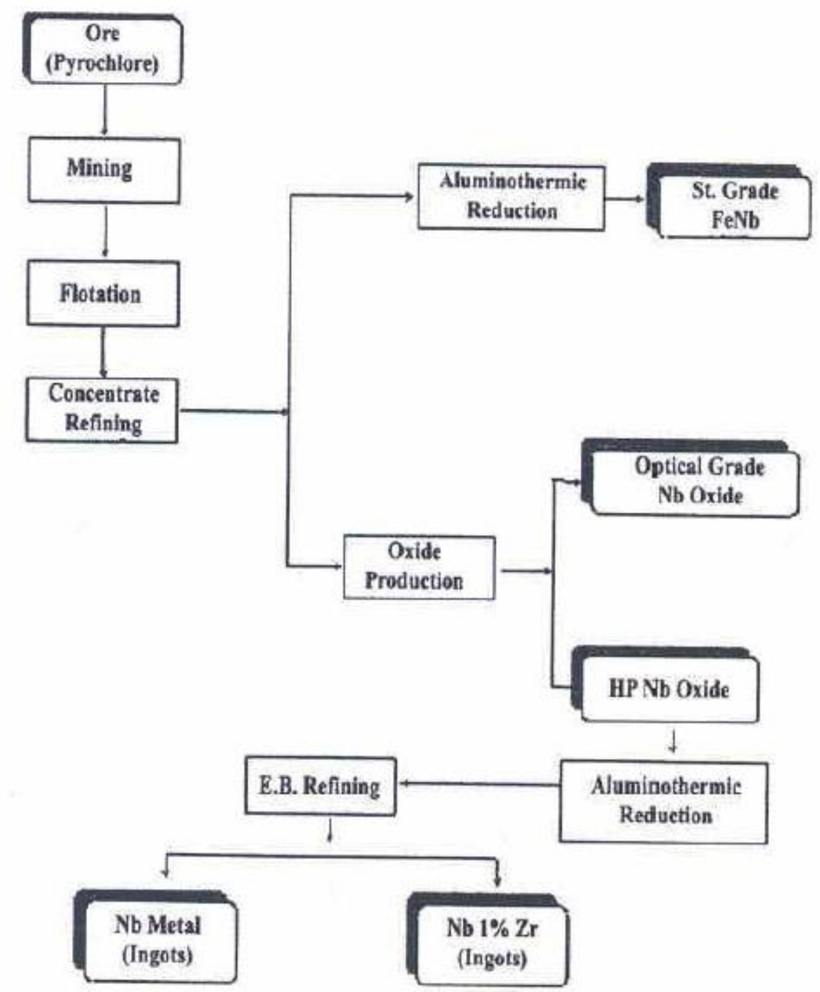
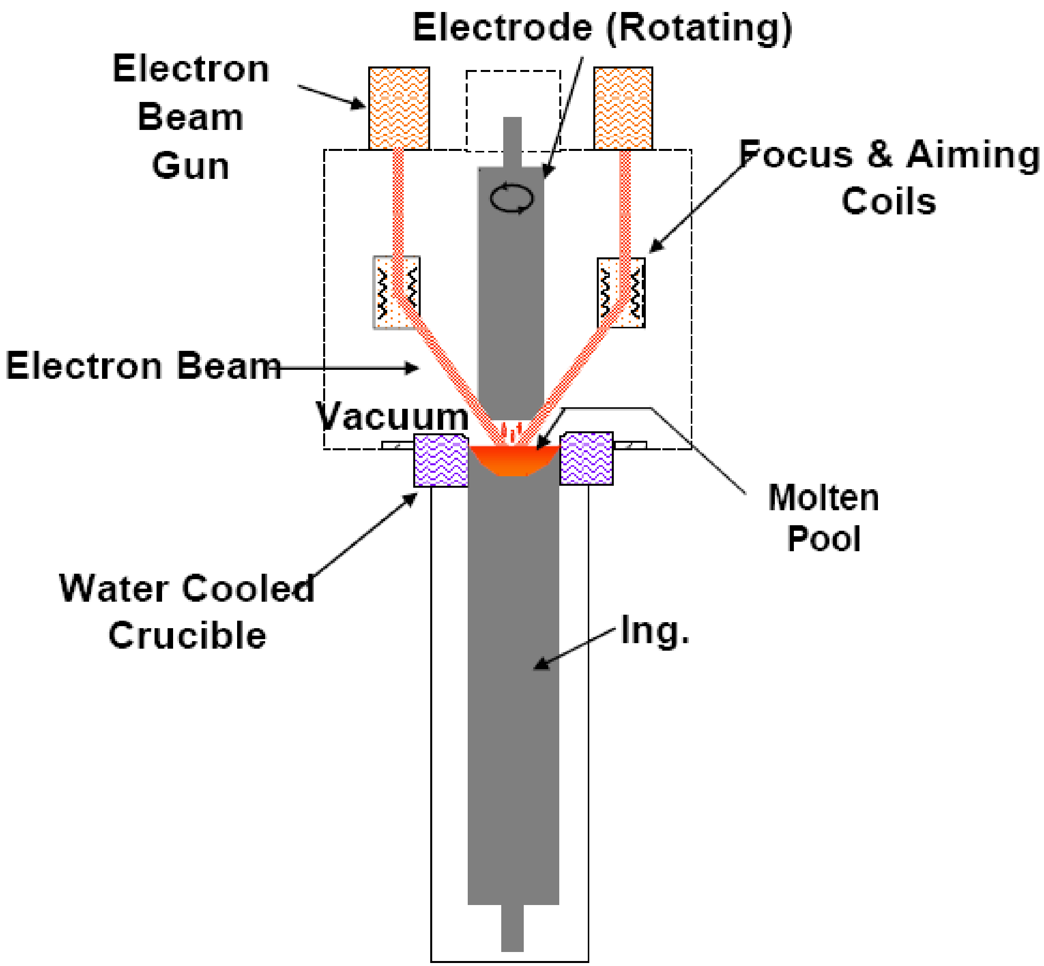


Fig. 3: Production flow chart at CBMM.

Electron Beam Melting

- Molten metal globules fall into a pool on the ingot which is contained in a water cooled copper cylinder (sleeve).
- Impurities are evaporated and pumped away.
- The pool is molten out to within a few mm of the crucible wall.
- During melting the ingot formed is continuously withdrawn through the sleeve.
- The rate of withdrawal has to be carefully coordinated with the rate of the material to insure complete melting of the feed material and proper outgassing.



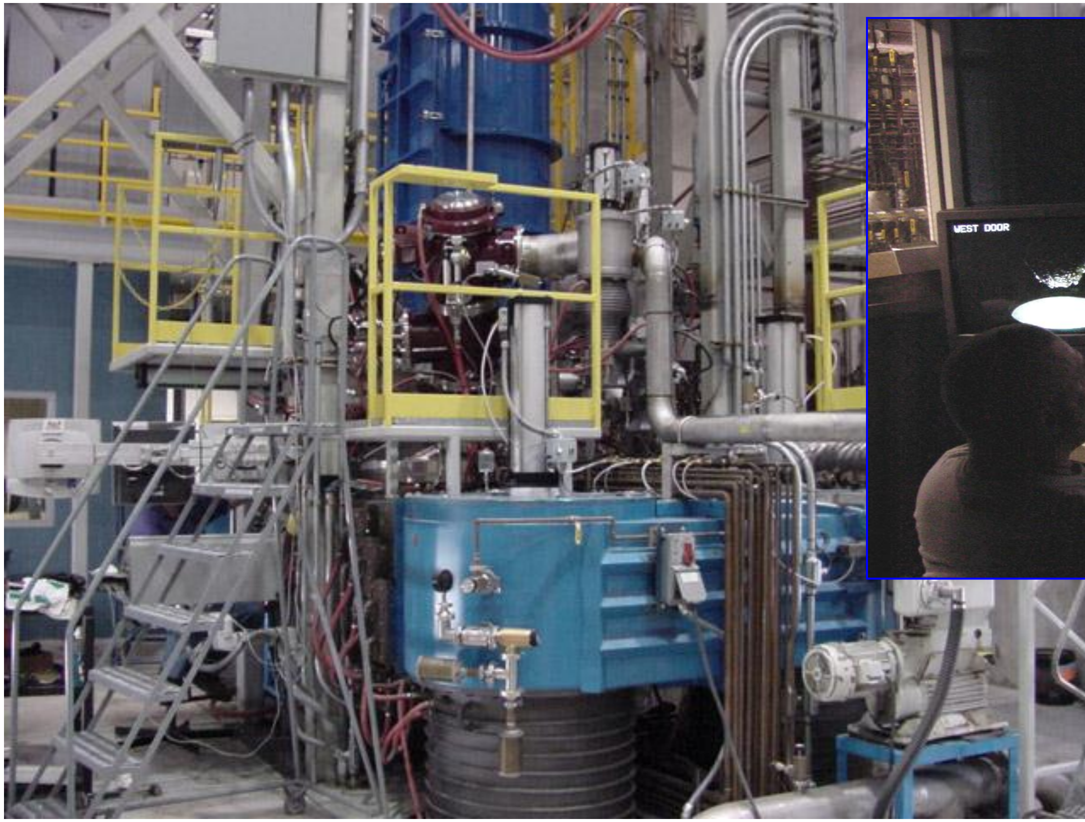
Electron beam melting of Nb

Electron Beam Melting

- As a result of the increasing demand for refractory metals in the last few decades, the electron-beam furnace has been developed to a reliable, efficient apparatus for melting and purification.

- There are several companies, which can produce high purity refractory metals in larger quantities: WahChang (USA), Cabot (USA), W.C.Heraeus (Germany), Tokyo Denkai (Japan), OTIC (China), CBMM (Brasil), H.C. Starck (Germany, USA)

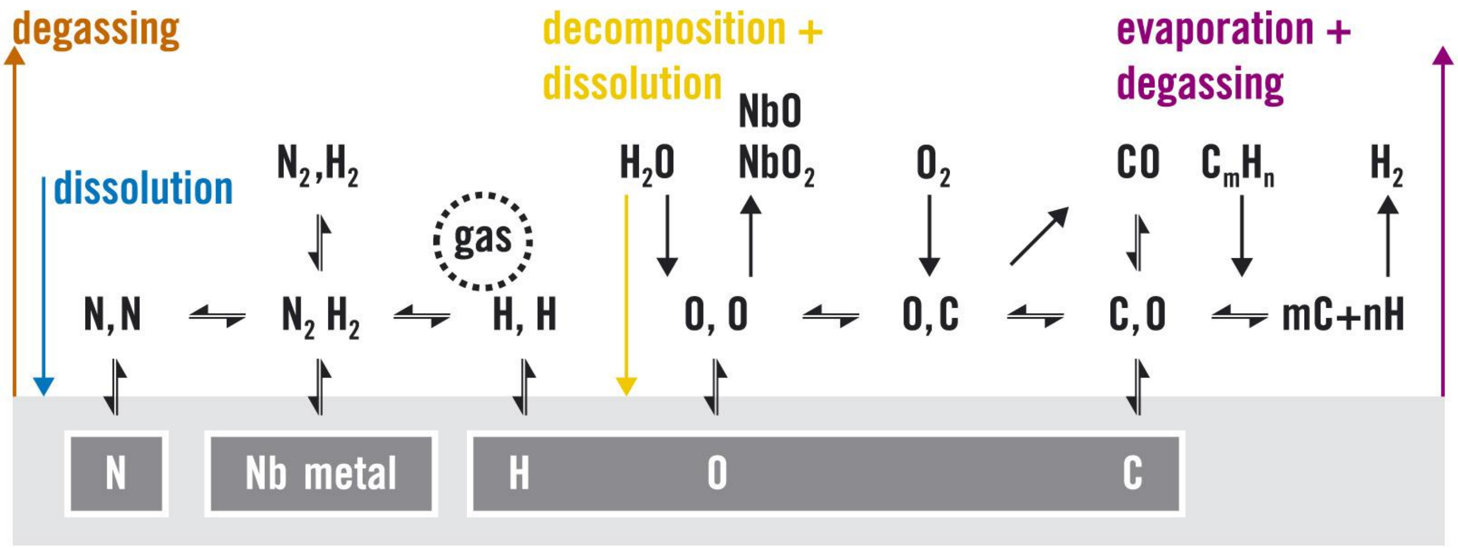
Electron Beam Refining Furnace



Furnace “S10” at ATI Wah Chang

- 4 900 mm diffusion pumps
- 200,000 l/sec
- 10-4 Torr
- 2,250 kW
- 3 EB guns
- Crucible diameter: 25-48 cm
- Ingot length: 2.9 m

Nb EB Refining



Metal-gas and gas-gas reactions during Nb EB refining

- **The heating temperature is a compromise between the maximization of purification and minimization of the material losses by evaporation.**
- **RRR=300-500 are reachable currently.**

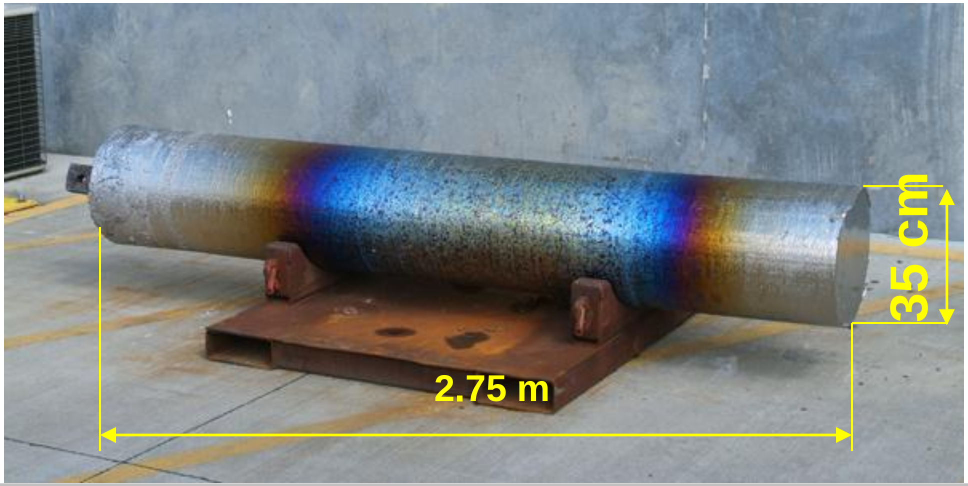
Nb EB Refining

- One problem sometimes observed with e-beam melted ingots is the nonhomogeneous distribution of impurities.
- The **skin** of the ingot has been found to contain more impurities than the inside.
- **Top to bottom inhomogeneity** has also been observed. The first part of the melt which usually ends up at the bottom getters impurities in the early stages of the melt.
- Machining away the skin and cutting away a short section from the bottom are recommended for a purer final product

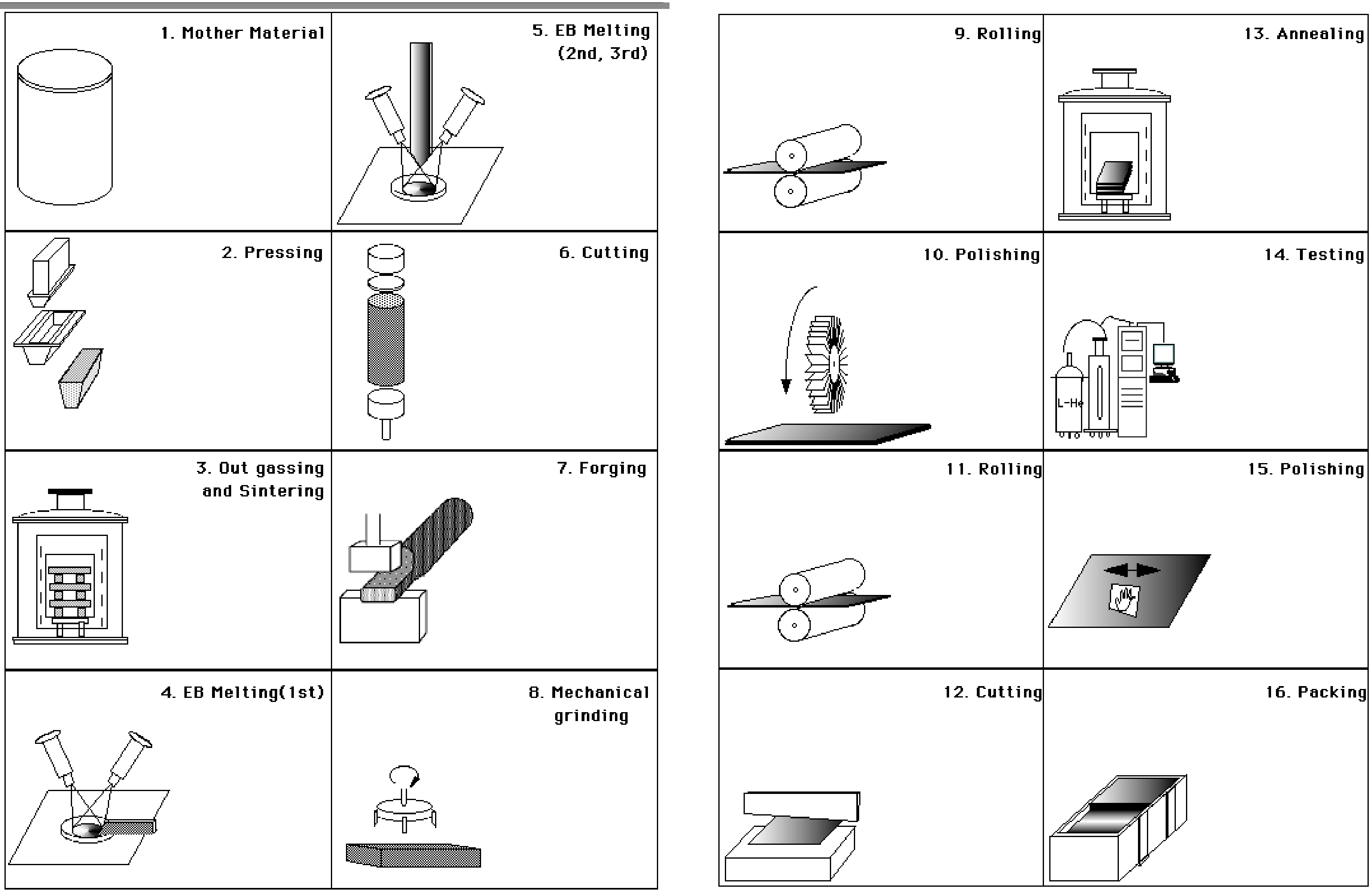
Niobium Ingot

Crucibles

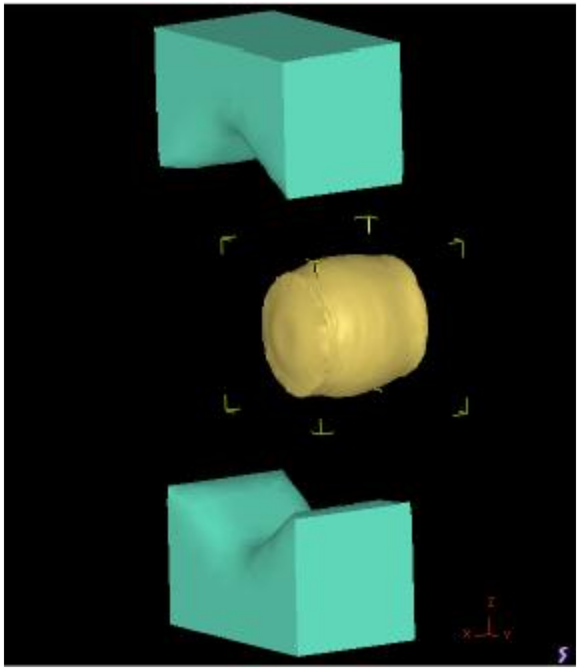
Intermediate

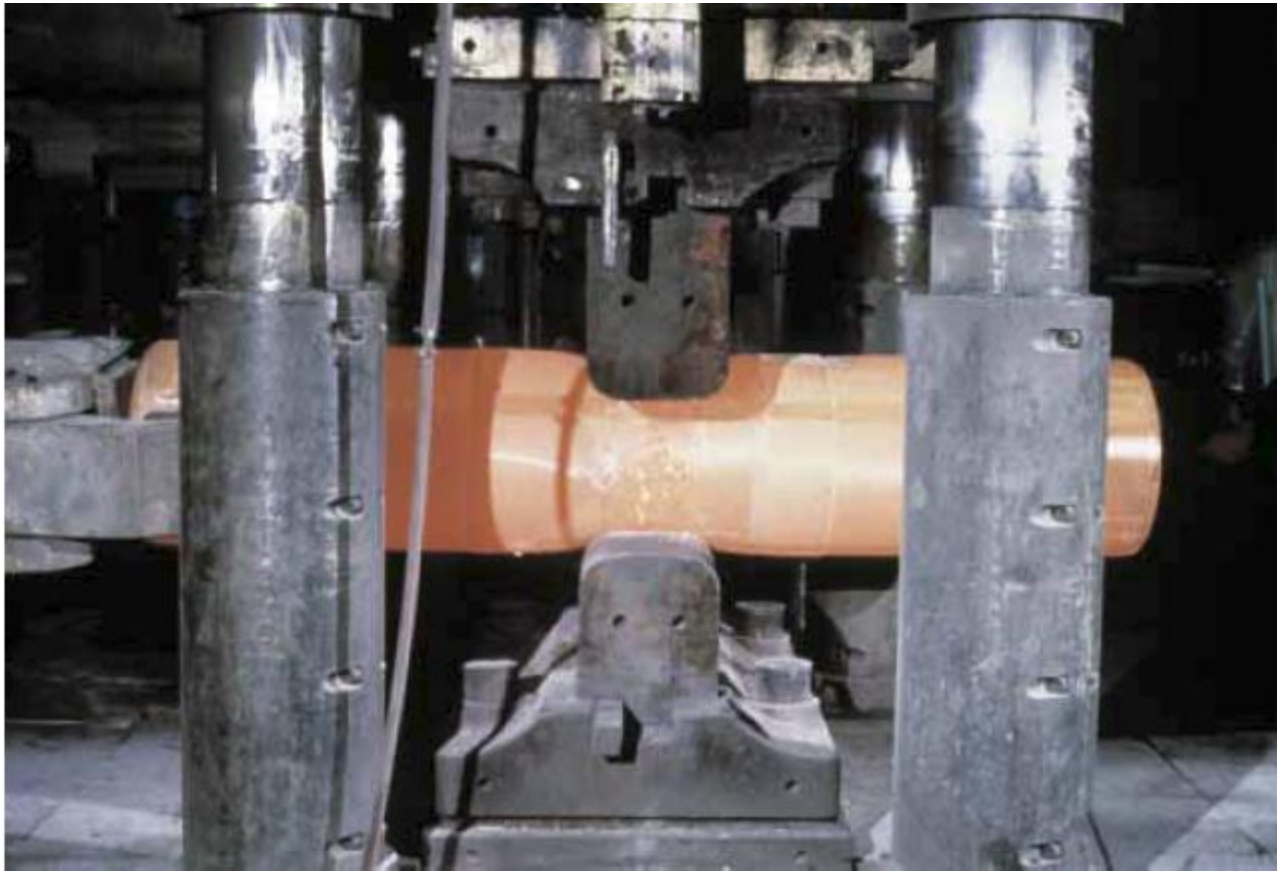


Fabrication of Fine-Grain Nb Sheets



Forging





2000 ton open die forge (Wah Chang)

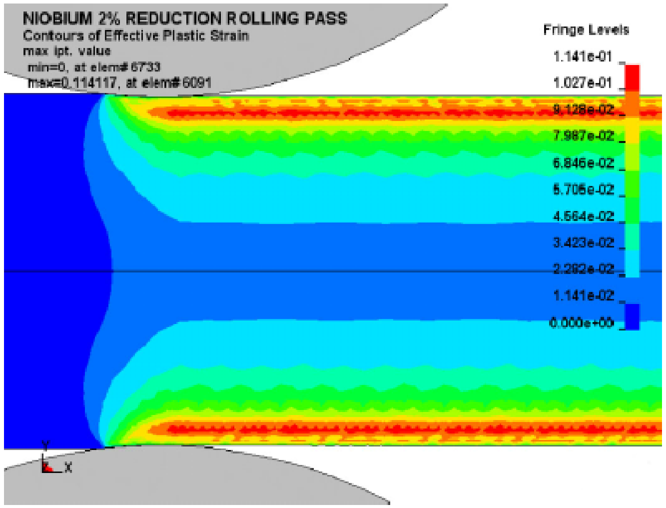
Rolling

700 mm wide cold rolling mill (Wah Chang)

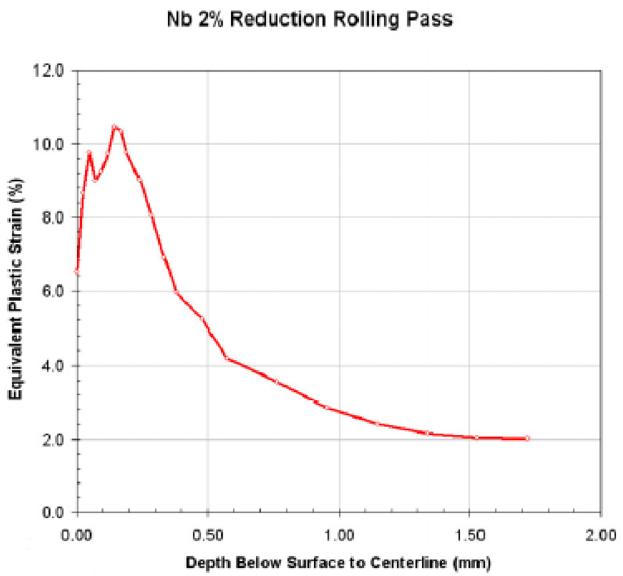
800 mm wide hot rolling mill (Wah Chang)

Hot rolling, used mainly to produce sheet metal is when industrial metal is passed or deformed between a set of work rolls and the temperature of the metal is generally above its recrystallization temperature. Cold rolling takes place below recrystallization temperature.

Damage Layer by Rolling

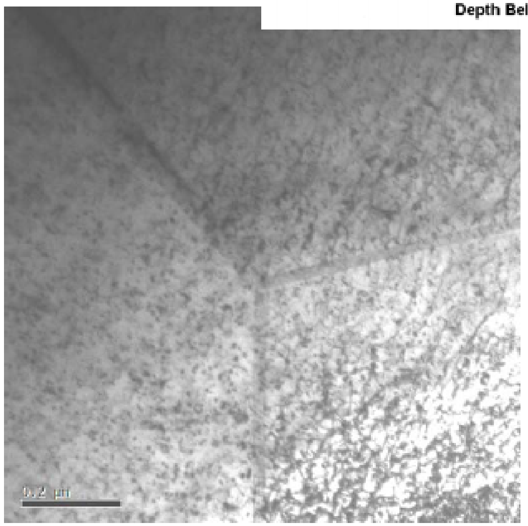


Finite element simulation of 2% reduction of 3.5 mm sheet with 1 cm diameter rolls. Strain is concentrated in the near-surface region



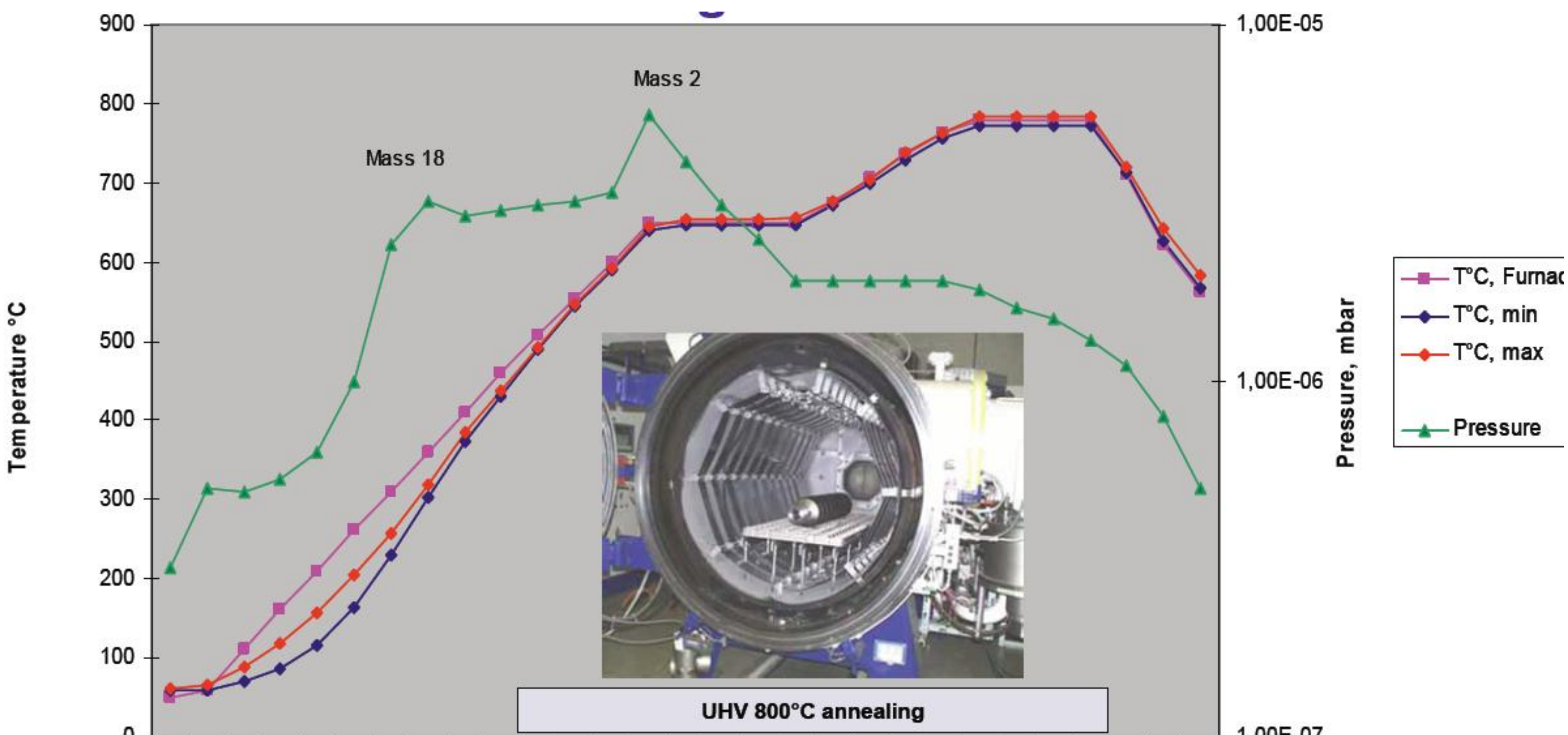
As-received RRR Nb Sheet,
20 μm below surface
(ion milled thin foil)

High dislocation density.



Transmission electron microscopy image (BFTEM)

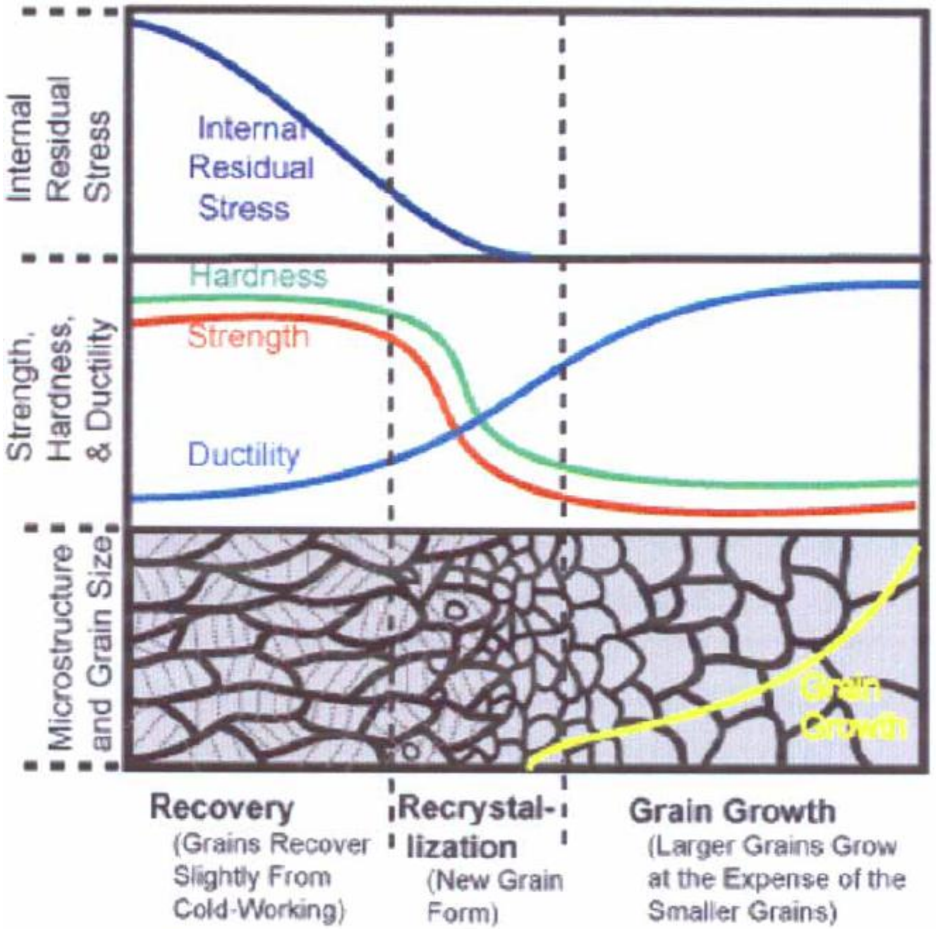
Annealing



	08:30	08:45	09:00	09:15	09:30	09:45	10:00	10:15	10:30	10:45	11:00	11:15
T°C, Furnace	50	59	112	161	210	261	310	361	411	460	507	554
T°C, min	60	60	70	87	117	165	229	304	374	430	489	544
T°C, max	61	65	89	119	157	205	257	319	384	438	492	547
Pressure	3,0E-7	5,0E-7	4,9E-7	5,3E-7	6,3E-7	1,0E-6	2,4E-6	3,2E-6	2,9E-6	3,0E-6	3,1E-6	3,2E-6

	11:30	11:45	12:00	12:15	12:30	12:45	13:00	13:15	13:30	13:45	14:00	14:15	14:30	14:45	15:00	15:15	15:30
T°C, Furnace	600	650	650	650	650	650	675	706	736	763	780	780	780	780	710	621	562
T°C, min	591	640	646	647	648	647	672	700	730	756	773	773	773	773	713	627	568
T°C, max	593	645	655	655	654	656	677	705	738	763	783	783	783	783	721	642	583
Pressure	3,4E-6	5,6E-6	4,1E-6	3,1E-6	2,5E-6	1,9E-6	1,9E-6	1,9E-6	1,9E-6	1,9E-6	1,8E-6	1,6E-6	1,5E-6	1,3E-6	1,1E-6	8,0E-7	5,0E-7

Annealing: recrystallization



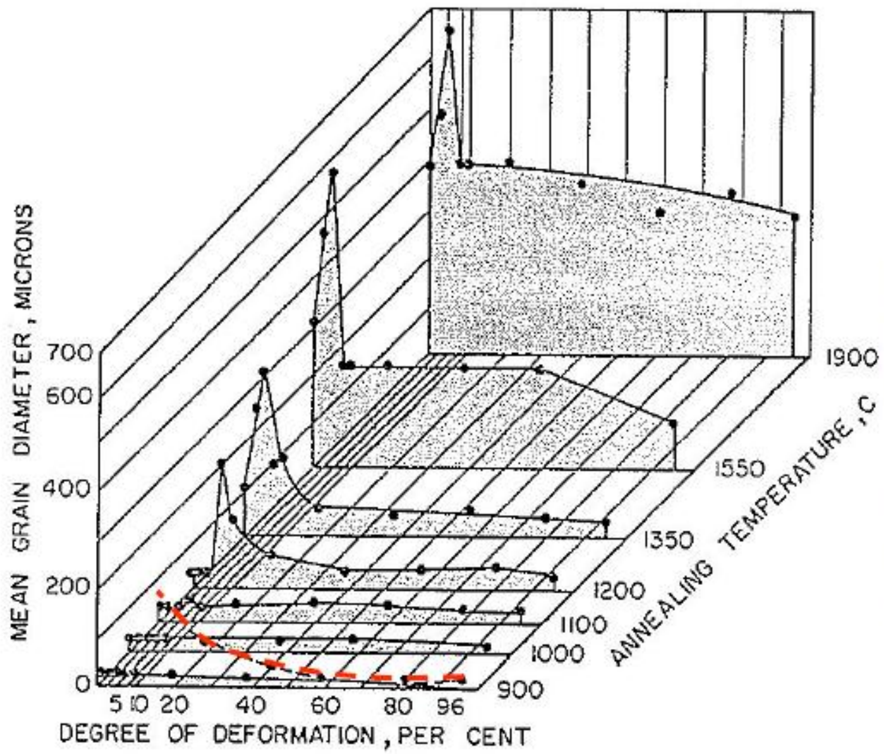
Choosing the proper annealing conditions is important to produce the correct grain size near 100% recrystallization and keep the highest possible purity (RRR).

Recovery: removing point defects, decrease and change direction of dislocations

Recrystallization: nucleation of new grains and growing of new crystals
Grain growth: increase in grain size

Recrystallization

Commercial "Pure Nb"
RRR ~ 50-100



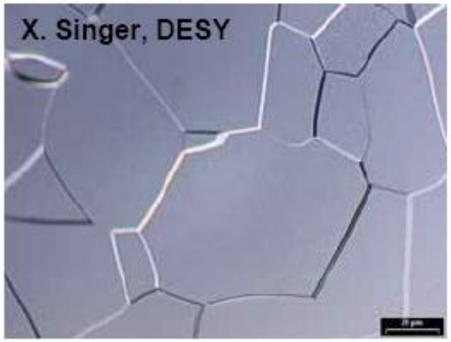
Recrystallization

We need recrystallized material

- deformation > 65% =>
  - uniform nucleation
  - small grains
- if purity ↑, $T_{recryst}$ ↓
  - RRR ≤ 100 => $T_{recryst}$ ≥ 900 C
  - RRR 300 => $T_{recryst}$ ~ 800 C*
  - RRR 400 => $T_{recryst}$ ~ 750 C ?

Not completely recrystallized Nb

Completely recrystallized Nb

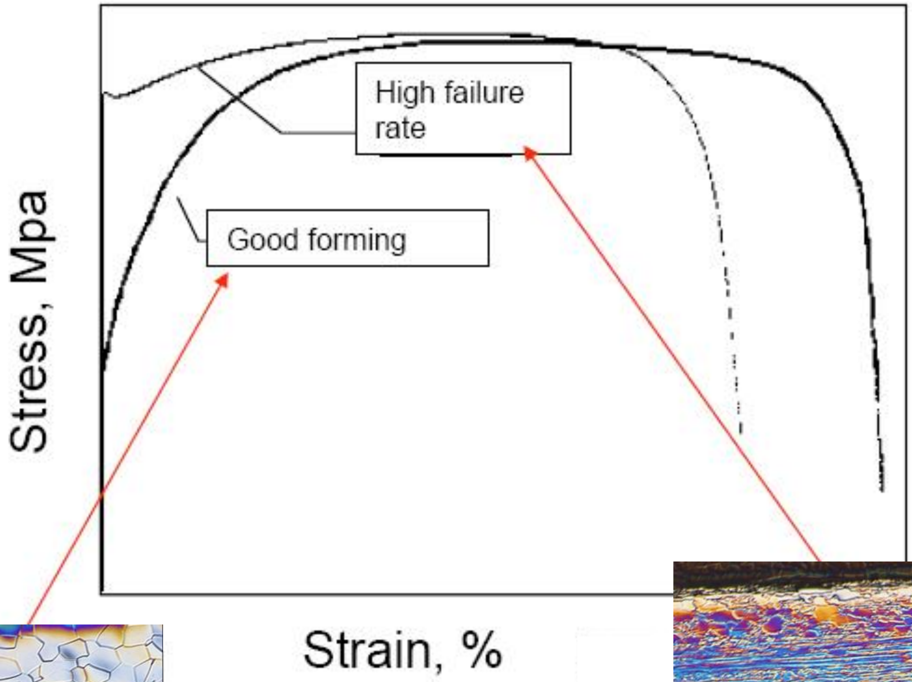


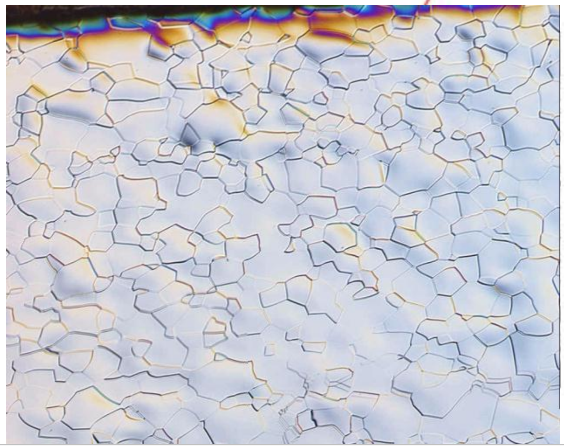
Recrystallization

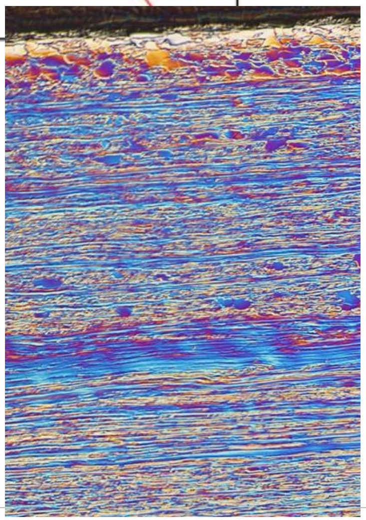
The grain structure influences the formability

Therefore the yield strength, σ0,2 is specified for XFEL as

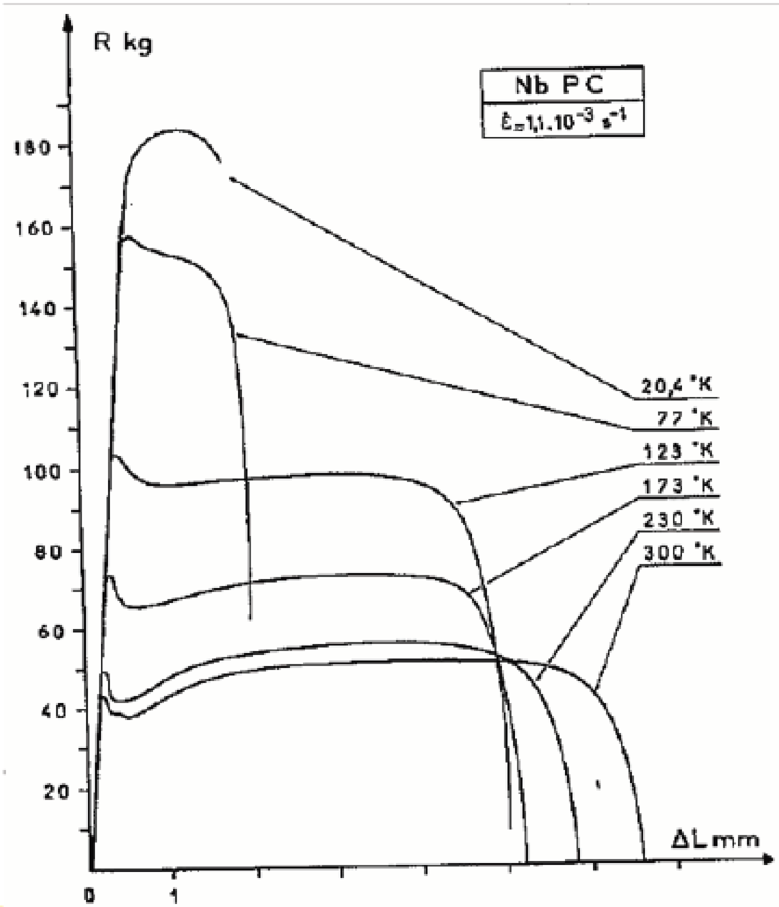
50<σ0,2<100 N/mm² (Mpa)







Nb Mechanical Properties at Low T



- Yield strength ↑↑ when T ↓
- ductility ↓ (T< 20 K => Nb is brittle)

Jefferson Lab

Old Dominion University

Nb Sheets: Technical Specifications

Concentration of impurities in wt.ppm				Mechanical properties	
Ta*	≤ 500	H*	≤ 2	Yield strength**, $\sigma_{0,2}$	$50<\sigma_{0,2}<100$ N/mm² (Mpa)
W*	≤ 70	N*	≤ 10	Tensile strength**	> 100 N/mm² (Mpa)
Ti*	≤ 50	O*	≤ 10	Elongation at break**	30 %
Fe*	≤ 30	C*	≤ 10	Vickers hardness** HV 10	≤ 60
Mo*	≤ 50	RRR*	≥ 300	Absence of foreign material inclusions*	Proven by scanning
Ni*	≤ 30	Recrystal. degree. Grain size* ,** ?	≈ 50 µm	Texture *, ** ?	

* - relevant for performance

** - relevant for successful fabrication

Nb Sheets Quality Control

RRR measurement

東京電解（株）

Tensile test

Tokyo Denkay (Japan)

Gas analysis

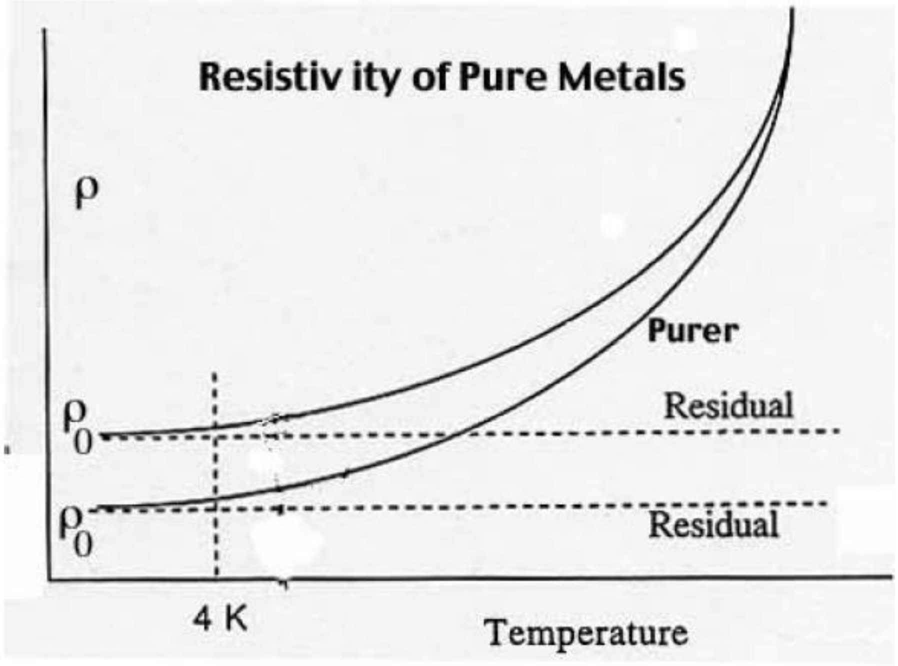
Gas analysis (Hydrogen, Oxygen, Nitrogen) ：HORIBA

Nb Purity: RRR

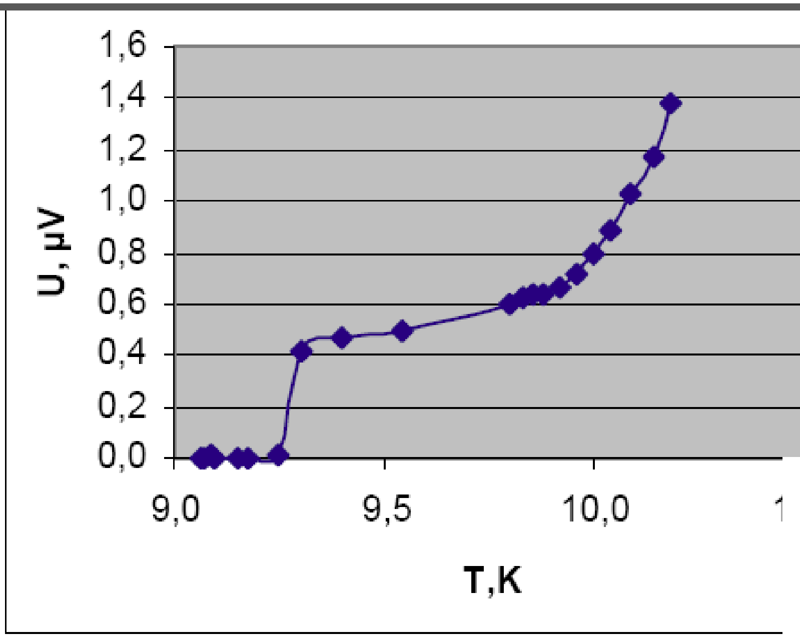
Electrical resistivity of metals at low temperatures is related to the impurity concentrations. The residual resistivity at T=0K is caused mainly by scattering of electrons by impurities.
Residual Resistivity Ratio:

$$RRR = \frac{\rho(295K)}{\rho(4.2K)}$$

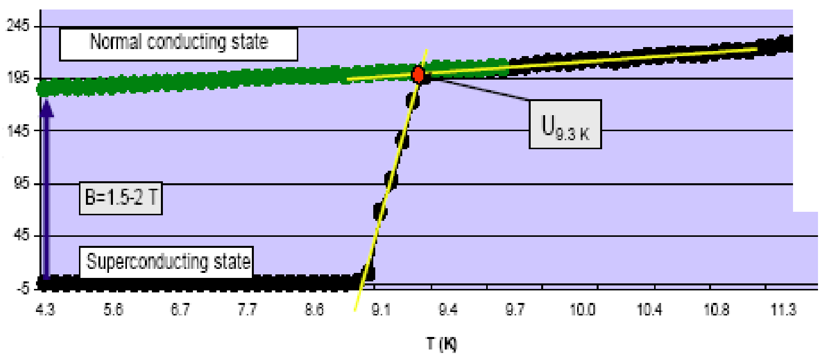
$$\rho(T) = \rho_{res} + \rho_{ideal}(T)$$

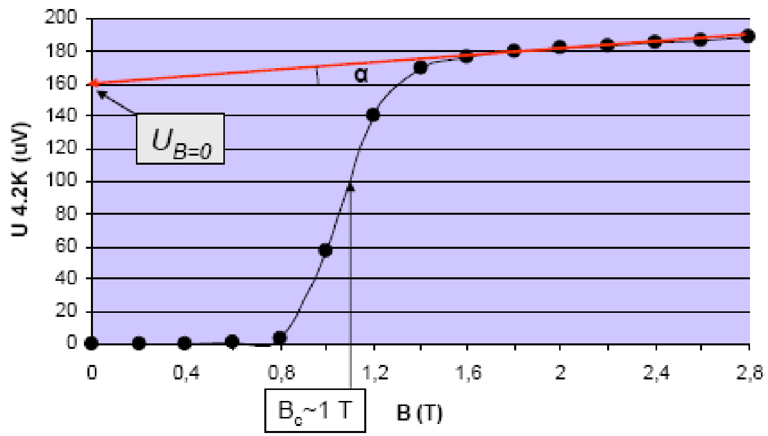


RRR Measurement



Temperature dependence of resistivity for superconducting Nb at temperatures close to Tc

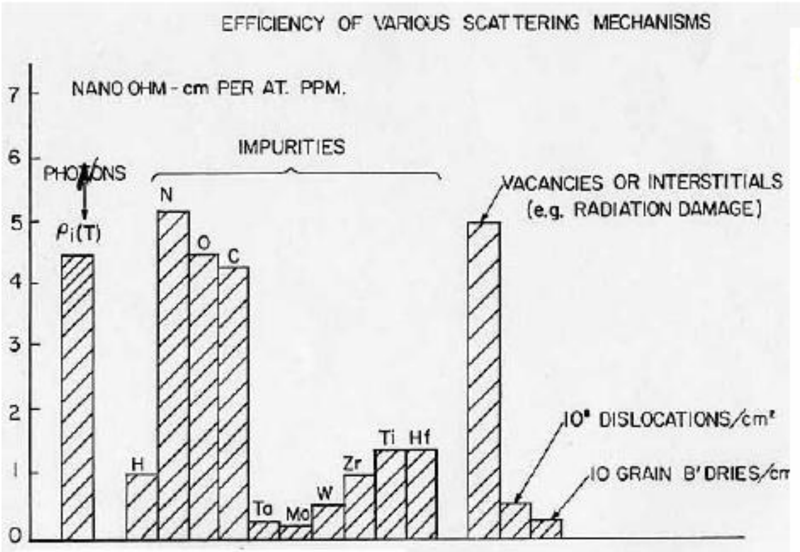




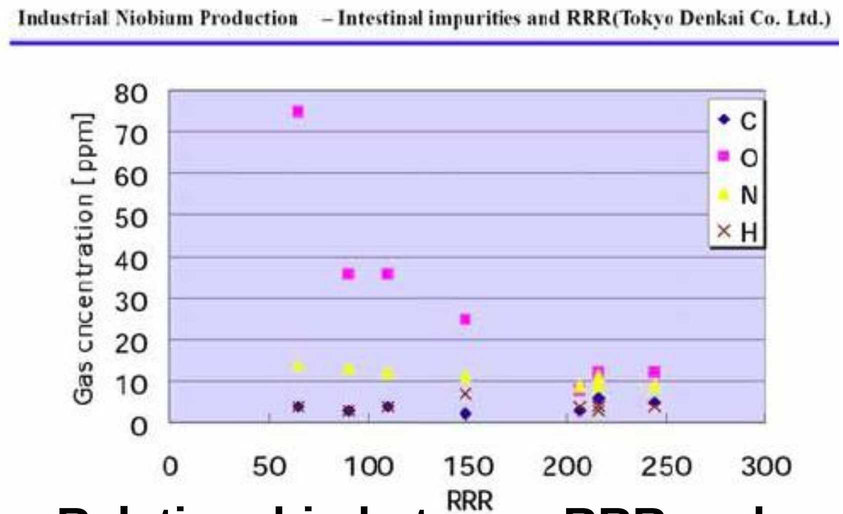
RRR determination by magnetic field extrapolation method

DC method: extrapolation of U(T) curve

Influence of Impurities on RRR



Contribution of different defects in the scattering mechanism:



Relationship between RRR and nonmetallic impurities measured by Tokyo Denkai

$$RRR = \frac{\rho(300K)}{\rho_{ideal}(4.2K) + \sum_i \frac{\partial \rho_i}{\partial C_i} C_i}$$

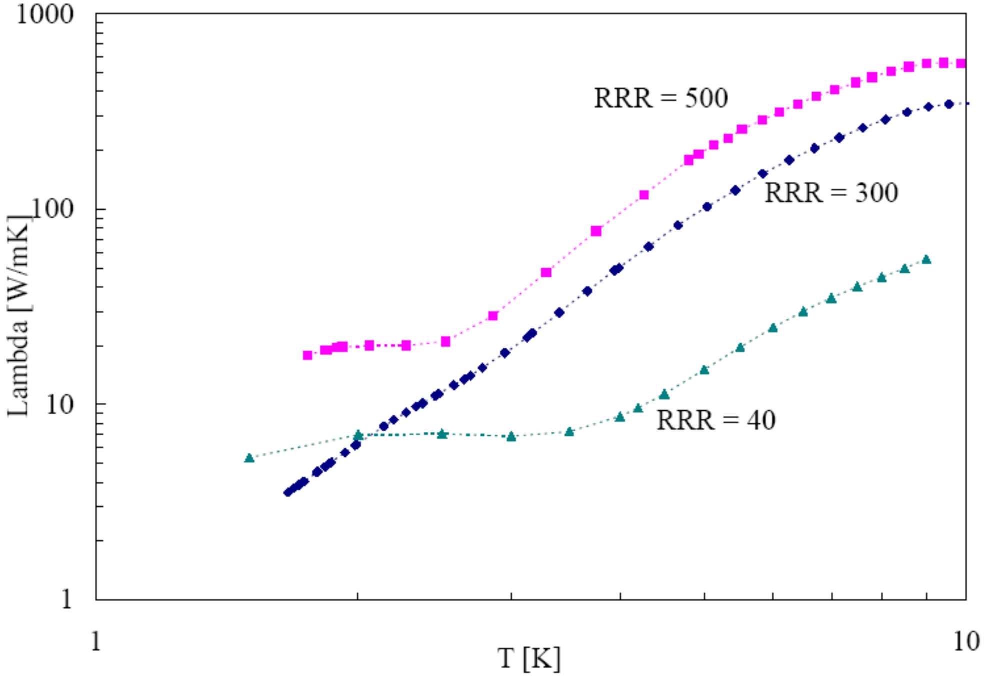
Expected RRR contribution for Nb for 1 wt ppm of impurities

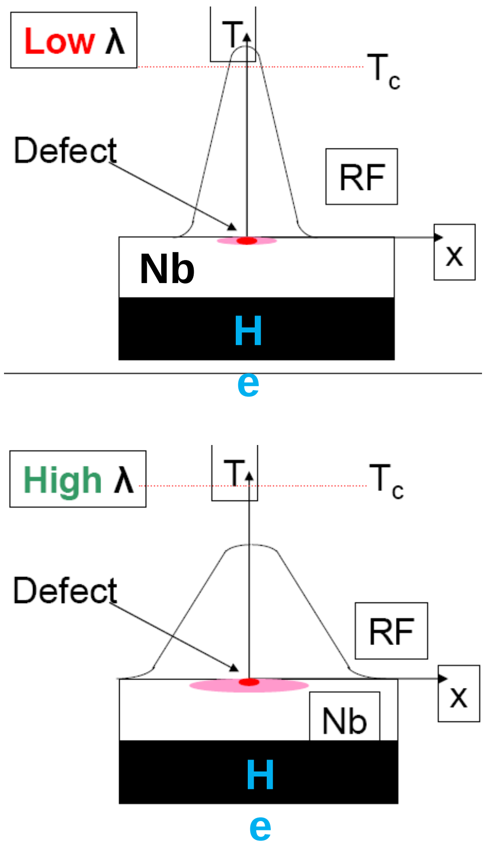
:nent	RRR	Element	RRR
H	2640	Zr	102 000–239 000
N	4230	Hf	200 000
C	4380	W	262 000–721 000
O	5580	Mo	717 000
Ti	53 700	Ta	1 140 000

$\rho(300K) = 14.6\ \mu\Omega$ cm

$RRR_{ideal} \cong 35{,}000$

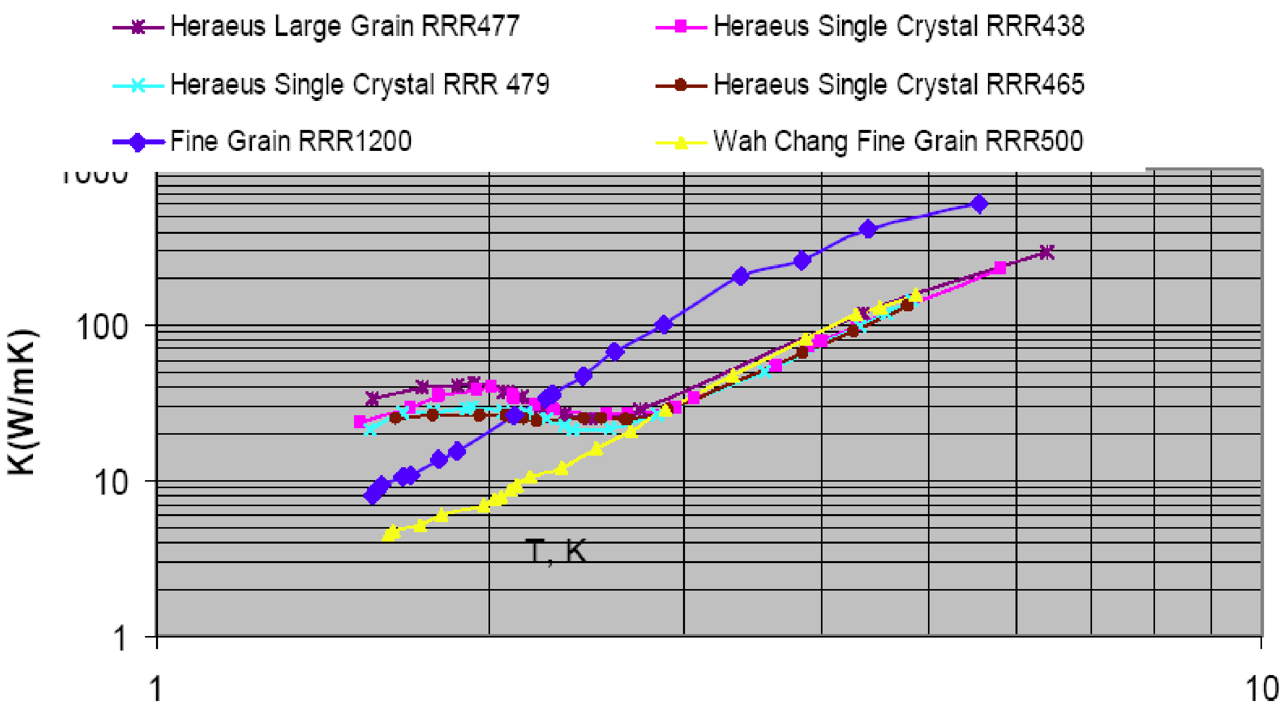
Nb Thermal Conductivity





Rule of thumb:
$\lambda(4.2K) = C \cdot RRR$
$C \sim 0.25$ W/(m K)

Nb Thermal Conductivity



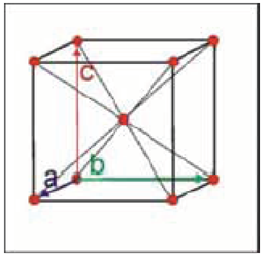
Phonon peak is clearly observed for single crystals/large grain samples.

$$\lambda(T,RRR,G)=R(y)\cdot\left[\frac{\rho_{295K}}{L\cdot RRR\cdot T}+a\cdot T^2\right]^{-1}+\left[\frac{1}{D\cdot\exp(y)\cdot T^2}+\frac{1}{B\cdot G\cdot T^3}\right]^{-1}$$

Electron term — **Lattice term**

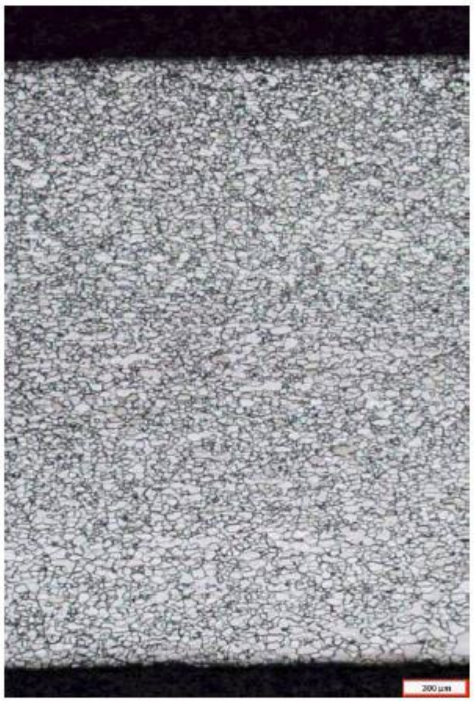
$y = \Delta/k_B T$
$R(y) = \lambda_{es}/\lambda_{en}$
$L \cong 2.45\times10^{-8}$ W/K^2
G: phonon mean free path ~ grain size

Texture

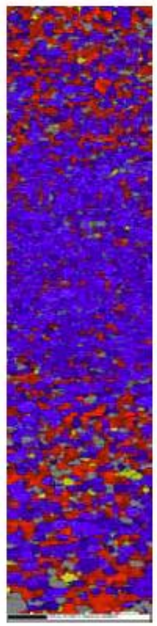


bcc lattice (body centered cubic)

3 mm Nb sheet

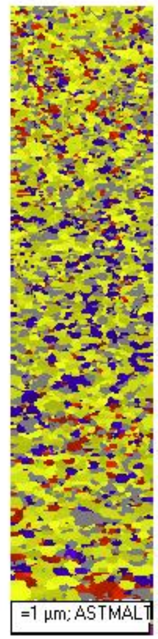


ND

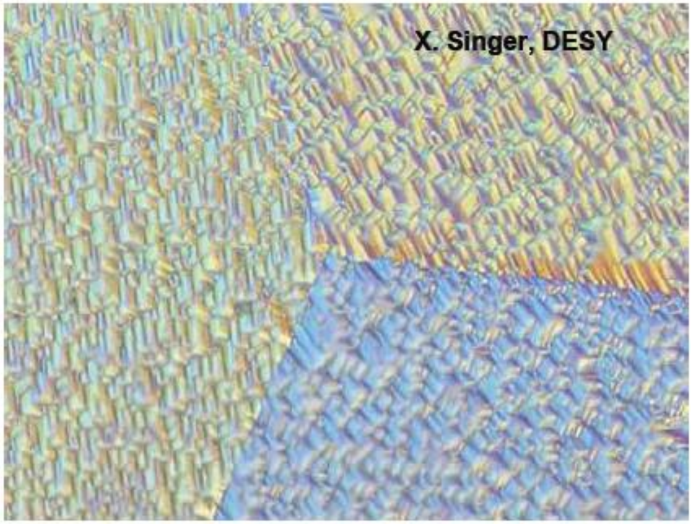


H.C.Starck

Z



Electron back scattering diffraction EBSD



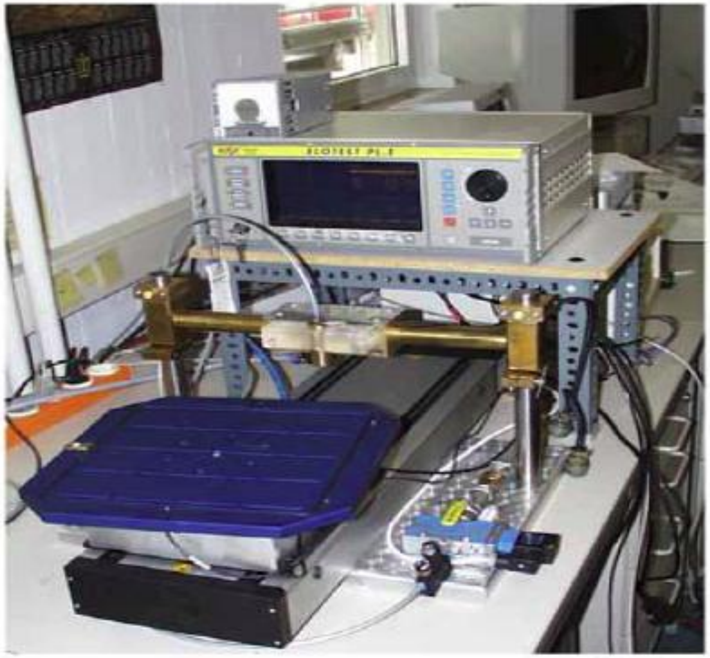
Microstructure of the three grains of Nb after proper etching (optical microscope). The crystal lattice in neighboring grains is the same (bcc) but has a different orientation

Niobium sheet after annealing. Colors refers to crystal orientations (orientation image)

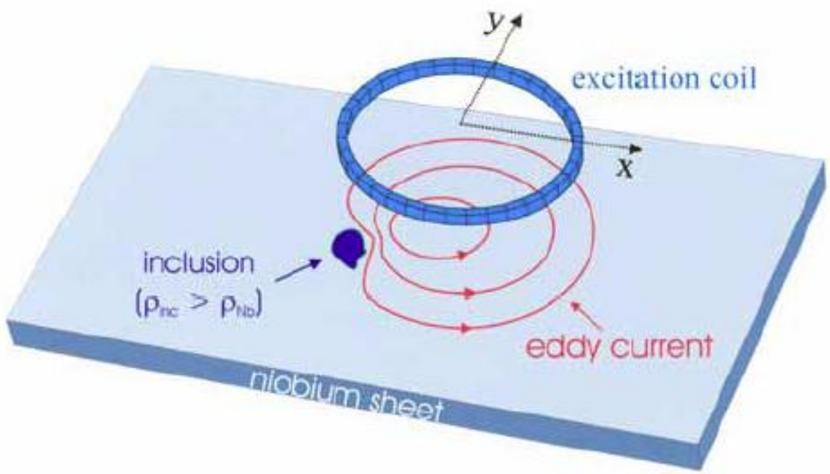
Price

- High RRR Nb (RRR ~ 300): ~ $ 530/kg
- Reactor grade Nb (RRR ~ 30): ~ $ 130/kg

Quality Control of Nb Sheets

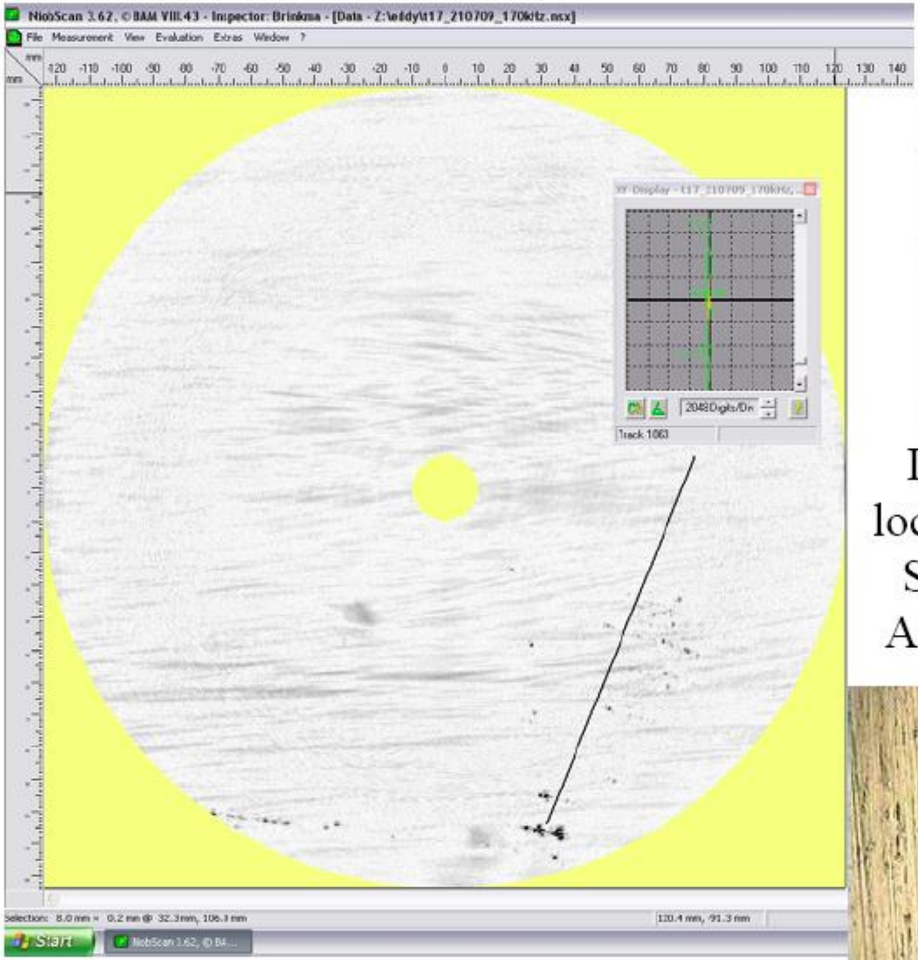


DESY eddy current scanning apparatus for niobium discs. 100% Nb sheets for TTF scanned and sorted out. Feedback to manufacturer was very important

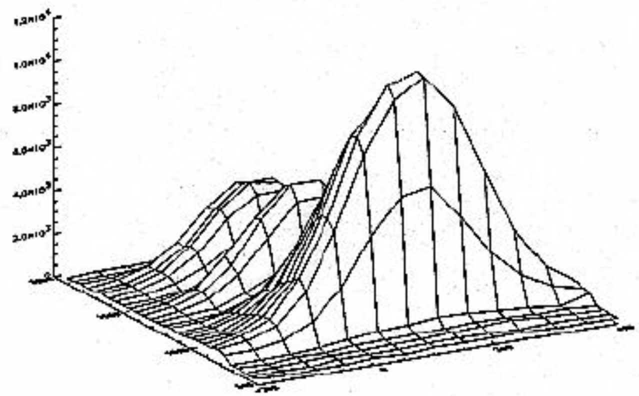


Principle of eddy current measurement

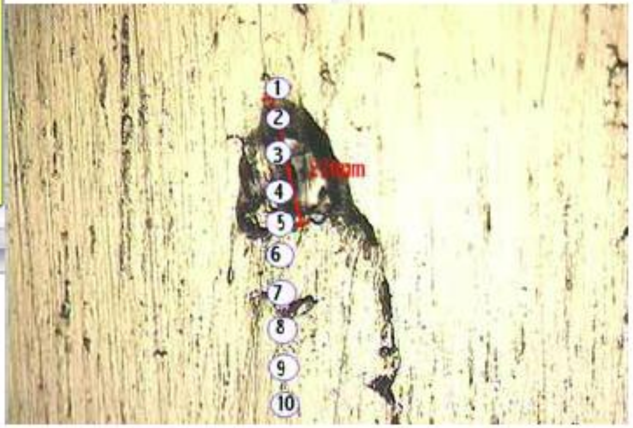
Defects in Nb Sheets



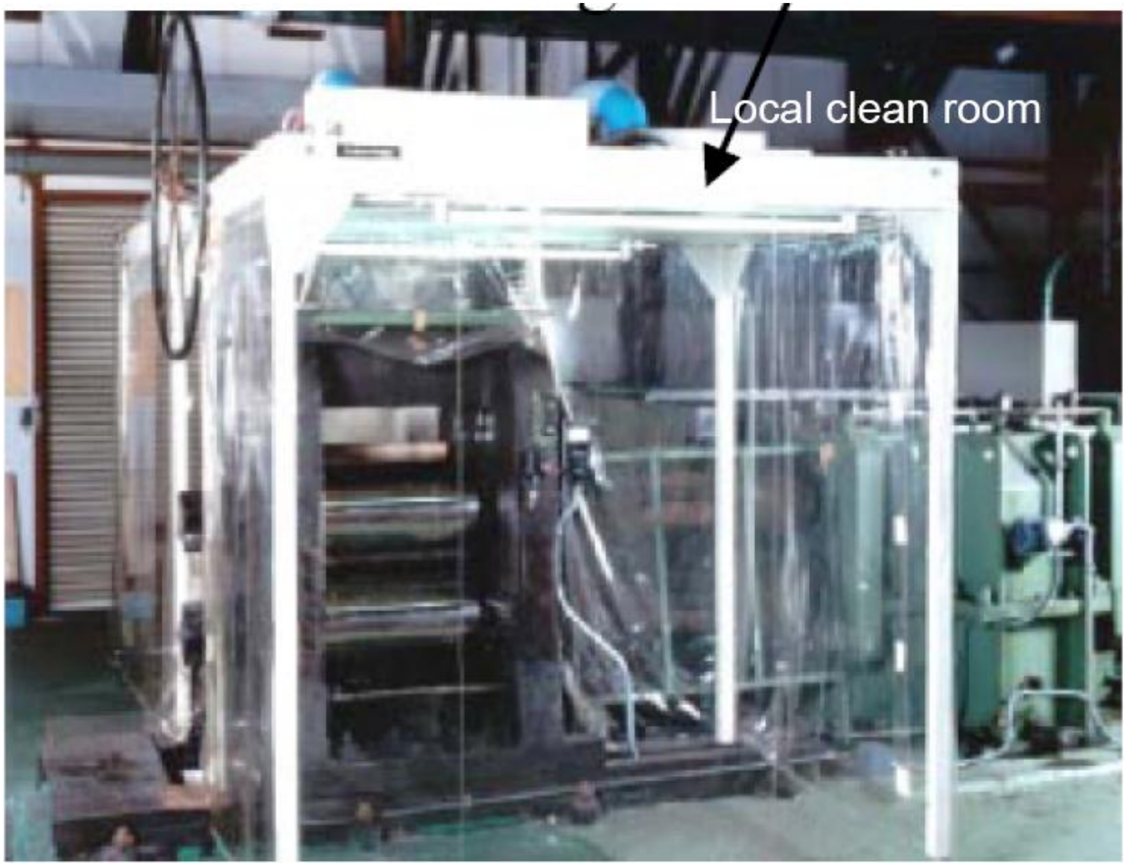
Iron particles, probably imbedded during rolling T17



Iron signal distribution in one of the locations of the Nb sheet T17 measured Synchrotron Radiation Fluorescence Analysis (SURFA) and defects image.

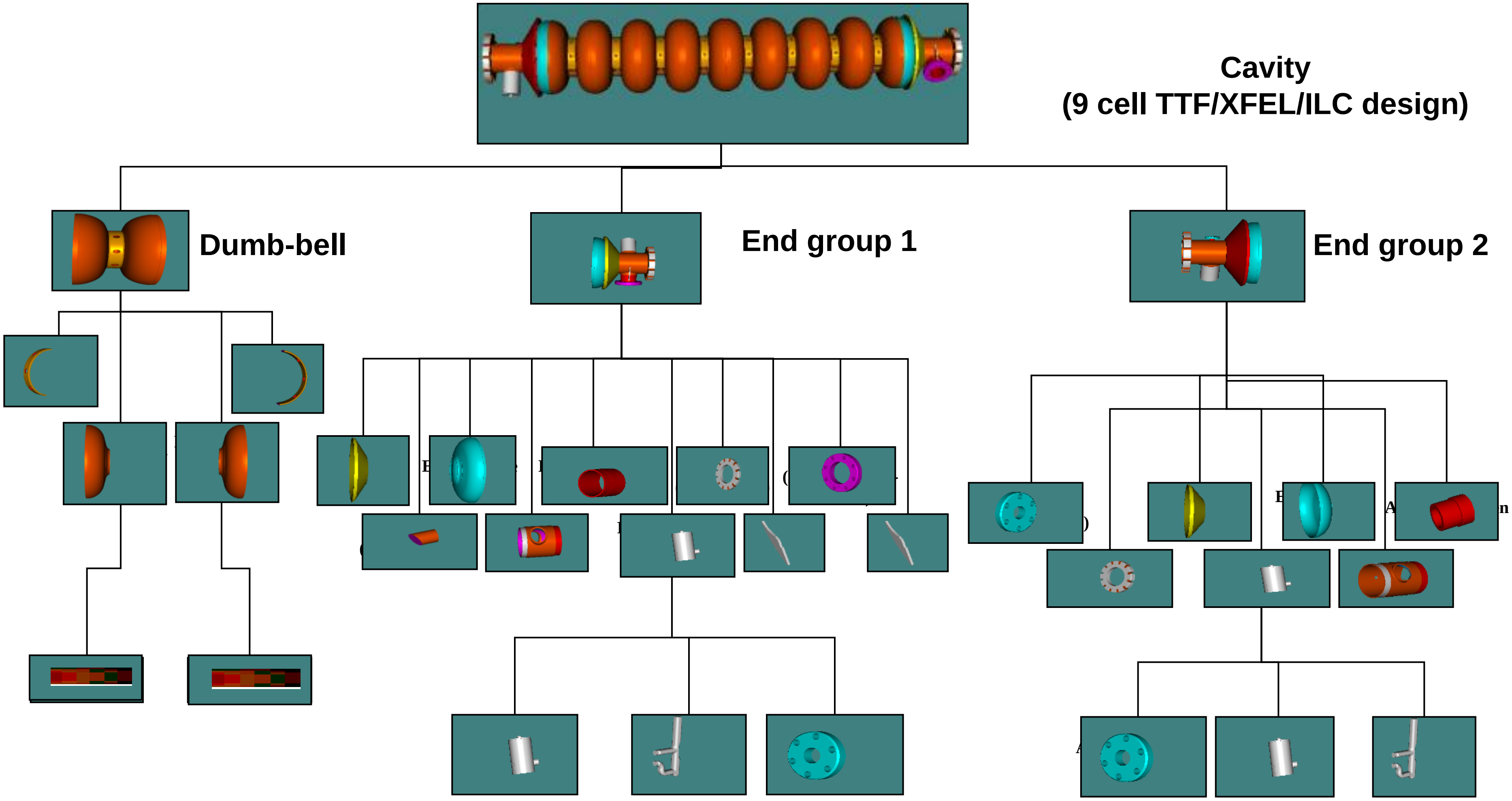


Feedback Example: Final Rolling

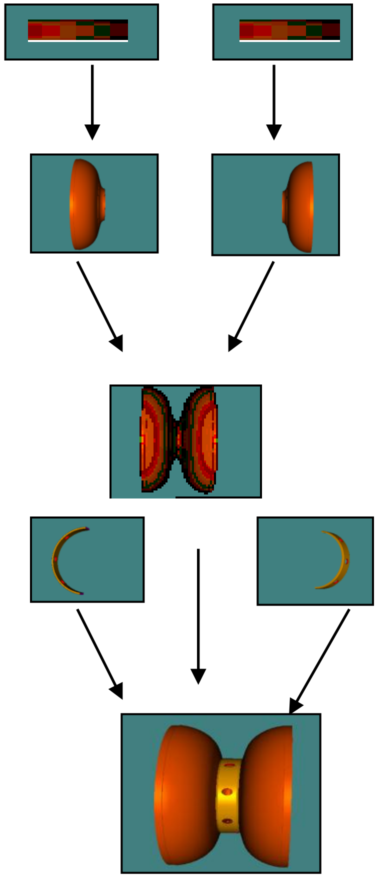


Example of the feedback to companies: Tokyo Denkai improved the cleanness around of the rolling equipment

Overview of Cavity Components (ILC)



Dumb-bell Fabrication

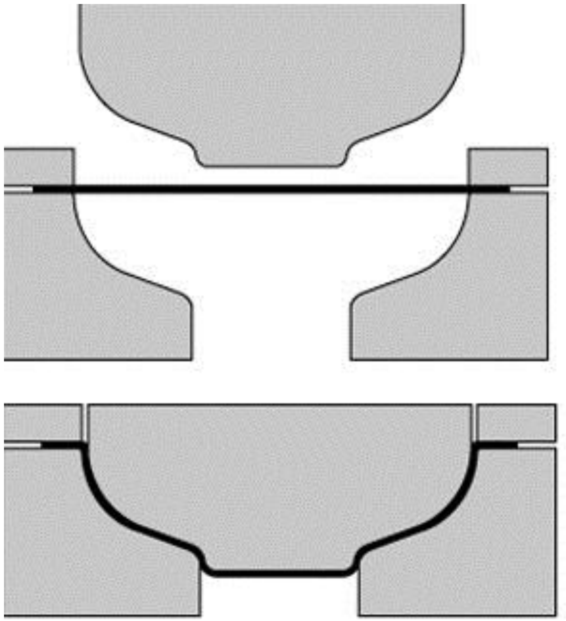


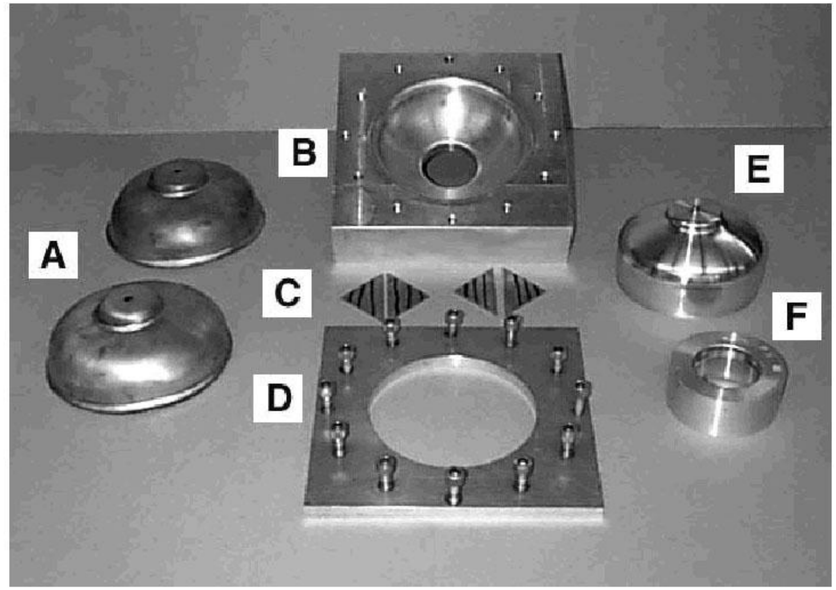
Dumb- bell

1. Deep drawing
2. Mechanical measurement
3. Cleaning (by ultra sonic cleaning + rinsing)
4. Trimming of iris region and reshaping of cups if needed
5. Cleaning
6. RF measurement of cups
7. Buffered chemical polishing + Rinsing (for welding of Iris)
8. Welding of Iris
9. Welding of stiffening rings
10. Mechanical measurement of dumb-bells
11. Reshaping of dumb-bell if needed
12. Cleaning
13. RF measurement of dumb-bell
14. Trimming of dumb-bells (Equator regions)
15. Cleaning
16. Intermediate chemical etching (BCP, 20- 40 µm) + Rinsing
17. Visual Inspection of the inner surface of the dumb-bell, local grinding if needed + (second chemical treatment + inspection)

Dumb-bell ready for cavity

Deep Drawing





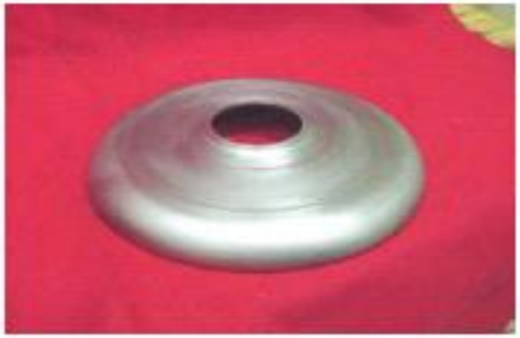
- Deep drawing with hydraulic press
  - 100 tons + 25 tons for iris coining for 10.25” discs (ILC)
  - 400 tons + 50 tons for iris coining for 15.5-16.5” discs (SNS)

Deep Drawing

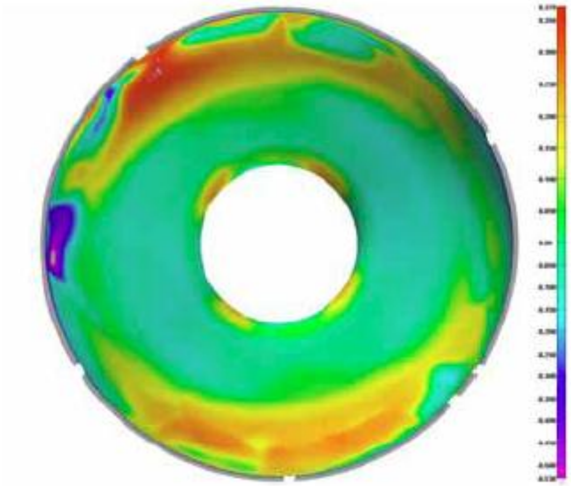


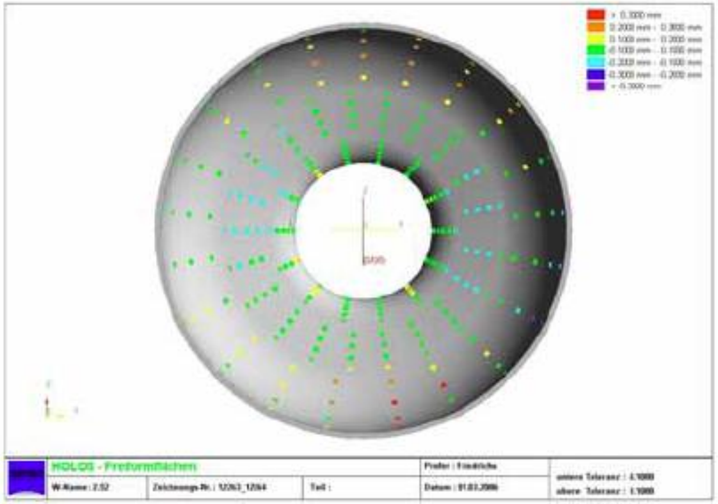





Shape Measurement





Shape accuracy: optical and mechanical 3D measurement of the half cell shape

Mechanical Grinding

- Mechanical grinding of visible local defects with aluminum oxide grinding discs

RF Measurements of Dumb-bells and Middle-Cups

Elongation ΔLe in the magnetic field region

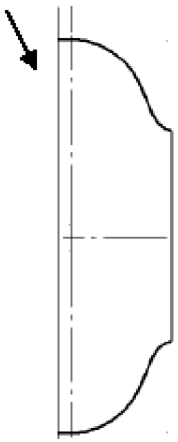
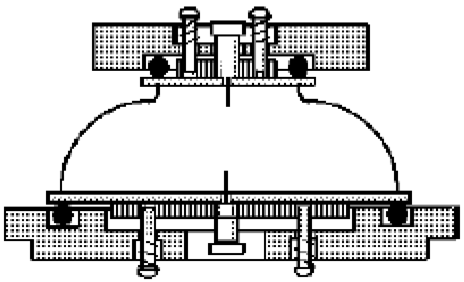
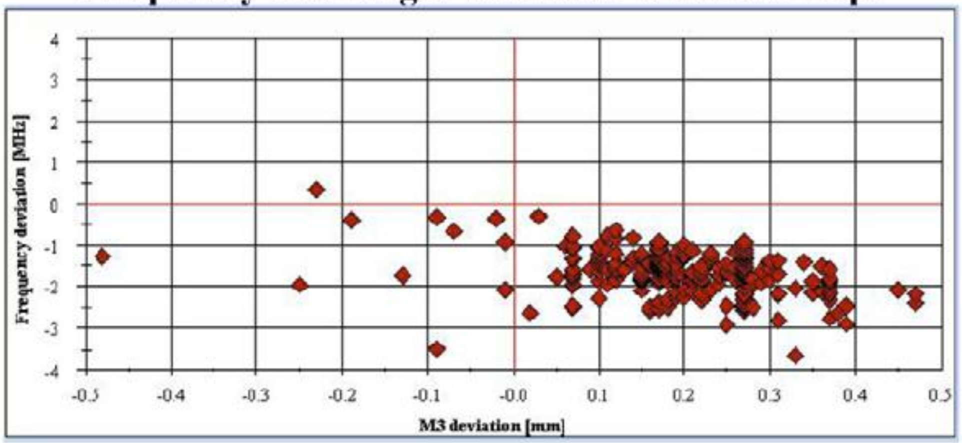


Figure 3: Trimming of the equator to adjust the elongation at the equator



Frequency and length deviation of middle cups



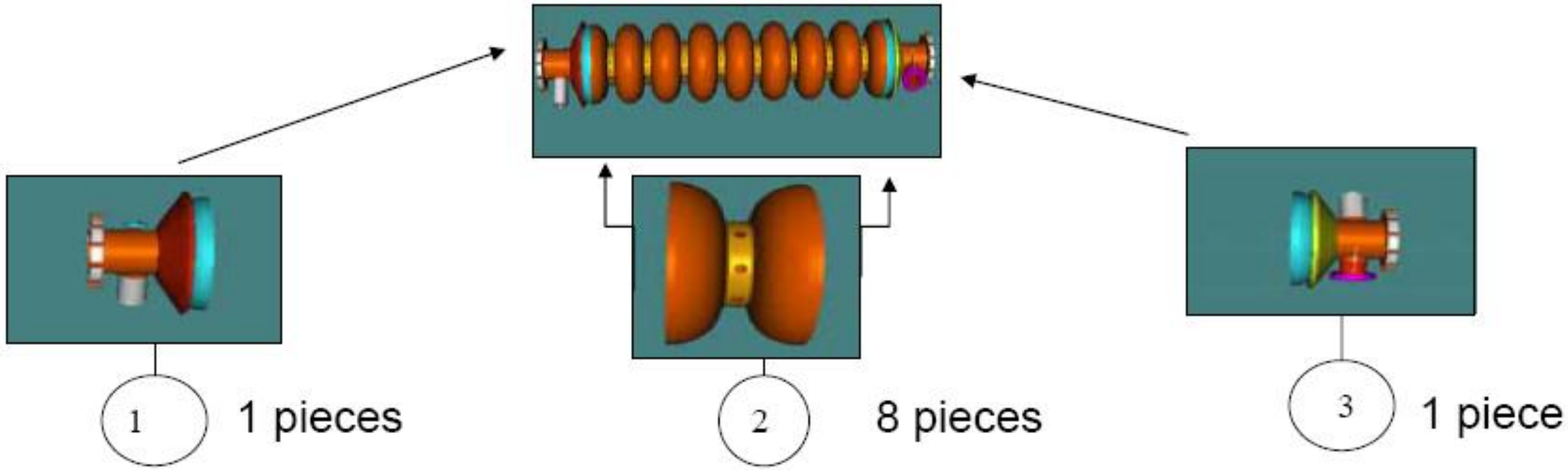
Wah Chang (EDMS-DB)

Measure frequency and length to determine how much to trim at the equator to obtain target frequency and length of the cavity fully welded

Cavity Parts

- Welding sequence:
  - Two cups form a dumb bell
  - Stiffening ring at iris
  - Welding together two dumb-bells
  - Add next dumb bell
  - Add end group
  - For mass production: weld all dumb bells at once

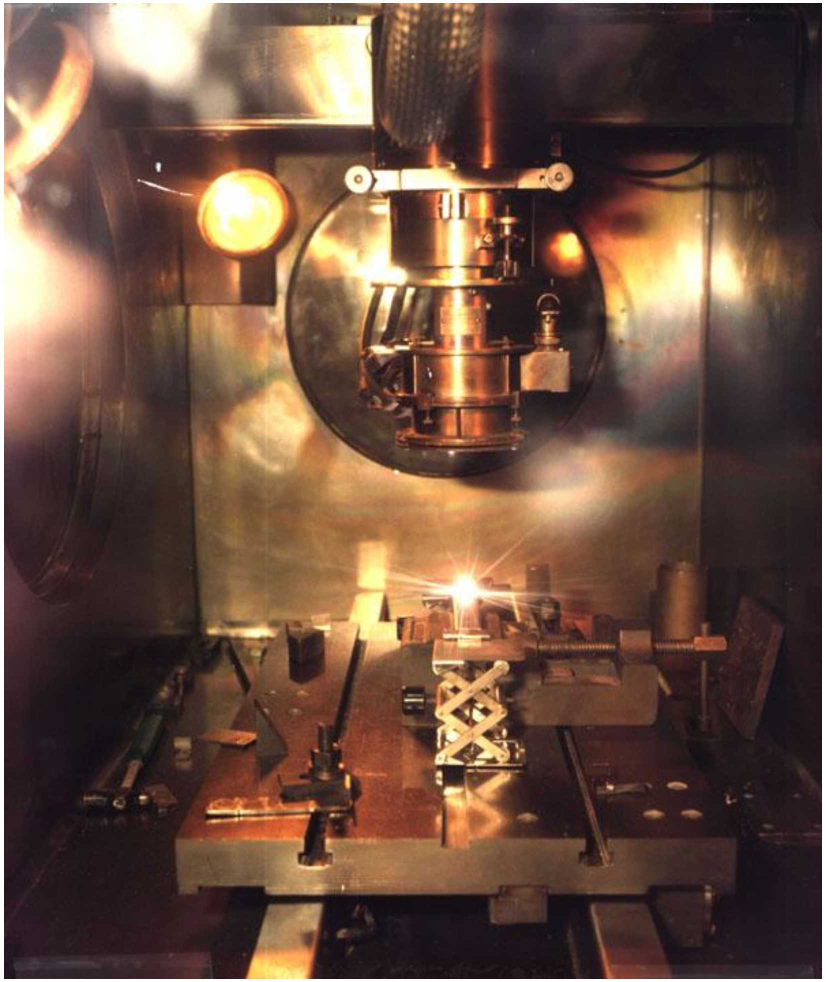
Cavity Welding Preparation Steps



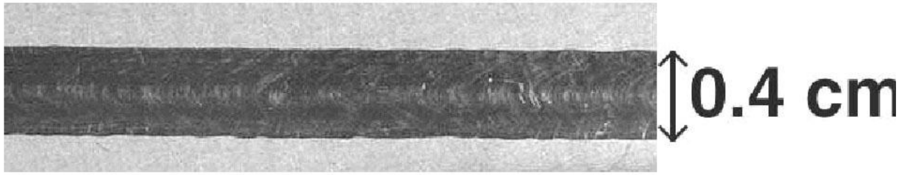
1. Degreasing and rinsing of parts
2. Drying under clean condition
3. Chemical etching at the welding area (Equator)
4. Careful and intensive rinsing with ultra pure water
5. Dry under clean conditions
6. Install parts to fixture under clean conditions
7. Install parts into electron beam (eb) welding chamber
   (no contamination on the weld area allowed)
8. Pump down to vacuum in the EBW chamber E^{-5} mbar
9. Welding and cool down of Nb to T< 150° C, venting
10. Leak check of weld

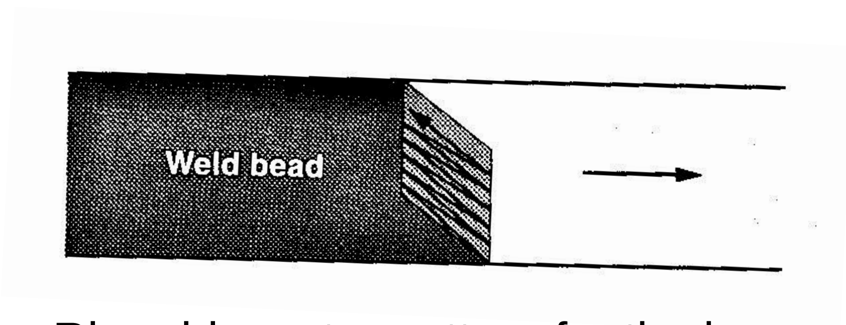
Electron Beam Welding

- Welding under good vacuum, 10^{-5} mbar range
- Broad welding seam
  - Operate with defocussed beam
  - Smooth underbead
- Overlap at end of welding to avoid accumulation of impurities
- Wait to cool down before opening chamber

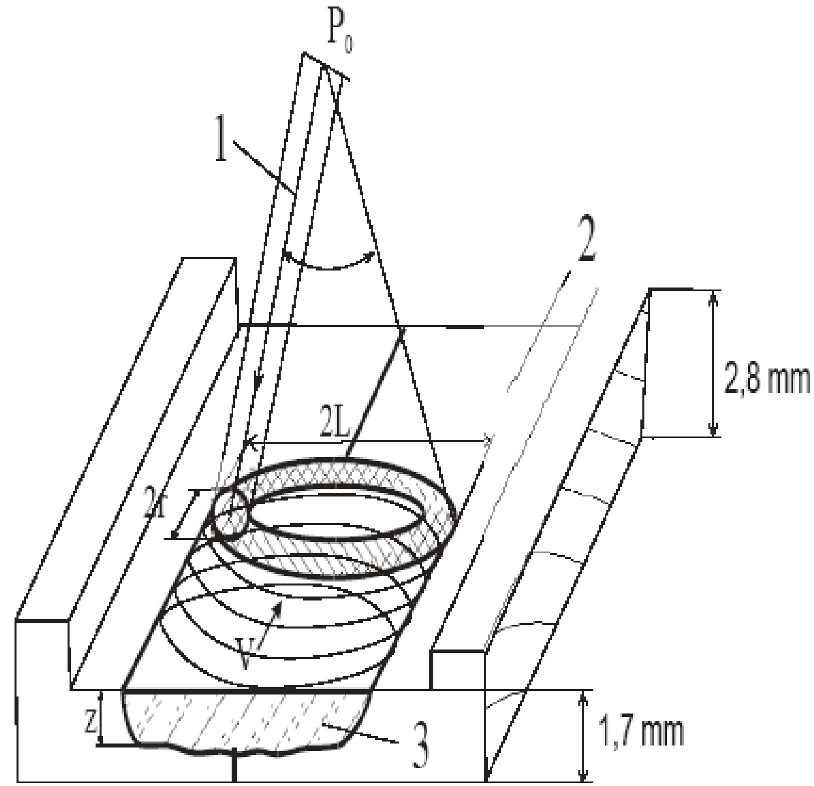


Electron Beam Welding





Rhombic raster pattern for the beam during EBW. This rastering produces a well-defined and reproducibly defocused beam



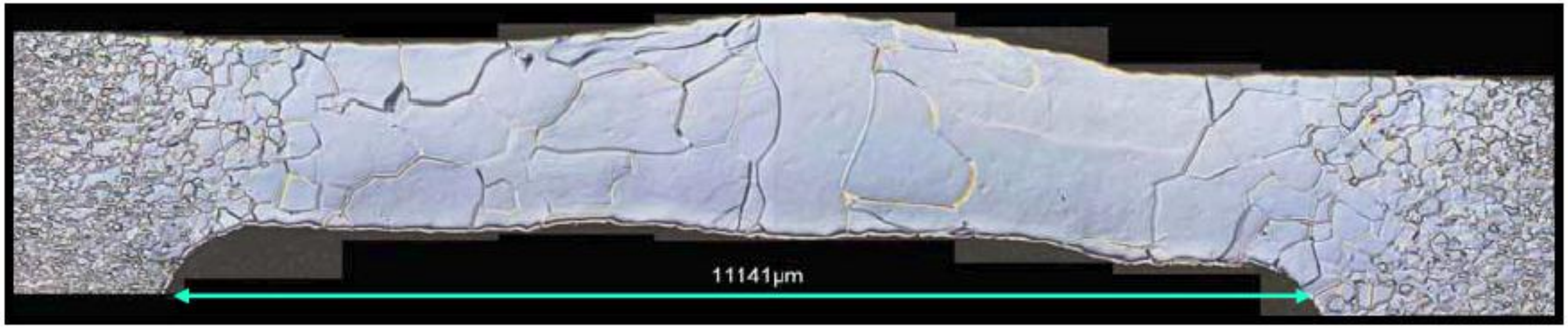
Welding Scheme (circular raster)

1-Electron beam (P_0-power of the beam, r-spot radius on the surface, L-scanning amplitude, V-velocity of the beam movement)

2-Nb sheet

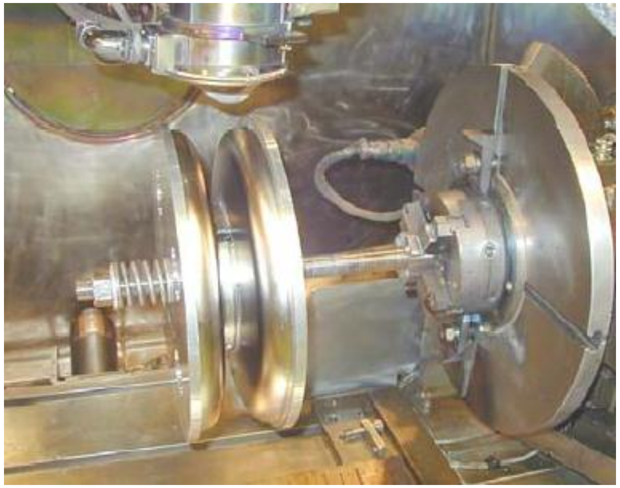
3-melting zone (z-depth of the melting zone).

Microstructure of Nb EBW Joint

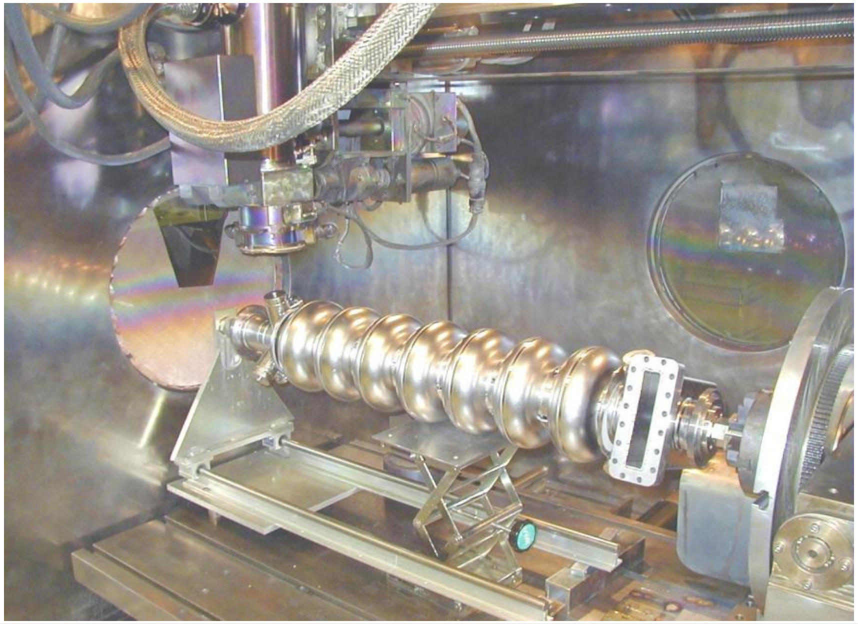


Microstructure of the EB welding area. The grain size is 50 ÷2000 μm

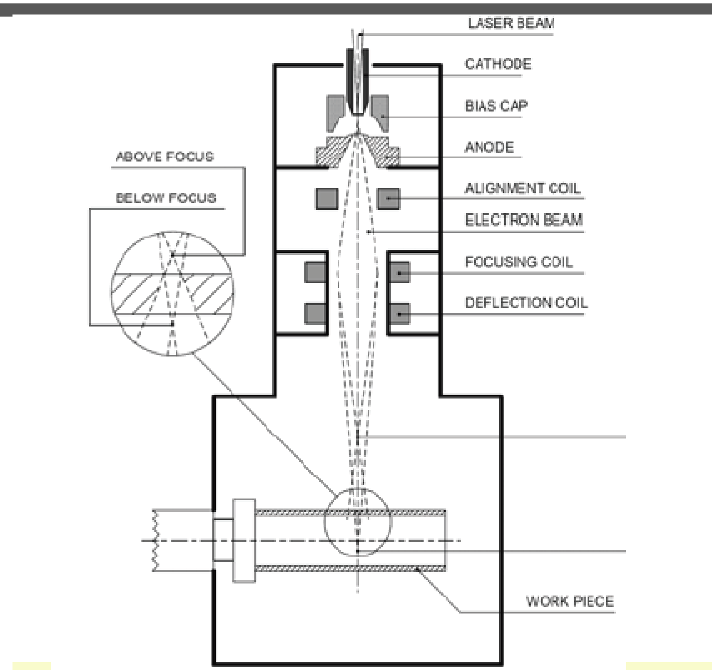
EBW Machine (JLab)



Tack- Welding:	4 tacks, focused beam
Voltage :	50 kV
Current:	15 mA
Rotational Speed :	20 inches/min
Distance of gun to work : 6 "	
Final weld Current:	33 mA
Rotational speed:	18"/min
Focussing:	elliptical pattern



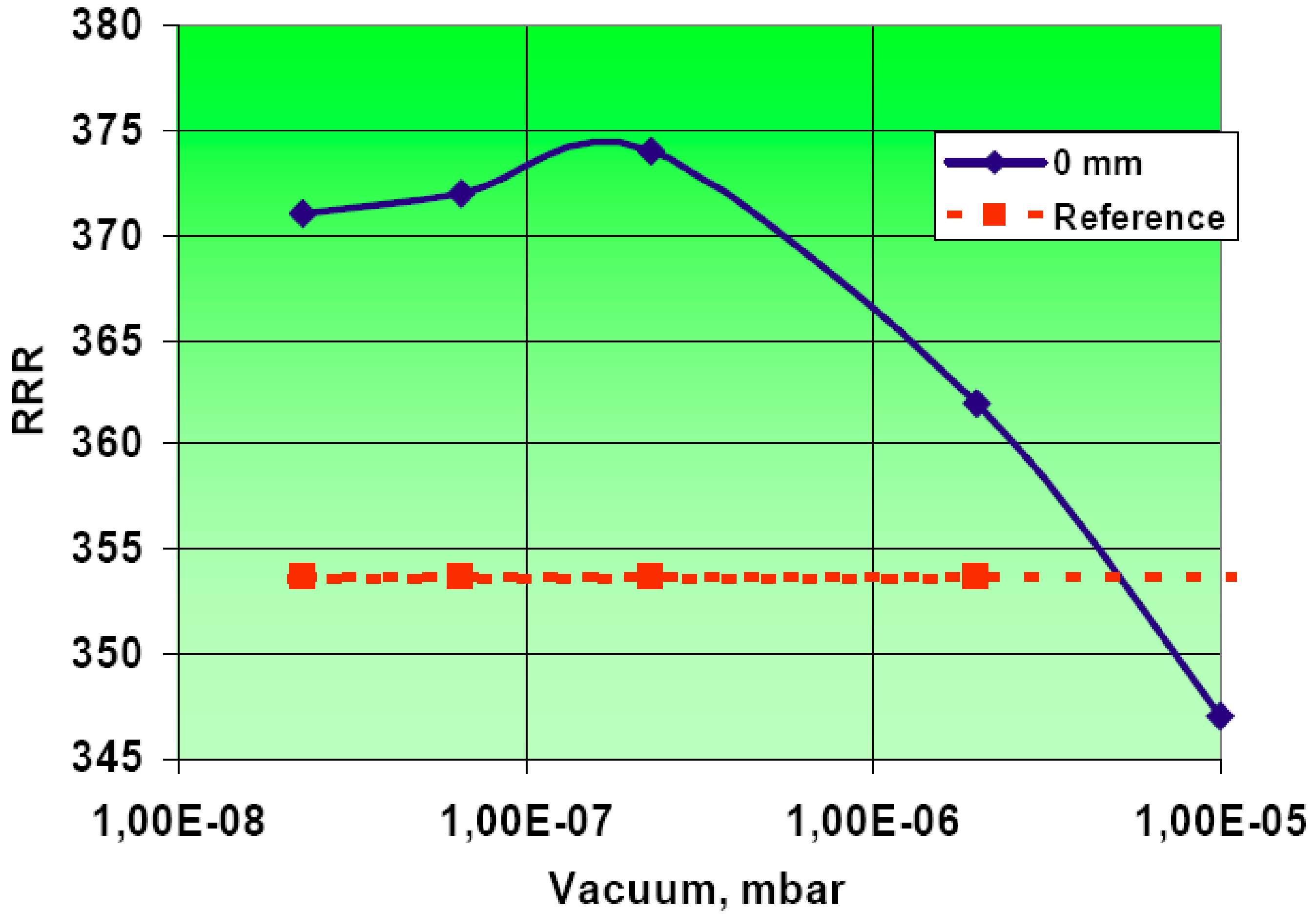
EBW Machine (DESY)



Specification of DESY
Electron Beam Welding Machine

Voltage: 70 - 150 kV
Beam power: max. 15 kW
Beam current: 0 bis 100 mA
Chamber size: 3300mm x 1400mm x 1600mm (ca. 7,4 m³)
Vacuum: > 5x10^{-6} mbar (ca. 2x10^{-8} mbar)
Pumping time: ca. 20 min =3x10^{-6} mbar
2 Cryogenic - Pumps: ca. 2 × 10.000 l/s
Displacement along the X-Axes ca. 1400 mm

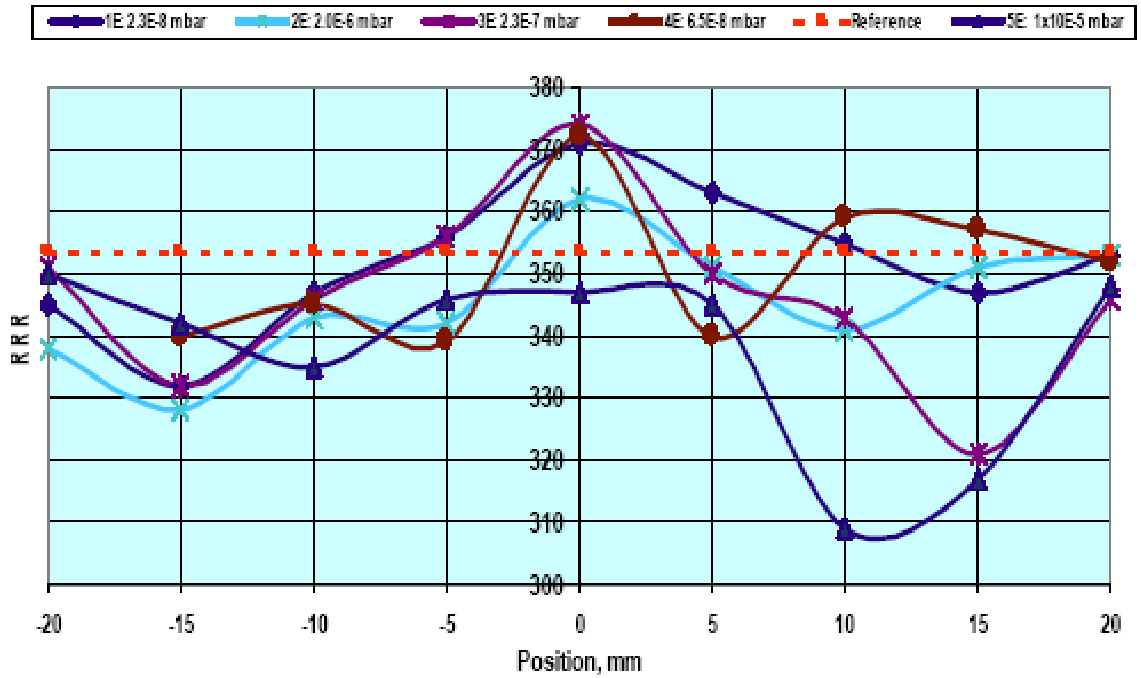
Nb RRR After EBW



RRR in the welding seam versus pressure in the welding chamber

The RRR degradation at welding seam started since pressure of ca. 10^{-5} mbar.

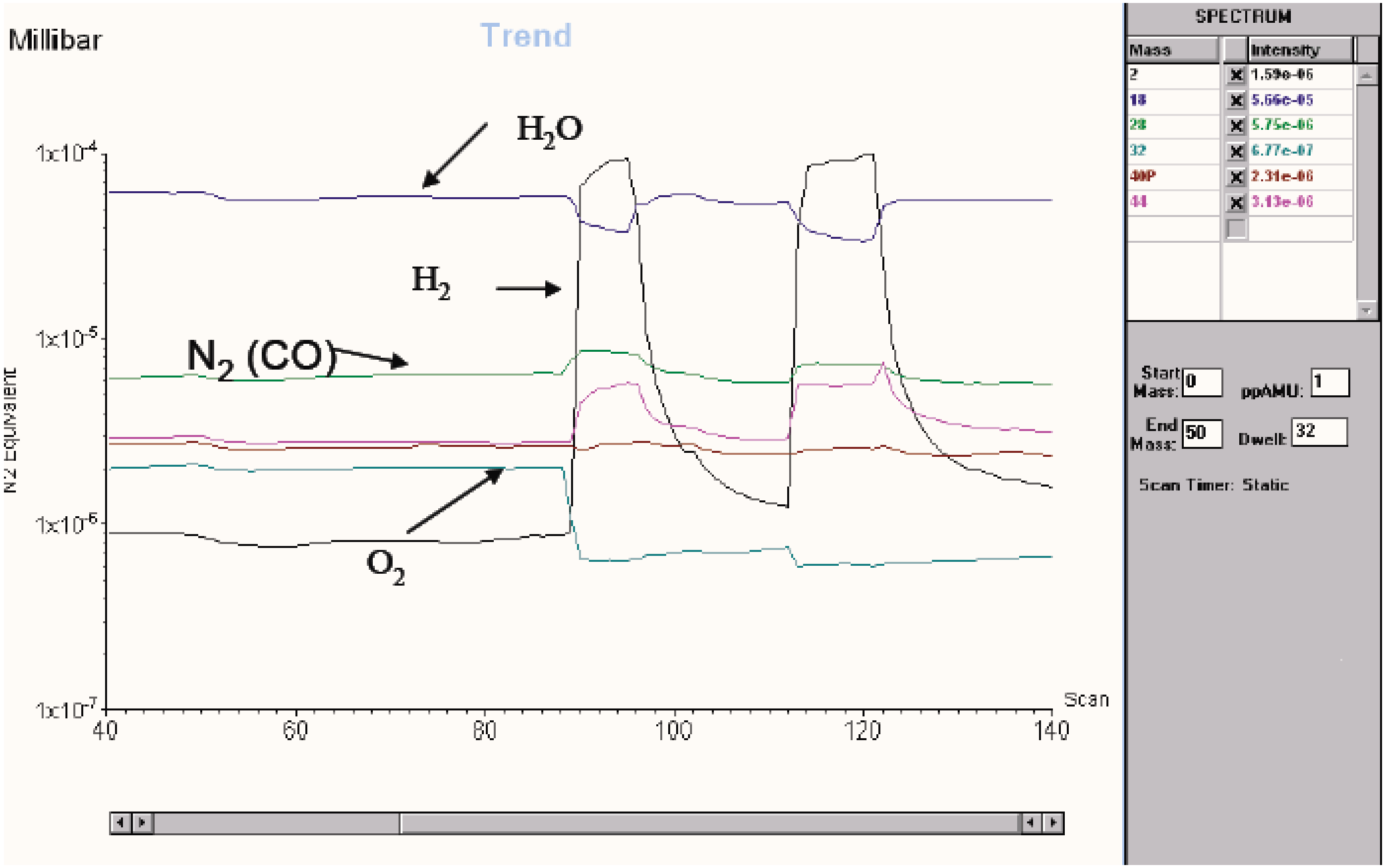
RRR Variation After EBW



RRR in the EB welding area versus distance from the welding seam at different pressures of DESY EBW facility

The RRR degradation can take place in the welding seam itself, but also in the thermally affected area and overlapping region

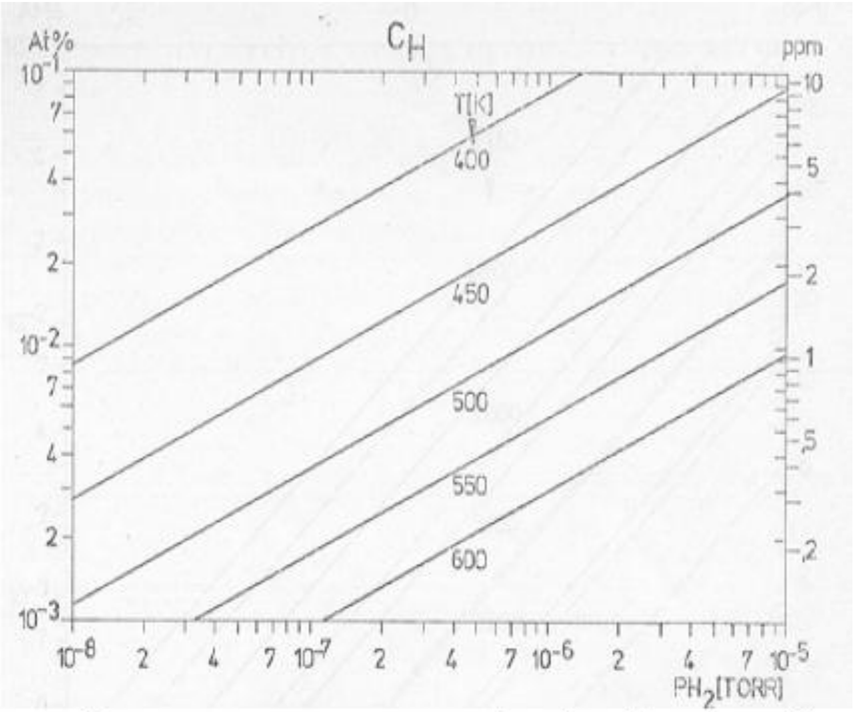
RRR Variation After EBW



- Water decomposition during welding
- Hydrogen from water and due to degassing
- Oxygen uptake

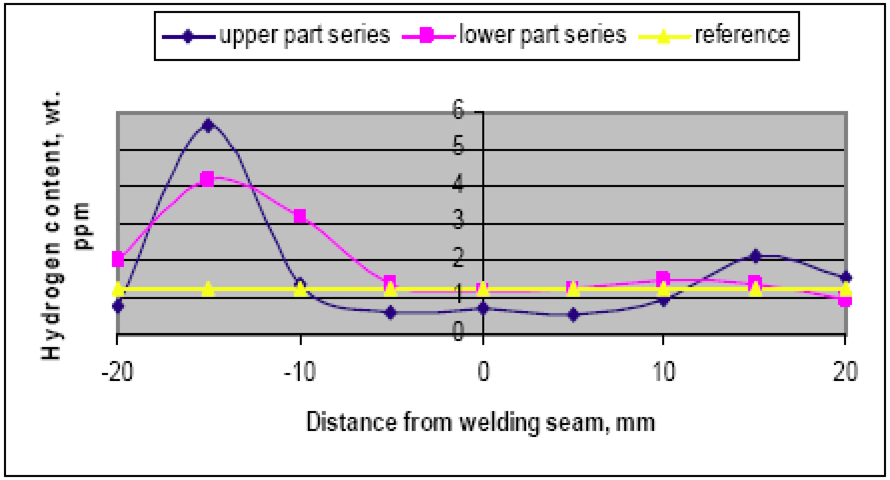
Partial pressure in the EB chamber during welding of Nb300 sample

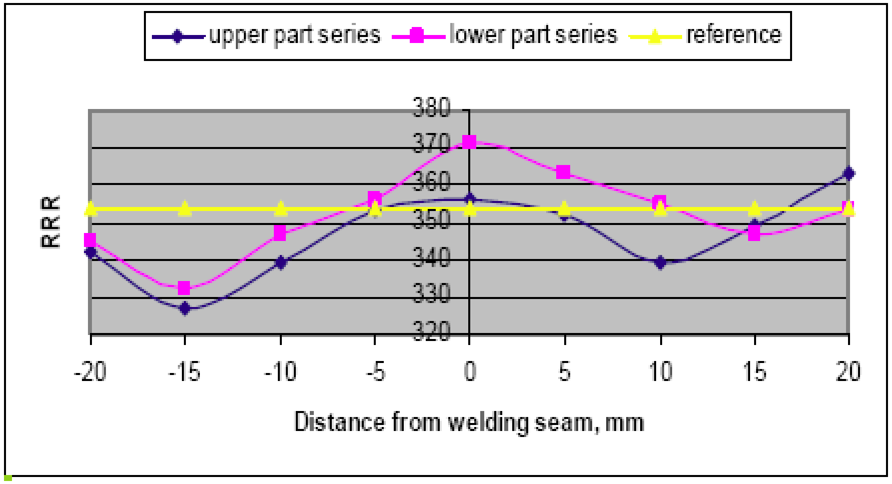
RRR Variation After EBW



Pressure – concentration isotherms of hydrogen in Nb in steady state condition

Absorption of hydrogen can take place at the area with moderate temperatures



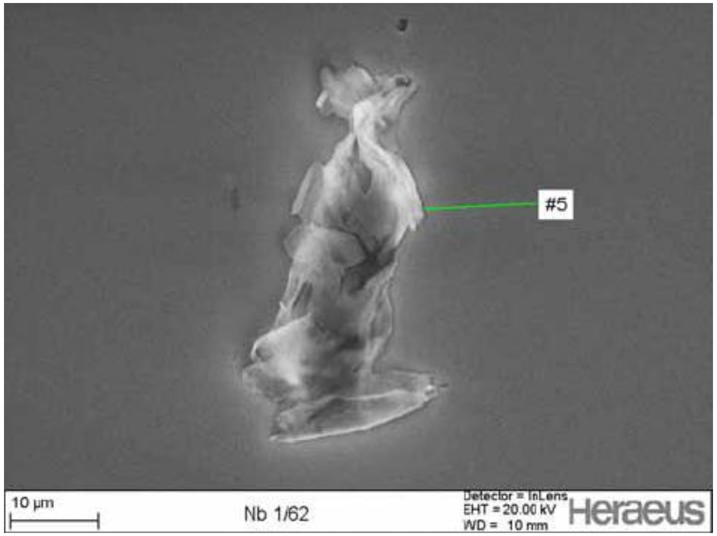


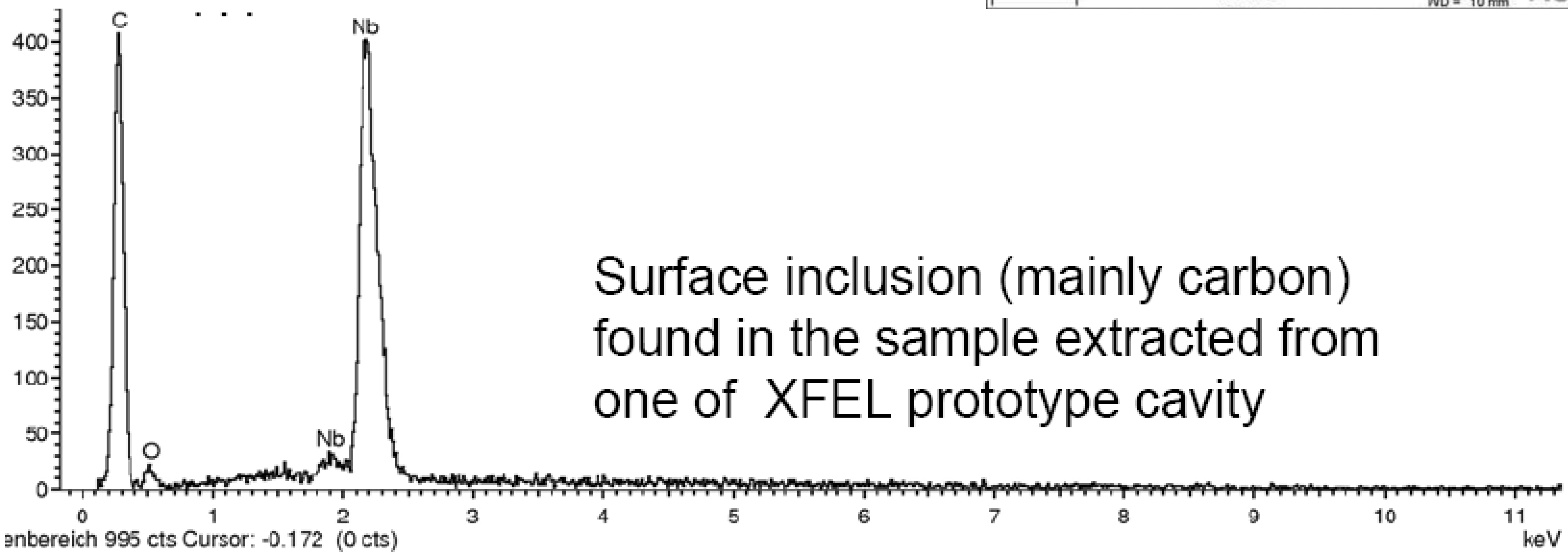
Comparison of RRR and hydrogen content in welding area (pressure 2.3×10^{-8} mbar)

Nb Contamination After EBW

Where the carbon come from?

- Diffusion pump
- Dirty EB chamber
- Not sufficient cleaning prior to weld…

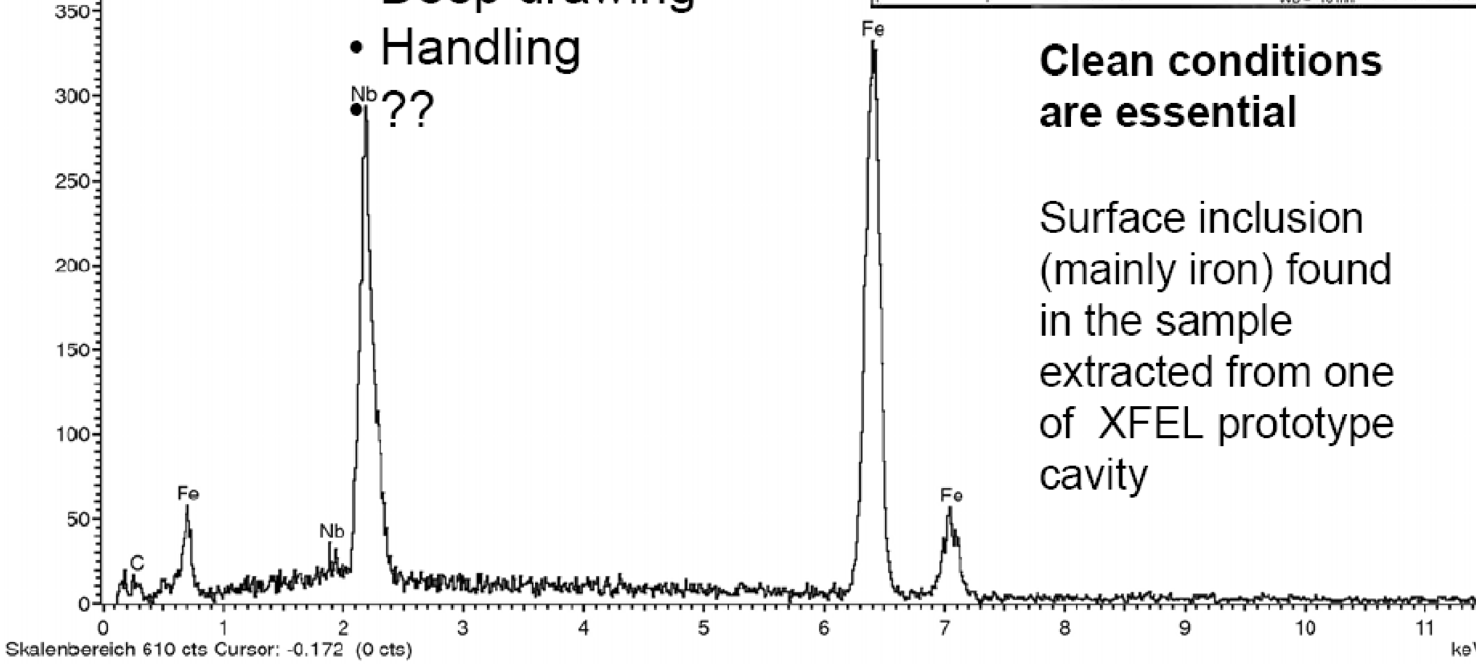




Surface inclusion (mainly carbon) found in the sample extracted from one of XFEL prototype cavity

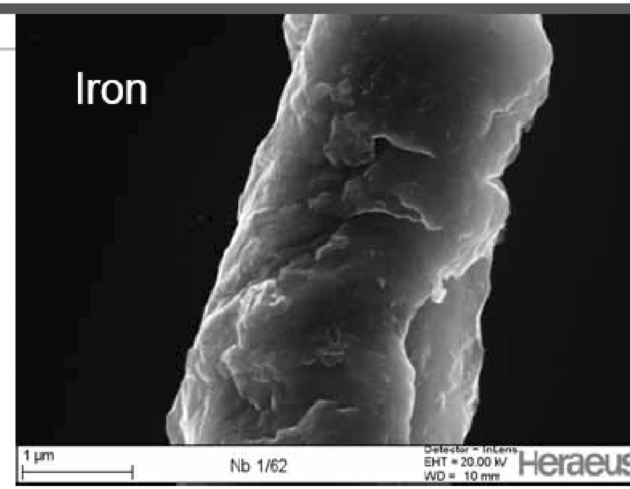
Nb Contamination After EBW

Example Fe (iron)



Where the Iron come from?

- Nb sheet fabrication
- Deep drawing
- Handling
- ??



Clean conditions are essential

Surface inclusion (mainly iron) found in the sample extracted from one of XFEL prototype cavity

Jefferson Lab

Old Dominion University

Welded Cavity Parts



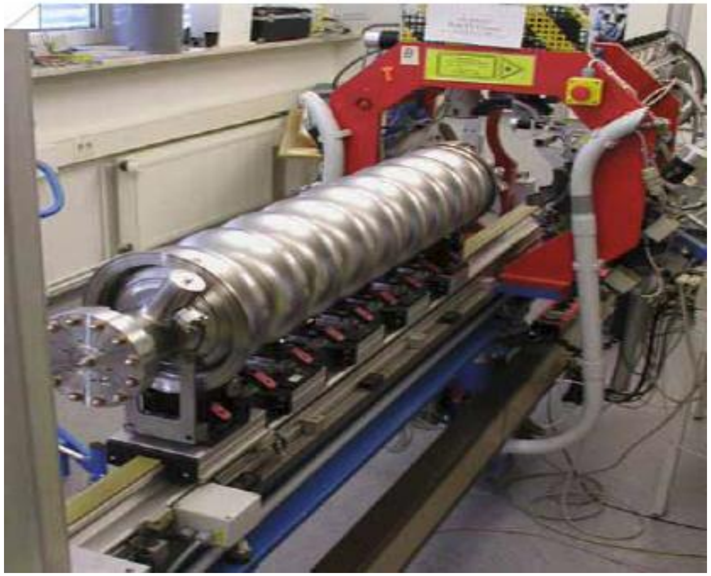






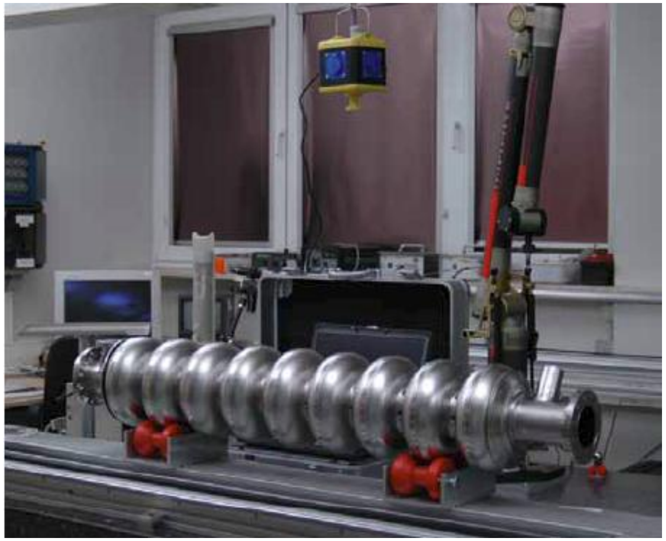
Welded Cavity Parts

Cavity Inspection

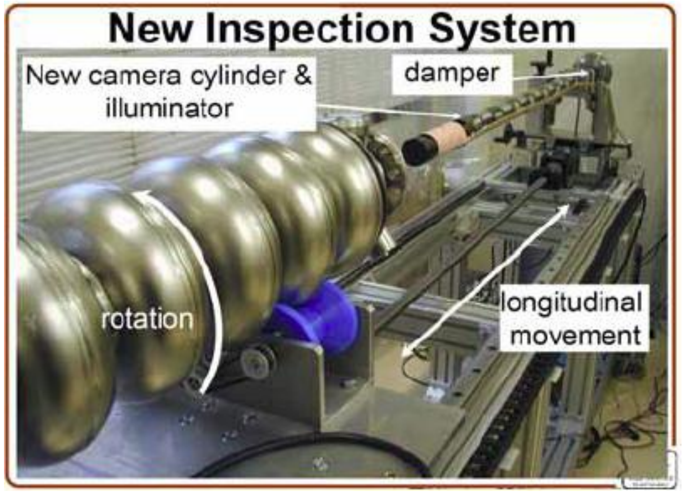


Eccentricity measurement

Dimensional check

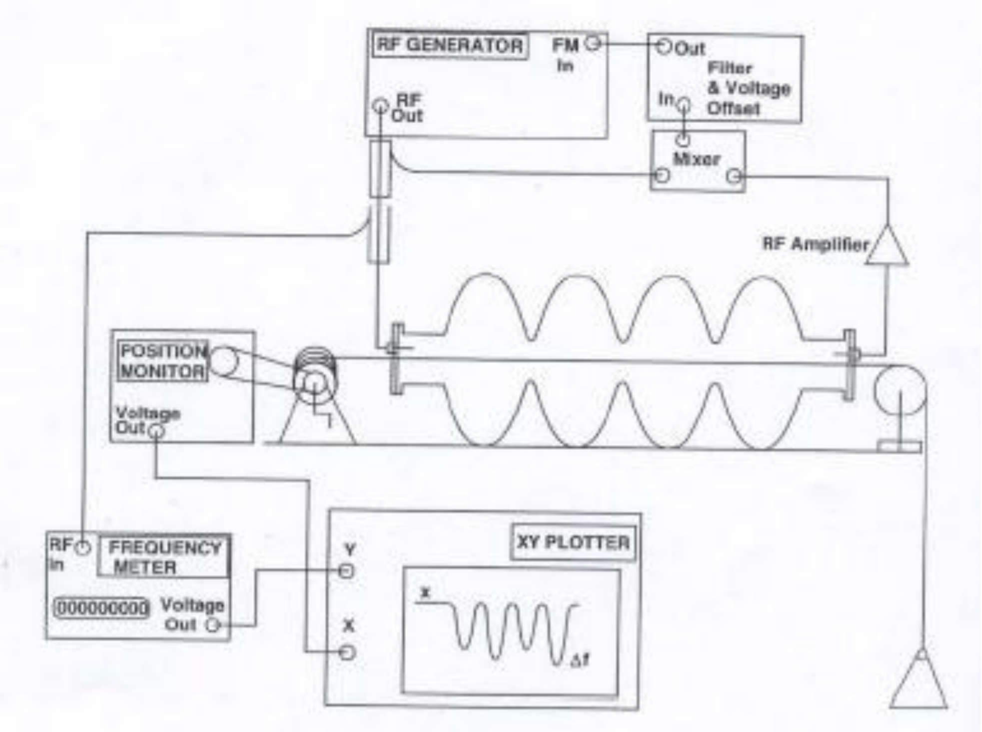


- Check of all mechanical tolerances
  - Take care with sealing surfaces
- Inspection of inner cavity surface
- Measure and adjust frequency and electrical field profile



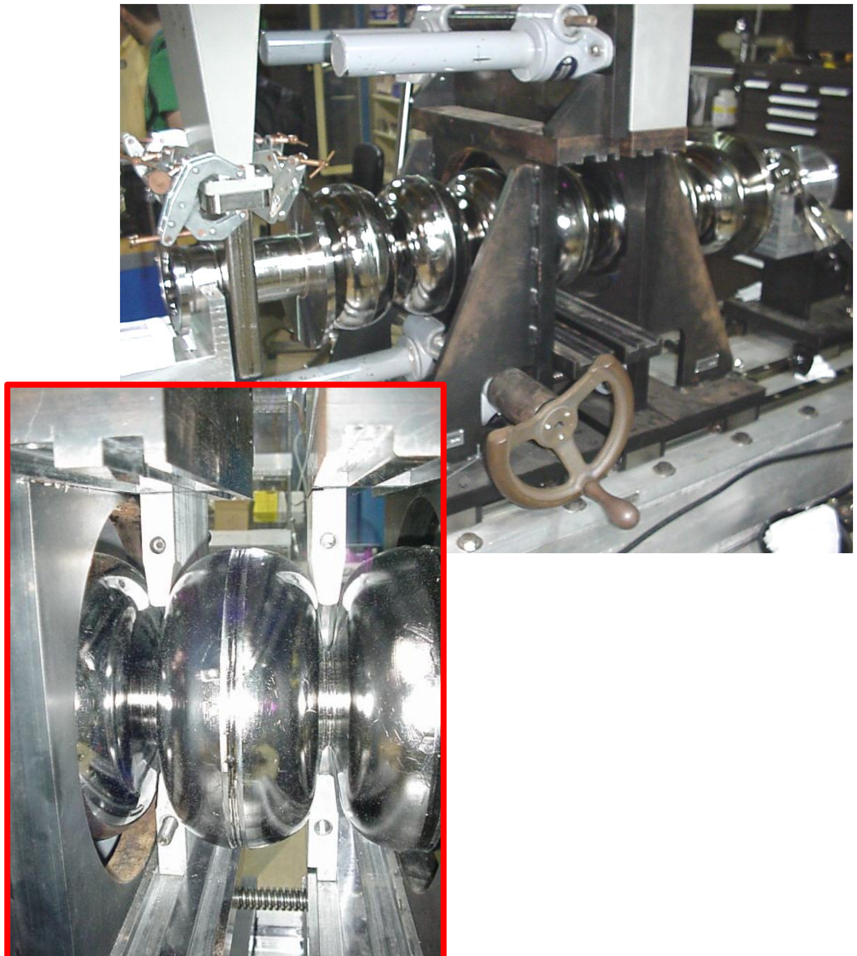
Cavity Tuning

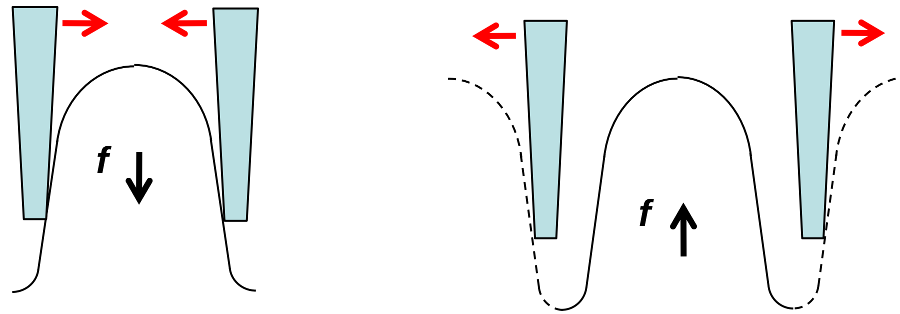
Set-up for field profile measurements: a metallic needle is perturbing the RF fields while it is pulled through the cavity along its axis; the stored energy in each cell is recorded.



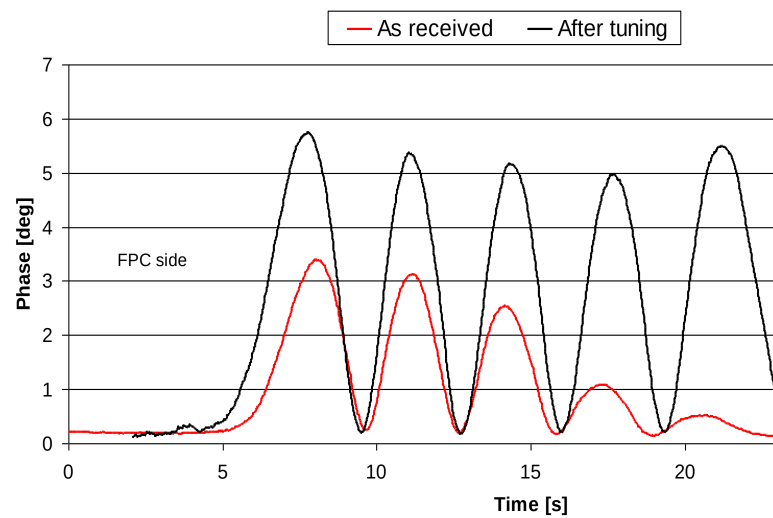
Cavity Tuning

- Small mechanical adjustments to the cavity's cells to obtain flat field profile and desired frequency





5-cell cavity



Cavity Tuning

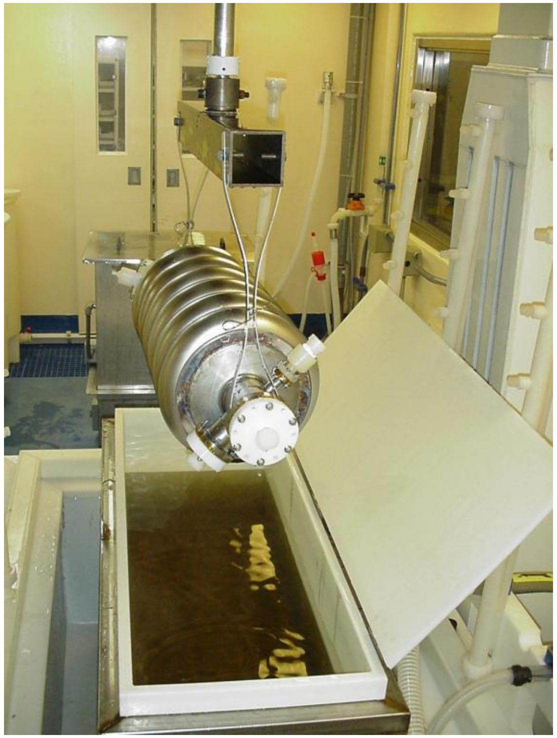
Computerized tuning machine at DESY

- Equalizing stored energy in each cell

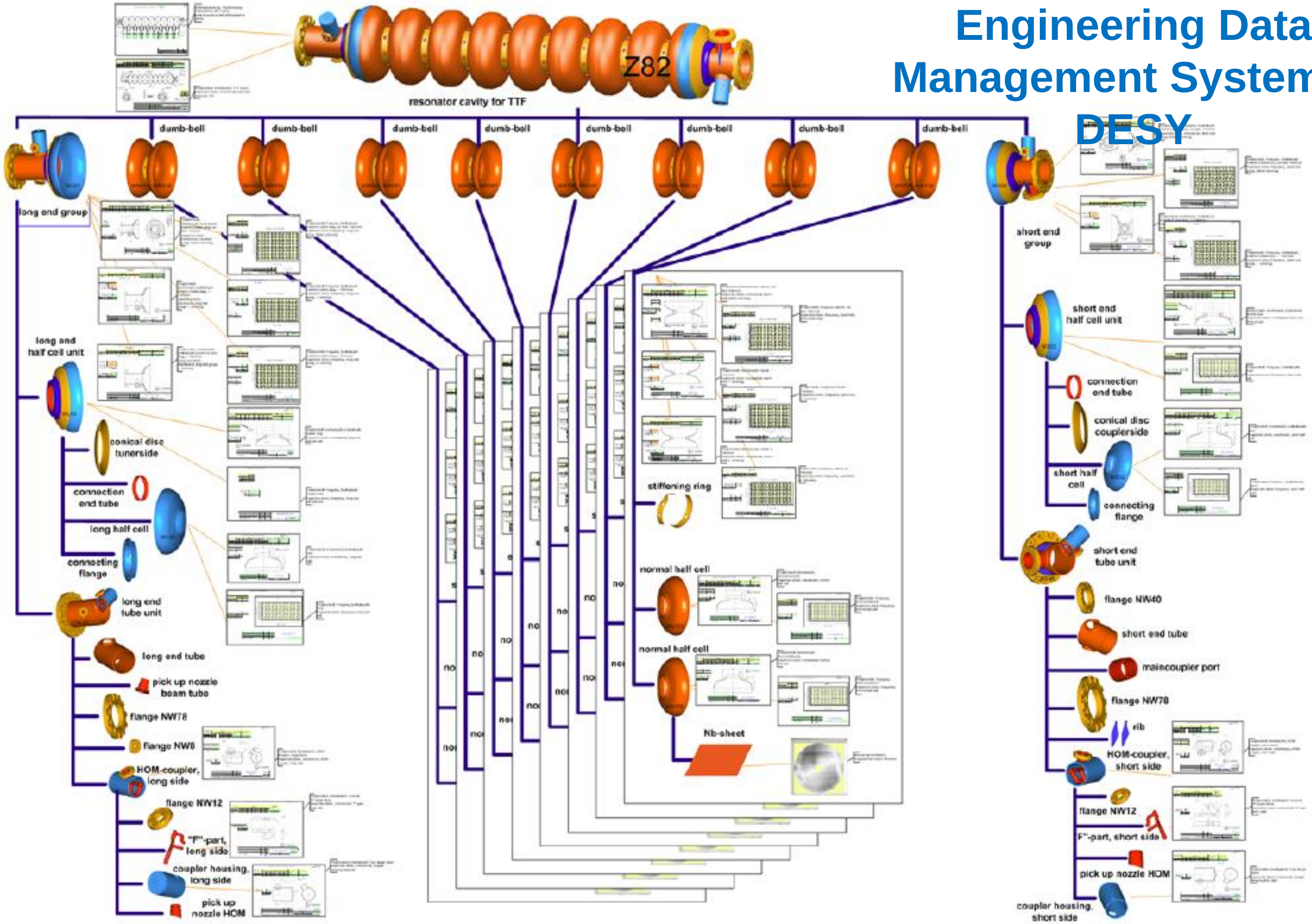
  by squeezing or pulling

- Straightening of cavity

External Chemistry



Industrialization of Cavity Fabrication

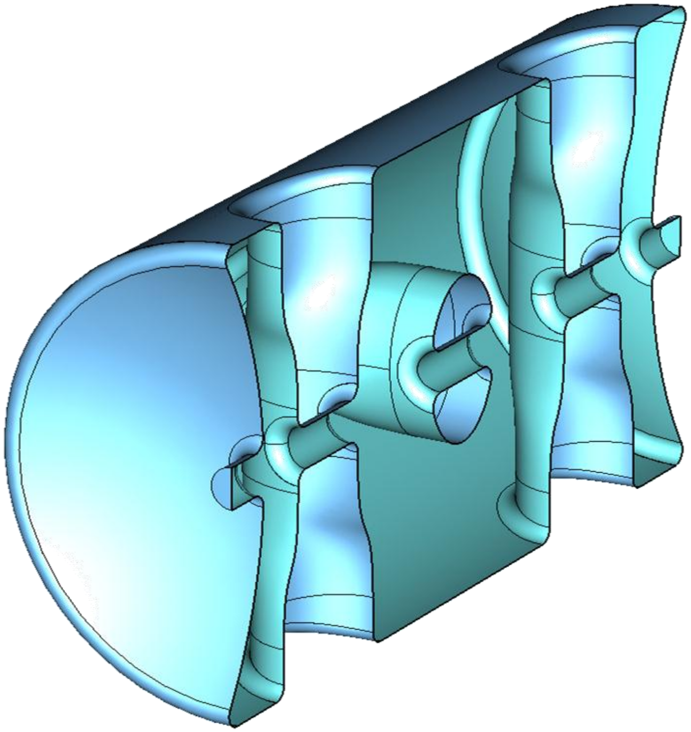


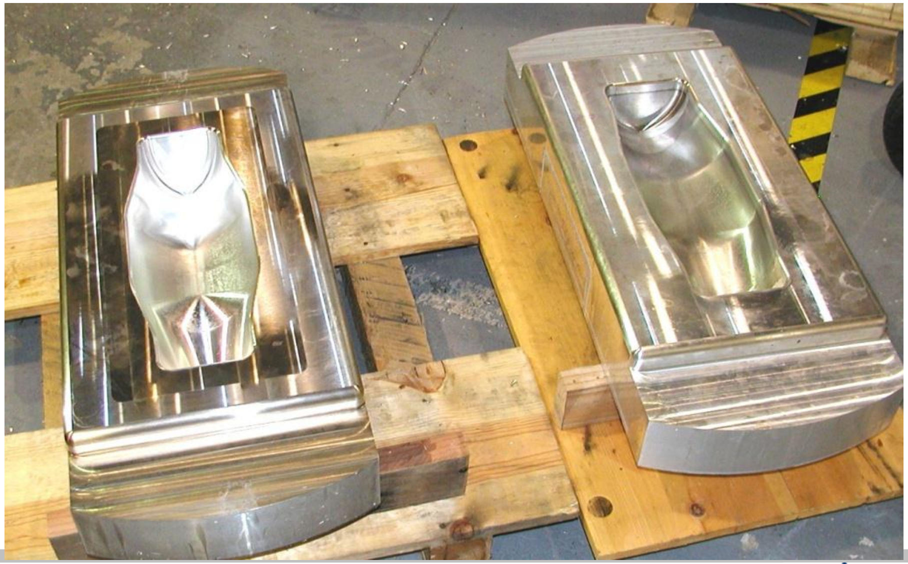
Engineering Data Management System at DESY

Low-β Cavity Fabrication

Cavity components prior to EBW (AES)

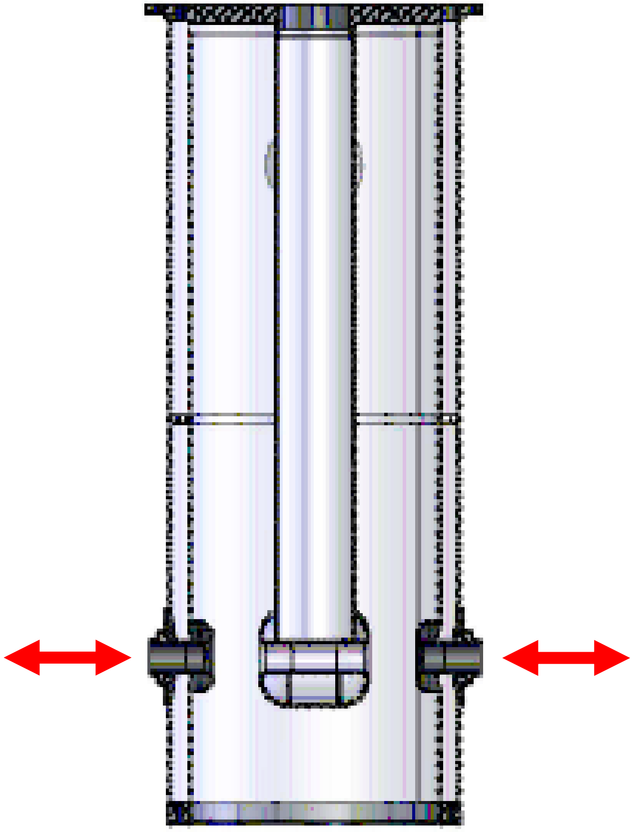
The ANL 345 MHz Triple-spoke cavities





Low-β Cavity Fabrication

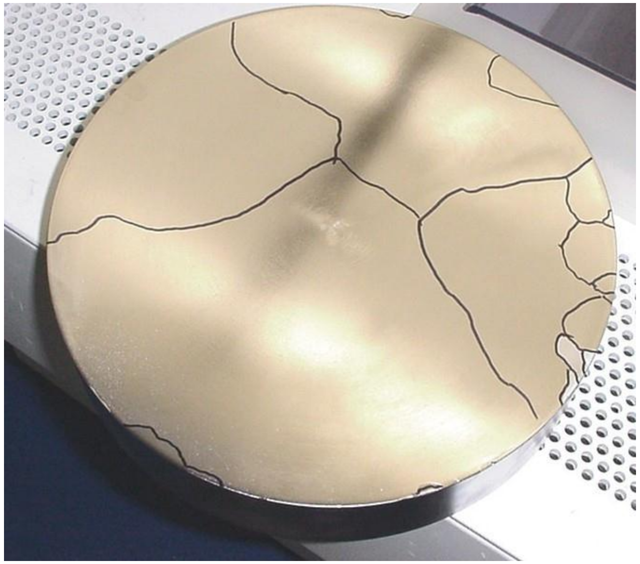
- Work out frequency tuning sequence to arrive at final frequency – build into parts initial sizing
- Plastic deformation can be used after manufacture to achieve the final frequency
- Somewhat risky in jacketed cavity since pressure is put on the welds
- Flexible tuning plate can be deformed safely over some limited range without risk to cavity



Cavity Fabrication R&D

- Large-grain/Single-crystal cavities
- Hydroforming
- Spinning

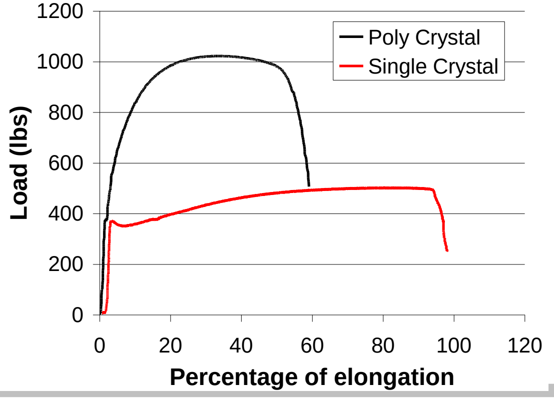
Large-Grain Nb

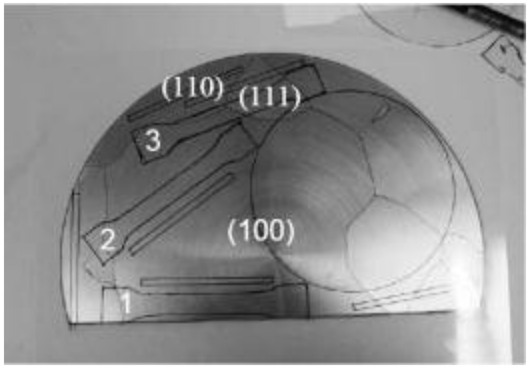


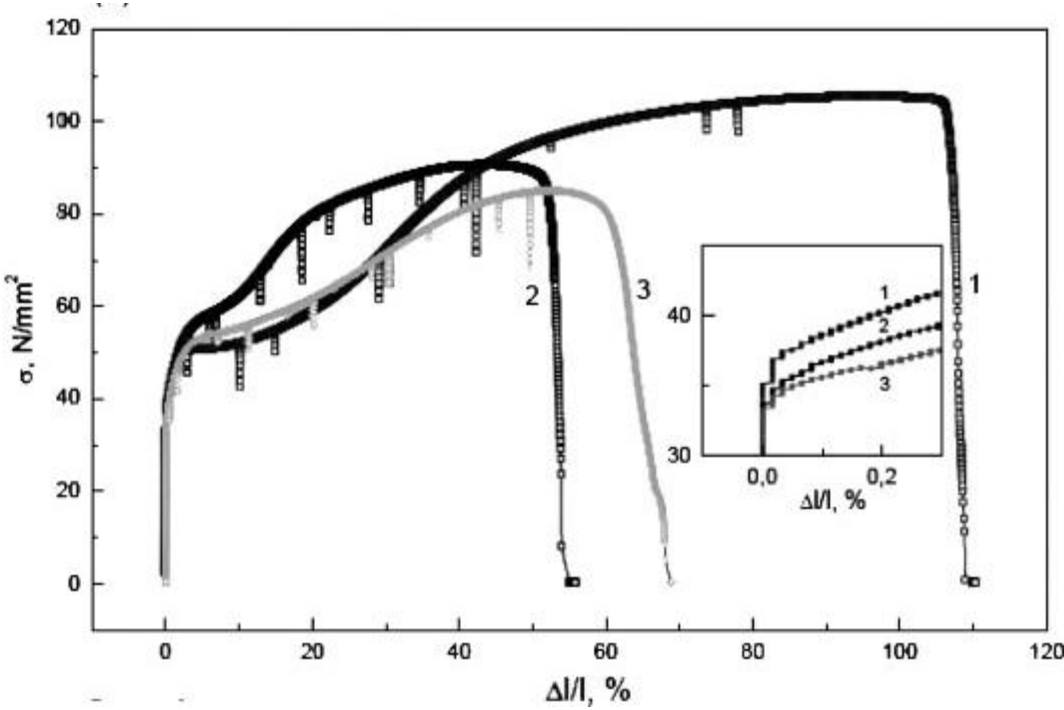
CBMM Large-grain Nb disc

RRR value: ~300

Ta

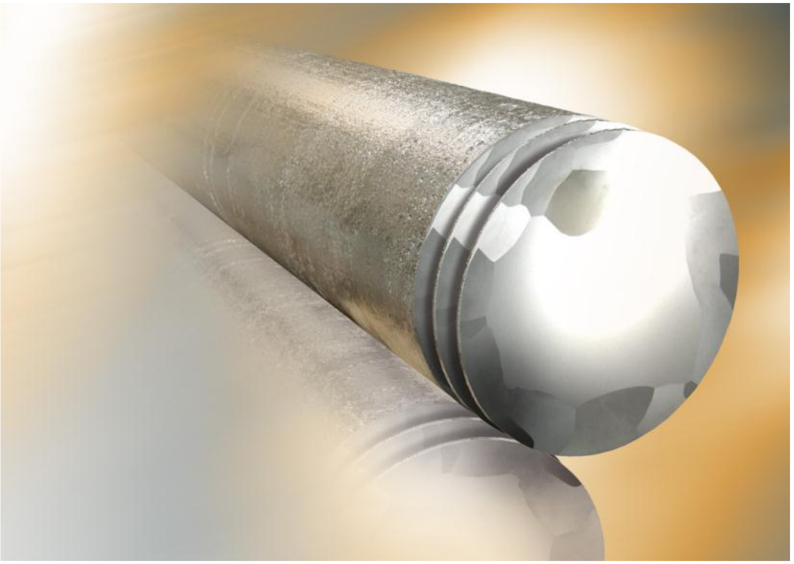




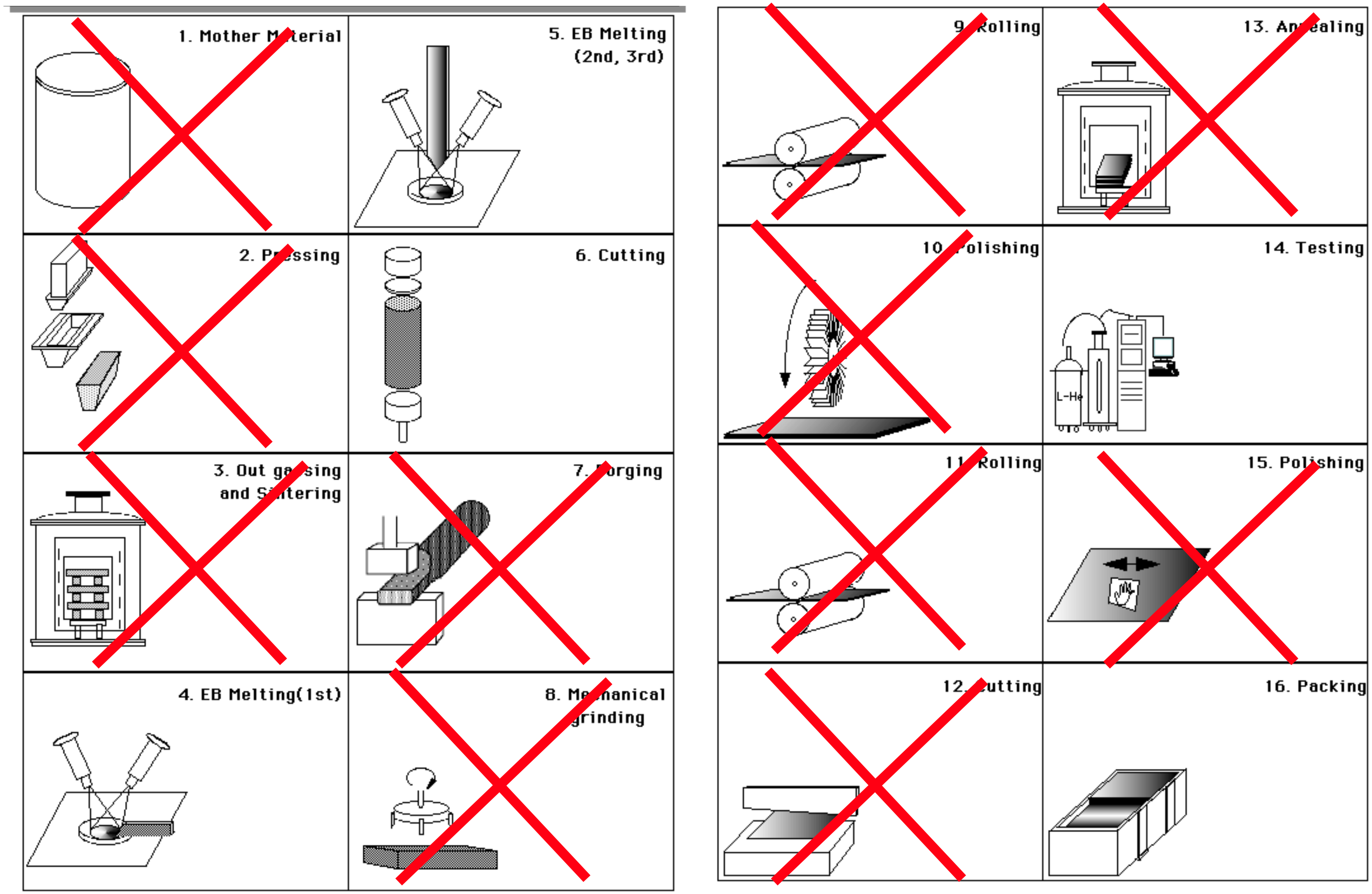


Large-Grain/Single-Crystal Nb Advantages

- Cost effective
- Reduced risk of contamination during sheet fabrication
- Simplified quality control
- Higher thermal conductivity at low temperatures (phonon peak)
- Smooth surfaces, comparable to EP, can be achieved by standard BCP
- Baking at 120°C works to reach high-fields



Large-Grain Nb Sheets



Material Suppliers

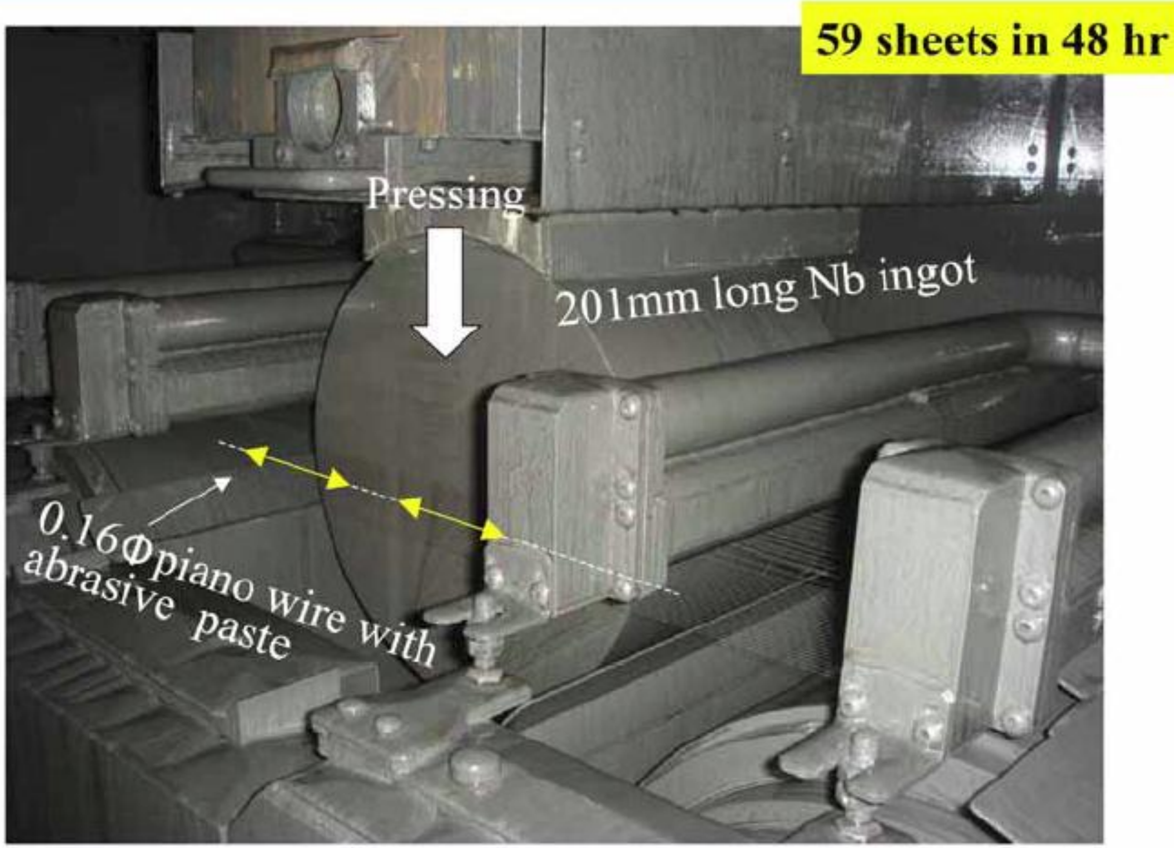
- Fine-Grain:
  - Tokyo Denkay (Japan)
  - ATI Wah Chang (USA)

- Large-Grain:
  - Tokyo Denkay (Japan)
  - ATI Wah Chang (USA)
  - OTIC (China)
  - CBMM (Brazil)
  - WC Heraeus (Germany)

Ingot Slicing

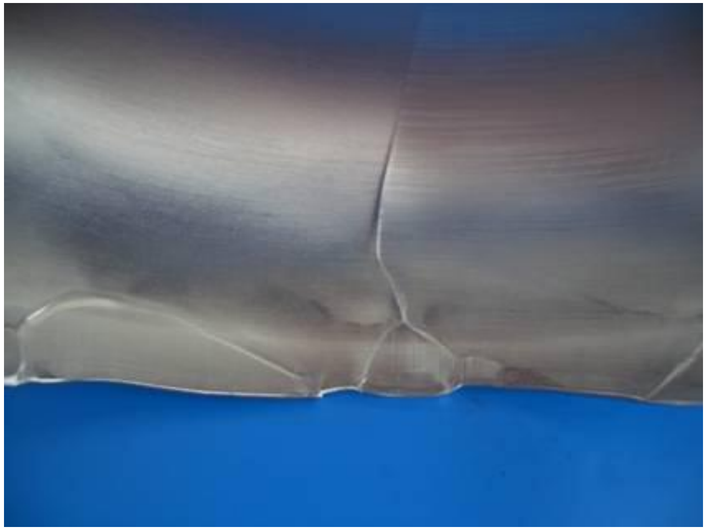
- Wire EDM (slow)
- Diamond saw
- Multi-wire

Successfully Multi-sliced 59 sheets (3.2t) from 201 mm long Nb Ingot



Large-grain Nb sheets are available up to 18" diameter

Deep Drawing Large-Grain Nb



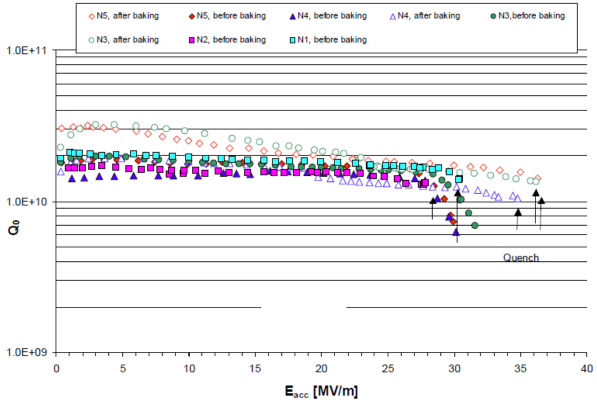
• Non-uniformity in the equator area
• Visible steps at grain boundaries
• Thinning at iris region if there is no large single crystal at the center

Large-Grain Nb Cavity Fabrication

- Same procedures as fine-grain Nb
- Assembly for equator welds a bit more complicated as cells are not as round as fine grain cells

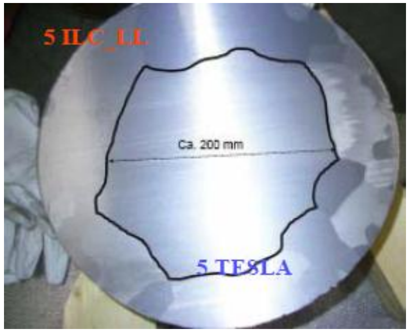
Large-Grain Single-Cell Studies

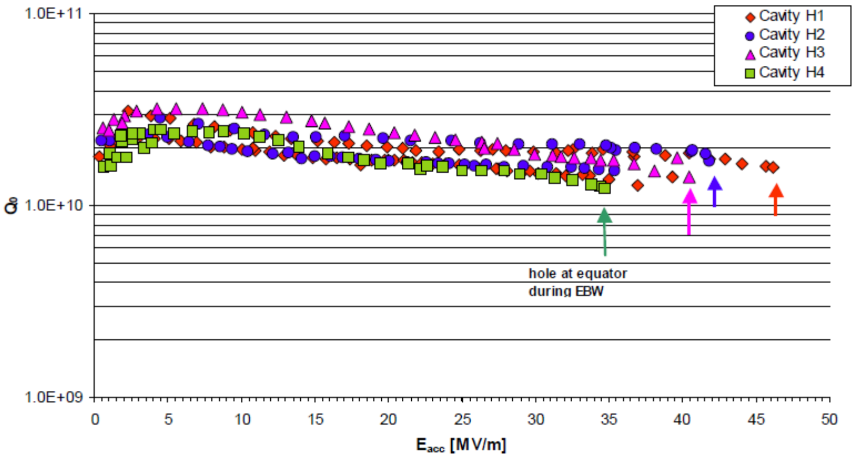
OTIC, RRR ~ 330



$<B_p> = 141$ mT ± 10%

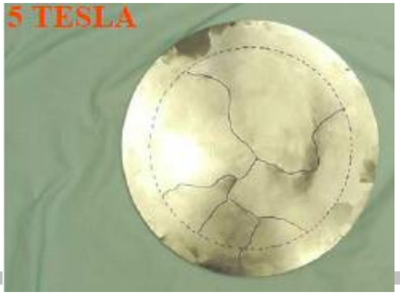
WC Heraeus, RRR ~ 500



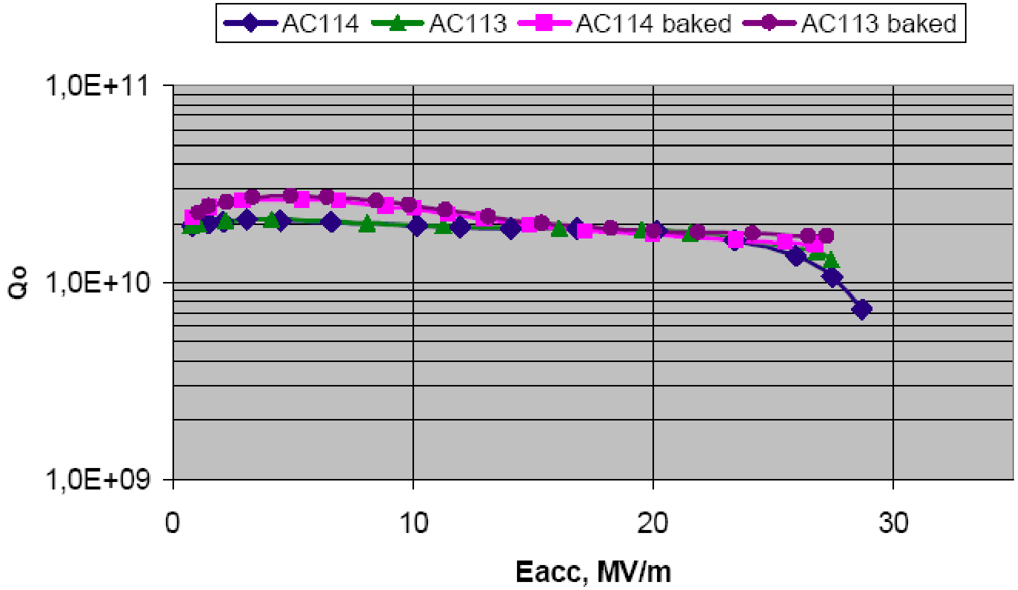


$<B_p> = 147$ mT ± 13%

CBMM, RRR ~ 280



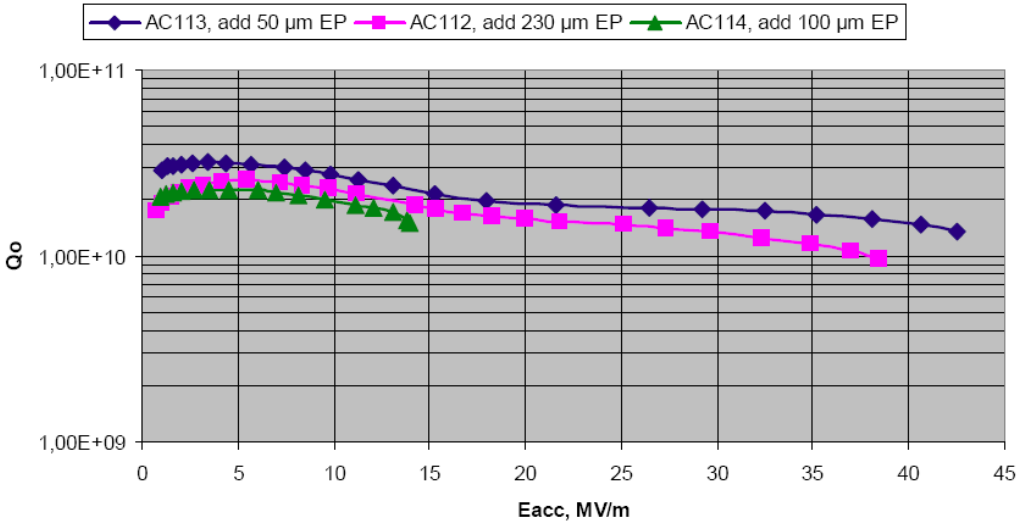
Large-Grain 9-Cell Results



- 11 Large-Grain 9-cell cavities at RI from Heraeus material

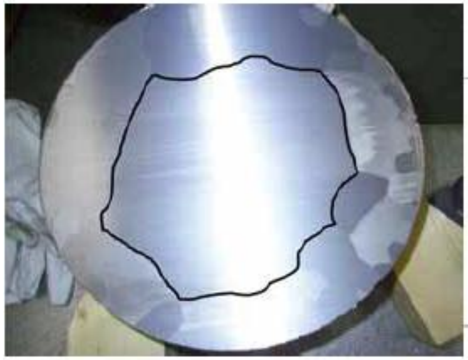
After 120 µm BCP & baking

After additional EP & baking

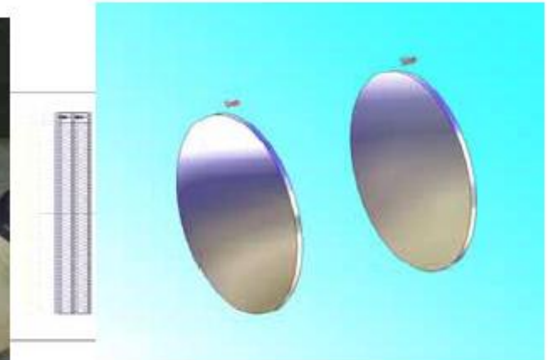


Single-Crystal Nb Cavity Fabrication

Single crystal cavity fabrication (DESY- JLab)

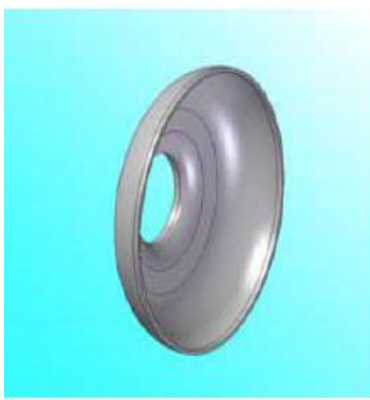


1. Take out central single crystal of definite thickness

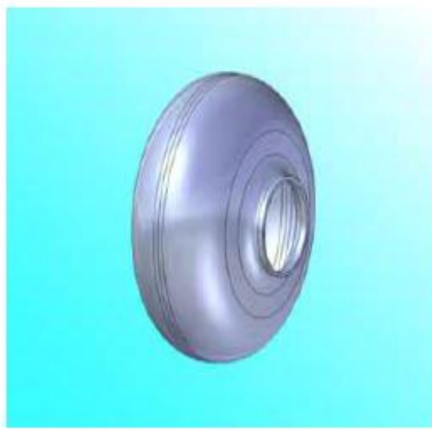


2. Cutting through the disc

3. Increasing of diameter by special rolling with an intermediate annealing



4. Deep drawing



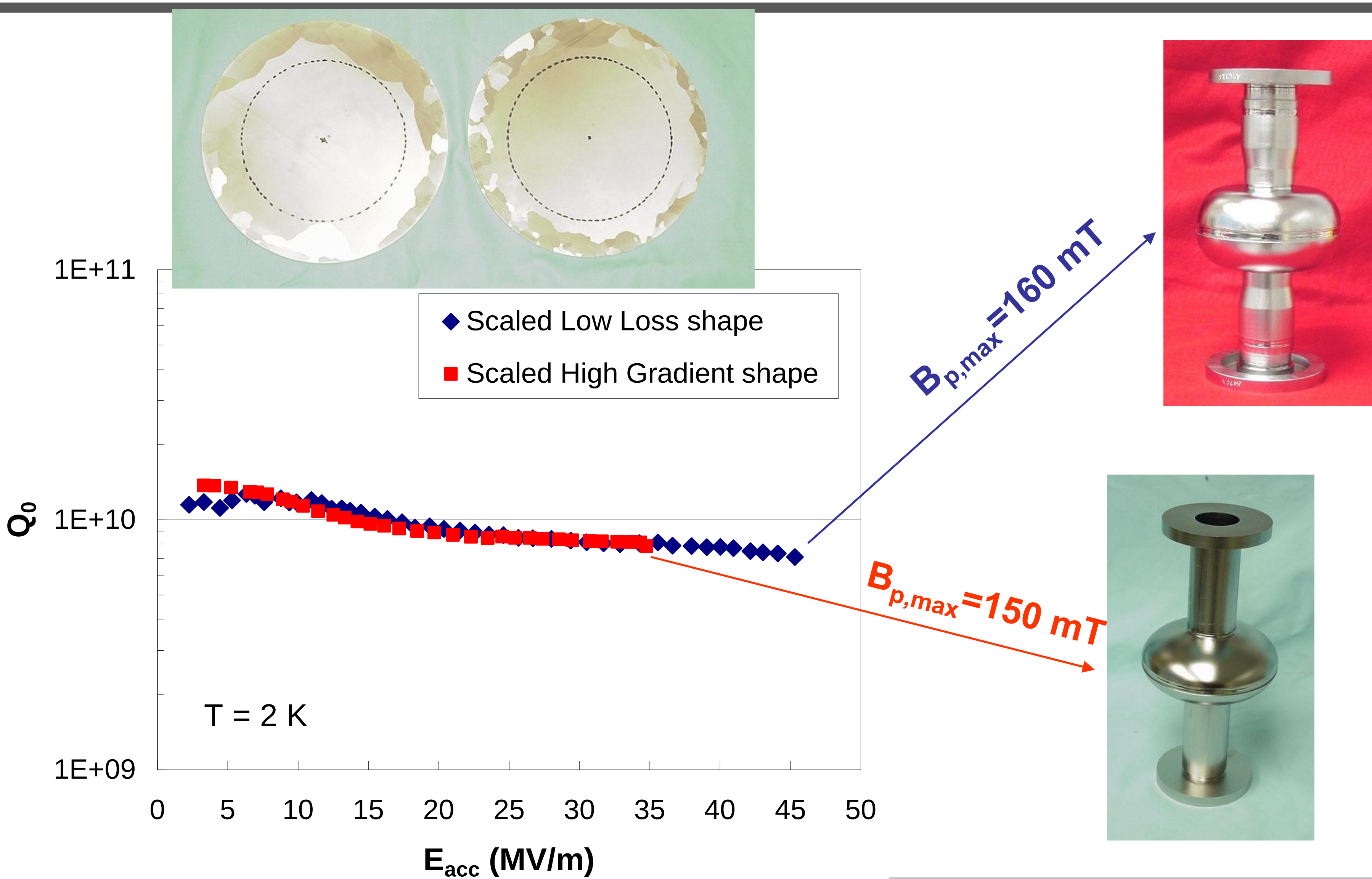
5. EB welding by matching the crystal orientation

Single Crystal Cavities with three different crystal orientation

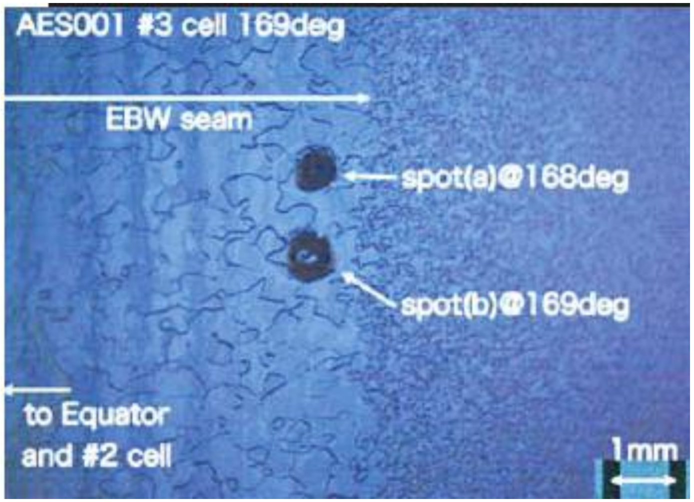
Single-Crystal Nb Cavity Results

Cavity #	$E_{acc,max}$ (MV/m)	$B_{peak,max}$ (mT)	$Q_0(B_{peak,max})$	Treatment
1	38	162	4×10^9	200μm BCP, 800°C 3h, HPR, 120°C 48h
2	45	160	7×10^9	200μm BCP, 800°C 3h, HPR, 120°C 24h
3 (1AC6)	41	177	1.2×10^{10}	250μm BCP, 750°C 2h, 120μm EP, HPR, 135°C 12h
4 (1AC8)	38.9	168	1.8×10^{10}	216μm BCP, 600°C 10h, HPR, 120°C 12h
5	38.5	166	7.6×10^9	170μm BCP, HPR, 120°C 12h

Single-Crystal Nb Cavities

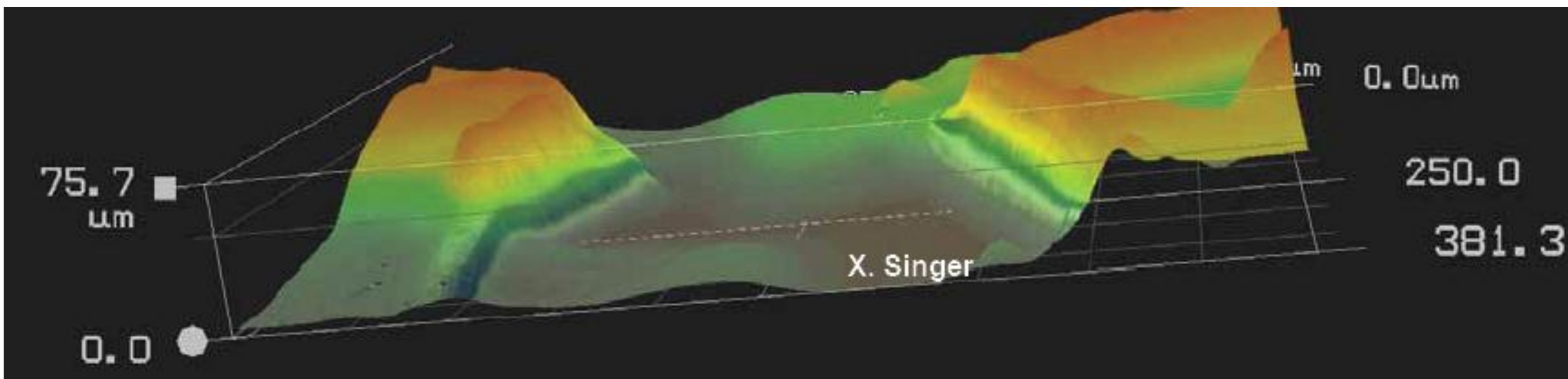


Seamless Cavities



- Eliminate equator welds and associated problems
- Cost effective

- Hydroforming
- Spinning

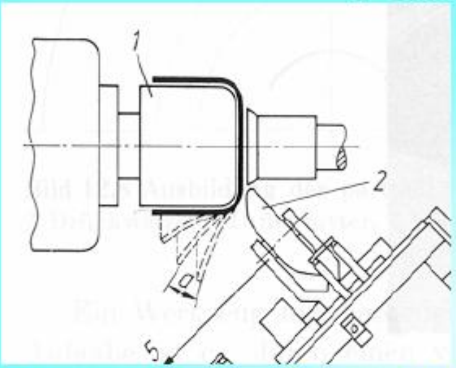


Example of welding connection of EP treated cavity. Up to 75 μm steps

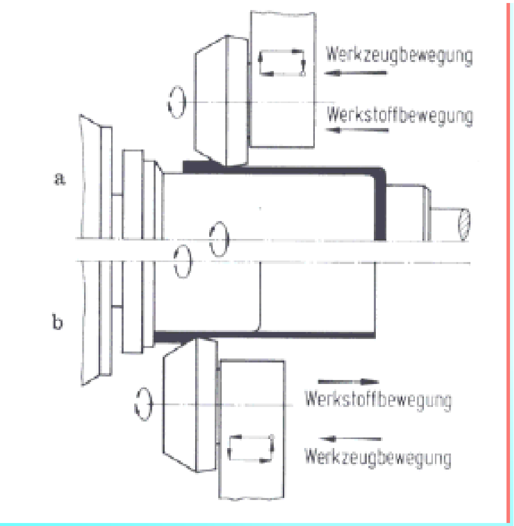
Hydroforming

- Tube of intermediate diameter between iris and equator
- Necking to form iris area
- Hydroforming (hydraulic expansion)

Tube Forming: Fine-Grain Nb



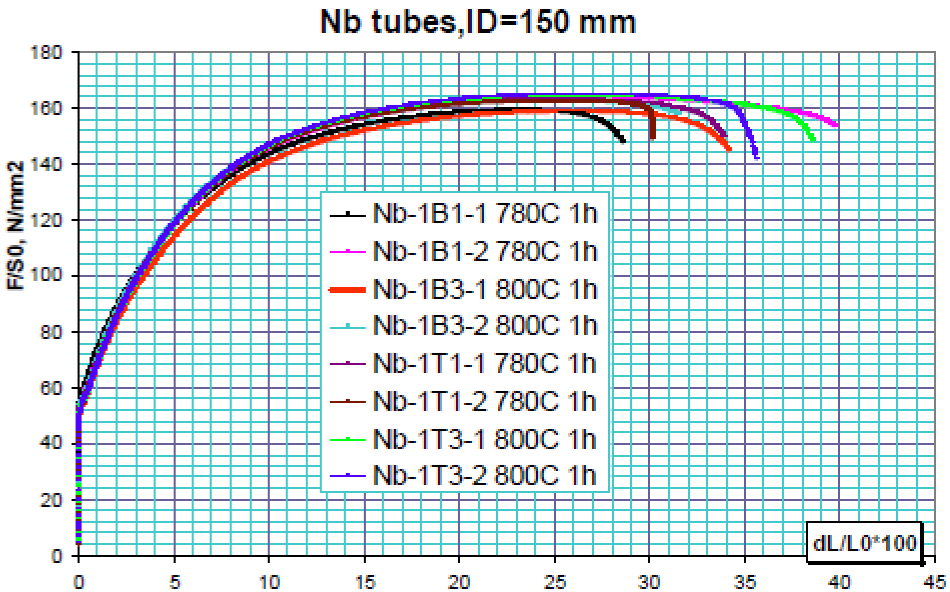
Pot with thick wall by spinning (or deep drawing)



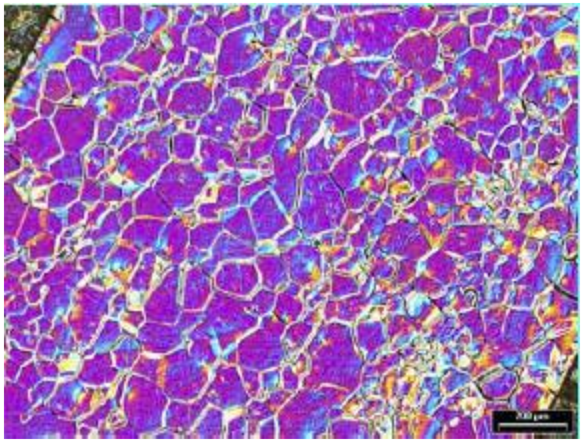
Flow forming

Flow forming over a cylindrical mandrel with three work rollers allows to produce long and very precise tubes from thick walled cylindrical part.
After optimization of several parameters shiny Nb surface and small wall thickness variations (less then +/-0,1 mm) have been achieved.

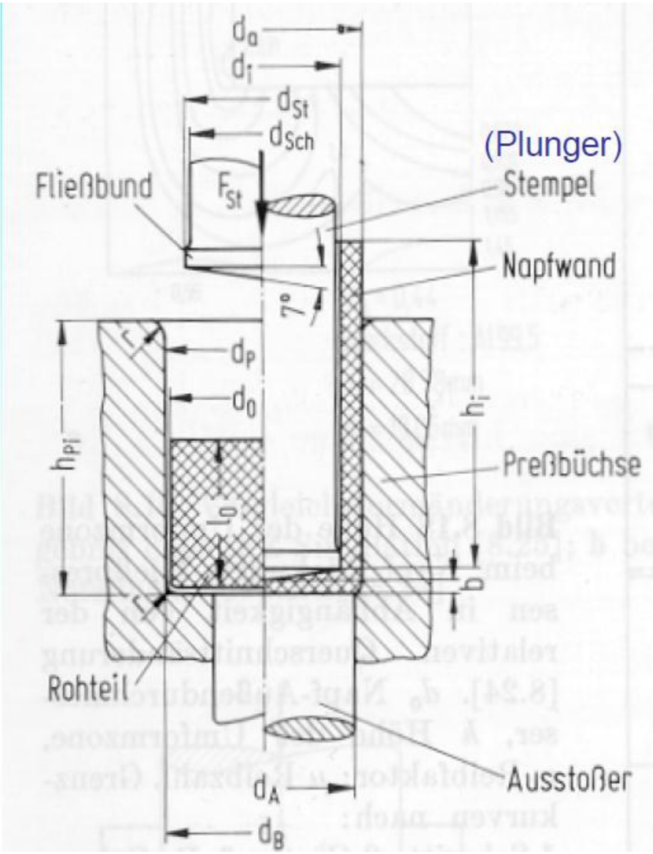
Tube Forming: Fine-Grain Nb



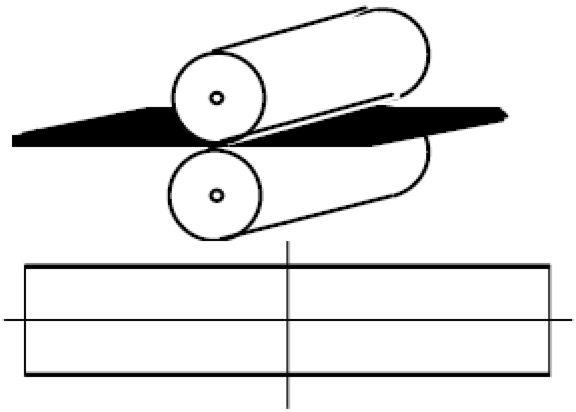
- Small and uniform grains
- Elongation at break > 30%



Tube Forming: Single-Crystal Nb

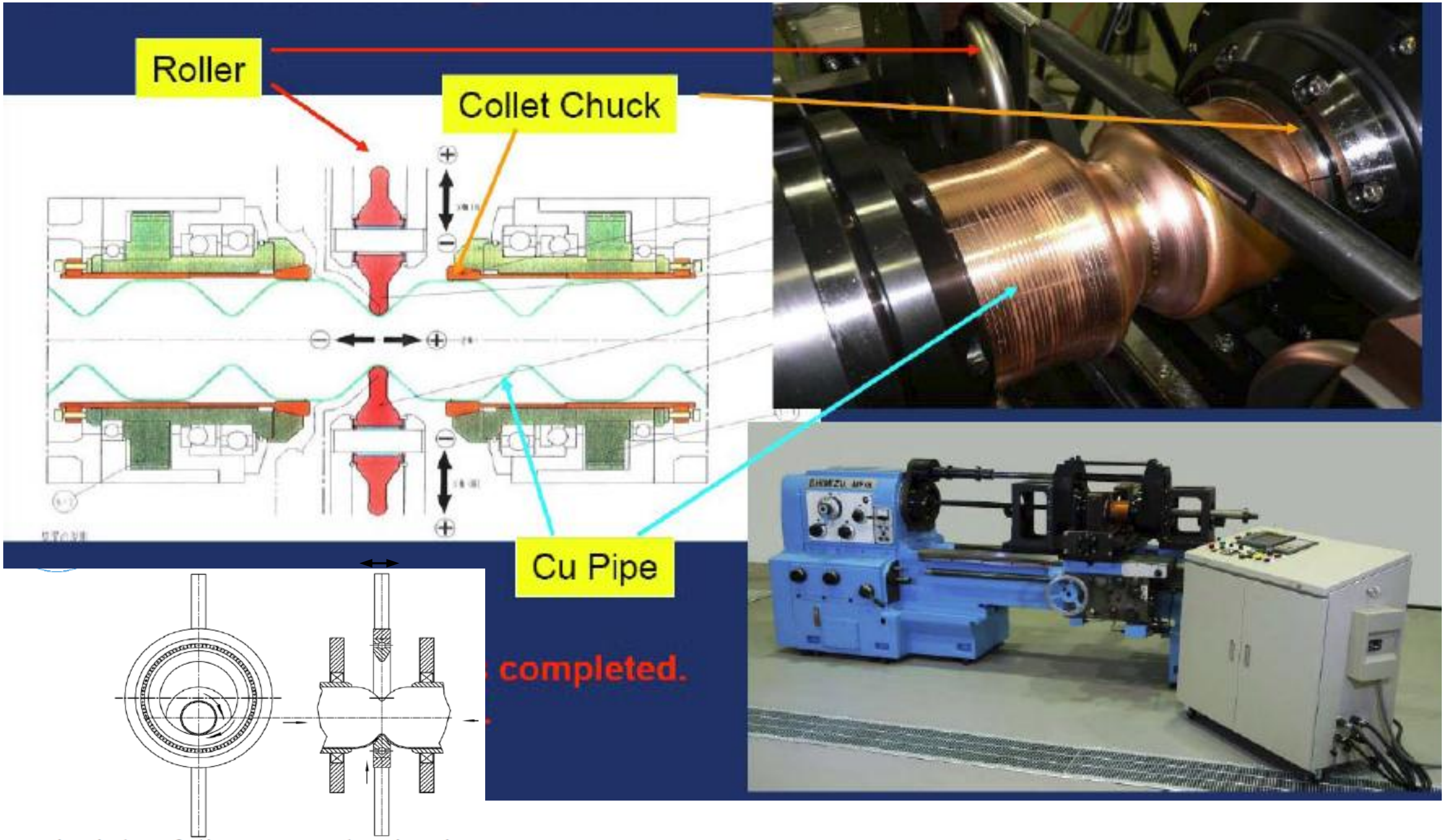


Seamless single-crystal tube by back extrusion



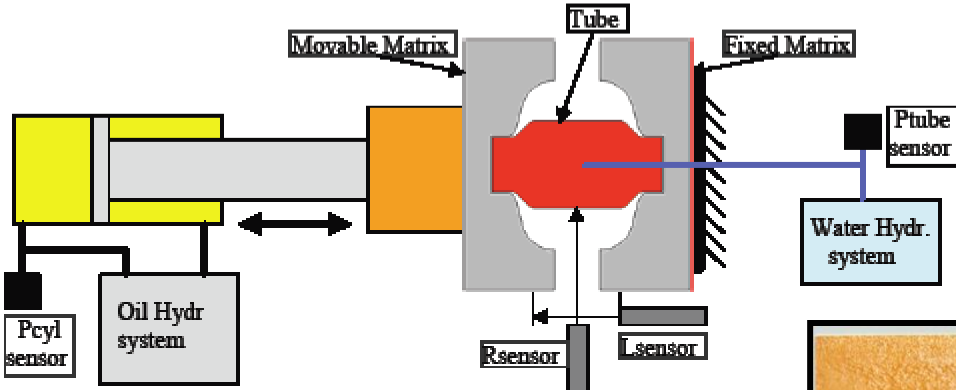
- Welded single-crystal tube:
  - Rolling of single-crystal with intermediate annealing
  - EBW with matching of the orientation

Necking

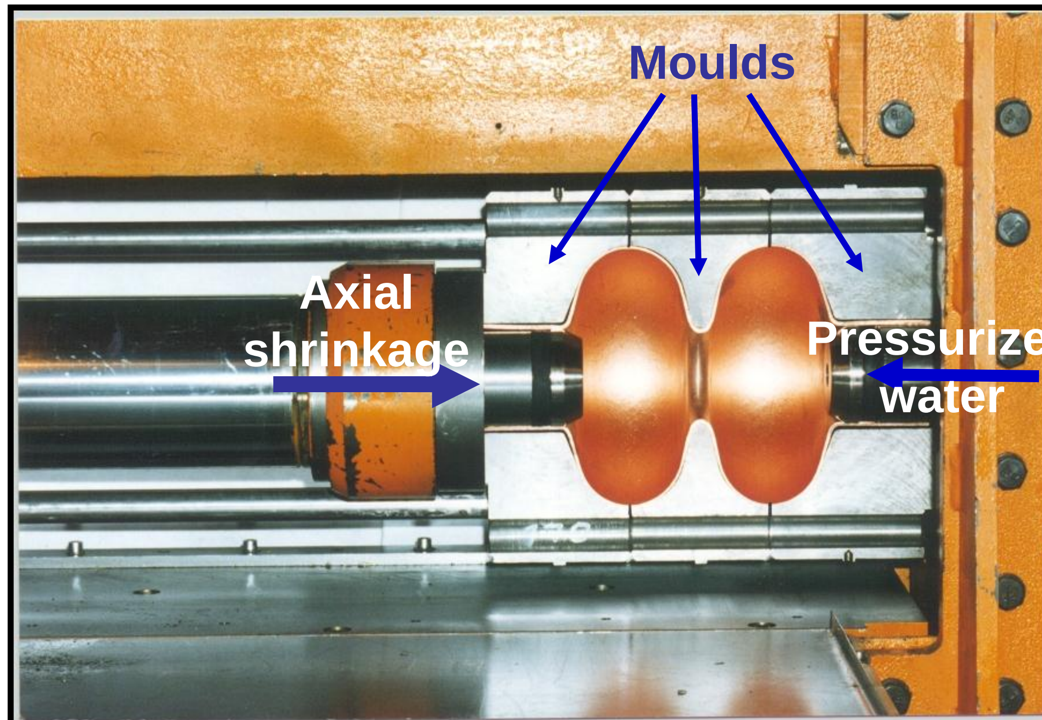


Principle of diameter reduction in the tube end and in the tube middle

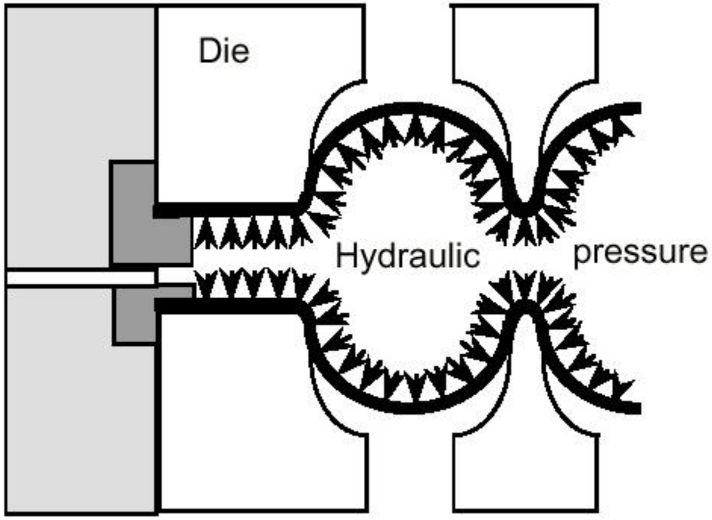
Hydroforming

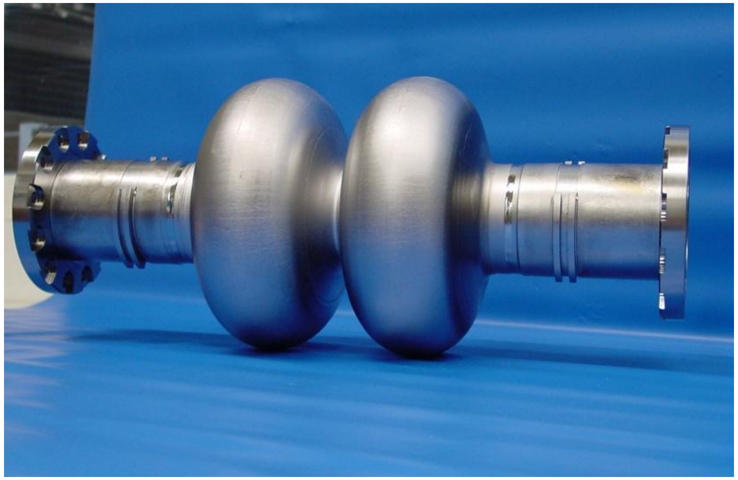


Relies on the correct relationship between applied internal pressure and axial displacement (strain rate) to remain below the plastic limit



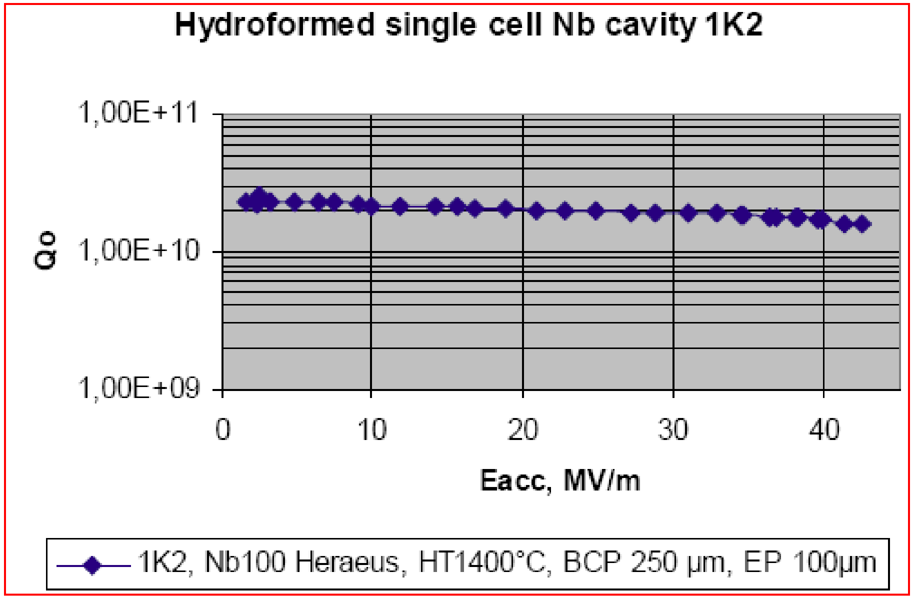
Hydroforming

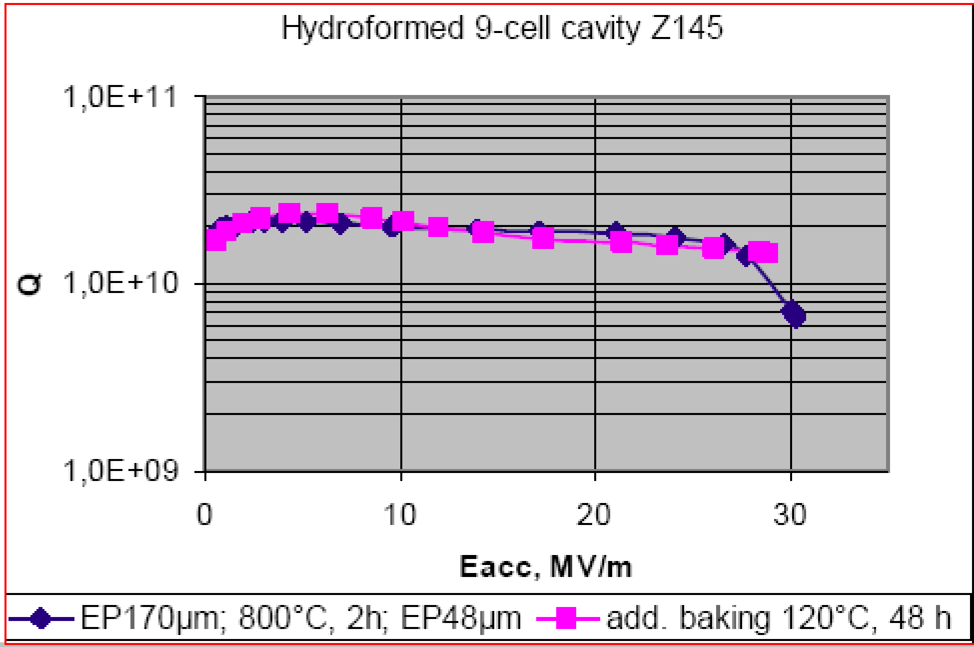




DESY hydroforming machine

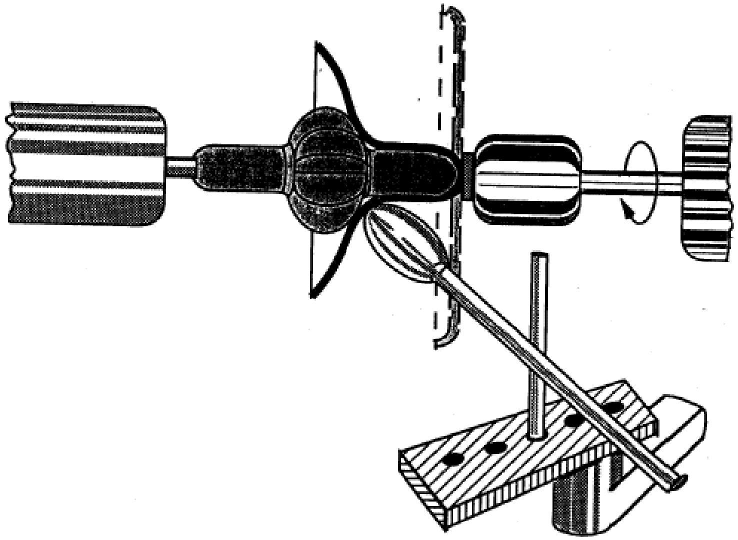
Hydroforming: Cavity Results

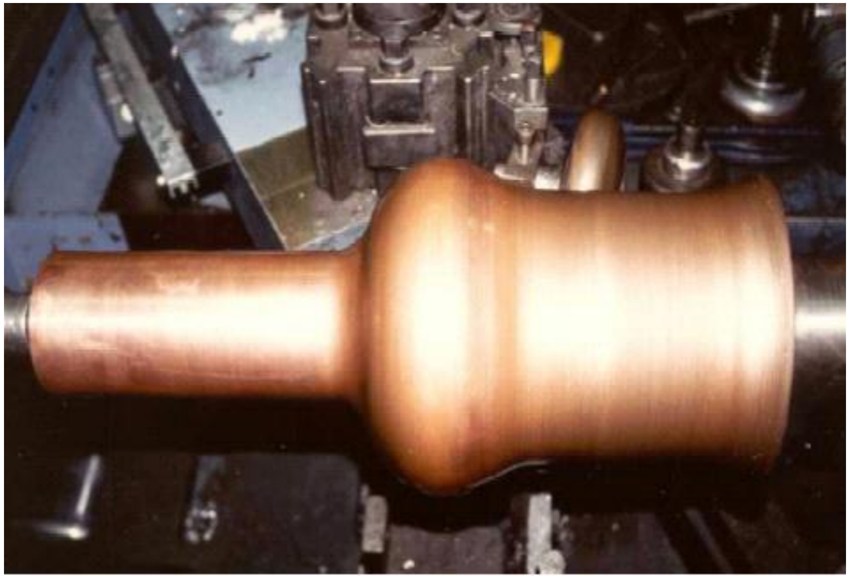




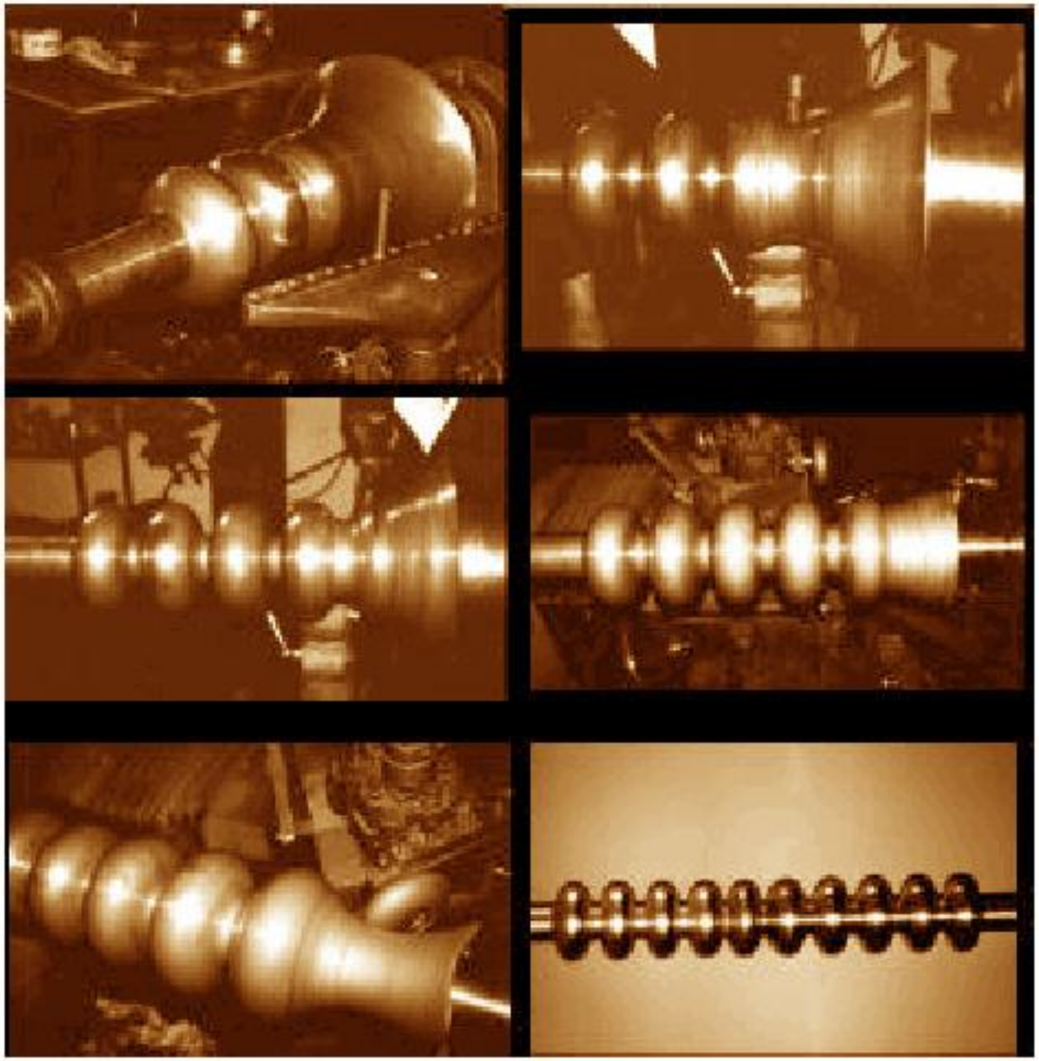
Spinning

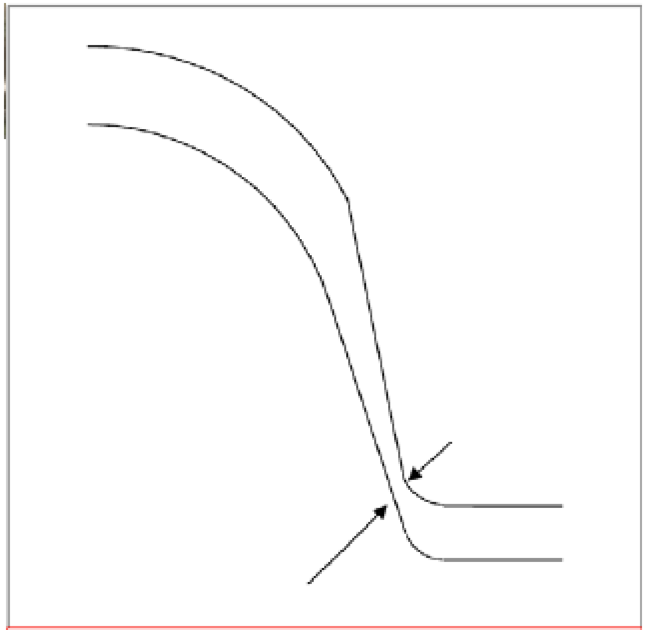
- Starting from discs or seamless tubes
- Collapsible mandrels
- Very rough surface after fabrication





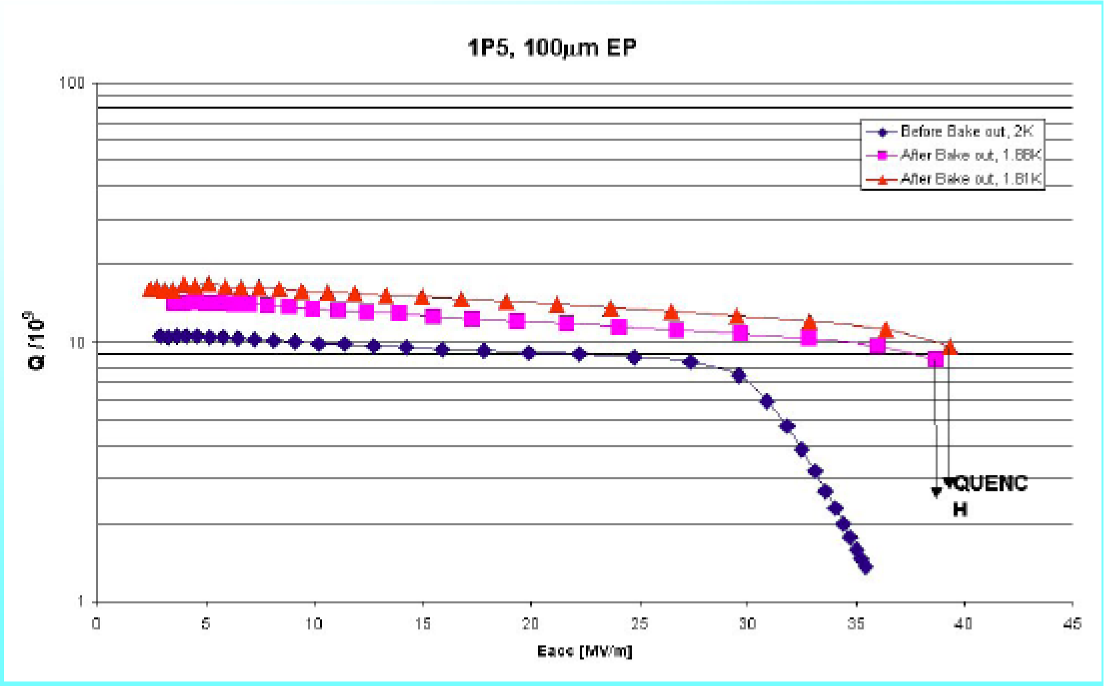
Spinning





The problem of excessive thinning at the terminal iris

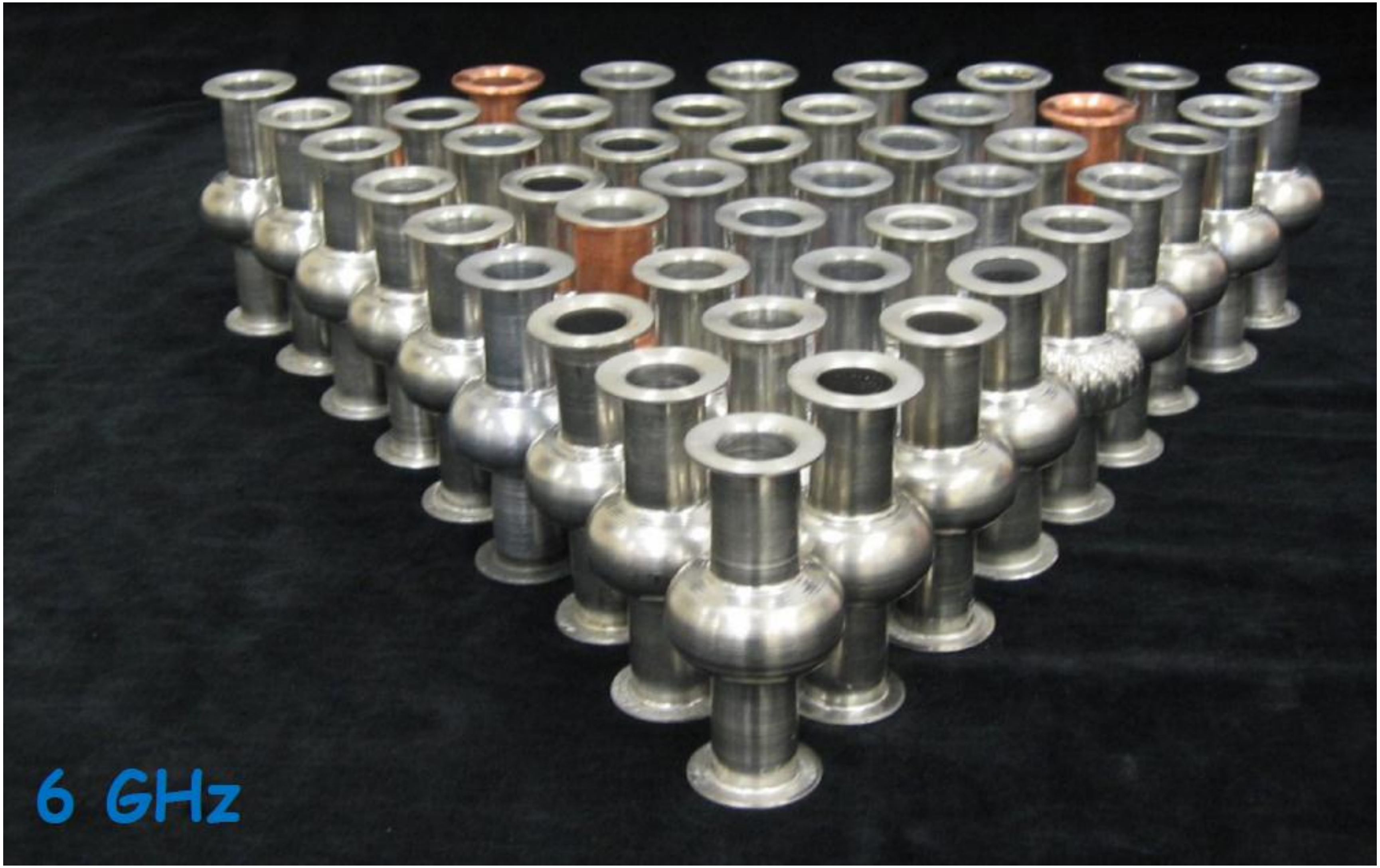
Spinning: Cavity Test Results



1.3 GHz single-cell cavity

1.3 GHz 9-cell cavity. Damaged after CBP, no test

Spinning: Cheap Sample Cavities



Nb/Cu Clad Material

Advantages

• cost effective: allows saving a lot of Nb (ca. 4 mm cavity wall has only ca. 1 mm of Nb and 3 mm Cu). Especially significant for large projects like ILC

• bulk Nb microstructure and properties (the competing sputtering technique does not have such advantages)

• the treatment of the bulk Nb BCP, EP, annealing at 800°C, bake out at 150°C, HPR, HPP can be applied (excluding only post purification at 1400°C).

• high thermal conductivity of Cu helps for thermal stabilization

• stiffening against Lorentz - force detuning and microphonics can be easily done by increasing of the thickness of Cu layer.

• fabrication by seamless technique allows elimination of the critical for the performance welds especially on equator

W. Singer SRF 2005

Nb/Cu Clad Cavity Fabrication

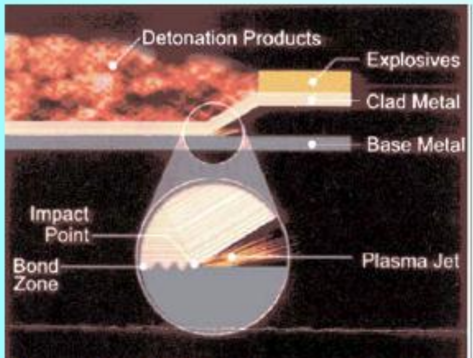
- Nb/Cu laminated material is formed into a tube by:
  - Explosion bonding
  - Back extrusion
  - Hot bonding

- Nb/Cu clad cavity if formed from the tube by hydroforming

- Beam tubes/End groups are welded to the thin Nb layer by EBW. The Cu backing must be removed and cleaned at the weld joints

Nb/Cu Tubes: Explosion Bonding

- Explosion bonding of seamless Nb tube 4 mm thick with Cu tube 12 mm thick
- Flow forming into Nb/Cu tube, wall thickness 1 mm Nb, 3 mm Cu



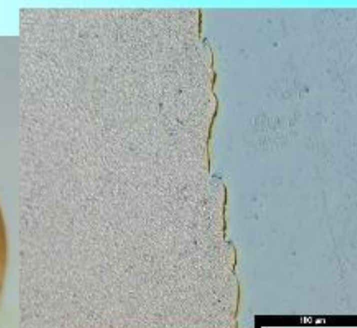
The bonding takes place by an explosively driven, high-velocity angular impact of two metal surfaces.

Explosively bonded NbCu tube

Flow forming of NbCu tube

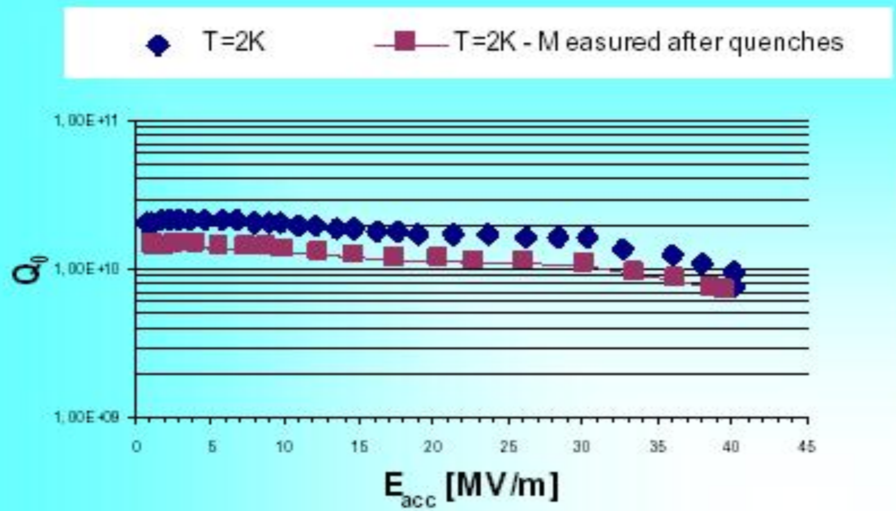
W. Singer SRF 2005

After flow forming



Structure of Nb/Cu interface

Nb/Cu Clad Cavities



NbCu single cell cavity 1NC2 produced at DESY by hydroforming from explosively bonded tube. Preparation and HF tests at Jeff. Lab: 180 μm BCP, annealing at 800°C, baking at 140°C for 30 hours, HPR (P. Kneisel).

40 MV/m without EP

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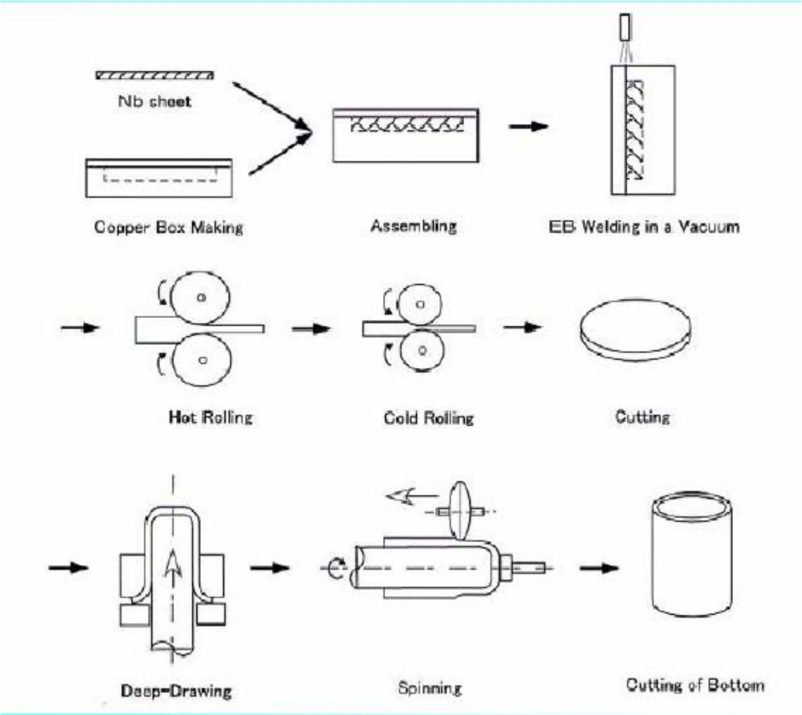
NbCu cavities hydroformed from explosively bonded tubes at DESY.

Difficult to get reproducibly high bonding quality. Hot bonding fabrication procedure of NbCu tubes seems to be more promising

Nb/Cu Tubes: Hot Bonding



Fabrication principle of sandwiched hot rolled Cu-Nb-Cu tube (KEK and Nippon Steel Co.)

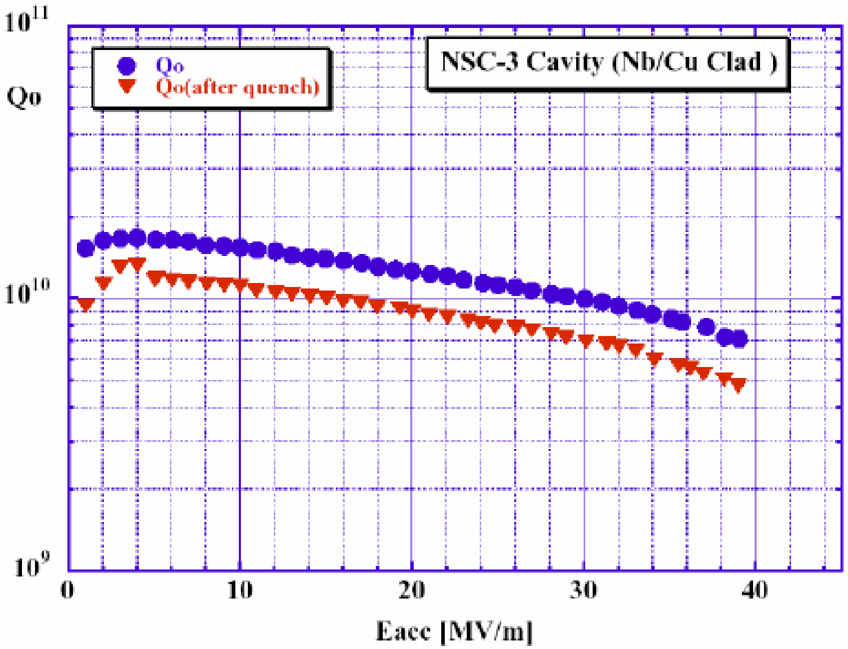
Hot roll bonded Cu-Nb-Cu tube produced at Nippon Steel Co.

Nb/Cu Clad Cavities

Single-cell Nb/Cu cavities from "sandwiched" tube

Four double cell NbCu clad cavities produced at DESY from KEK tubes (no cracks on the inside surface)

Hot roll bonded tube fabrication at Nippon Steel Co., hydroforming at DESY, Preparation and RF tests at KEK



NSC-3: Barrel polishing, CP(10 mμ), Annealing 750ºC x 3h, EP(70 μm) K.Saito

Nb/Cu Clad Cavities Issues

- Possibility of leaky welds because of Cu contamination
- Nb/Cu cavities still quench, resulting in Q-degradations
- Cooldown needs to be very uniform because of thermo–currents
- Cooldown of cryomodules would need modification
- Cracks sometimes appear in iris region during fabrication