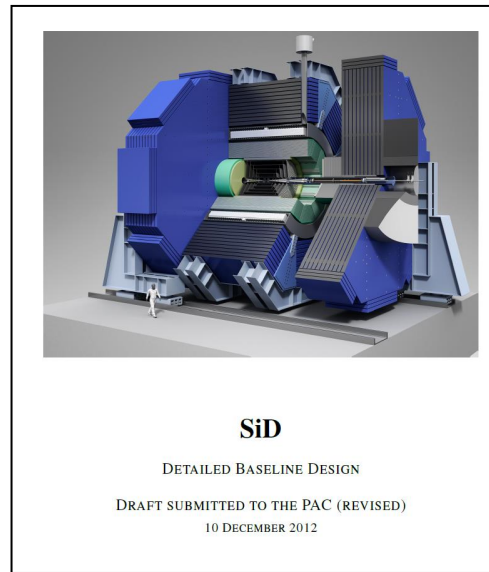
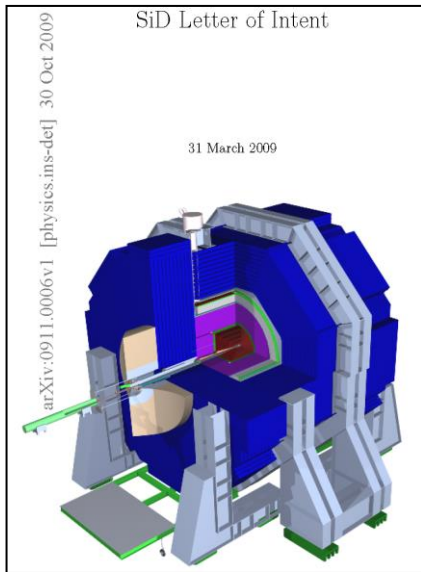


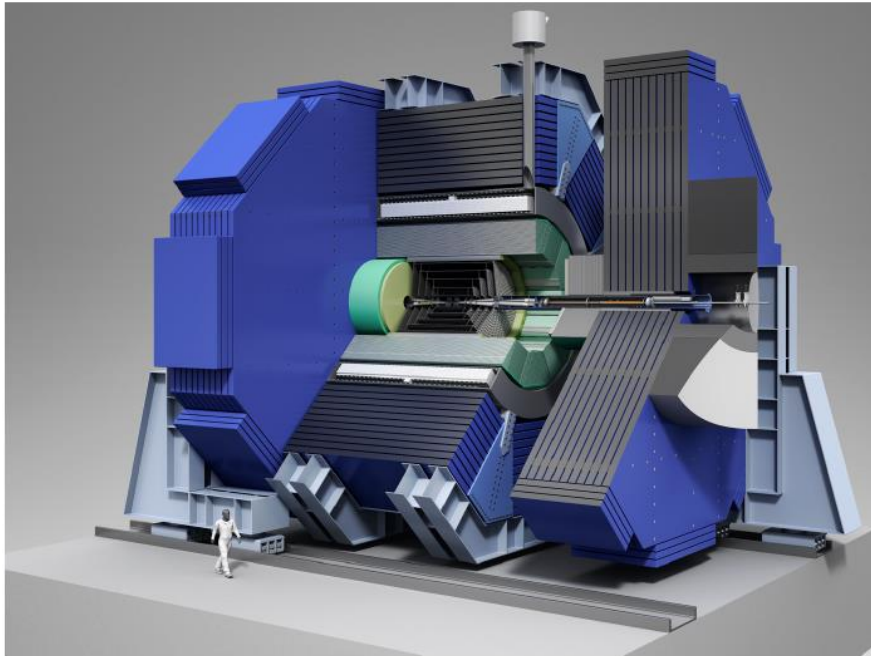
SID MDI & Engineering

Marco Oriunno (SLAC), Nov. 12, 2013
LCWS13, TOKYO

Slowly but Steadily



Detailed Baseline Document - MDI



SiD

DETAILED BASELINE DESIGN

DRAFT SUBMITTED TO THE PAC (REVISED)

10 DECEMBER 2012

7 Engineering, Integration and the Machine Detector Interface

7.1 Introduction

7.2 IR Hall Layout Requirements and SiD Assembly Concepts

7.2.1 Vertical Access (RDR style)

7.2.2 Horizontal Access (Japan style)

7.2.3 Detector Access for Repairs

7.3 Detector Exchange Via a Sliding Platform

7.3.1 Introduction

7.3.2 Platform

7.3.3 Vibration analysis and Luminosity Preservation

7.3.4 Push Pull Detector Exchange Process and Time Estimate

7.4 Beampipe and Forward Region Design

7.4.1 Introduction to the Near Beamline Design

7.4.2 Beampipe

7.4.3 LumiCal, BeamCal, Mask and QD0 Support and Alignment

7.4.4 QD0-QF1 interface

7.4.5 Vacuum System and Performance

7.4.6 Feedback and BPMs

7.4.7 Wakefield and Higher Order Mode Analysis

7.4.8 Frequency Scanning Interferometric (FSI) Alignment of QD0 and QF1

7.4.9 Routing of Detector Services

7.5 Impact on the Adjacent Detector While SiD is Operational

7.5.1 Radiation Calculations

7.5.2 Fringe Fields and Magnetics

Steps toward a real SiD

Some national body (ies) (Japan and collaborators?) commits to linear collider **2014**

Optimize SiD + Value engineering : lower costs and preserve performance

Prepare serious TDR with technical prototypes and serious cost estimate. 3 years: **2017**

Requires a fully reviewed TDR. Assume the review process, with minor iterations, takes 1 year. **2018**

Ready for Construction...Adding time for collaboration formation...

From here to Commitment

1. A Technical Design Report should include:
 - Clear baseline choices for all subsystems
 - Final subsystem dimensions & clearances
 - Reasonably complete mechanical designs including tooling
 - Prototypes and Testbeam
 - Serious cost estimate
2. We presently have < 0.5 Mechanical Engineers total in SiD. This would have to go to 2 FTE's to begin to make mechanical progress.
3. In the intensive TDR stage, this should be ~10 FTE's + similar number of designers.
4. The Electronic Engineering is in better shape.
5. System Engineering (Interfaces) needs serious effort, particularly cryogenics interfaces . Japanese codes (e.g. radiation, B fields, seismic, transport, etc) need to be studied. Need to encourage US-Japan collaboration proposal.

Machine – Detector Interface

There is ~1.5 m radial difference between SiD and ILD. The SiD platform is 3.8 m thick. The platforms appear to add a year to the construction schedule. Revisit platforms??

SiD $L^* = 3.5$ m; ILD $L^* = 4.5$ m. BNL design dimensions for the SiD QD0 are needed.

Support and vibration issues need continued work.

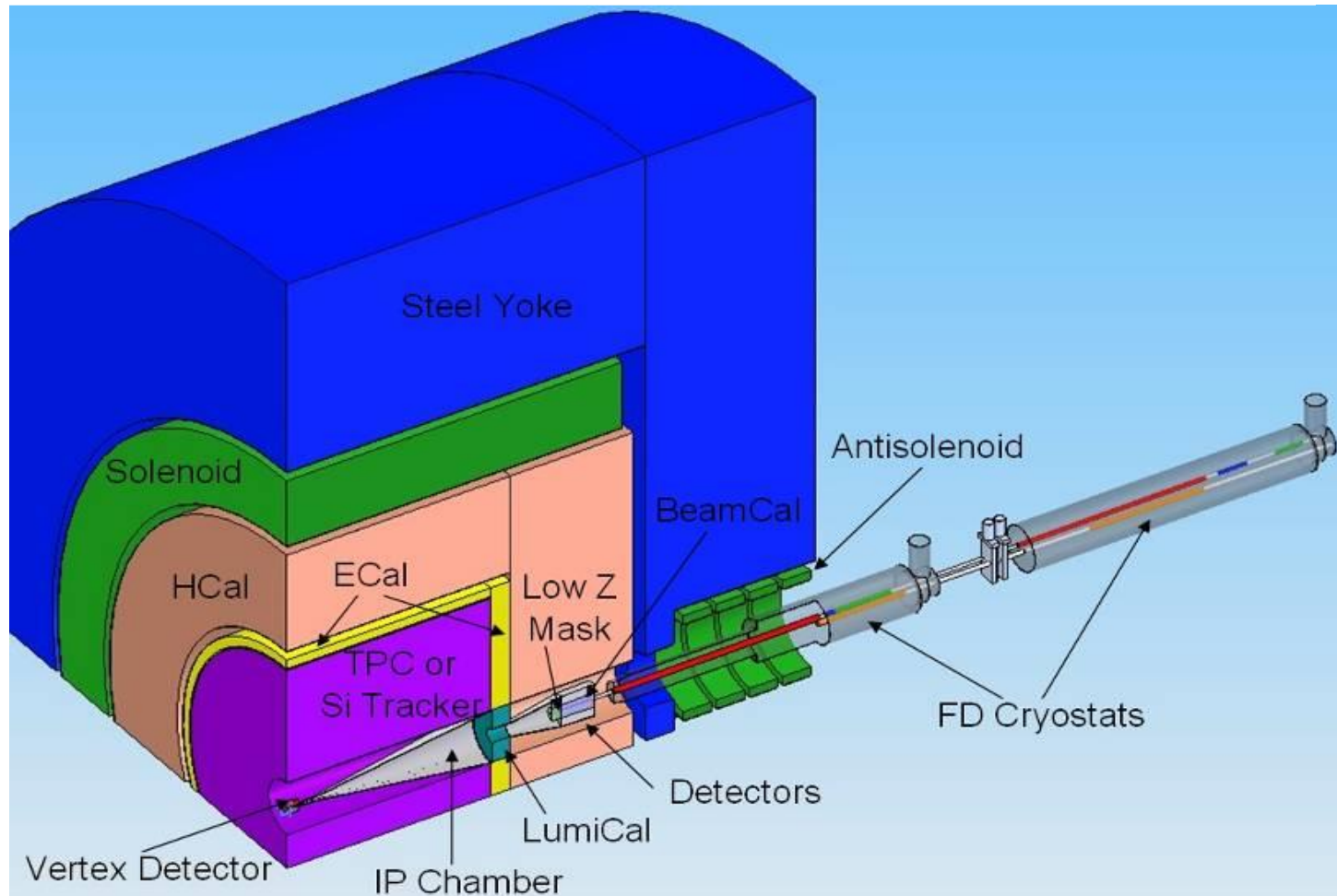
Critical Issues for Mechanical Engineering

It is believed – within the engineering group – that while there are *plenty* of other difficult problems to work on, they do not have the impact or logjam effect of optimization.

There is an enhanced effort on MDI issues at SLAC. We will try to focus them on Critical Issue 2 – Support of the detector, quads, and vibrations and costs.

Interaction Region deliverable

“Provide reliable collisions of ultra small beams (~few nanometers), with acceptable level of background”



Vacuum Spec from Beam Gas Scattering

- Scattering inside the detector is negligible up to **1'000 nT**

250 GeV e- \longrightarrow OD2.4 cm x 7 m long gas (H₂/CO/CO₂)
only Moller scattering off atomic electrons is significant.

Luminosity backgrounds (pairs, $\gamma\gamma\rightarrow$ hadrons) are much higher

Within the IP region there are **0.02 - 0.04 hits/bunch (3-6 hits TPC)** at an average energy of about **100 GeV/hit** originating QD0–200 m from the IP.

Therefore 1 nT from QD0–200 m is conservative.

On the FD protection collimator there are **0.20 charged hits/bunch (33 hits TPC)** at an average energy of about **240 GeV/hit** and **0.06 photon hits/bunch (9 hits TPC)** at an average energy of about **50 GeV/hit** originating 0–800 m from the IP.

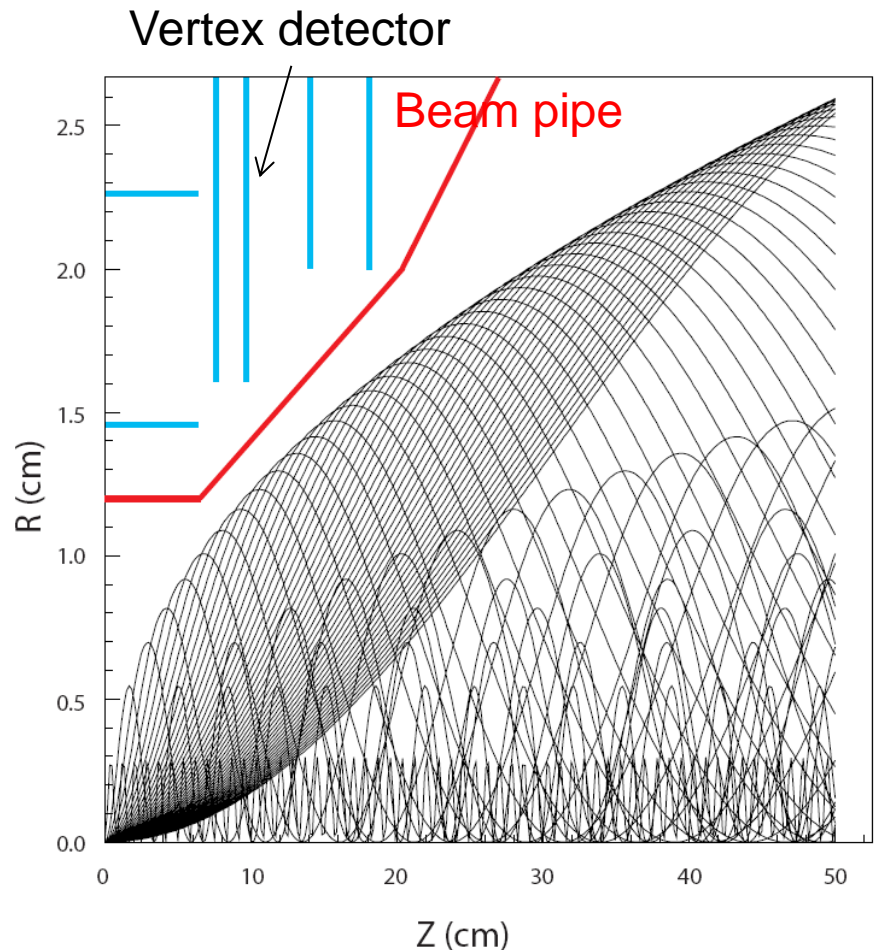
Therefore 10 nT from 200–800 m.

Beyond 800 m from the IP the pressure could conceivably be at least an order of magnitude higher than 10 nT, pending look at BGB background in the Compton polarimeter and energy spectrometer.

Pair edge and Beam pipe design

~200 k pairs/BX are produced.
Pairs develop a sharp edge and
the beam pipe must be placed
outside the edge.

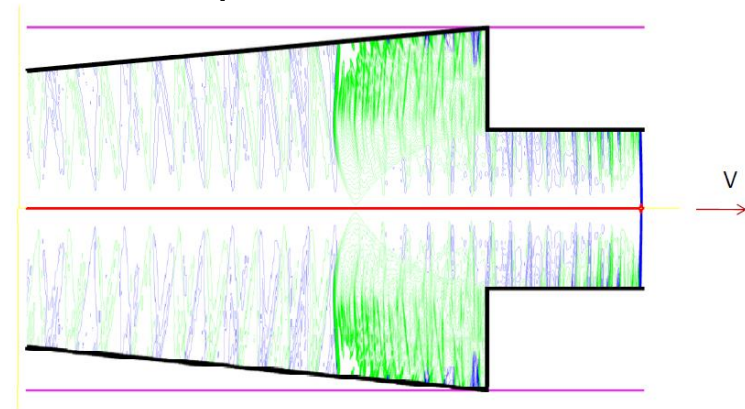
The pair edge is critically
dependent on the IP beam
parameters.



HOM heating at the IP and in QD0 (S.Novokhatski, SLAC)

- *Beam fields*
- *Wake potentials and loss power*
- *Trapped and propagating modes*
- *Frequency spectrum*
- *Resistive wake fields*
- *Total power loss*

Example of Wakefields



- The amount of beam energy loss in IR is very small.
- Spectrum of the wake fields is limited to 300 GHz
- Average power of the wake fields excited ~30 W nominal (6 kW pulsed)
- In the QD0 region the additional losses are of 4W (averaged) .
- BPMs and kickers must be added.

Limits of static magnetic field

Ministerial ordinance of Economic industrial ministry in Japan :

The technical standard regarding electric installation, 27th provision 2, 2011

less than $200\mu\text{ T}$ (2G) in the place where the person enters easily

Guidelines on LIMITS OF EXPOSURE TO STATIC MAGNETIC FIELDS, ICNIRP, HEALTH PHYSICS 96(4):504-514; 2009

ICNIRP : International Commission on Non-Ionizing Radiation Protection

Table 2. Limits of exposure^a to static magnetic fields.

Exposure characteristics	Magnetic flux density
Occupational ^b	
Exposure of head and of trunk	2 T
Exposure of limbs ^c	8 T
General public ^d	
Exposure of any part of the body	400 mT (4KG)

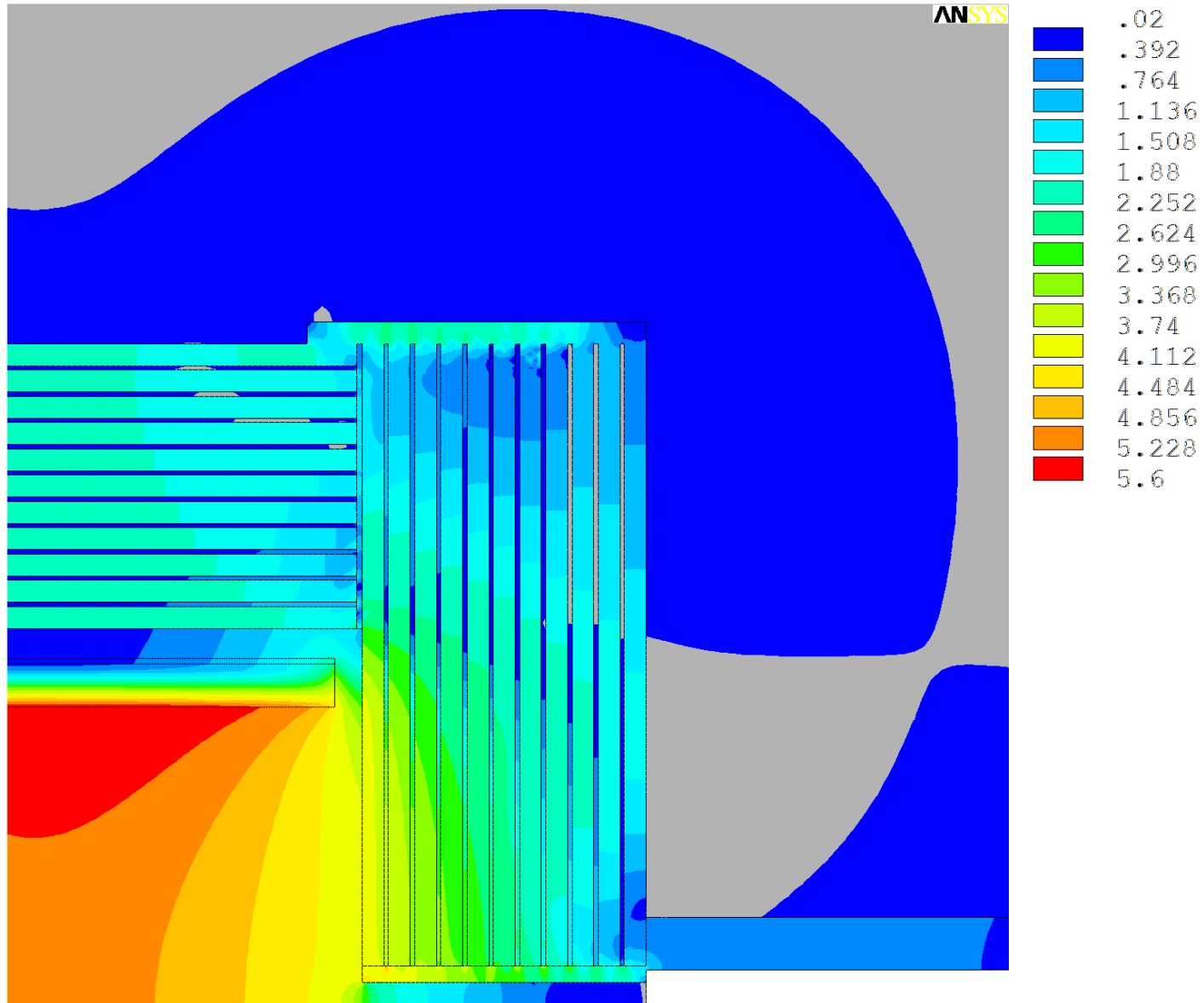
^a ICNIRP recommends that these limits should be viewed operationally as spatial peak exposure limits.

^b For specific work applications, exposure up to 8 T can be justified, if the environment is controlled and appropriate work practices are implemented to control movement-induced effects.

^c Not enough information is available on which to base exposure limits beyond 8 T.

^d Because of potential indirect adverse effects, ICNIRP recognizes that practical policies need to be implemented to prevent inadvertent harmful exposure of persons with implanted electronic medical devices and implants containing ferromagnetic material, and dangers from flying objects, which can lead to much lower restriction levels such as 0.5 mT . (5G)

Fringe Field for a quadrant view of SiD Cut off @ 200 Gauss





Radiation Rules at KEK

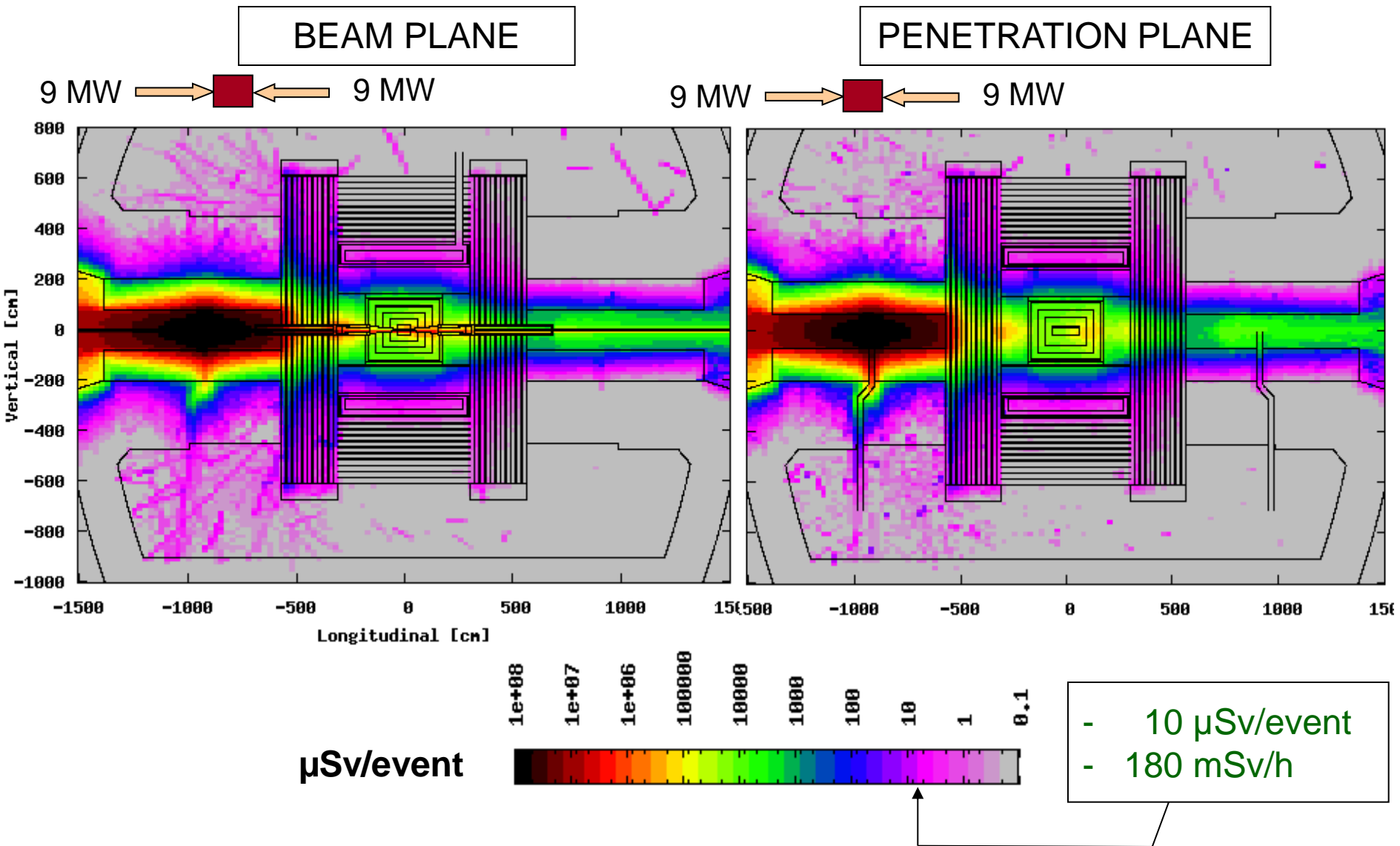
- Normal operation
 - 0.2 $\mu\text{Sv/h}$ for Non-designated area (K1)
 - 1.5 $\mu\text{Sv/h}$ for Supervised area (K2) **experimental hall**
 - 20 $\mu\text{Sv/h}$ for Simple controlled area (K3)
 - 100mSv/h for access restricted
- Shielding **100 $\mu\text{Sv/event}$**
- Mis-steering beam loss
 - **1 hour integration of dose rate should not exceed 1.5 $\mu\text{Sv/h}$ using radiation monitor.**

(Terminate injection and wait 1 hour)

SiD and ILD : Shielding capability of 250 mSv/h / 18 MW = 0.014 mSv/h/kW is required everywhere to meet SLAC requirement

20 R.L. Cu target in IP-9 m. Large pacman.

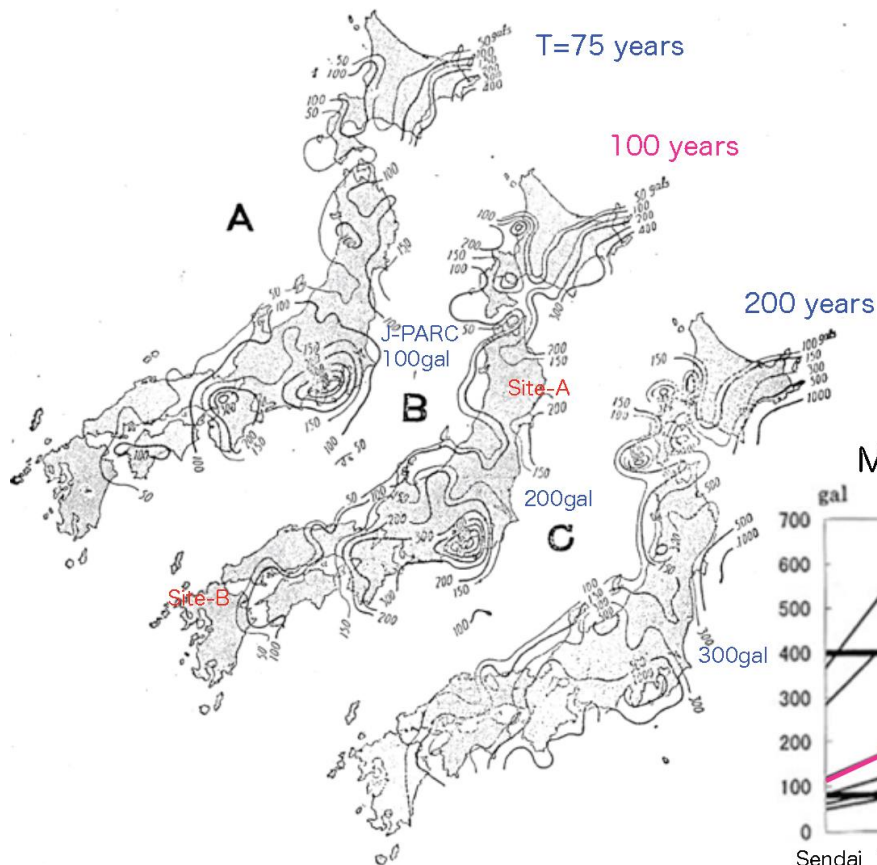
M.Santana, SLAC



Seismic Map Japan

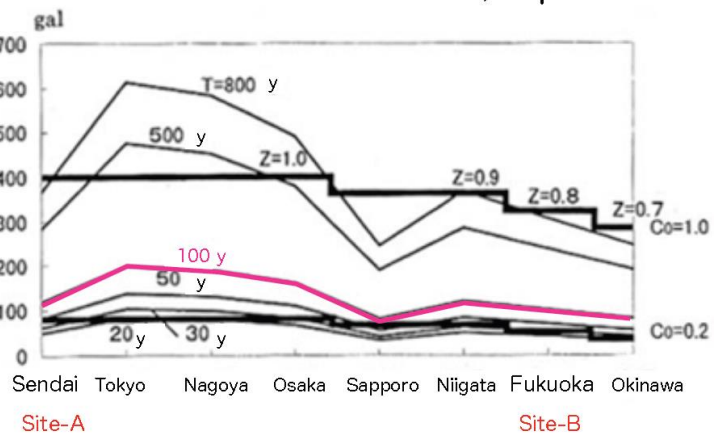
Seismic Hazard Map in Japan : Maximum acceleration (gal)
in recurrence intervals of earthquake

Kawasumi map : based on earthquakes from 679 to 1,948 in Japan



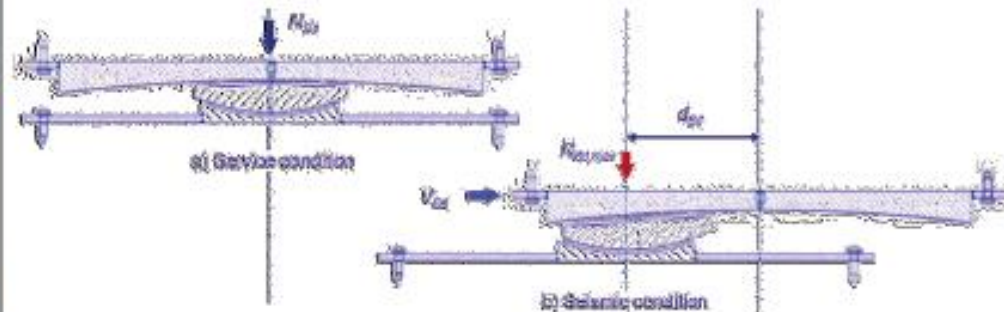
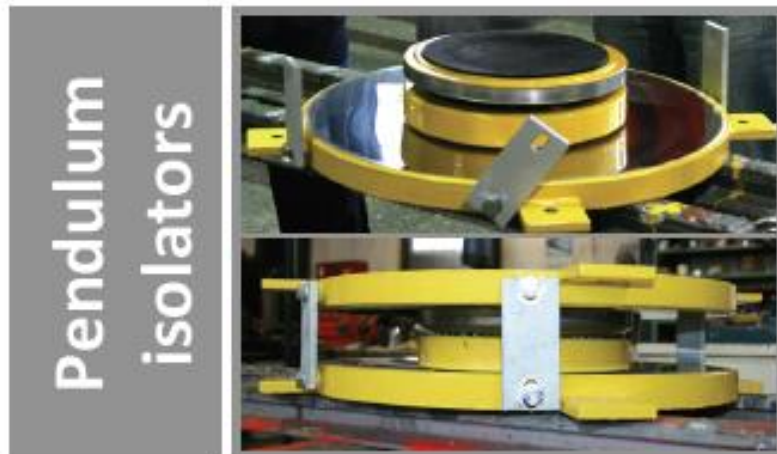
Kitakami Site :
Ultimate Limit State 1g
Service Limit state 0.15g

Max. acceleration in cities, Japan



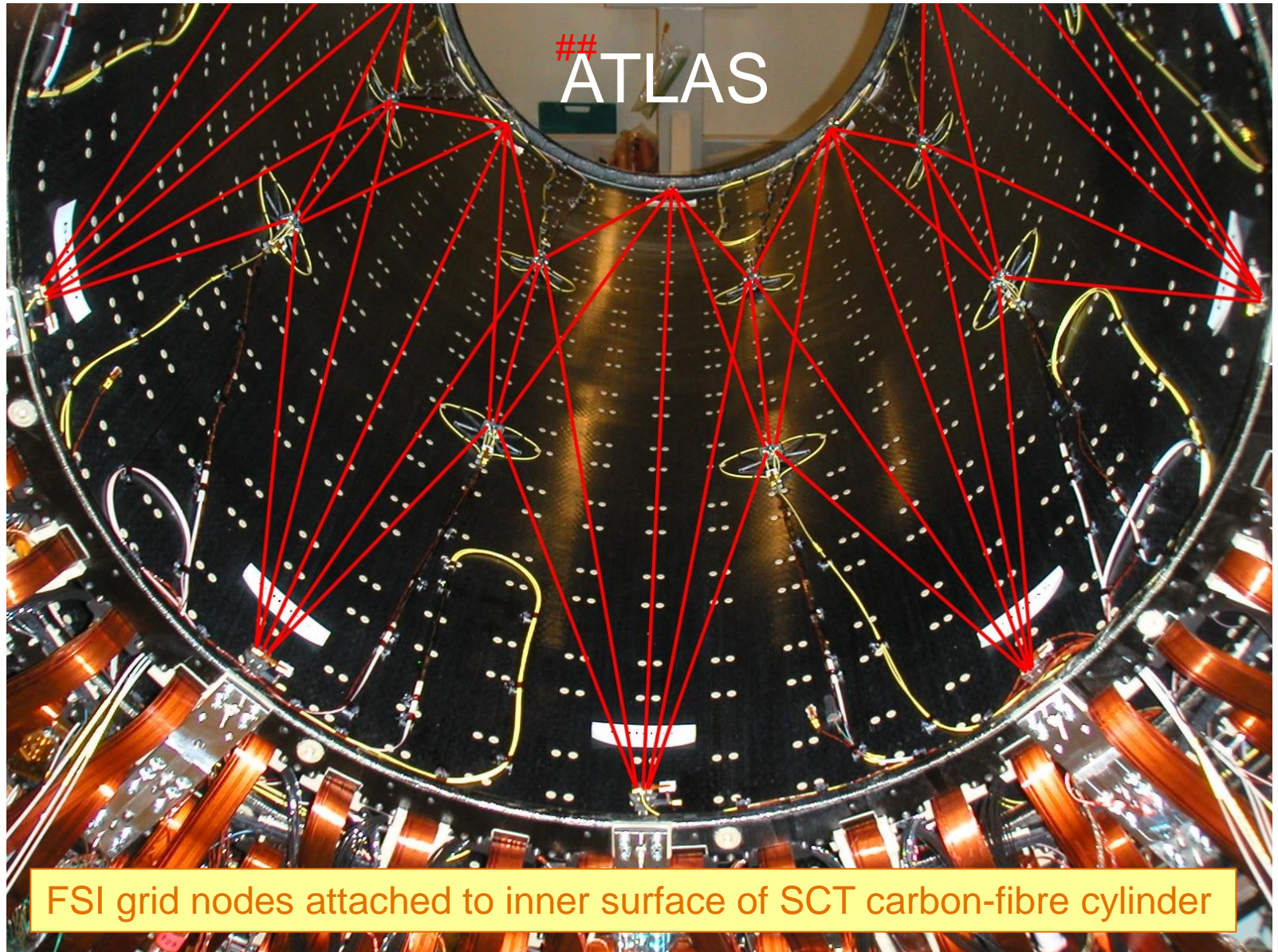
Detector Seismic isolation

- Friction pendulum isolators beneath the detector feet;
- Energy dissipation due to dynamic friction;
- Reliable technology;
- No high compliance elements (e.g. rubber) improves the positioning of the detector;



F.Duarte Ramos, CERN

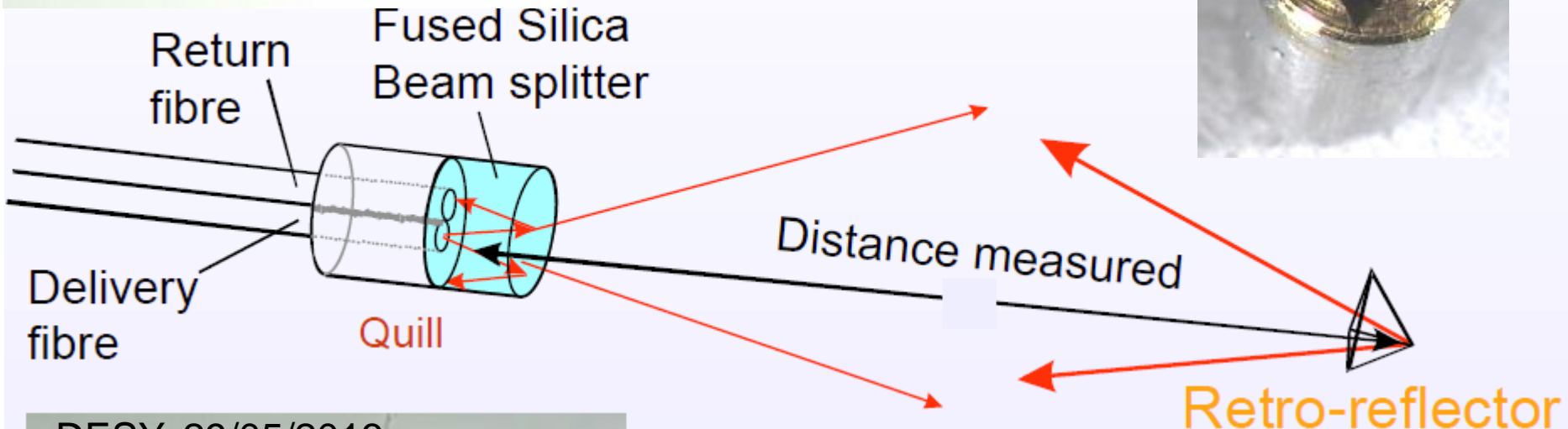
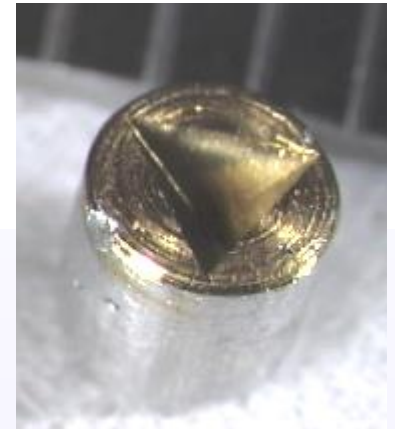
FSI alignment system, precision $\sim 1\mu\text{m}$

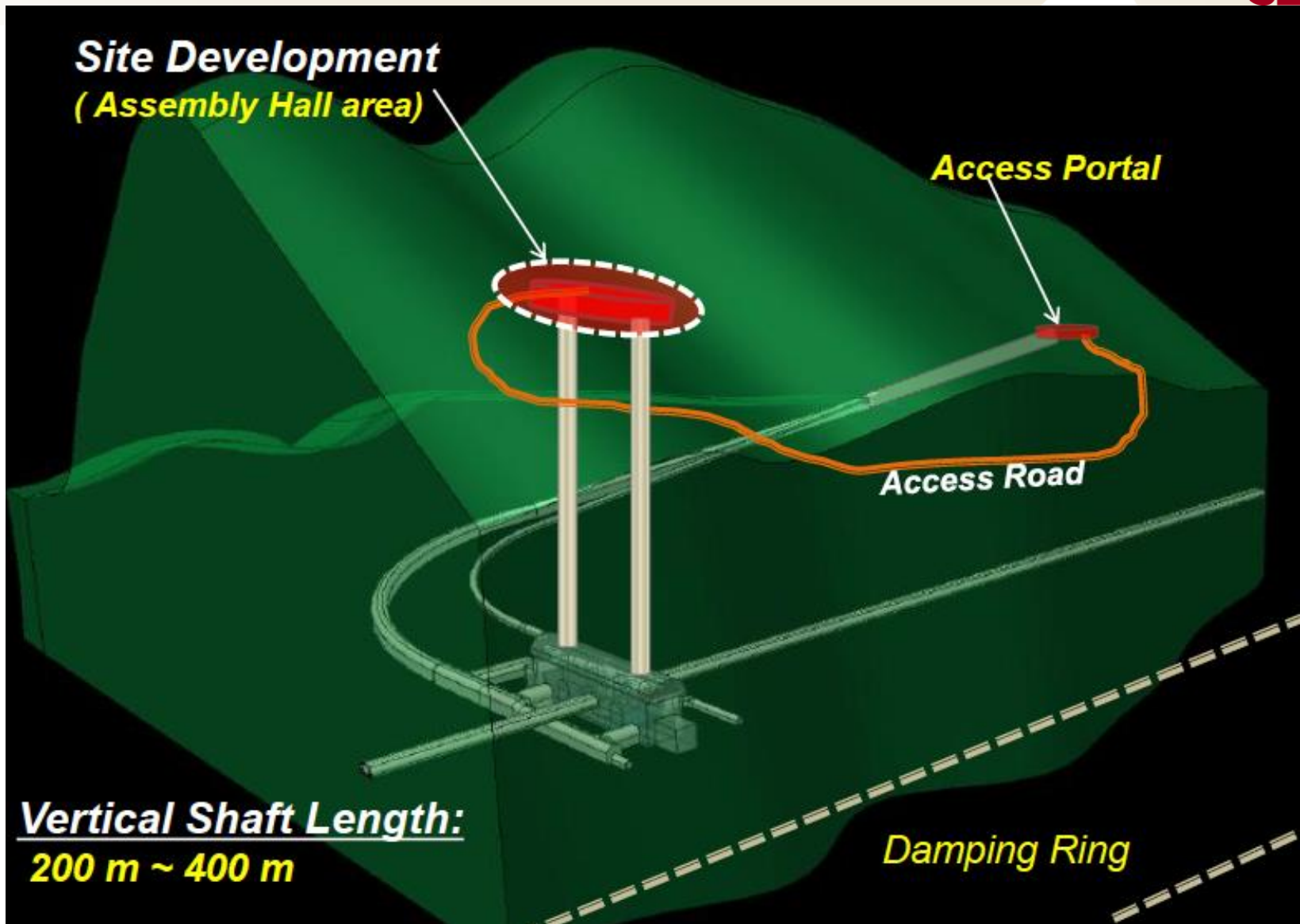


Detector Alignment – Frequency Scan Interferometry

Front-end components of

- minimal mass
- high radiation tolerance





Lean Detectors ?

Toyota Factories pioneered Lean Assembly :

“preserving value with less work”

Fight The Seven Muda (futilities)

Transportation, Inventory, Motion, Waiting, Over-processing, Over-production, Defects.

Big Detectors for Big Science must be Lean :

Time vs labor (Costs)

Time vs Technology drive (Increasing Performances)

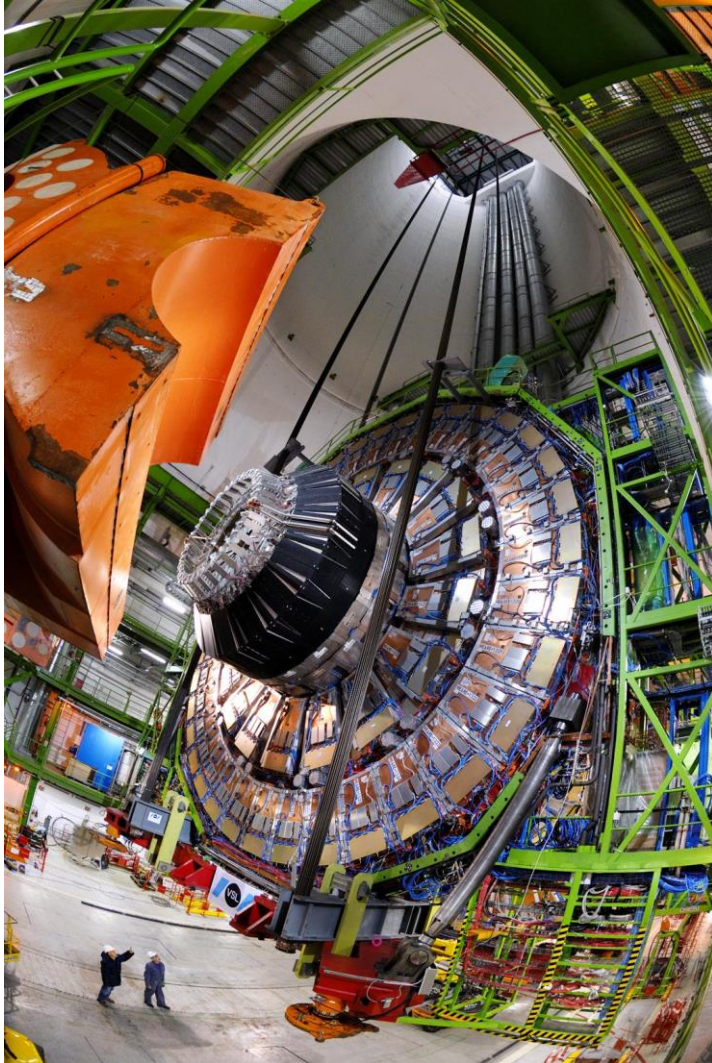
Low Maintenance (Costs)

High Upgradability (Costs and Scientific reach)

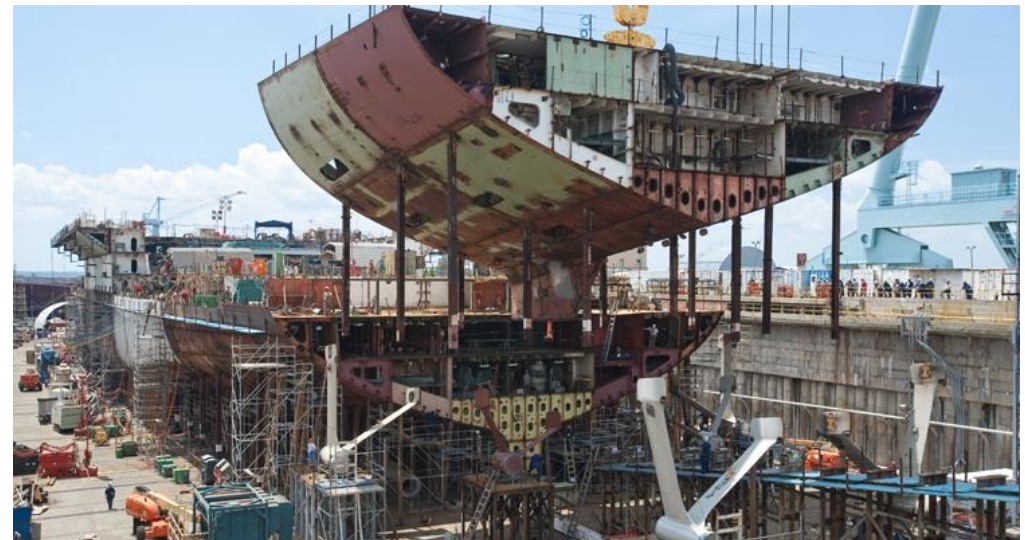
Shorter commissioning to get nominal performances

International Competition

Lean assembly – Some Examples

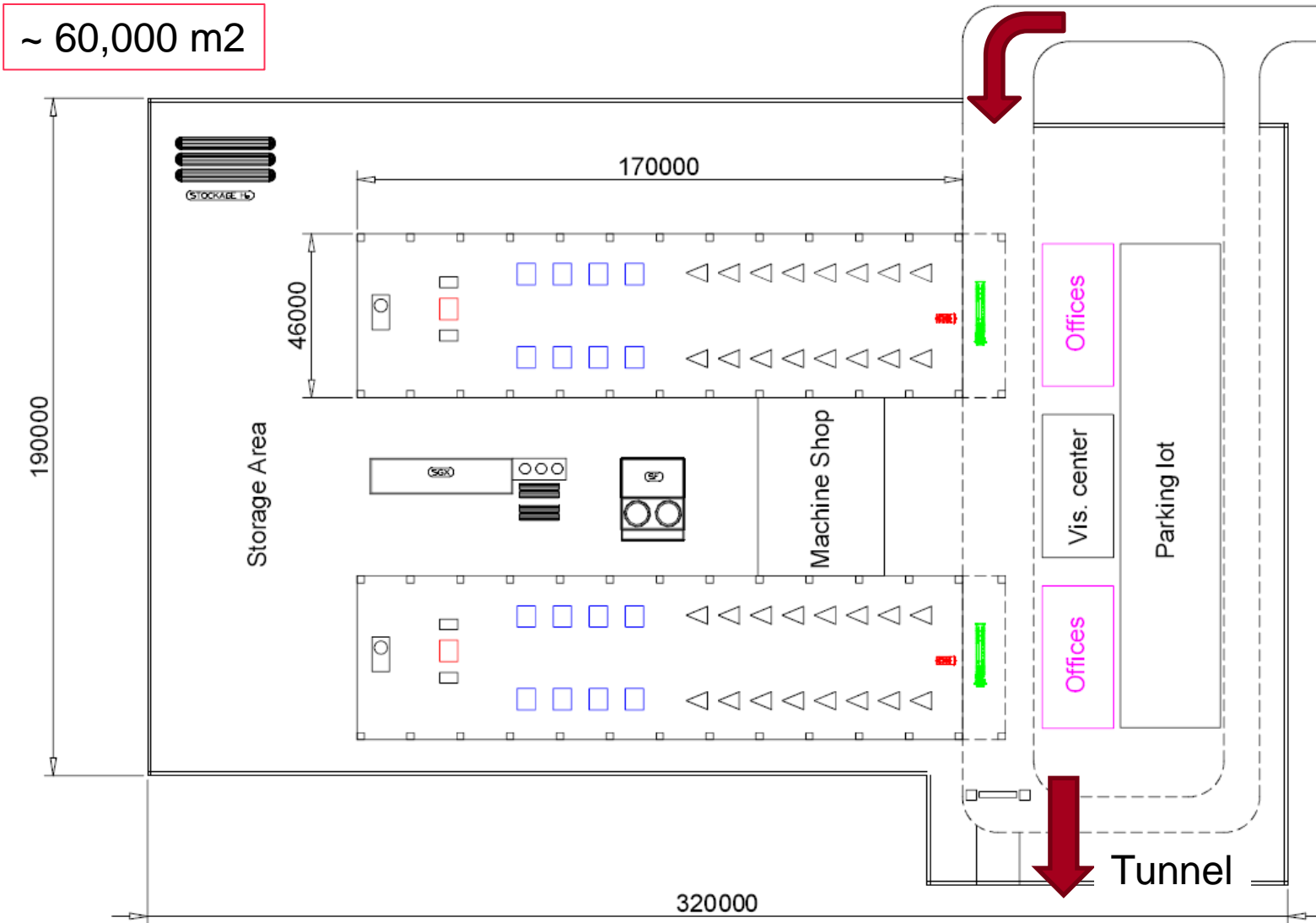


CMS Detector

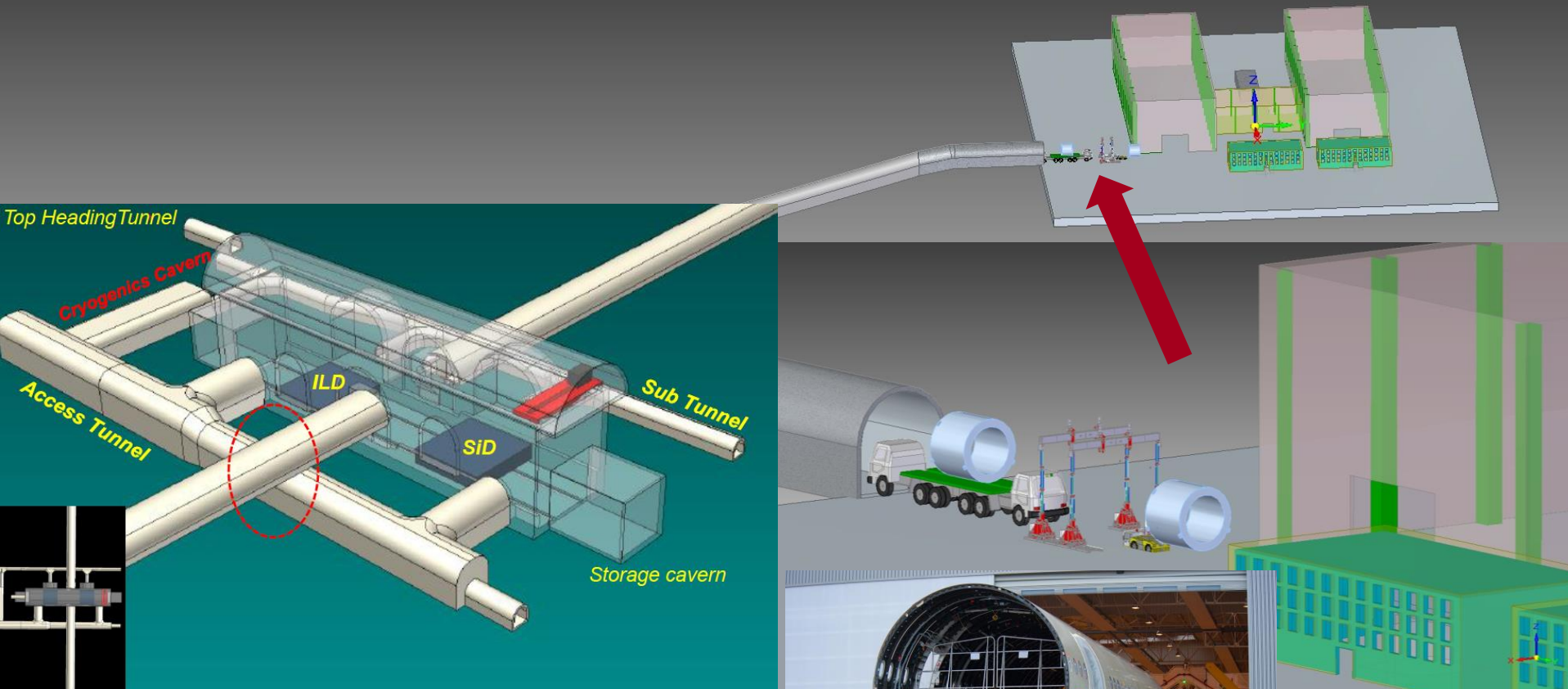


Shipbuilding

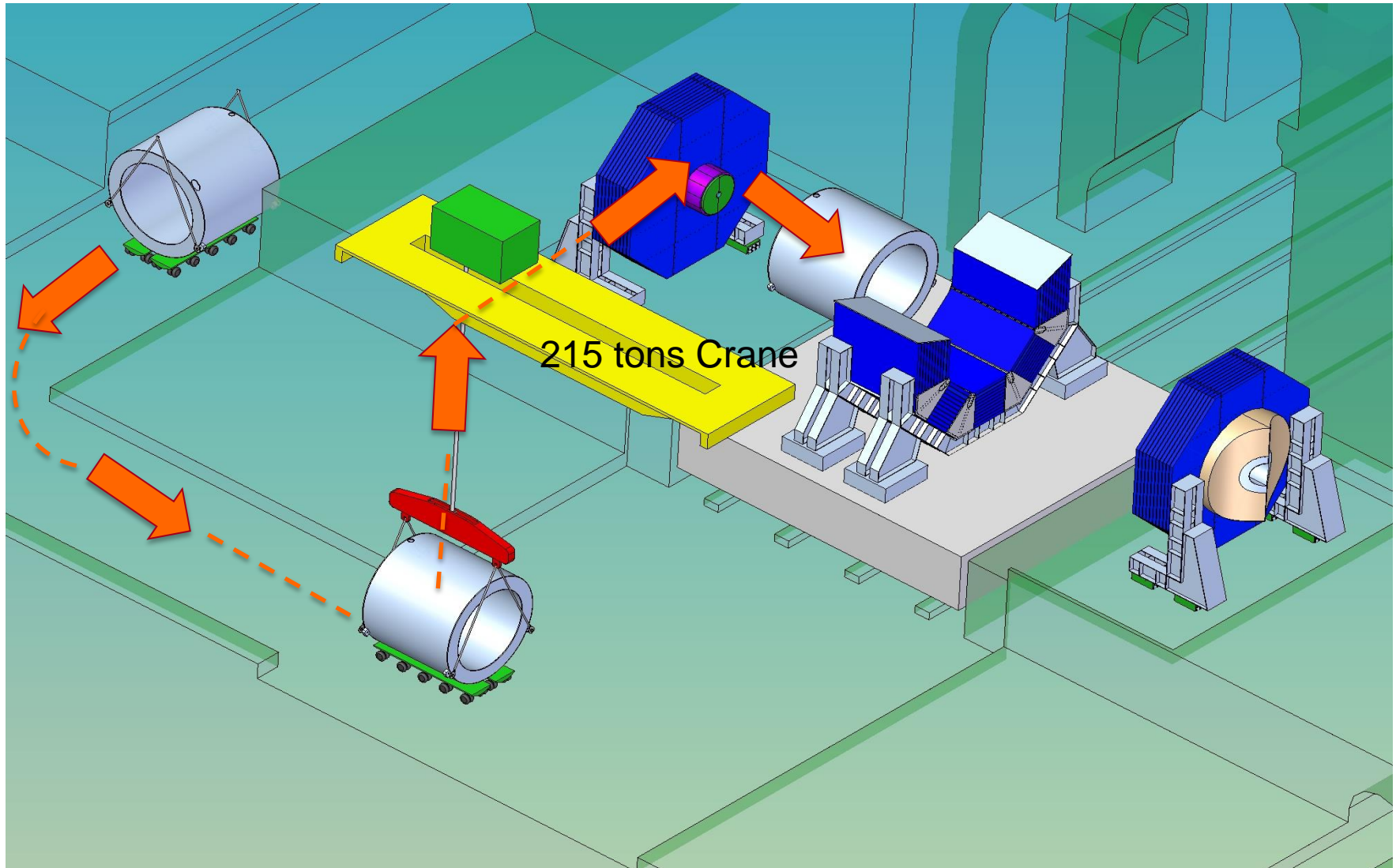
Kitakami Access Yard – Proposal



Kitakami Access Yard



Magnet Installation – Japanese Site

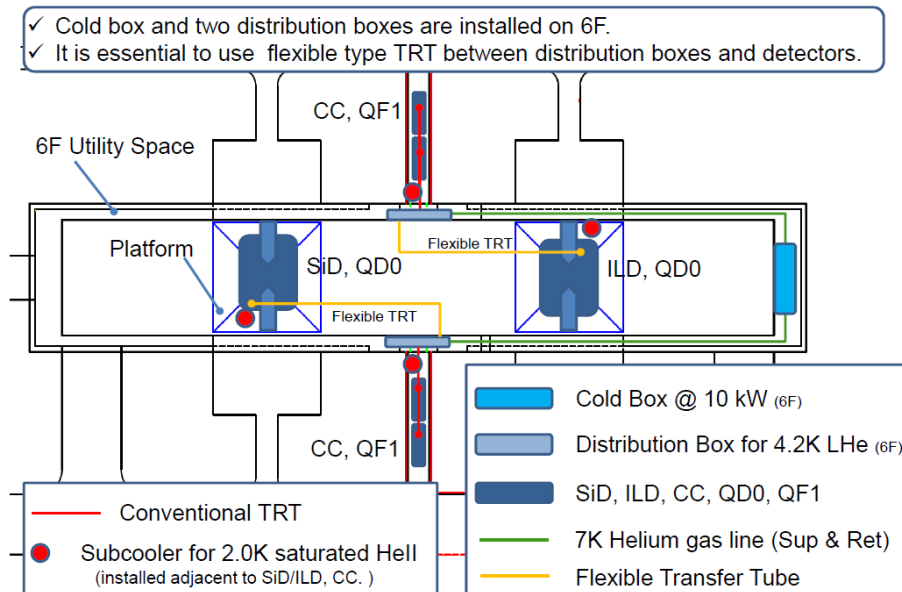


Cryogenic Layout : Two options

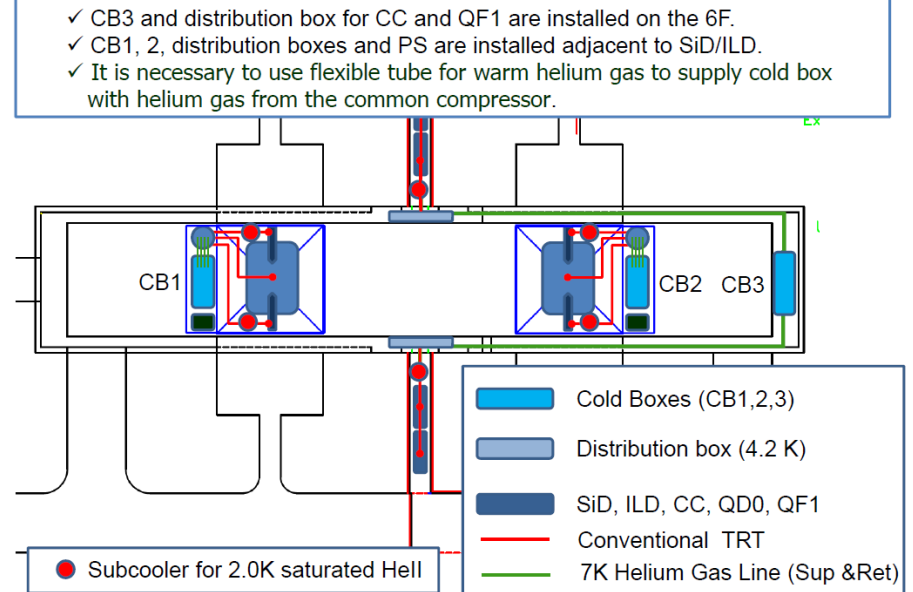
Plan A : Cold Boxes are stationary. Cold Transfer lines to each detector. **Reliability for push-pull. Not off-the-shelf.**

Plan B : Cold Boxes on the platform. Warm Transfer lines to each cold box. **Vibrations, fringe field effects, space**

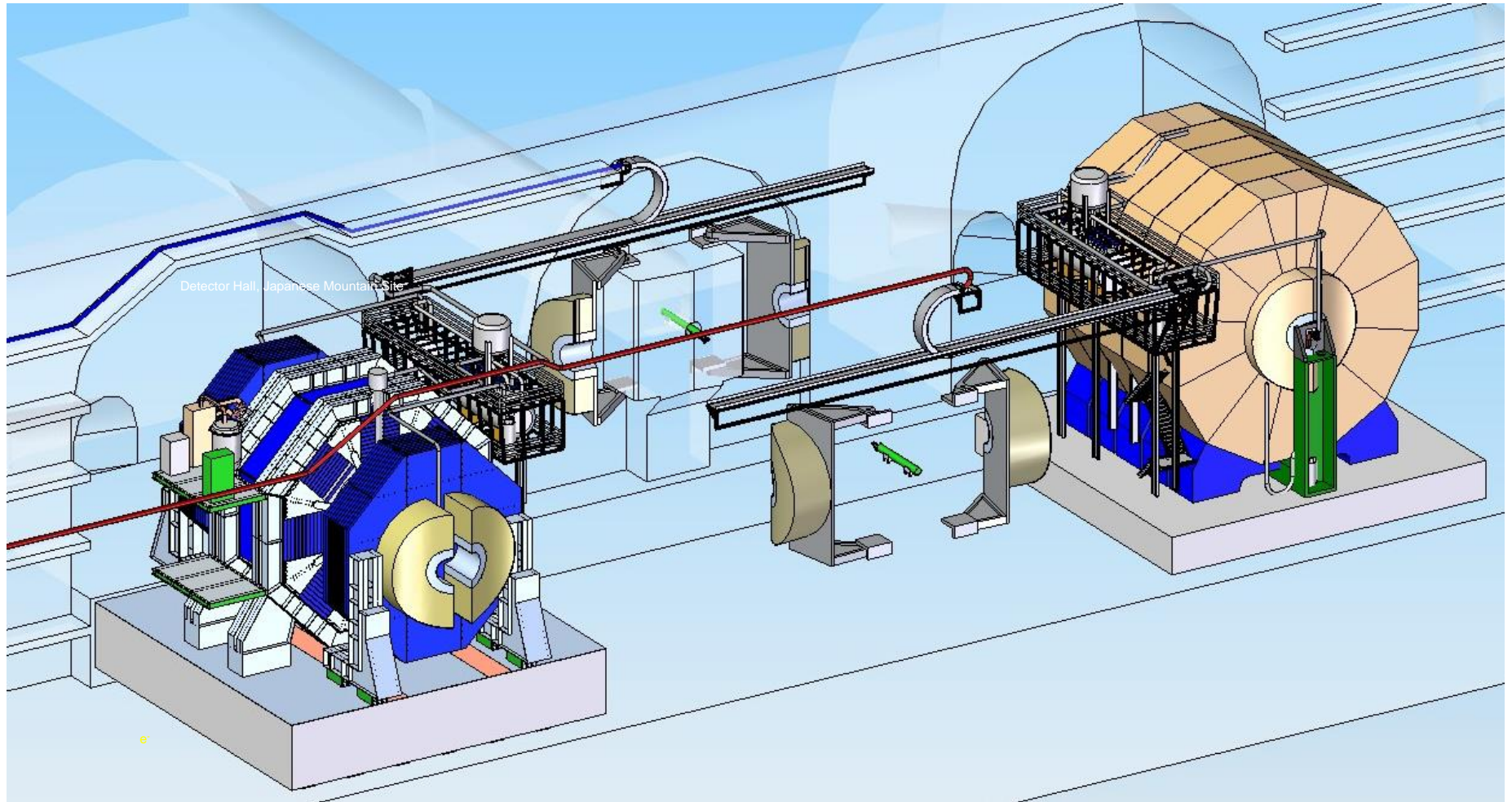
Plan-A: Layout of cryogenic equipment



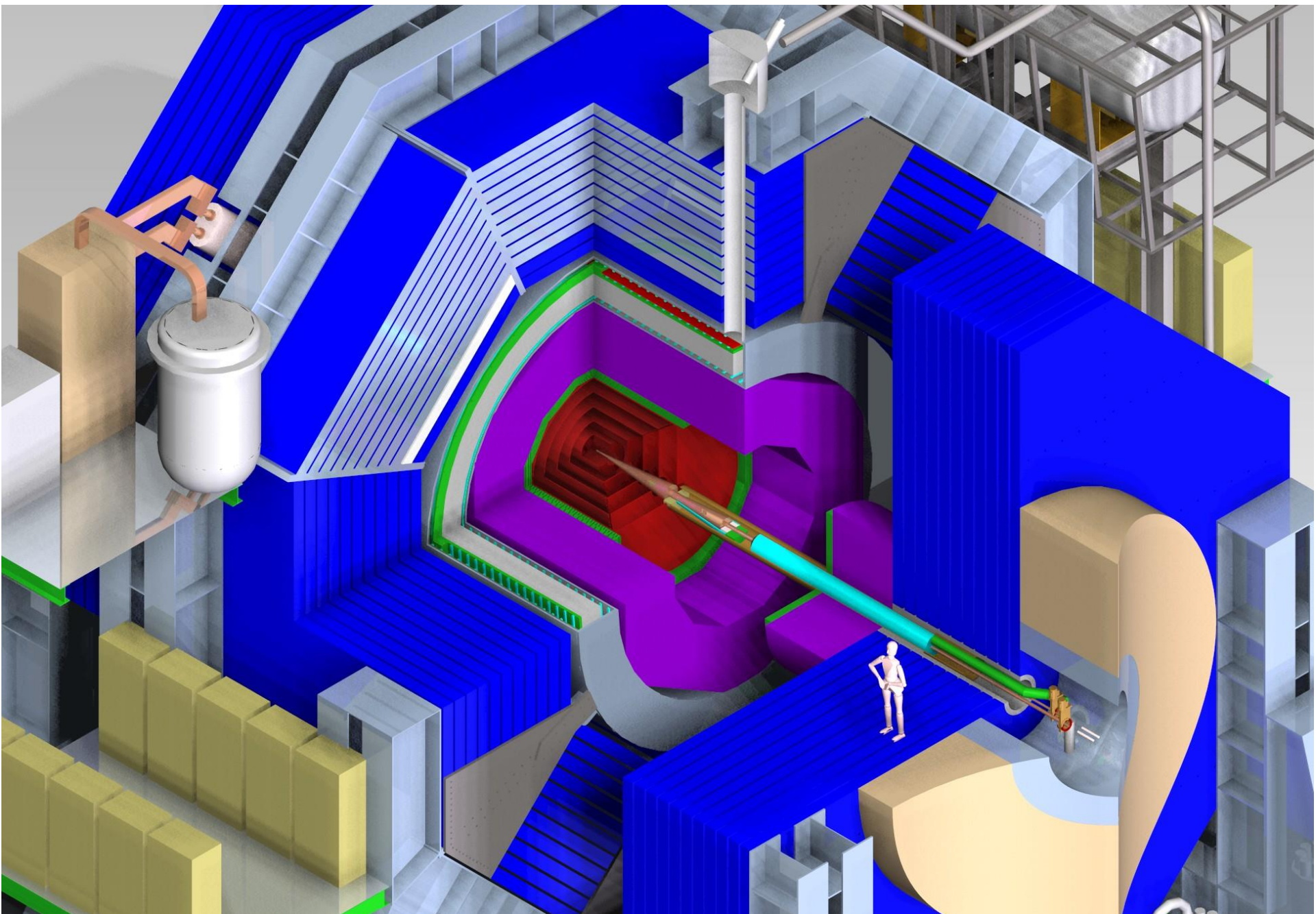
Plan-B: Layout of cryogenic equipment



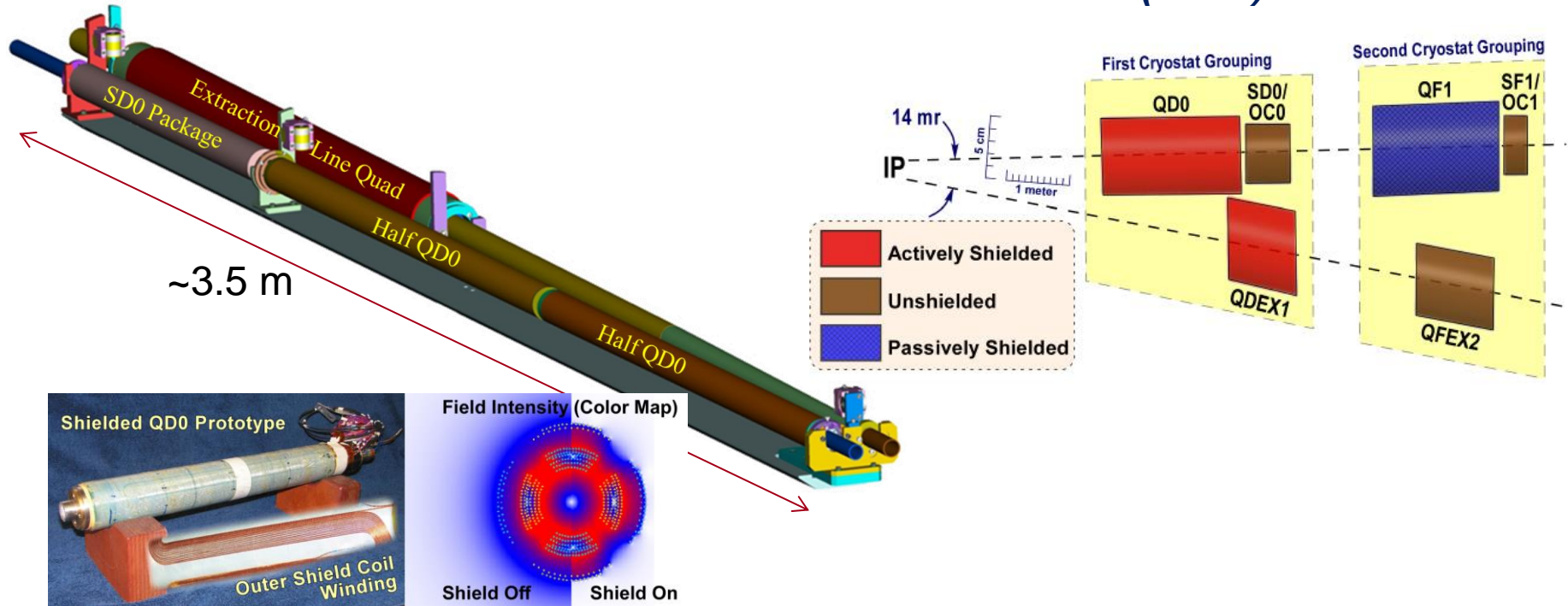
Push-Pull : Engineering Concept



LHe refrigerator and LHe2 for the QD0's above level on metallic structure.

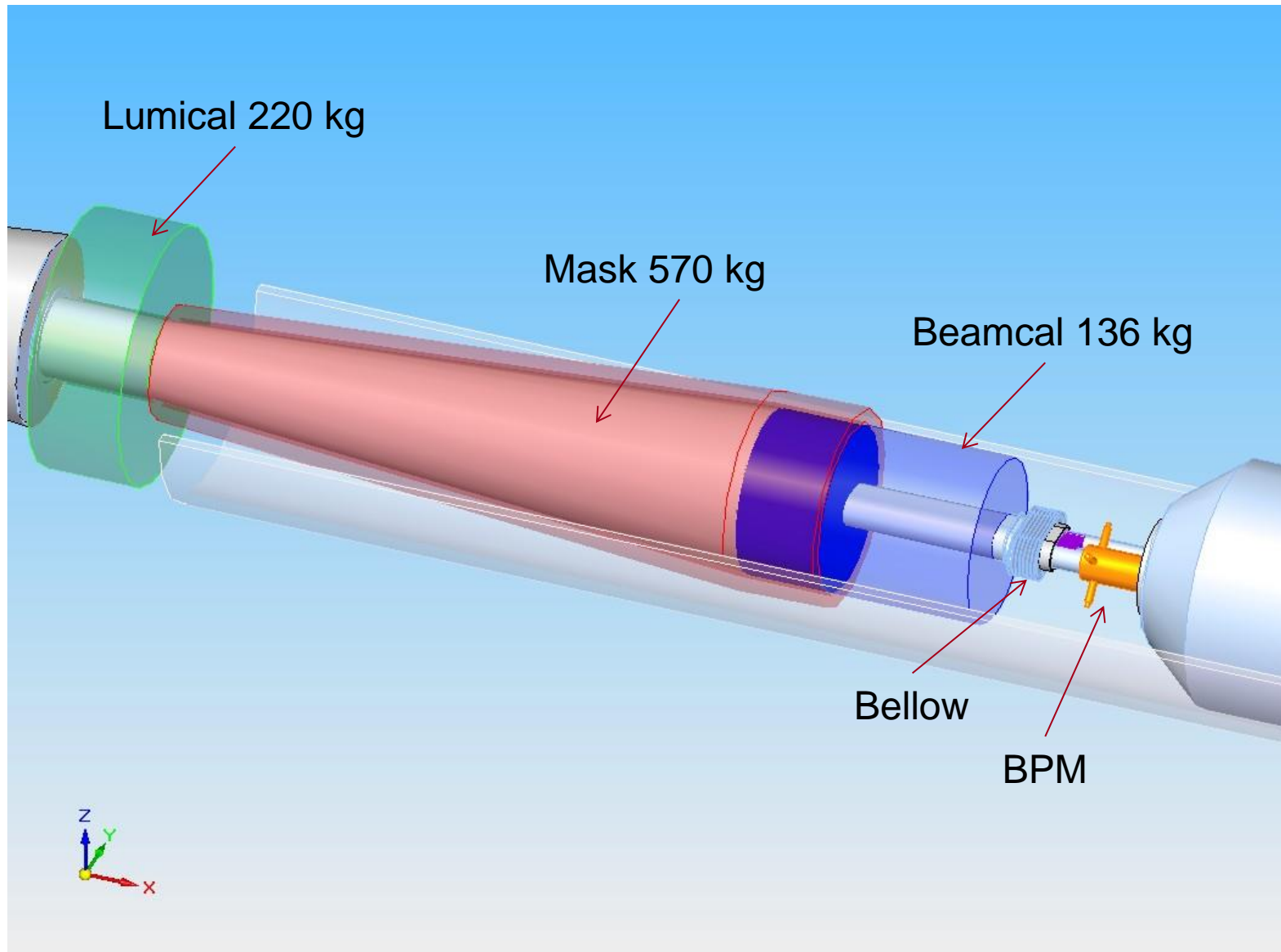


ILC QD0 : Cold Mass 2K Helium (BNL)



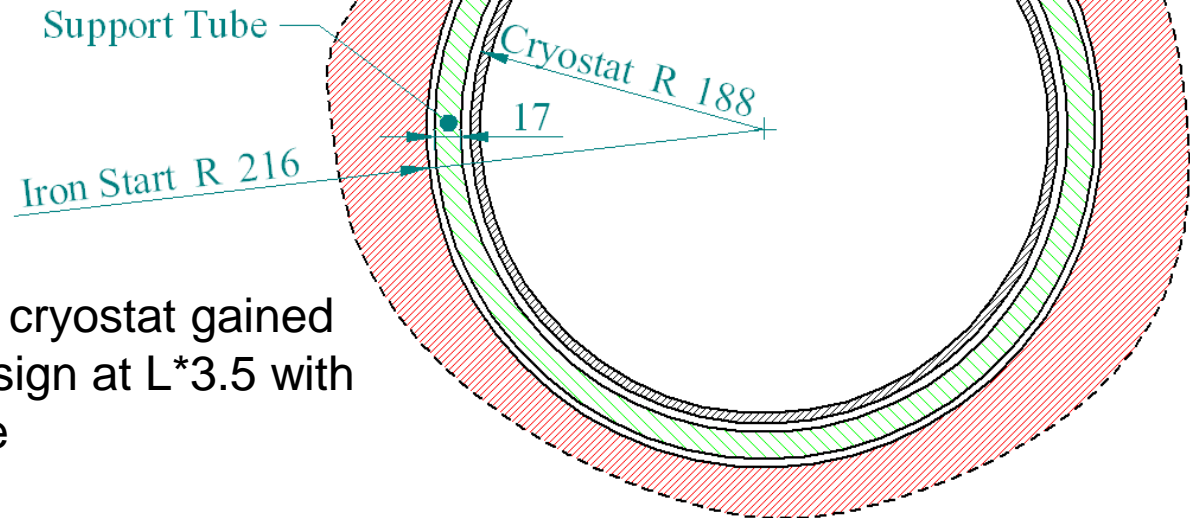
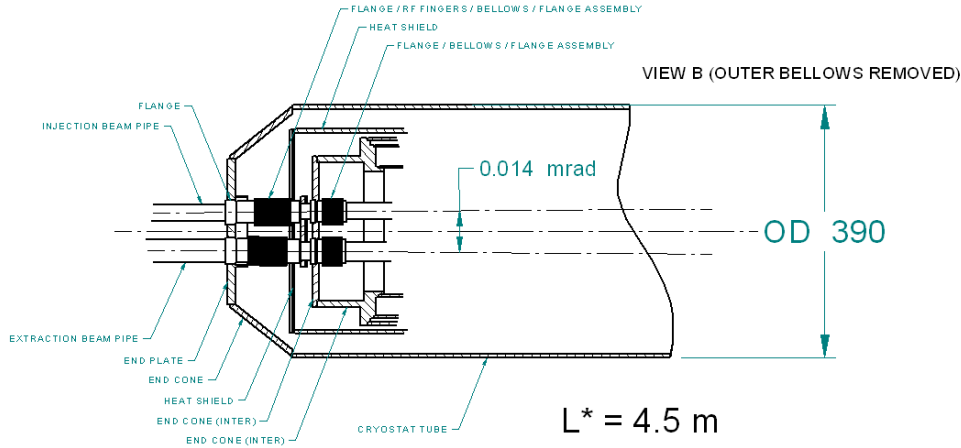
- Technology of the superconducting final focus magnets has been demonstrated by a series of short prototype multi-pole coils.
- QD0 magnet split into two coils to allow higher flexibility at lower energies.
- The quadrupoles closest to the IP are actually inside the detector solenoid.
- Actively shielded coil to control magnetic cross talk
- Additional large aperture anti-solenoid in the endcap region to avoid luminosity loss due to beam optics effects.
 - Large aperture Detector Integrated Dipole (DID) used to reduce detector background at high beam energies or to minimize orbit deflections at low beam energies.

SID Forward Region



Space Requirements

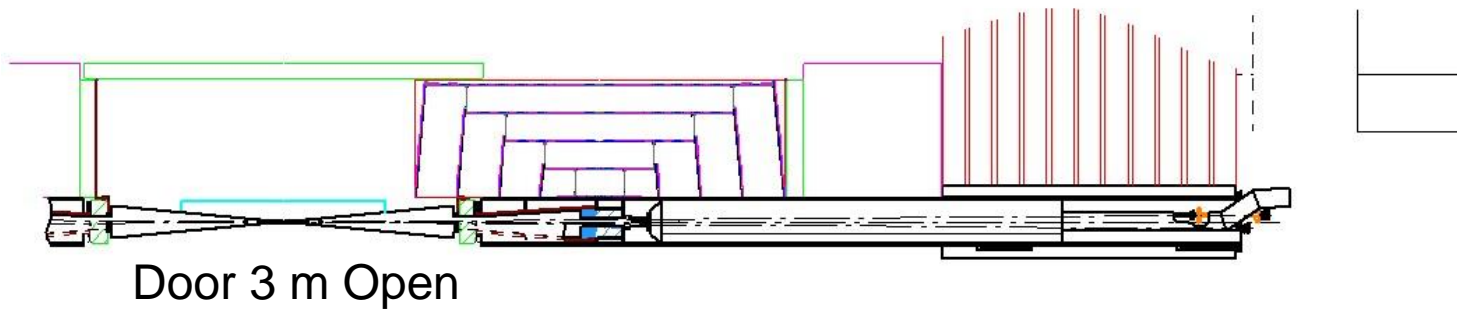
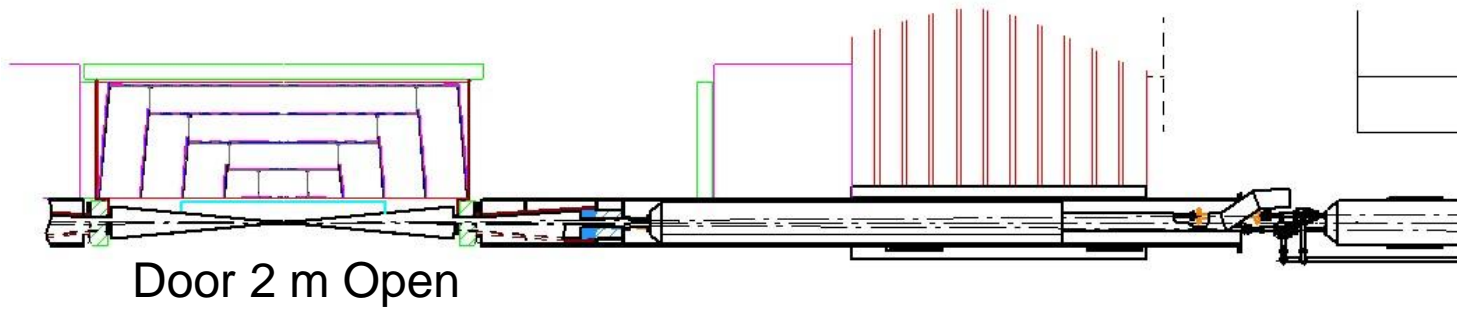
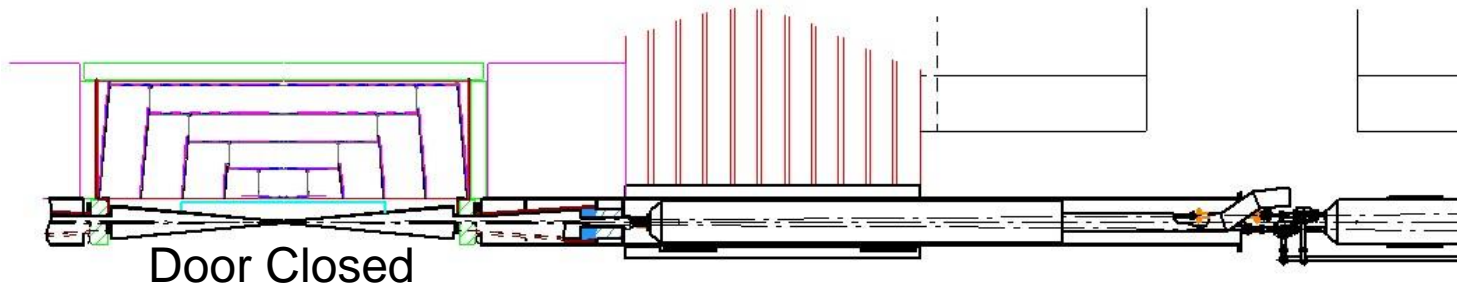
Current QD0 Prototype is designed for $L^* 4.5 \text{ m}$



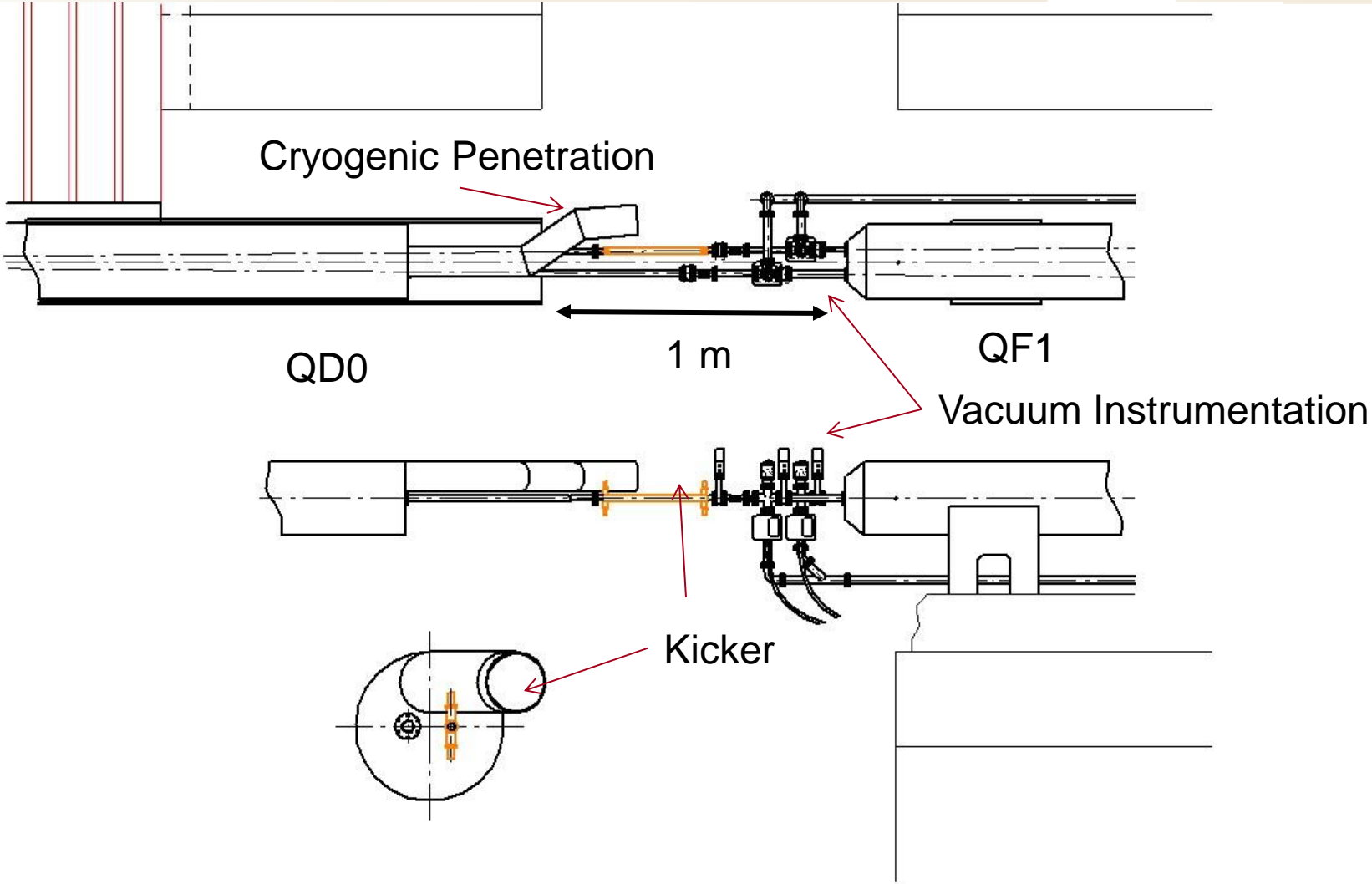
14 mm reduction of the QD0 cryostat gained moving the present QD0 design at $L^* 3.5$ with the 14mrad crossing scheme
(1 m x 14 mrad = 14 mm)

$L^* 3.5 \text{ m}$ cross section

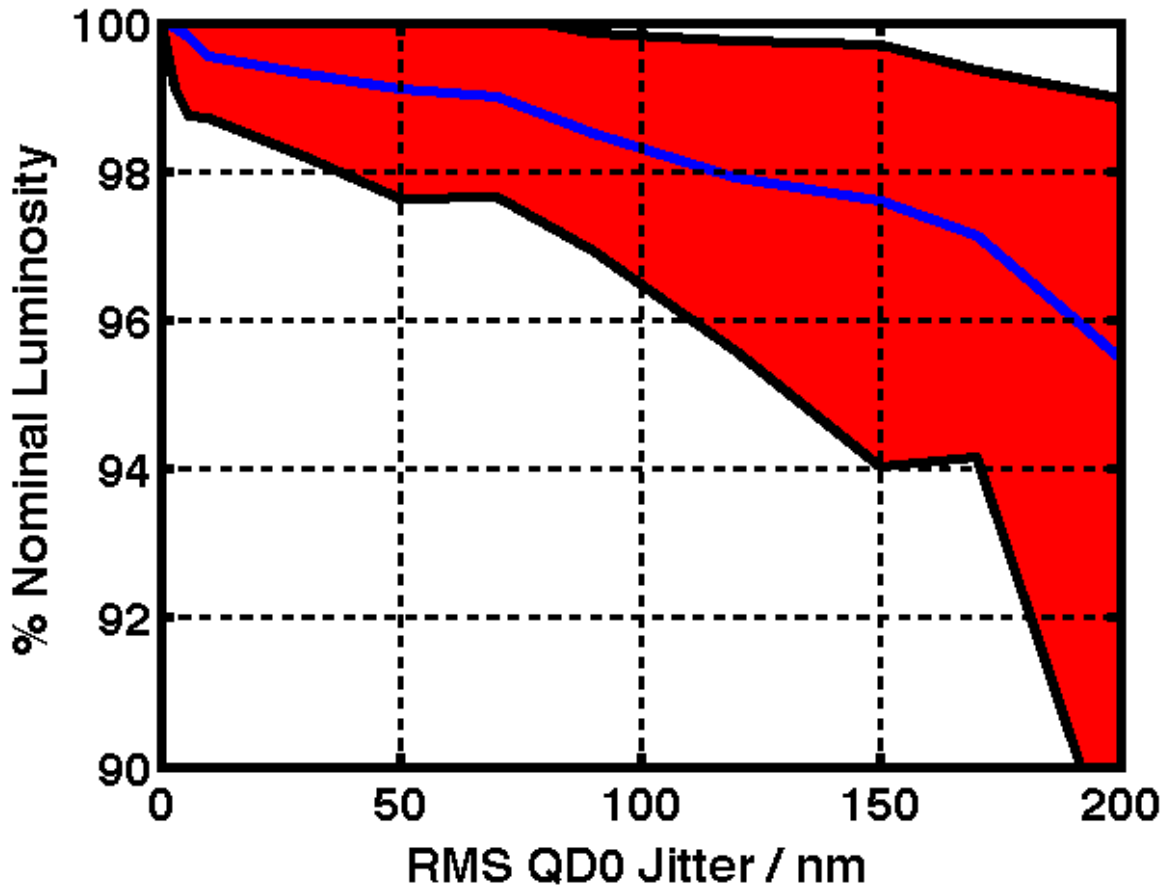
Forward Region Diameter – Tracker maintenance



Interface QD0-QF1: Critical for Fast&Reliable Push-Pulls



Luminosity Loss vs. QD0 Jitter

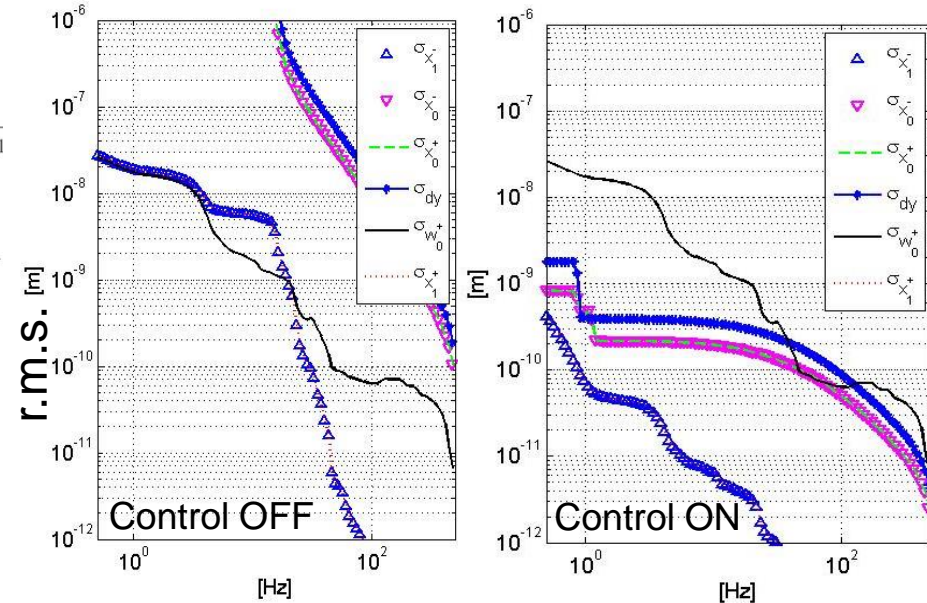
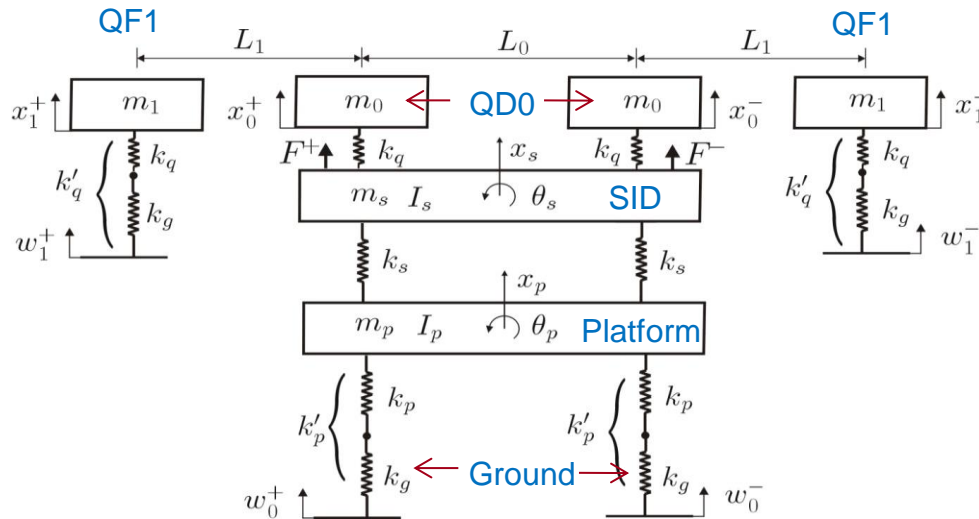


Data shown gives % nominal luminosity for different levels of uncorrelated QD0 jitter.

- 100 pulses simulated per jitter cases with FFB
- Mean, 10% & 90% CL results shown for each jitter point from 100 pulse simulations

Tolerance to keep luminosity loss <1% is <50nm RMS QD0 jitter.

Vibration Study (C.Collette, D.Thsilumba,ULB)



1. Ground Motions measured at the SLD detector hall
2. Conservative spectrum of the technical noise on the detector.
3. The model predicts that the maximum level of *r.m.s.* vibration seen by QDO is well below the capture range of the IP feedback system available in the ILC. With the addition of an active stabilization system on QDO, it is also possible to achieve the stability requirements of CLIC.
4. Experimental measurements of the technical noise instrumenting CMS during LS1 with permanent vibration sensors

Summary

Many of the requirements of the MDI and the Detector Engineering are well established, but a vigorous Engineering effort needs to be deployed to spec them out.

Additional R&D is required on few cases.

The limiting factor at this stage is the Manpower (Engineers and Draftsmen) required to spec out the requirements in a consistent engineering design. It is not an SID specific problem.

The choice of a site (Kitakami) eliminates some options, although is not a game changer at this stage since the Engineering Design is still very conceptual.

EXTRA SLIDES

SID key design features

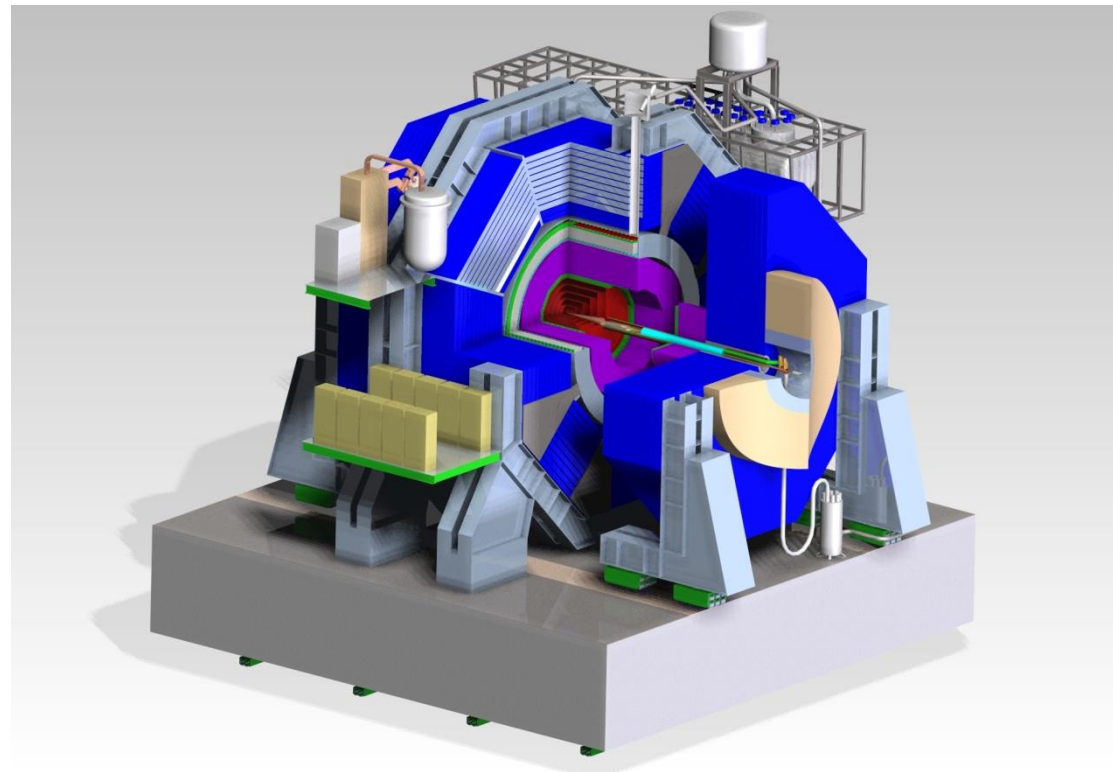
Compact design with 5 T Solenoid

Single Ring Barrel ~ 4'000 tons

Self Shielded: Stray Fields & Radiation

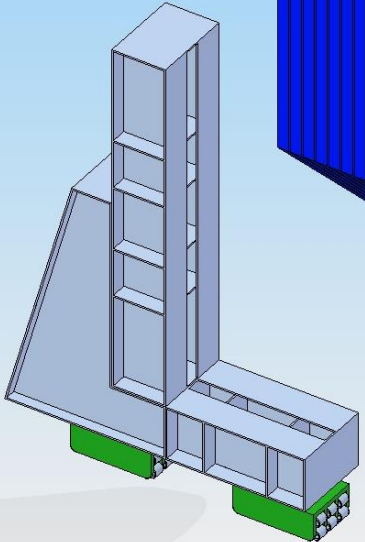
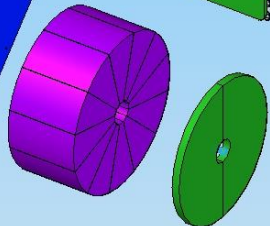
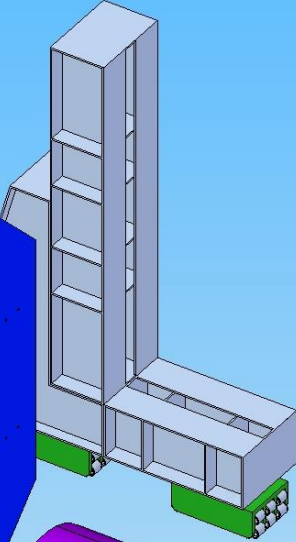
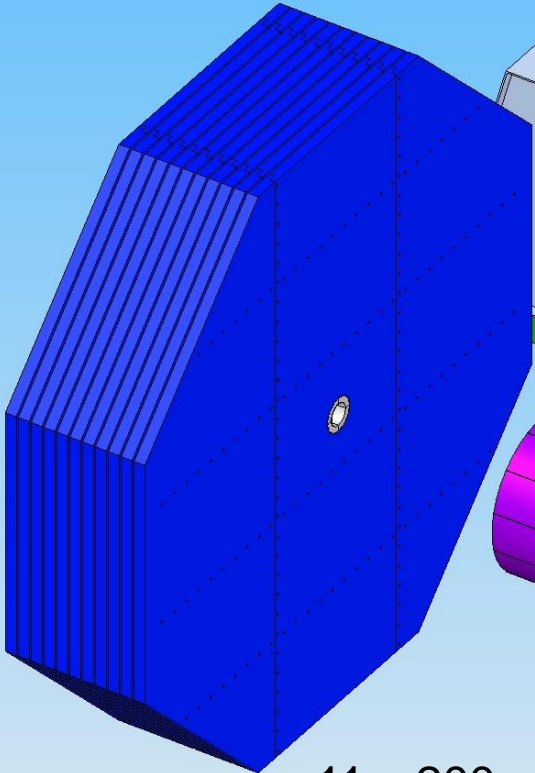
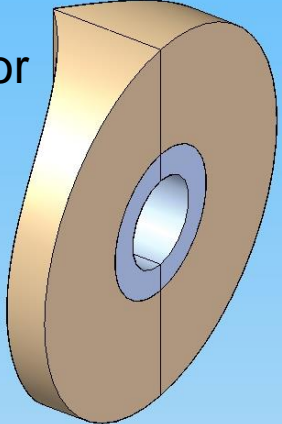
Short L^* with QD0's supported from the doors

Barrel Ecal	60
Barrel Hcal	450
Coil	192
Barrel Iron	3287
Total Barrel	3990
Endcap Ecal	10
Endcap Hcal	38
Endcap Iron	2100
Pacman	100
Feet	60
BDS	5
Total Door (x1)	2313
Total SiD	8615



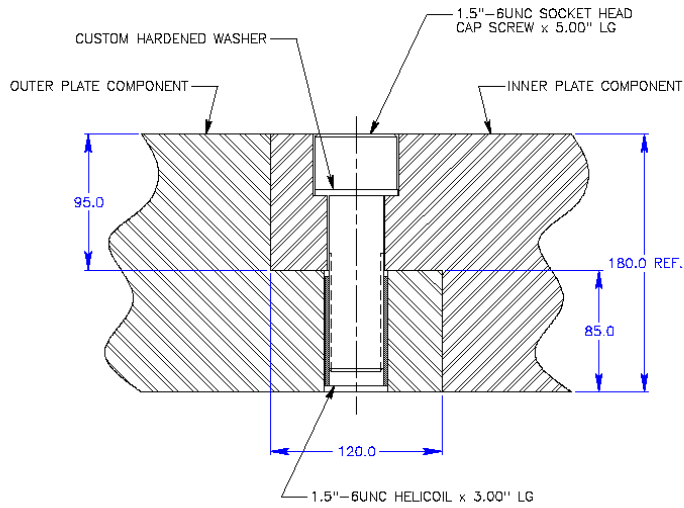
End Door

Pacman
on the door

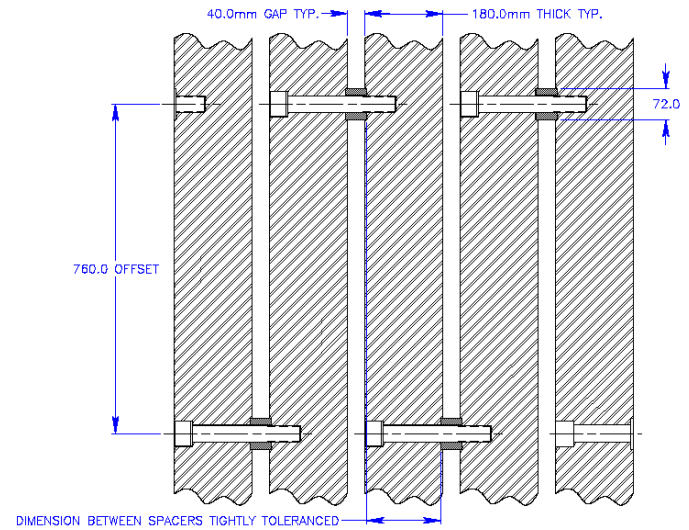


11 x 200mm Iron plates
40mm gap

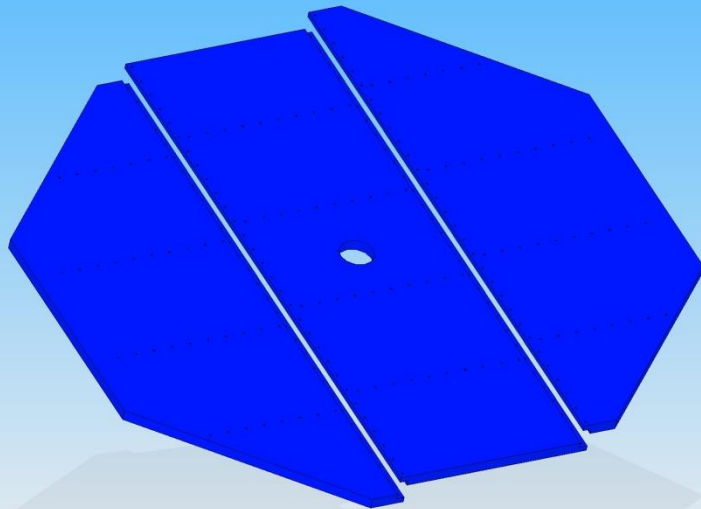
Total Mass ~ 2'300 Tons



Intraplate connections

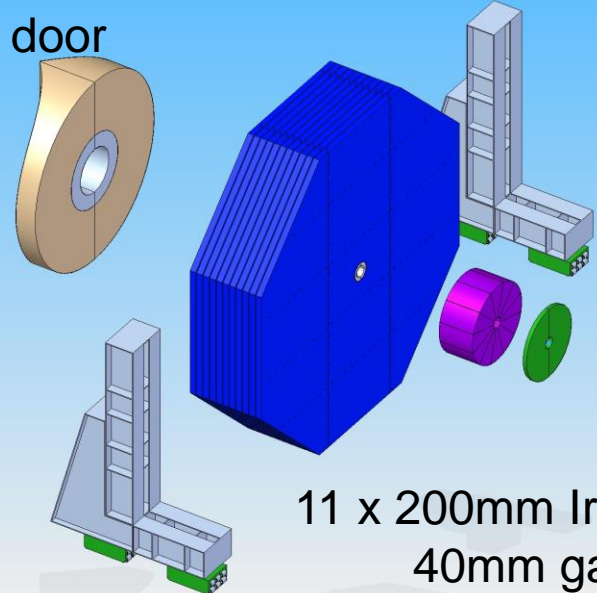


Spacer Offset



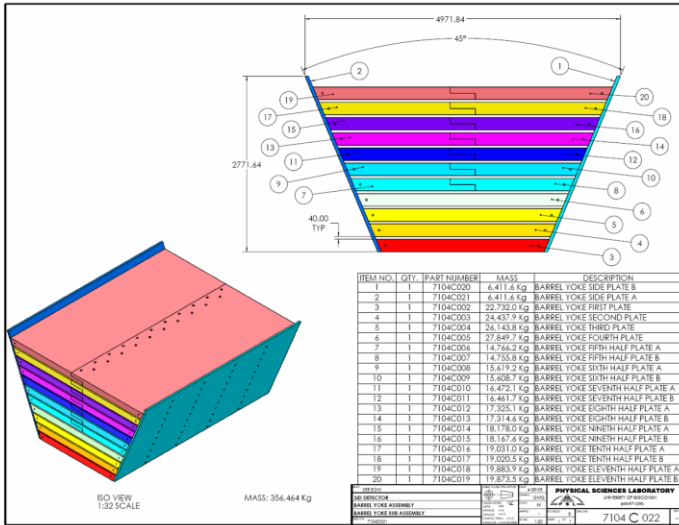
Pacman
on the door

Total Mass ~ 2'300 Tons



11 x 200mm Iron plates
40mm gap

Iron Barrel Yoke layout

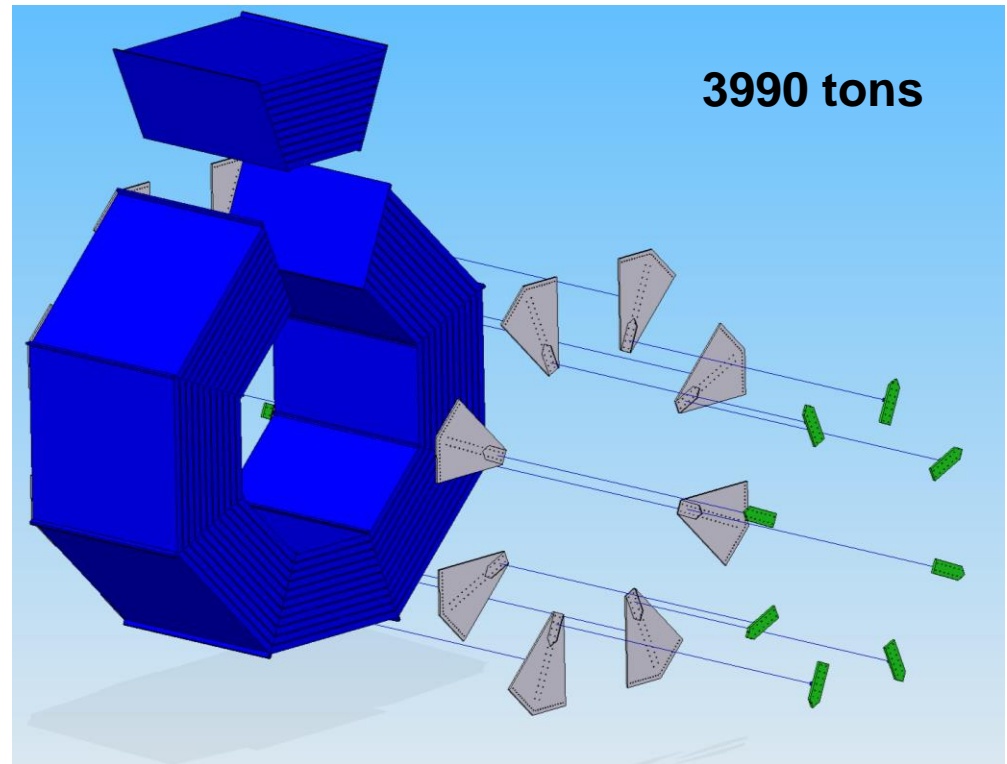
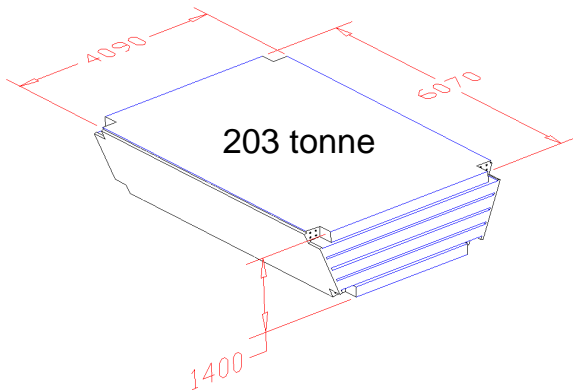


Bolted assembly, 144 plates 200 mm thick, 40mm gap
 Opportunity to make blank assembly at the factory before shipping
 Preliminary Contacts with Kawasaki Heavy Industries

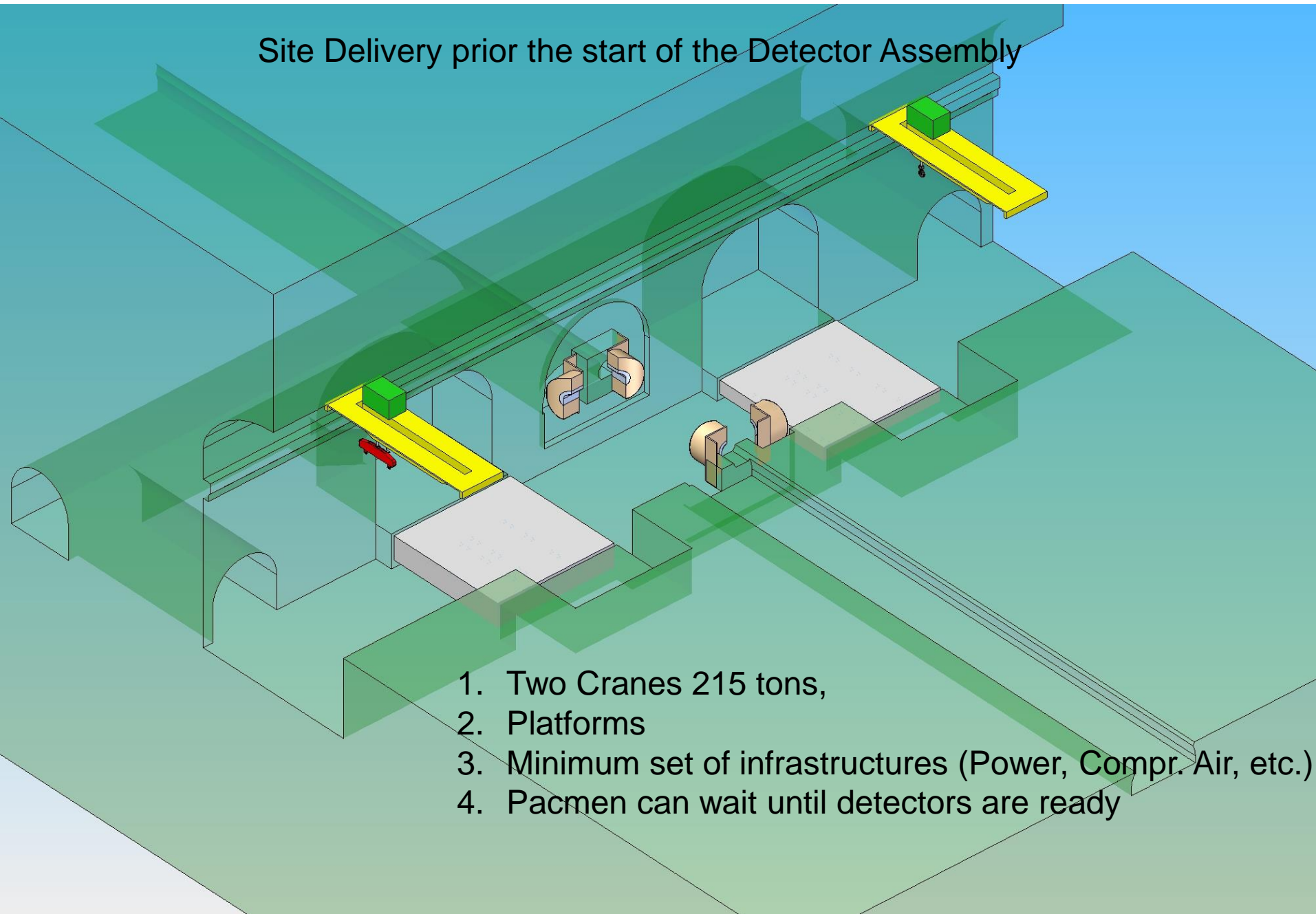
- Plate thickness tolerance for each: 0.1mm
- Plate flatness: 4mm (in a plate)
- Fabrication (assembling & welding) tolerance: 2mm
- Full trial assembly: capable (but need to study)

211 tonne

Max. Crane capacity 215 Tons

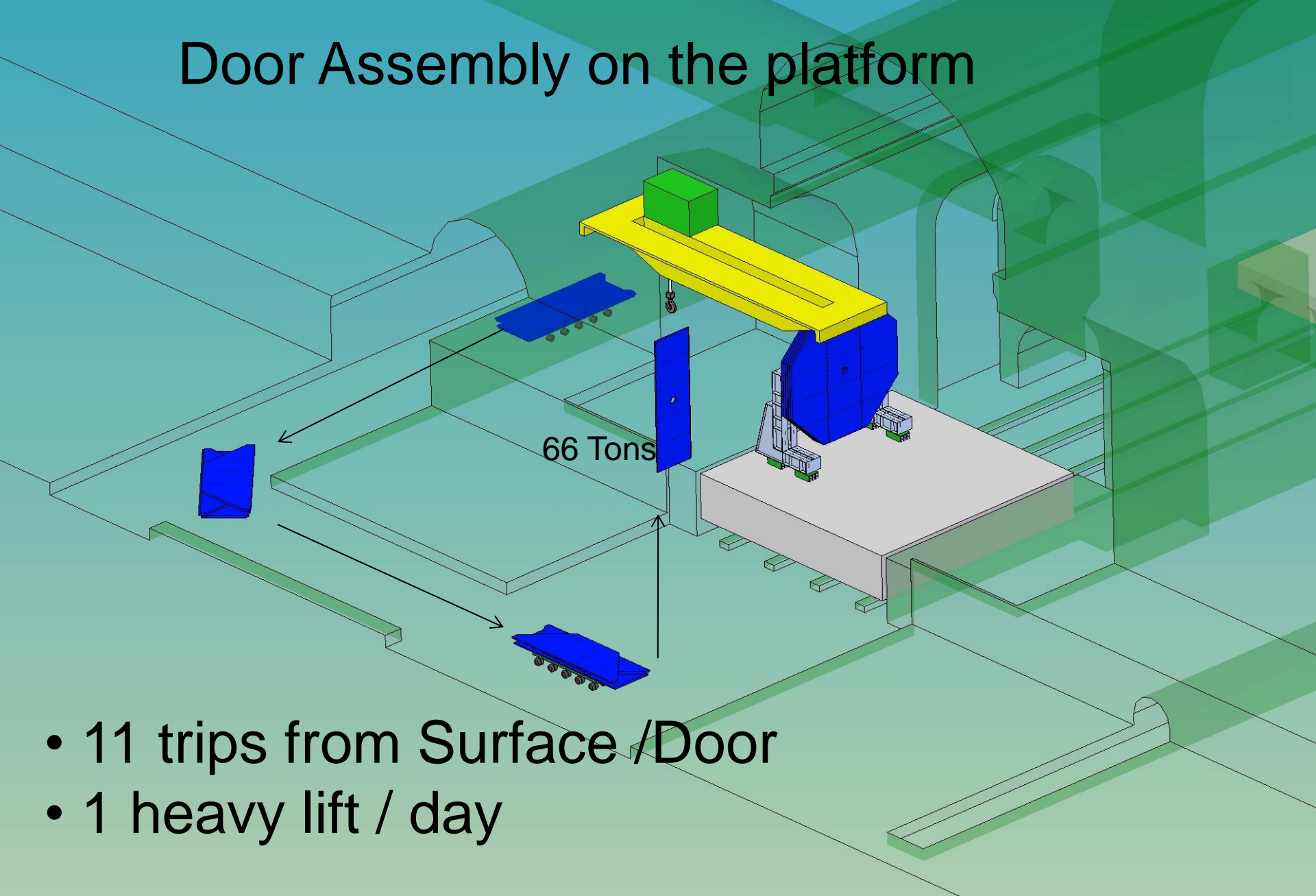


Site Delivery prior the start of the Detector Assembly

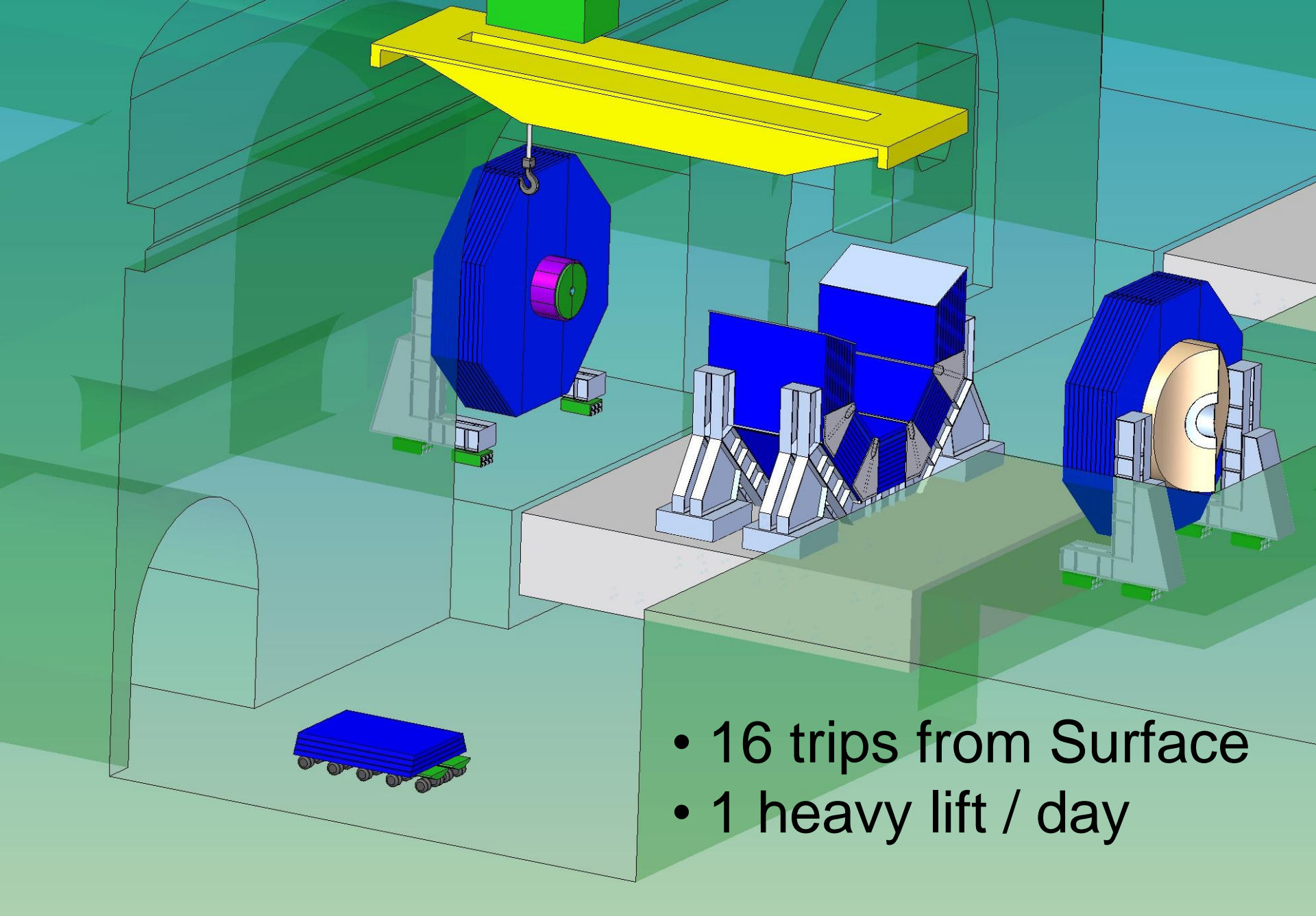


1. Two Cranes 215 tons,
2. Platforms
3. Minimum set of infrastructures (Power, Compr. Air, etc.)
4. Pacmen can wait until detectors are ready

Door Assembly on the platform

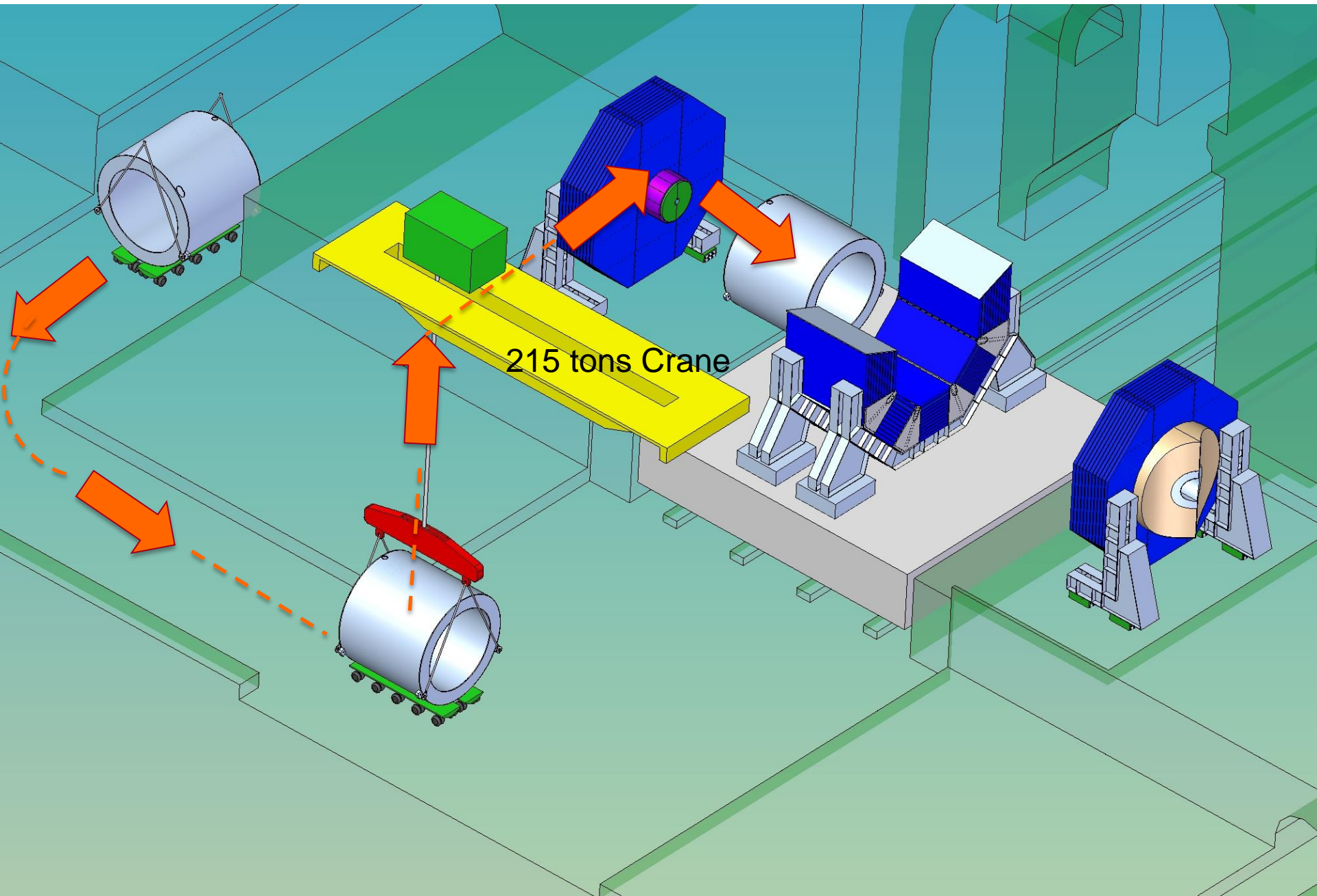


- 11 trips from Surface /Door
- 1 heavy lift / day

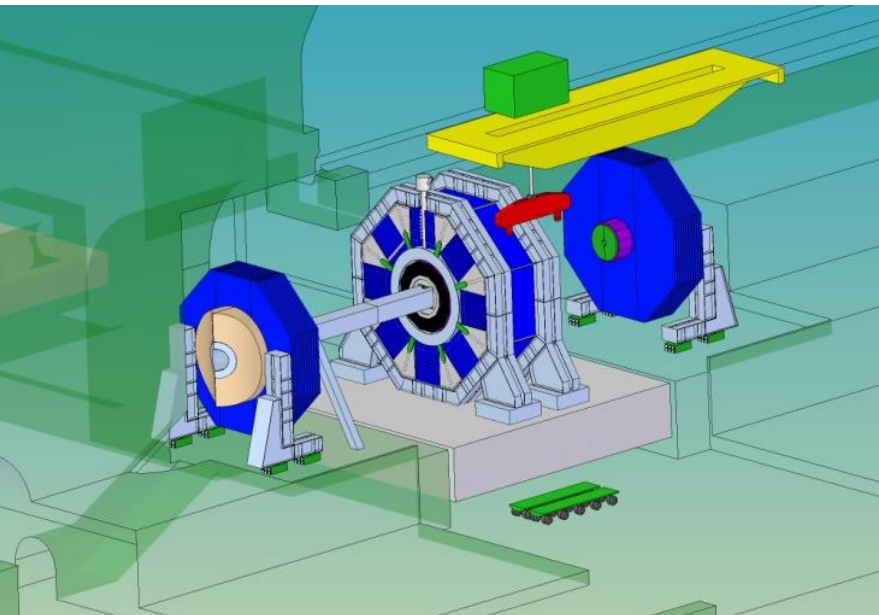
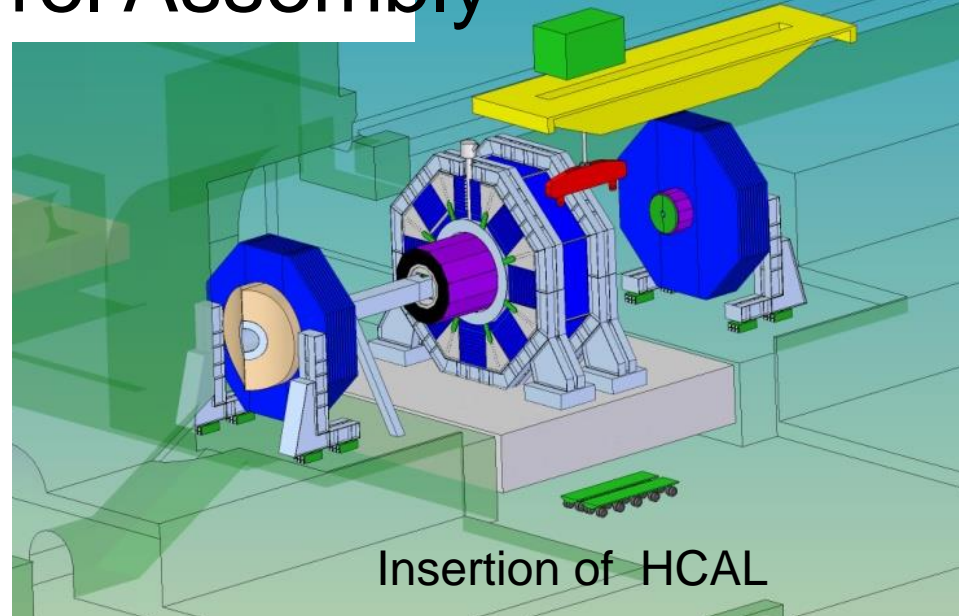
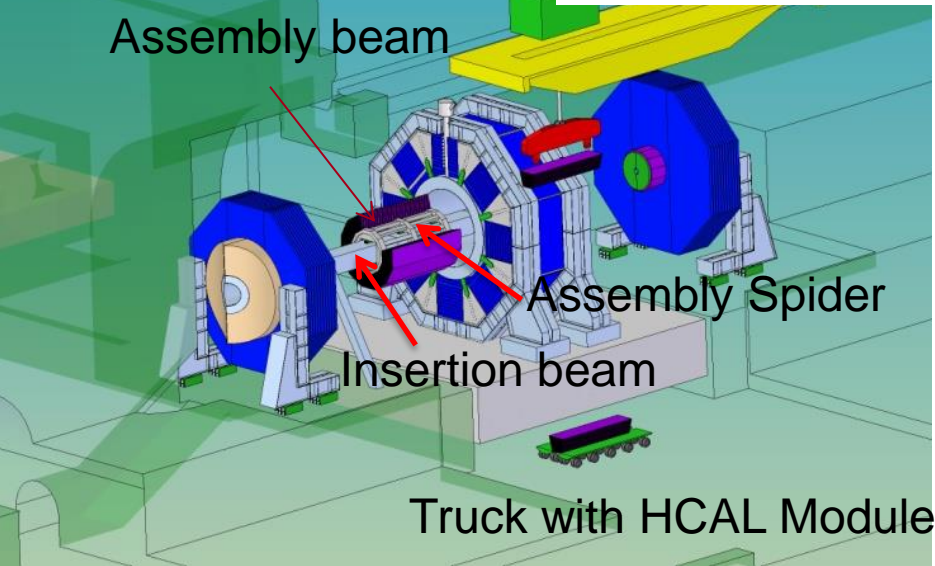


- 16 trips from Surface
- 1 heavy lift / day

Solenoid Installation



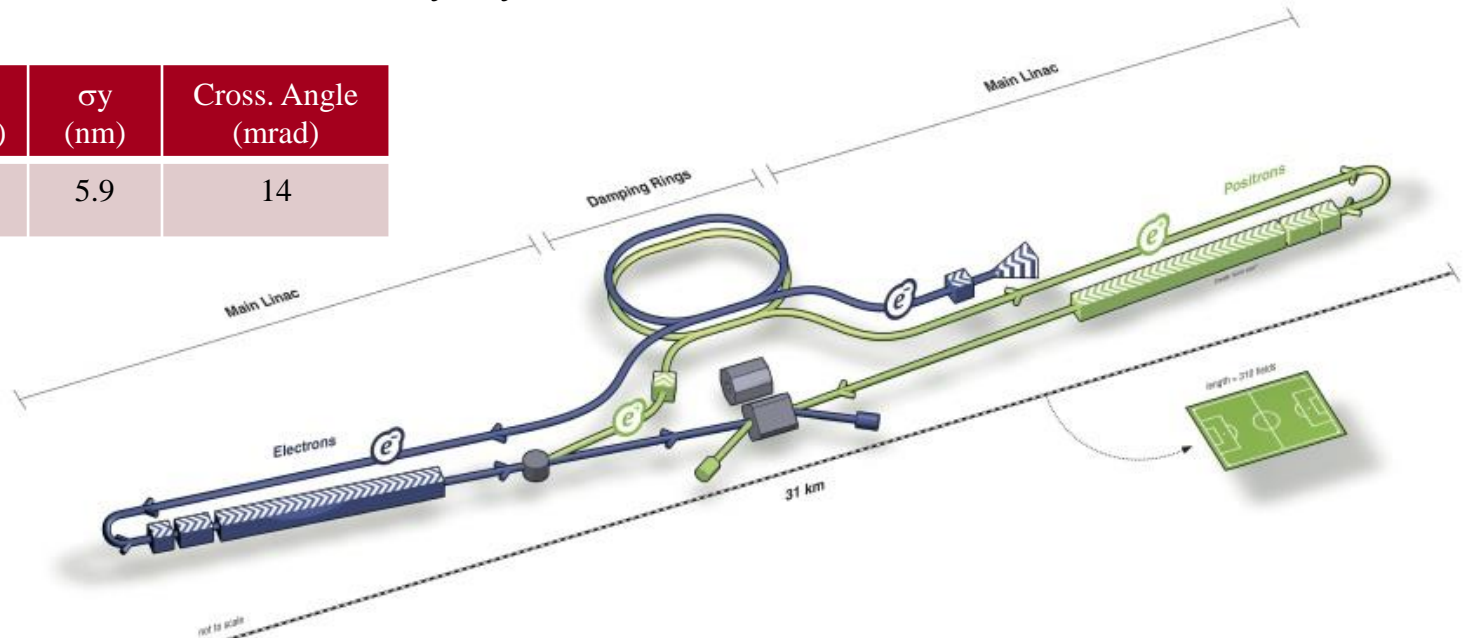
HCAL Barrel Assembly



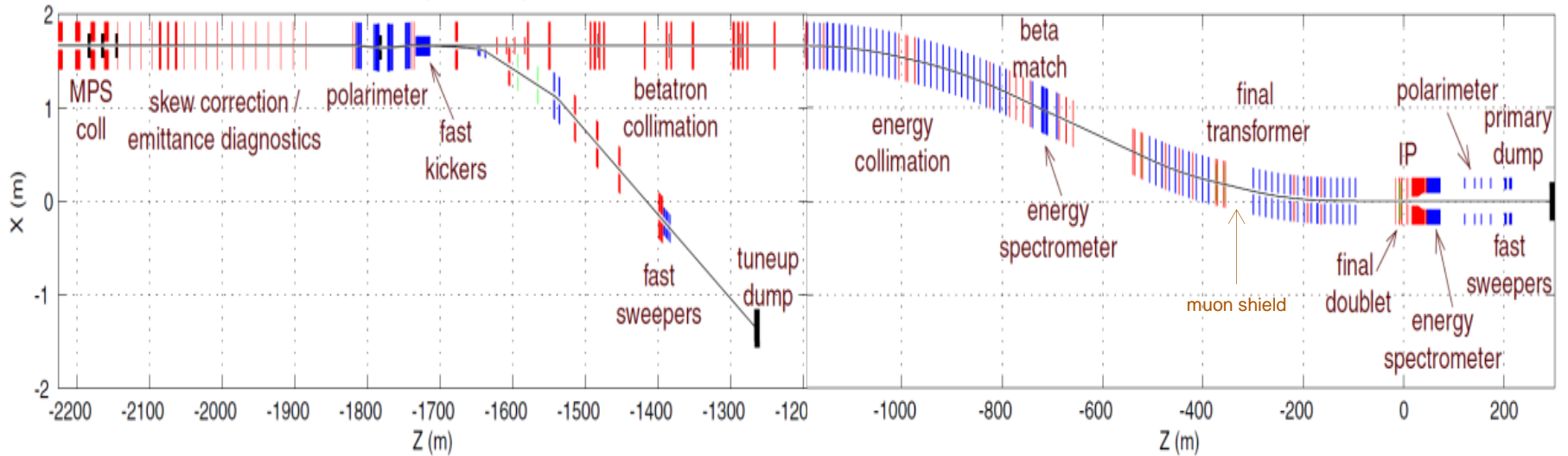
SLD, Liquid Argon Calorimeter
Assembly Beam

Beam Delivery System, ILC 500 GeV cm

IP Beam Parameter	σ_x (nm)	σ_y (nm)	Cross. Angle (mrad)
ILC 500 GeV _{cm}	474	5.9	14



ILC e- BDS (500 GeV cm)

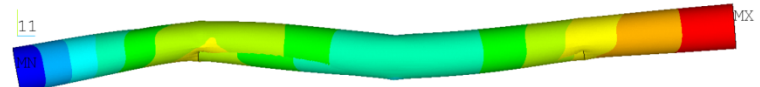


ILC BDS, ± 2.2 km

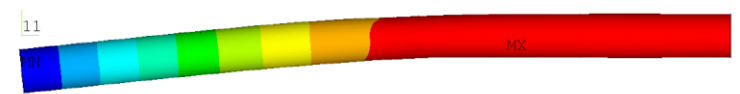
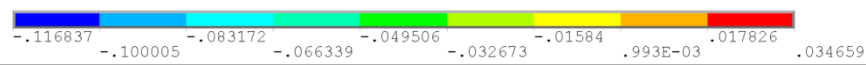
Displacements (mm)

NODAL SOLUTION
 STEP=1
 SUB =1
 TIME=1
 UY (AVG)
 RSYS=0
 DMX =.116897
 SMN =-.116837
 SMX =.034659

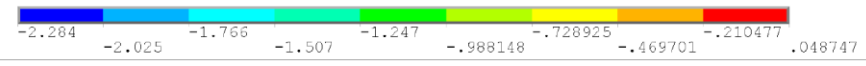
TIME=1
 UY (AVG)
 RSYS=0
 DMX =2.286
 SMN =-2.284
 SMX =.048747



Door Closed, Max sag = 0.1 mm

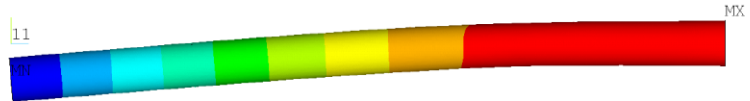


Door Open 2 m, Max sag = 2.3 mm

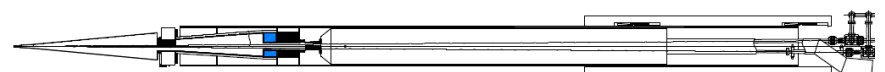
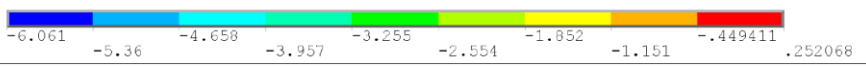


NODAL SOLUTION
 STEP=1
 SUB =1
 TIME=1
 UY (AVG)
 RSYS=0
 DMX =6.065
 SMN =-6.061
 SMX =.252068

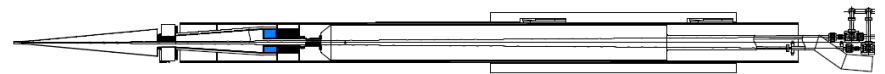
MAR 19 2012
 17:02:32



Door Open 3 m, Max sag = 6 mm



Door Open 3 m

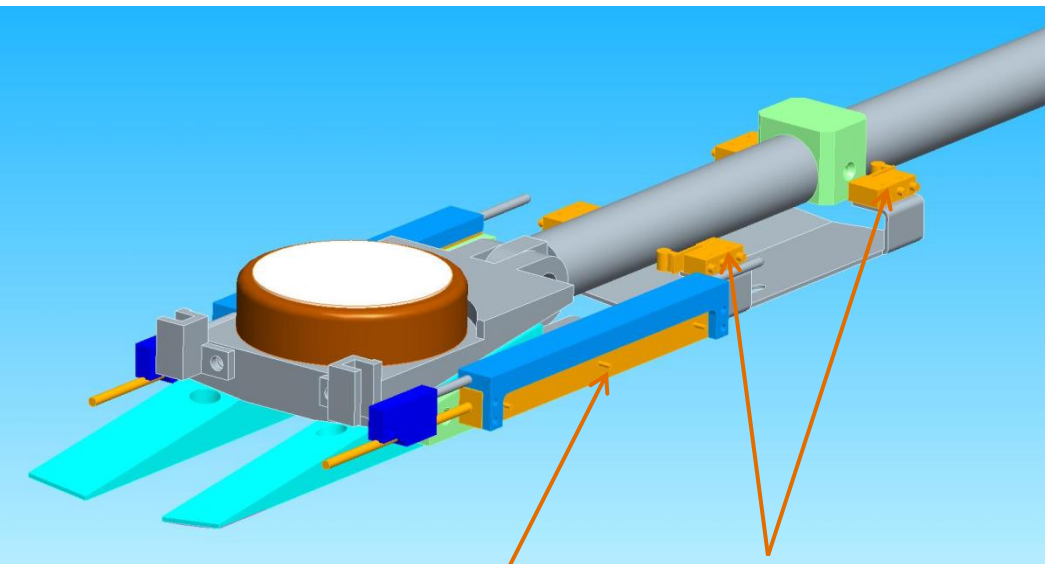
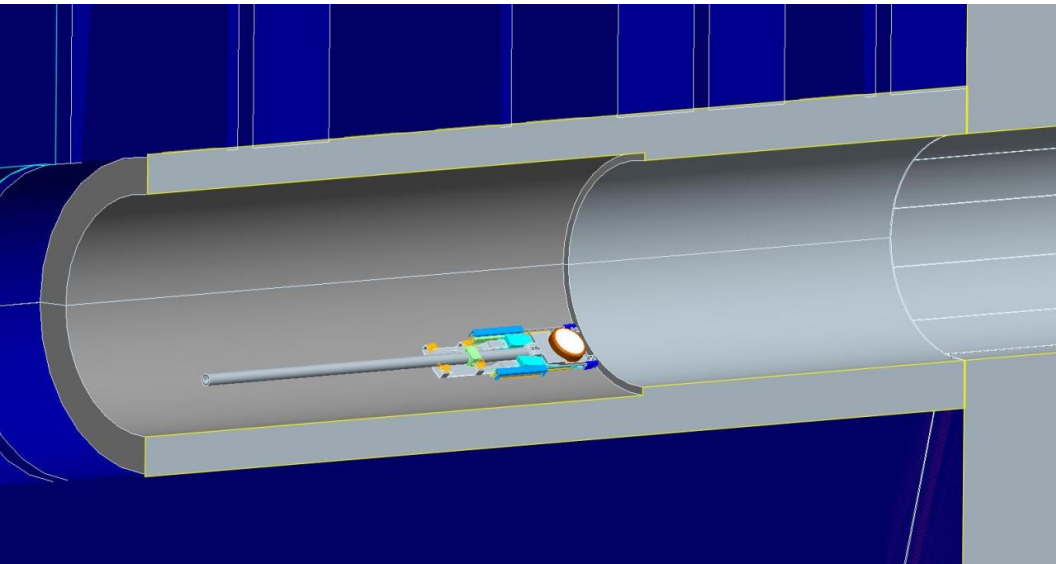


Door Open 2 m



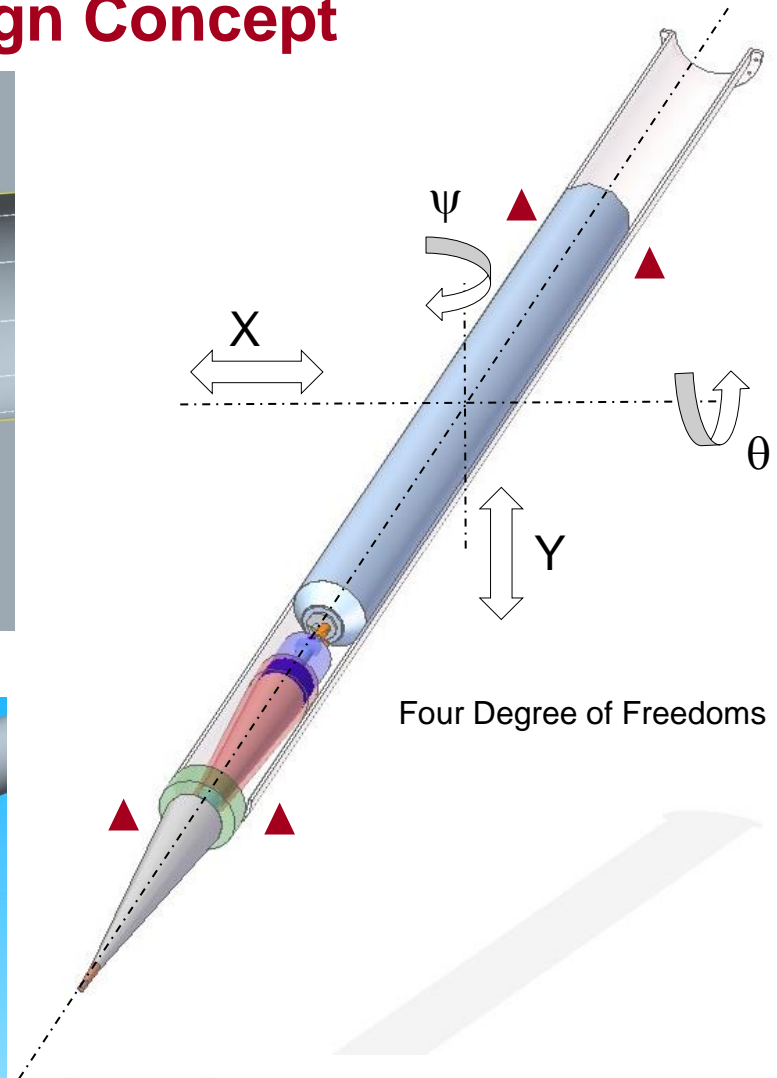
Door Closed

QD0 Wedge Design Concept



Potentiometer

Limit
Switches



Four Degree of Freedoms

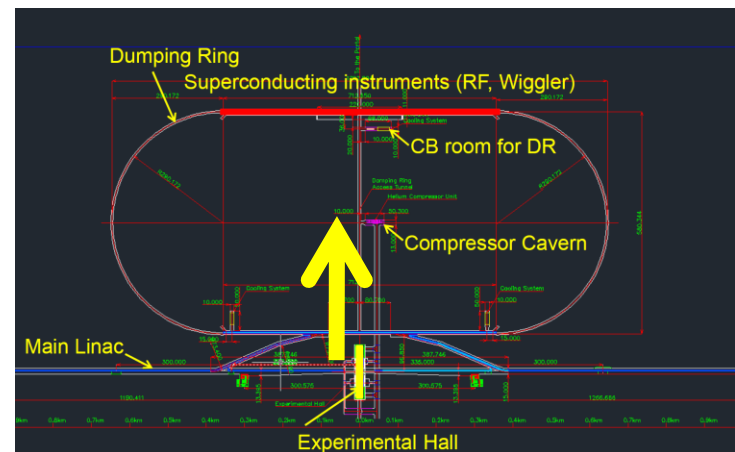
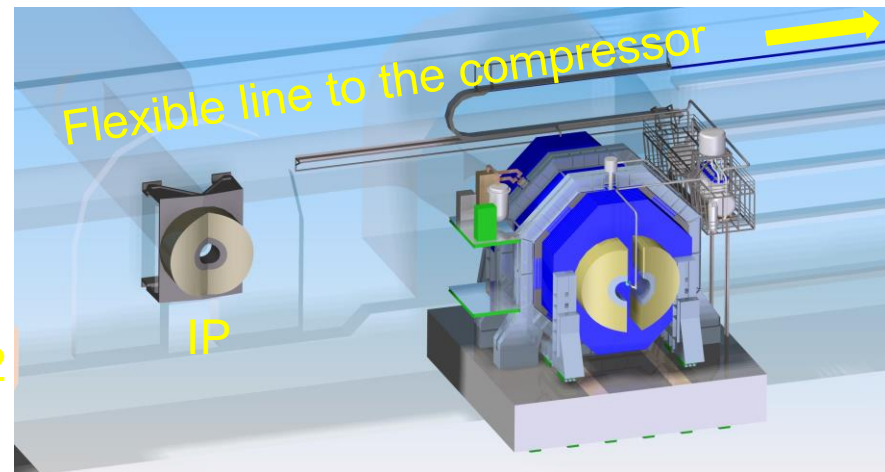
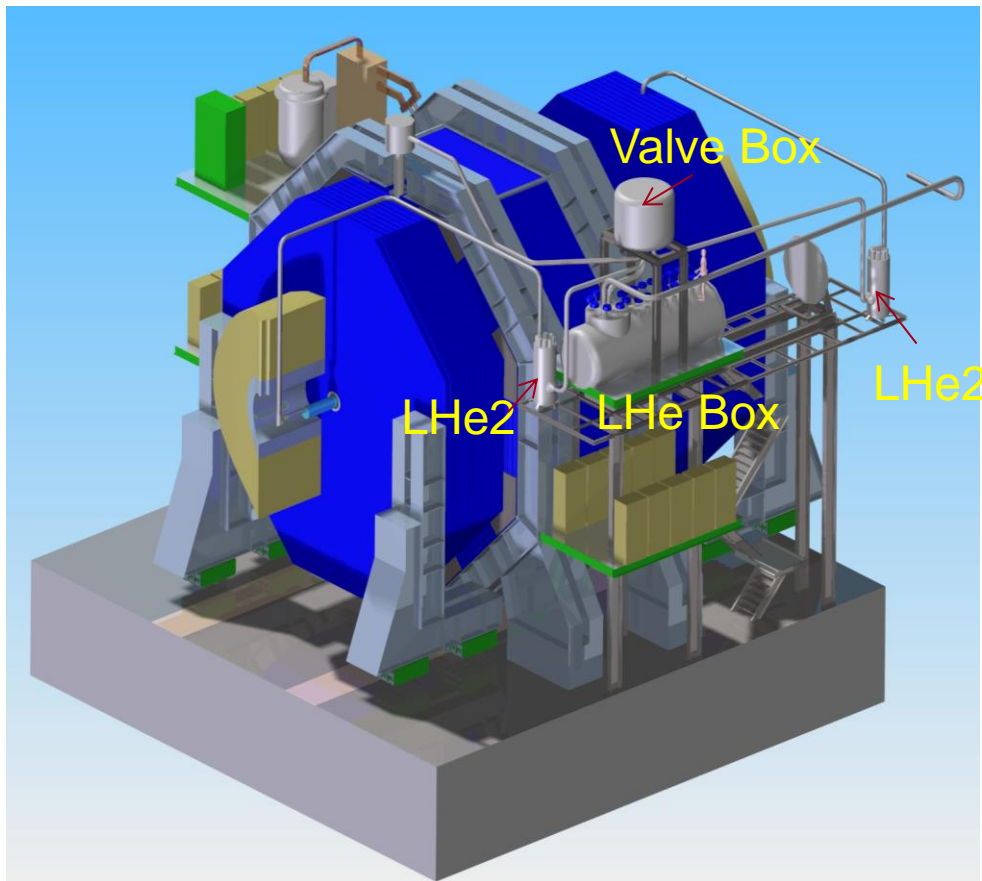
Total Pad Travel as is = .475in

Height of pad and distance of displacement will be changed pending analysis on sagging of beam line.

Conceptual design only at this point

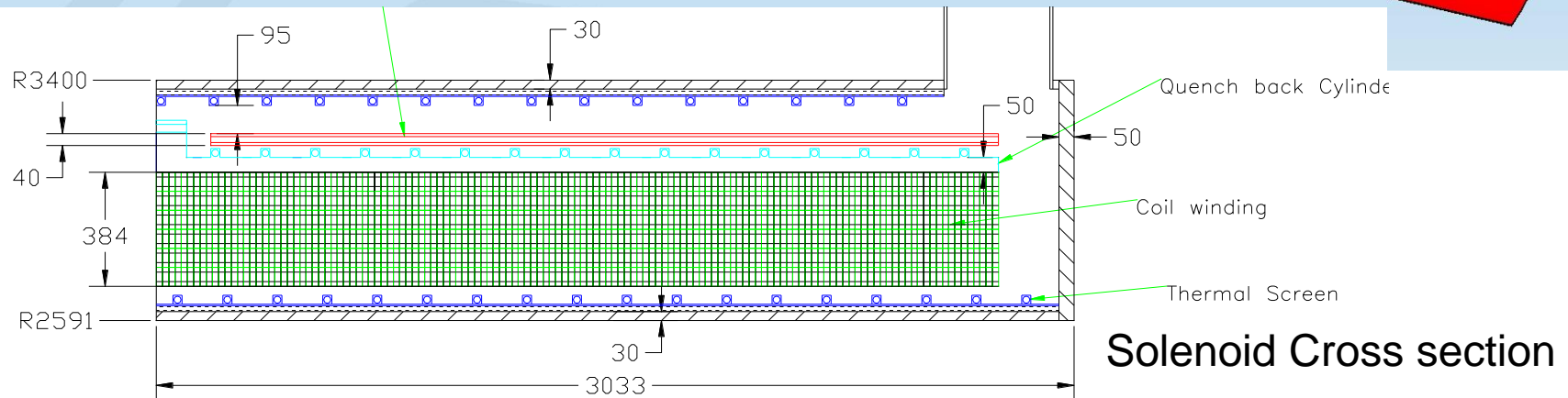
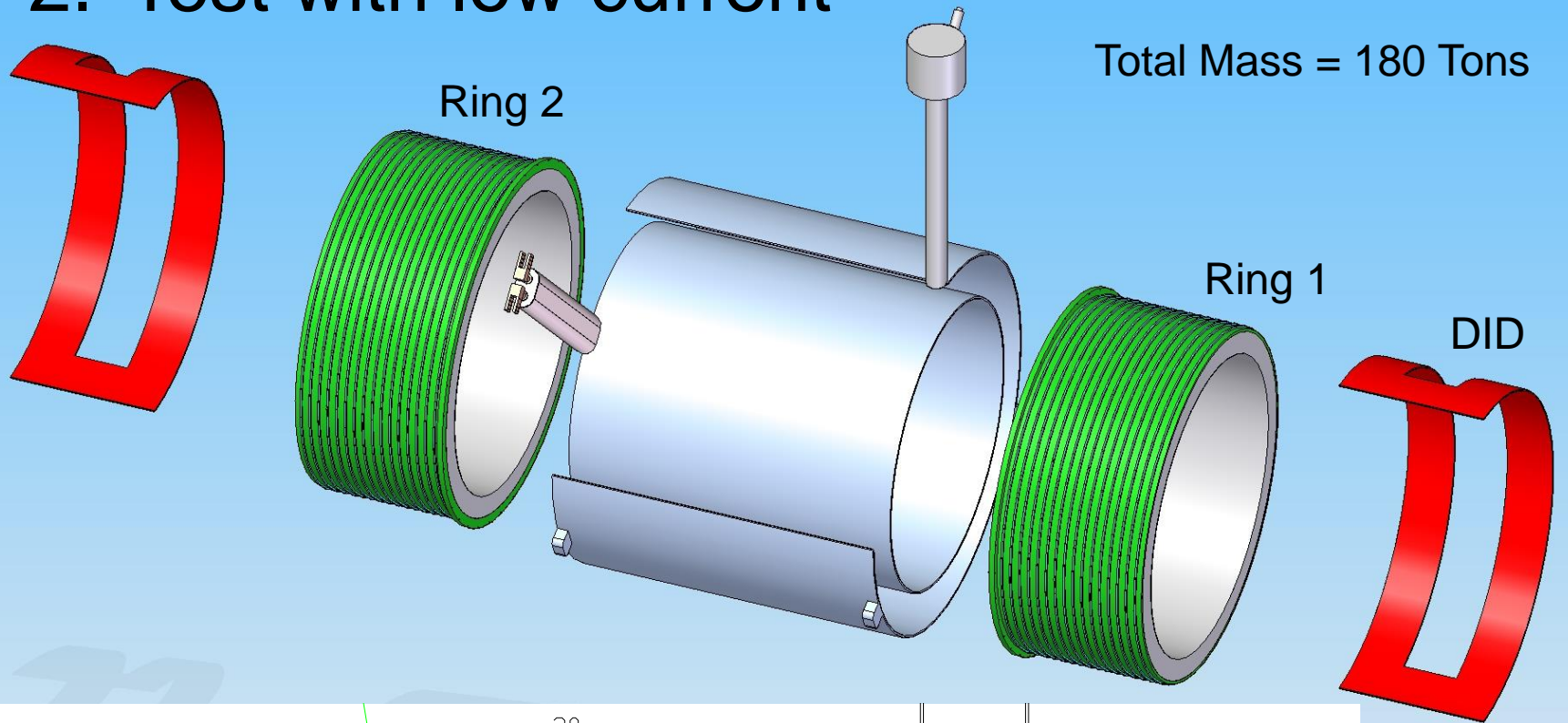
Integration of the Cryogenic plant on the platform

Main LHe refrigerator and LHe2 for the QD0's above level on metallic structure.

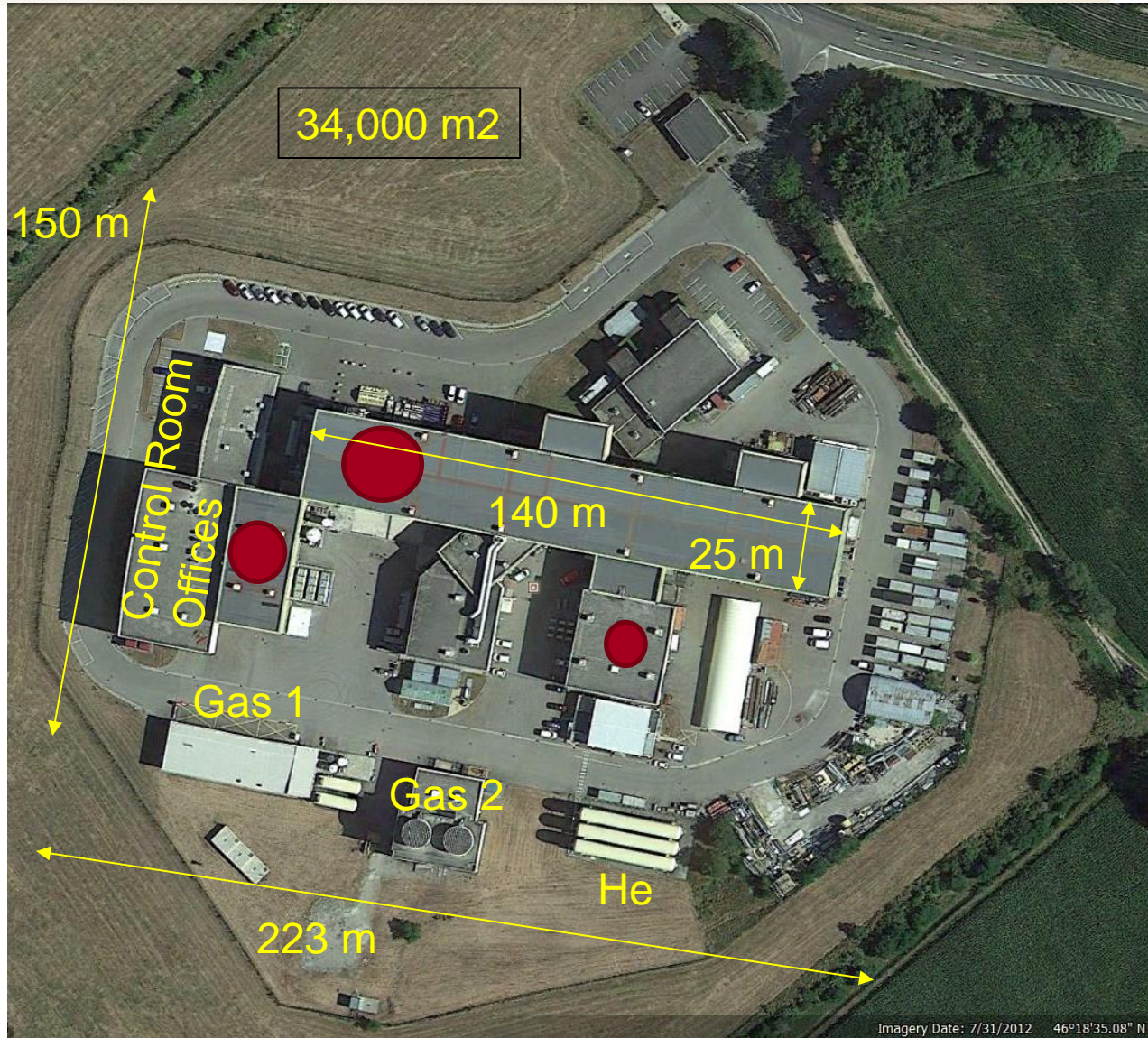


1. Assembly on Site (surface)

2. Test with low current



Assembly Yard - CMS



SPS beam extraction - North area (CERN)

