





## Impedance budget and effect of chamber coating on CLIC DR beam stability

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## Outline

- Introduction
- Highlights of the first results
- Experimental part
- Future planning

## Introduction (I) Damping Rings

CLIC	DR	parameters	

CLIC Dit parameters	
Parameters	CLIC@3TeV
Energy [GeV]	2.86
Circumference [m]	427.5
Energy loss/turn [MeV]	4.0
RF voltage [MV]	5.1
Stationary phase [°]	51
Momentum compaction factor	1.3e-4
Damping time x/s [ms]	2/1
Number of dipoles/wigglers	100/52
Dipole/wiggler field [T]	1.0/2.5
Rend gradient [1/m <sup>2</sup> ]	_1 1
Bunch population [ $10^9$ ]	4.1
Horizontal normalized emittance [nm.rad]	456
Vertical normalized emittance [nm.rad]	4.8
Bunch length [mm]	1.8
Longitudinal normalized emittance [keVm]	6.0

- Small emittance, short bunch length and high current
- Rise to collective effects which can degrade the beam quality

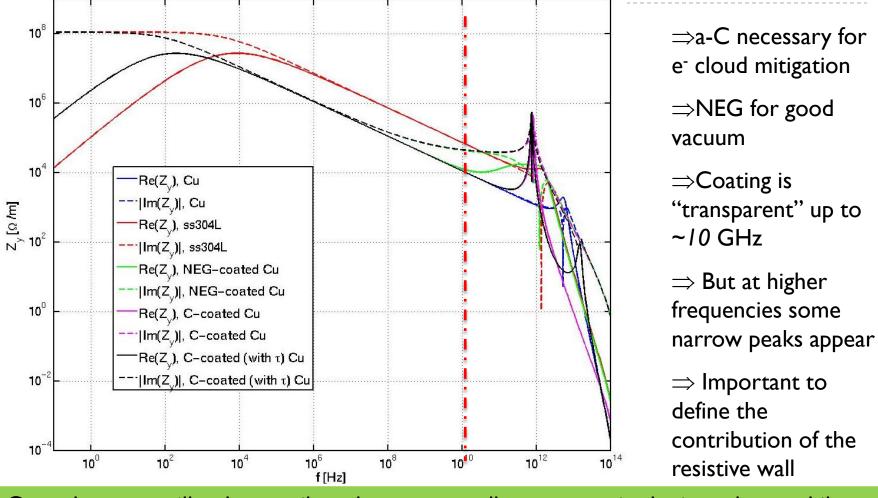
# Introduction (II) Collective effects

- Focus on instabilities driven by impedance
- Define the conditions to ensure safe operation under nominal conditions
- Define an impedance budget

#### To suppress some of the collective effects, coating will be used

- Positron Damping Ring (PDR): electron-cloud effects → amorphous carbon (aC)
- Electron Damping Ring (EDR): fast ion instabilities → need for ultra-low vacuum pressure → Non-Evaporable Getter (NEG)
- Only some of the scenarios are simulated so far...

## Resistive Wall Vertical Impedance: Various options for the wigglers pipe



Coated copper will only contribute by a very small percentage in the impedance while coated stainless steel will have a larger contribution

#### First results (I)

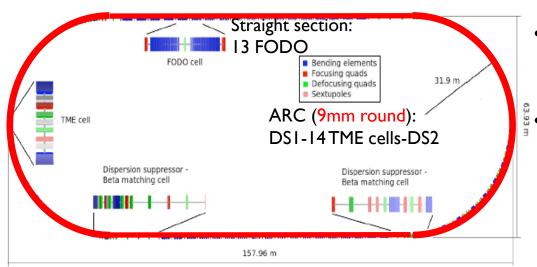
Single bunch simulations without space charge to define the instability thresholds

#### HEADTAIL code

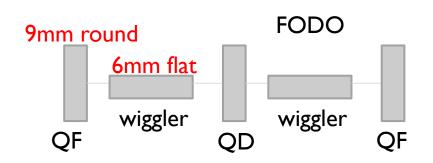
- Simulates single/multi bunch collective phenomena associated with impedances (or electron cloud)
- Computes the evolution of the bunch by bunch centroid as a function of time over an adjustable number of turns

#### First results (II)

# Estimating the machine impedance budget with a 4-kick approximation



- A uniform coating of NEG, 2µm thickness, was assumed around the ring made from stainless steel
- The contributions from the resistive wall of the beam chamber were singled out for both the arc dipoles and the wigglers

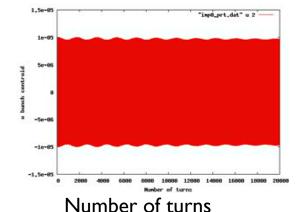


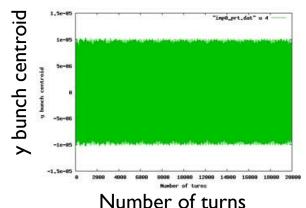
#### I kick $\rightarrow$ broadband resonator ( $S_{kick} = Im$ )

- 2 kick  $\rightarrow$  arc (L=270.2m, 9mm, round, <bx>=2.976m, <by>=8.829m,  $S_{kick}$ =150m)
- 3 kick →wigglers (L=104m, 6mm, flat, <bx>=4.200m, <by>=9.839m, S<sub>kick</sub>=41.3m)
- 4 kick  $\rightarrow$  rest of the FODO (L=53.3m, 9mm, round,  $\langle bx \rangle = 5.665$ m,  $\langle by \rangle = 8.582$ m,  $S_{kick} = 39.2$ m)

#### First results (III)

Estimating the machine impedance budget with a 4-kick approximation – single bunch simulations

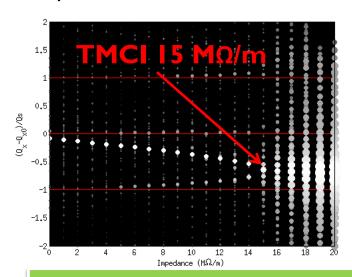


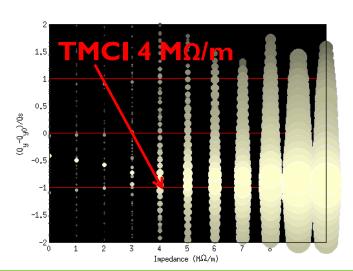


**HEADTAIL** output: Position of the centroid over the number of turns

> FFT/ Sussix

Mode spectrum of the horizontal and vertical coherent motion as a function of impedance



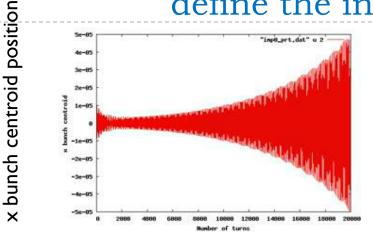


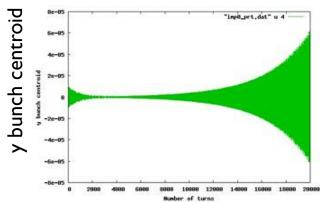
For zero chromaticity, the (remaining) impedance budget is estimated at 4 M $\Omega$ /m (7 M $\Omega$ /m for the BB only)

x bunch centroid position

## First results (III)

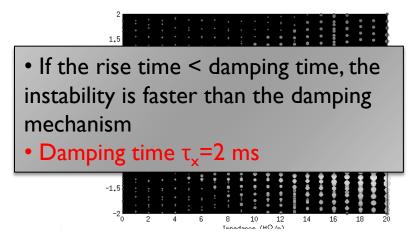
Single bunch simulations without space charge to define the instability thresholds

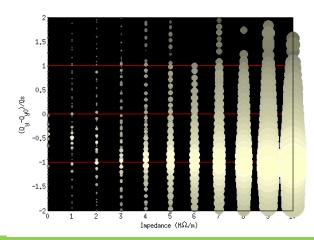




ξx	0.055
ξ <sub>y</sub>	0.057

- Another type of instability occurs, called the head-tail instability
- Compare the rise time of instability with the damping time to define the threshold



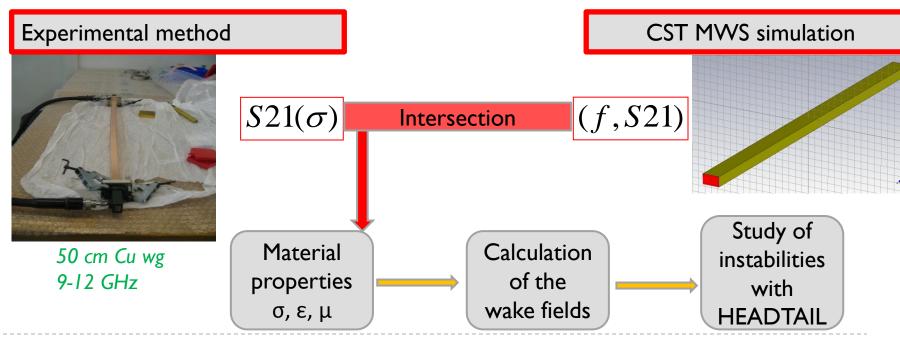


- No mode coupling observed
- •Higher TMCI thresholds
- Mode 0 is damped
- Higher order modes get excited (m = -1)

For positive chromaticity, the impedance budget is estimated now at 1 M $\Omega$ /m (4 M $\Omega$ /m for the BB only)

## Material EM properties characterization

- ⇒Unknown material properties of NEG and a-C at high frequencies (CLIC@ 500 GHz)
- ⇒Combine experimental results with CST simulations to characterize the electrical conductivity of *NEG*
- ⇒Powerful tool for this kind of measurements



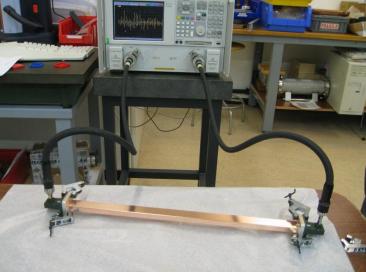
## Experimental Method (I)

## Waveguide Method

- First tested at low frequencies, from 9-12 GHz
- Use of a standard X-band waveguide, 50 cm length
- Network analyzer
- ▶ Measurement of the transmission coefficient S<sub>21</sub>



Experimental setup



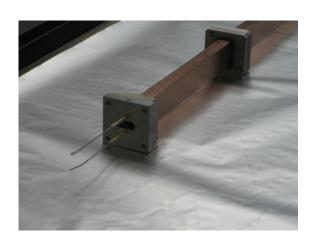
X band Cu waveguide of 50 cm length

## Experimental Method (II)

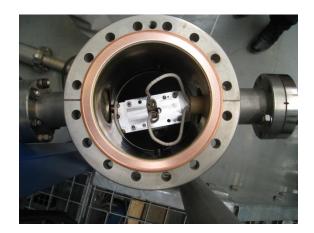
- NEG coated Cu waveguide
  - Same Cu waveguide used before is now coated with NEG
- Coating procedure
  - ▶ Elemental wires intertwisted together produce a thin Ti-Zr-V film by magnetron sputtering

Coating was targeted to be as thick as possible (9 µm from first x-rays

results)



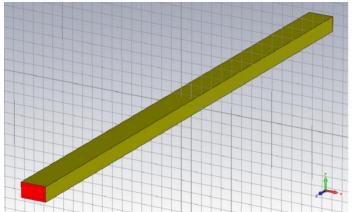




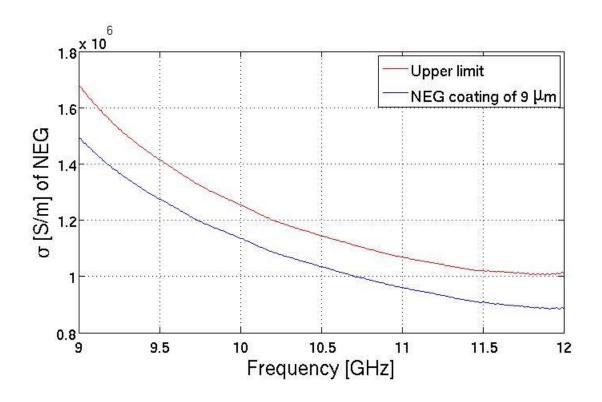
## 3D EM Simulations (I) CST Microwave Studio

- Software package for electromagnetic field simulations
- The tool Transient Solver also delivers as results the Sparameters
- CST is used to simulate the Cu waveguide (same dimensions as the ones used in the experiment → simulating the experimental setup)

X band Cu waveguide simulated with CST MWS



# 3D EM Simulations and measurements (II) Conductivity of NEG



- Upper limit for the conductivity of NEG in this frequency range
- Preliminary results

- •Is there an important effect depending on the conductivity of NEG?
- •HEADTAIL simulations for  $\sigma_{NFG} = 1.6 \cdot 10^6 \text{ S/m}$

## Results on the impedance budget (4 kicks) Effect of NEG conductivity & coating

Pipe material/ coating	Chromaticity	Threshold in $x$ plane (M $\Omega$ /m)	Threshold in y plane (MΩ/m)	Impedance budget (MΩ/m)
ss/ NEG $2\mu m$ ( $\sigma_{NEG} = 10^6 \text{ S/m}$ )	0	15	4	4
	$\xi x = 0.055/\xi y = 0.057$	2	I	ı
ss/ NEG 2μm (σ <sub>NEG</sub> = 1.6 10 <sup>6</sup> S/m)	0	16	5	5
	$\xi x = 0.055/\xi y = 0.057$	2	I	
ss/ Cu 10 μm / NEG 2 μm (σ <sub>NEG</sub> = 1.6 10 <sup>6</sup> S/m)	0	16	5	5
	$\xi x = 0.055/\xi y = 0.057$	2.5	2	2

The characterization of NEG properties is important

Different coating doesn't have a very big effect

# Experimental part (II) Beam dynamics measurements at SLS

- CLIC damping rings target ultra-low emittance in all 3 dimensions for relatively high bunch density
- SLS: Vertical emittance reduced to a minimum value of **0.9±0.4pm** (CLIC damping rings target vertical emittance) which is a **new world record**
- SLS ideal for beam dynamics measurements
- Validate the models used by comparing to a real machine

- ⇒ First MD sessions: the goal was to measure the beam transfer function (BTF) in both transverse and longitudinal plane, test the diagnostics and the scripts to collect the data to ensure future successful MD sessions
- $\Rightarrow$  Future MD sessions: single bunch measurements, tuneshift with intensity

#### Future work - planning

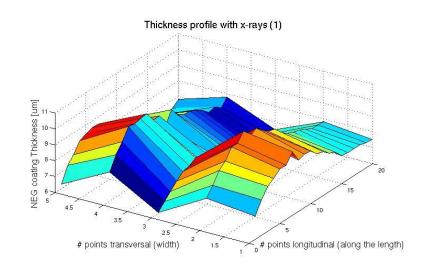
- ⇒Multi-kick code to simulate several impedance contributions (kickers, cavities, etc)
- $\Rightarrow$ Effect of coating in impedance (wigglers, rest of the ring)  $\Rightarrow$  possible scenarios of materials  $\Rightarrow$  NEG/aC coating
- $\Rightarrow$ Space charge influence on the coherent modes  $\Rightarrow$  indications from the theoretical study of A.Burov
- ⇒Damping mechanism to predict instabilities
- ⇒Effect of the resistive wall with coating by studying the effect of its long range part (multi-bunch effects) with the goal of defining specifications for the transverse feedback system
- ⇒Study the thresholds to preserve also the stability in the longitudinal plane
- ⇒Waveguide measurements for NEG/aC coating on copper and stainless steel
- ⇒Beam dynamics measurements at SLS (single bunch tuneshift over intensity, impedance with IBS measurements)

## Challenges...

- Ultra high brilliance of the beams
- ▶ Small emittances and small chambers → collective effects
- Those regimes are becoming more and more important for existing lepton machines as well as for future ones (CLIC/ILC)
- Low Emittance Lepton Rings unexplored regimes
  - Effect of coating
  - How space charge will affect the TMCI thresholds- is not negligible as it is for other lepton machines. Theoretical studies exist but never been applied to simulations.

## Challenges...

- Measure properties at high frequencies...
  - Up to 500 GHz/ 500 GHz Network analyzer (EPFL)
  - Very short waveguides, Y-band (0.5 x 0.25 mm)
- Challenges
  - Manufacture of the small waveguide
  - Coating technique
  - Profile measurements
- Simulation
  - Non-uniform coating



## Acknowledgements

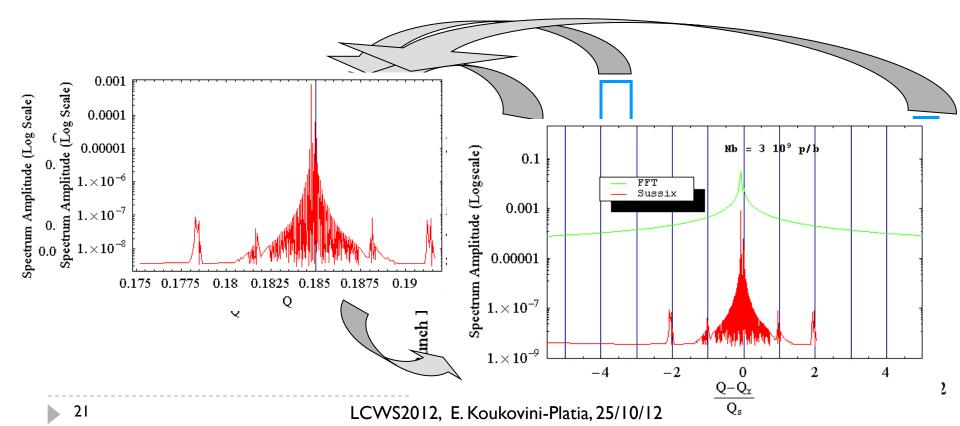
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- M. Dehler
- G. De Michele
- N. Milas
- Y. Papaphilippou
- A. Streun

- A.T. Perez Fontenla
- G. Arnau Izquierdo
- S. Lebet
- M. Malabaila
- P. Costa Pinto
- M. Taborelli

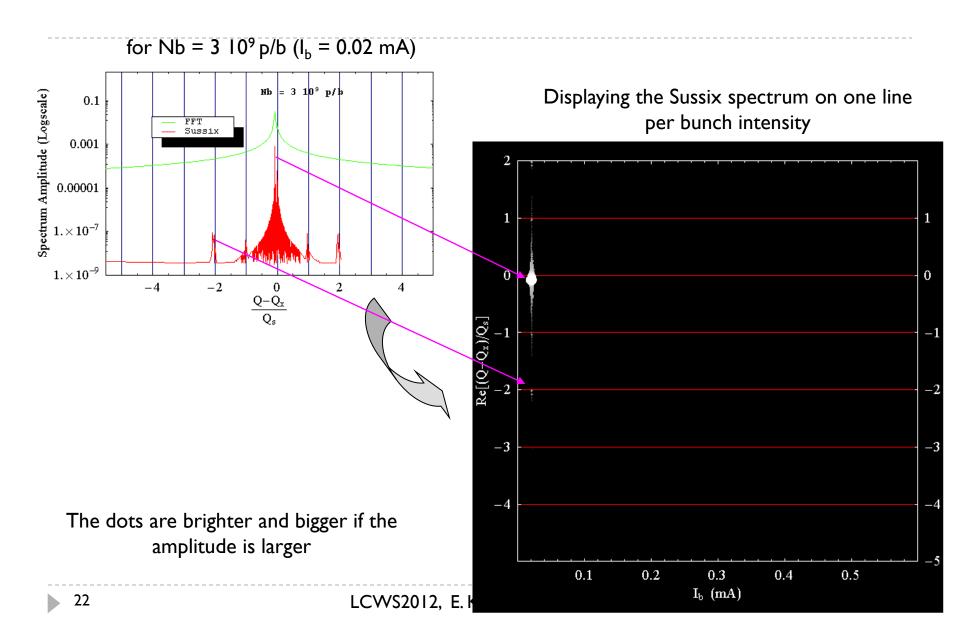
## Backup slides

#### Methods: What to do with HEADTAIL outputs?

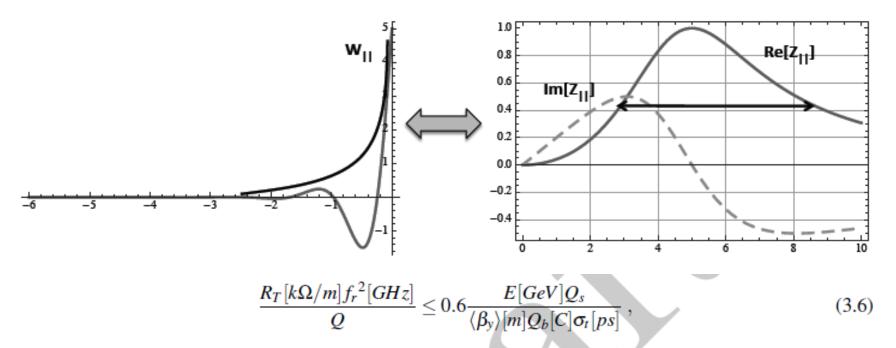
- Extract the position of the centroid of the bunch (vertical or horizontal) turn after turn  $\rightarrow$  simulated BPM signal
- 2. Apply a classical FFT to this simulated BPM signal (x)
- 3. Apply SUSSIX\* to this same simulated BPM signal (actually  $x j \beta_x x'$ )
- 4. Translate the tune spectrum by  $Q_{x0}=0$  and normalize it to  $Q_s$



## Another visualization of the tune spectrum



## **Broadband Resonator**



where  $R_T$  is the transverse impedance in  $k\Omega/m$ ,  $f_r = \omega_r/2\pi$  represents the resonant frequency in GHz where  $\omega_r$  is the resonant angular frequency of the resonator and is assumed to be the cut off frequency of the beam pipe, Q the quality factor,  $\langle \beta_y \rangle$  the average beta value in the y-plane in m,  $Q_b = Ne$  the bunch charge in Coulomb and  $\sigma_t = \sigma_z/\beta c$  represents the r.m.s. bunch length in ps. Since the CLIC DR bunch is short, compared to the wavelength of electromagnetic waves propagating in the beam pipe, Eq. (3.6) can be used to predict the TMCI threshold of around 10.7 M $\Omega/m$  for the transverse broad-band resonator in the vertical plane for Q = 1 and  $f_r = 5$  GHz.

## Example of the 4 kicks applied

