

# Gain Stabilization of SiPMs

Uni Bergen:  
FZU Prague:

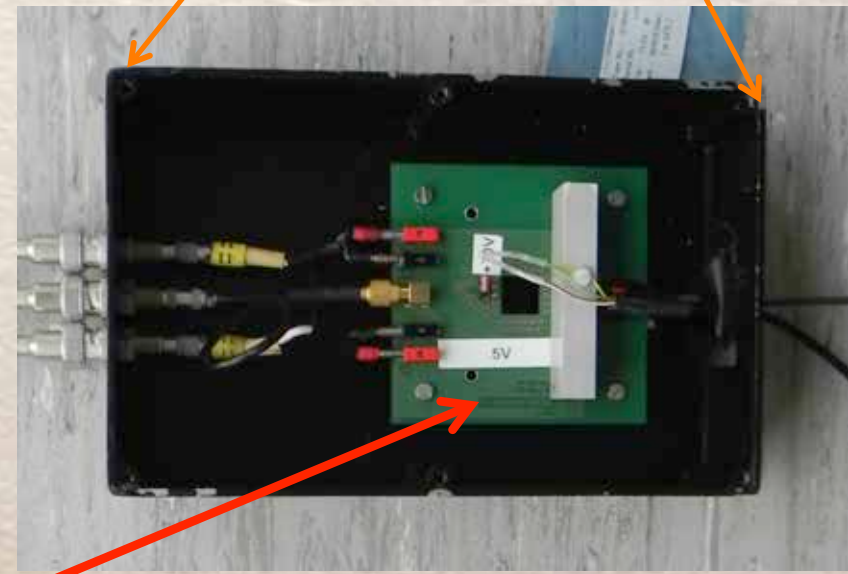
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# Introduction

- The gain of SiPMs depends both on bias voltage and on temperature
  - Gain decreases with temperature
  - Gain increases with bias voltage
- For stable operations, we need to keep gain constant
- In an analogue hadron calorimeter with millions of channels, this is a difficult task due to temperature variations
- Thus, it is desirable to adjust  $V_{\text{bias}}$  to compensate for T changes to keep the gain constant
- Goal: build a  $V_{\text{bias}}$  regulator to keep gain constant (<1%)
- First, we need to measure SiPM gain vs temperature
  - determine  $dV/dT$  to obtain constant gain
  - build  $V_{\text{bias}}$  regulator prototype to demonstrate proof of principle
- This is work conducted in the framework of the EU project AIDA

# SiPM Test Setup

- We work in a climate chamber at CERN that is accurate to  $0.1^{\circ} \text{C}$
- Use digital oscilloscope read out by PC, low voltage & bias voltage power supplies
- Use pulse generator for LED signal
- Shine blue LED light on detectors

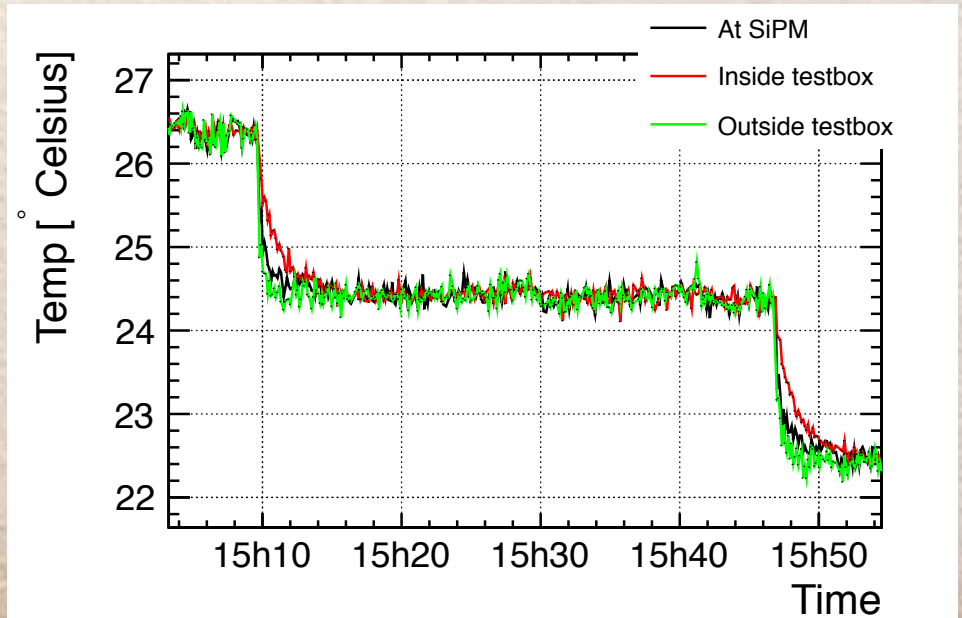
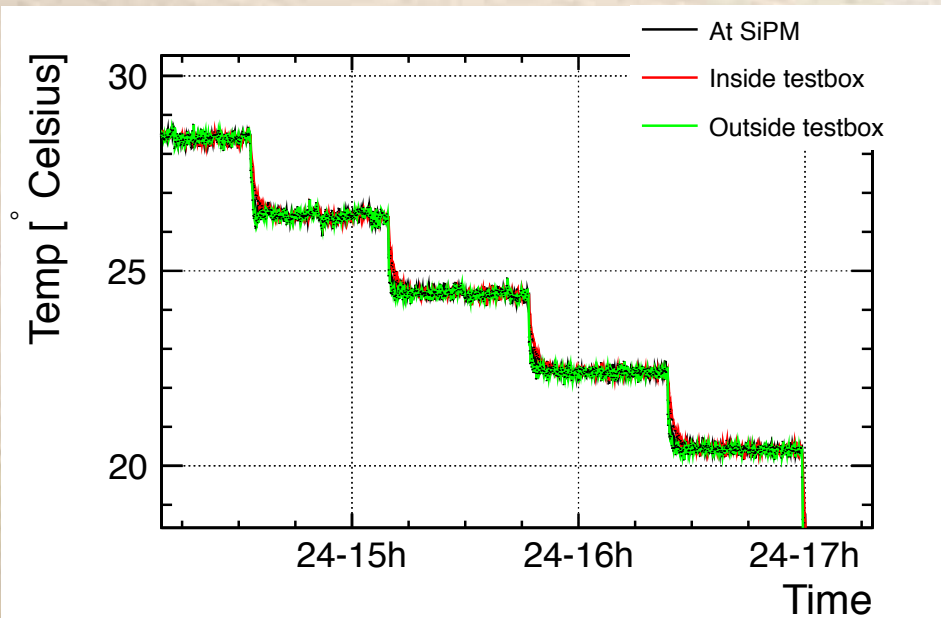
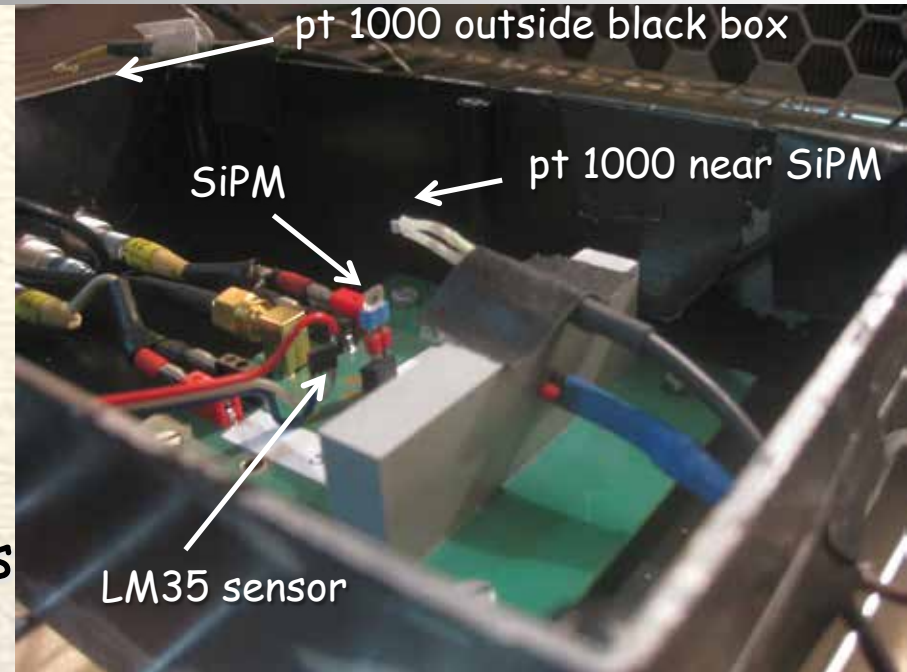


SiPM + preamp + T sensor + LED<sub>3</sub>



# Temperature Measurement

- Use 3 pt 1000 sensors
  - Near SiPM, inside/outside black box
- Use LM35 sensor to measure T to perform gain correction
- Vary T from 5°C to 40°C in 5°C steps except in 20°-30°C range use 2°C steps
  - $T_{SiPM} \sim T_{SET} + 0.4^{\circ}C$ ,
  - offset is same over entire range



# SiPM Detectors Tested

- We measured the  $dG/dT$  &  $dG/dV$  dependence for 15 SiPMs from 3 manufacturers

- We tested the  $V_{bias}$  adjustment on 4 SiPMs:

- CPTA 857
- CPTA 1677
- KETEK W 12
- Hamamatsu 11759

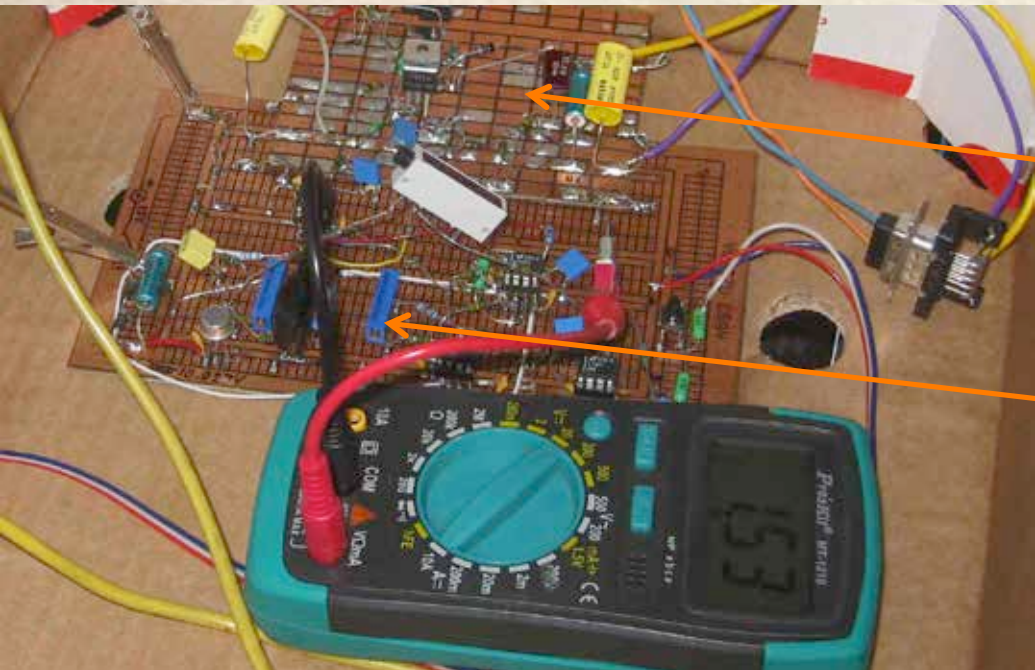
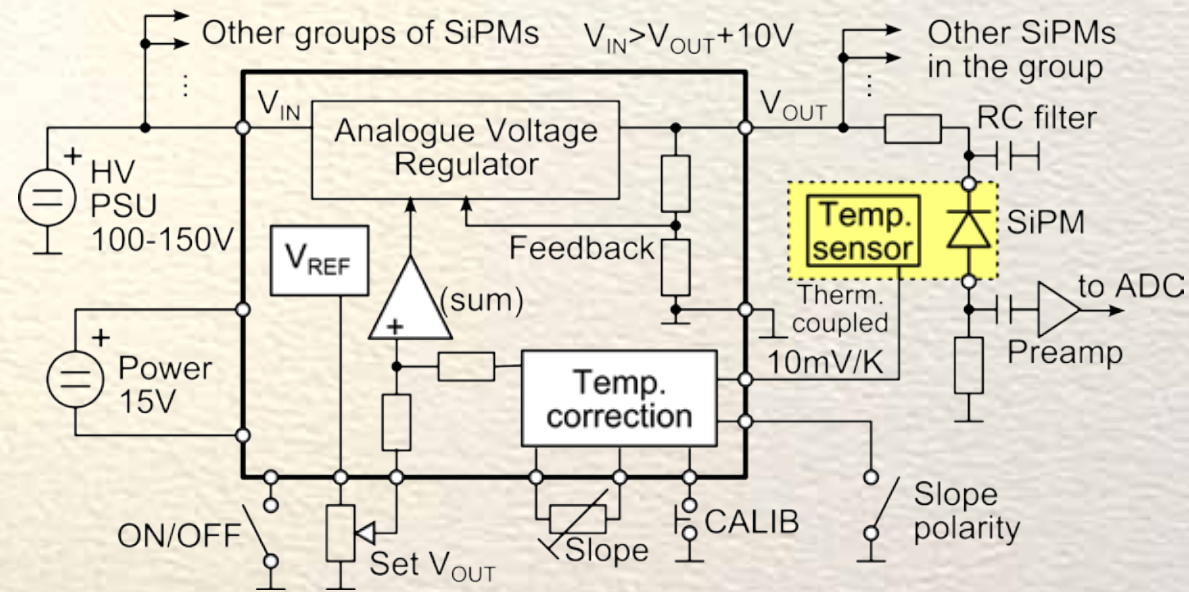
- Show results for the first 3

Manufacturer and Type #	Sensitive area [ $mm^2$ ]	Pixel pitch [ $\mu m$ ]	#pixels	Typical $V_{bias}$ [V]	Typical $G$ [ $\times 10^5$ ]	Serial #
Hamamatsu						
S10943-8584(X)	$1 \times 1$	50	400	71.69	7.49	11759
S10943-8584(X)	$1 \times 1$	50	400	71.57	7.49	11766
S10943-8584(X)	$1 \times 1$	50	400	71.50	7.48	11770
S10943-8584(X)	$1 \times 1$	50	400	71.33	7.48	11771
Sample A	$1 \times 1$	20	2500	66.7	2.3	A1
Sample B	$1 \times 1$	20	2500	73.3	2.3	B1
Sample A	$1 \times 1$	15	4440	67.2	2.0	A2
Sample B	$1 \times 1$	15	4440	74.0	2.0	B2
CPTA						
	$1 \times 1$	40	796	33.4	7.1	857
	$1 \times 1$	40	796	33.1	6.3	922
	$1 \times 1$	40	796	33.3	6.3	975
	$1 \times 1$	40	796	33.1	7.0	1065
	$1 \times 1$	40	796	33.3	14.6	1677
KETEK						
MP15 V6 ?	$2(1.2 \times 1.2)$	15?	?	-28	?	W8
MP20 V4 ?	$3 \times 3$	20?	?	-28	?	W12

- Note that CPTA sensors were attached to  $3 \times 3$   $cm^2$  scintillator tiles while the other sensors were directly illuminated by blue LED

# Layout of the Adaptive Power Regulator

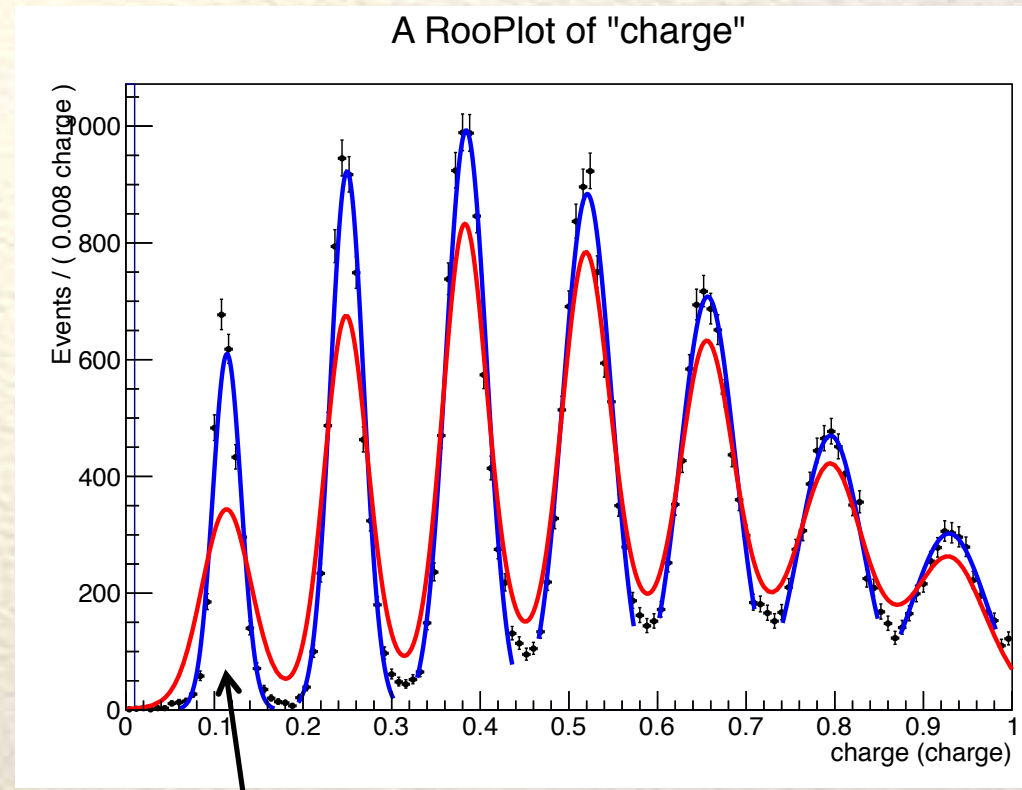
- Design  $V_{bias}$  regulator that operates in 10 V to 80 V region plus T correction effects
- Temperature slope:  $<1$  to 100 mV/K, both positive and negative



- First design of prototype board
- Analogue voltage regulator
- Voltage reference

# Gain Determination

- Determine gain by fitting Gaussian functions to peaks of single pe spectra
- Define gain as
  - Distance between 1 pe & 2 pe peaks (MPPCs)
  - distance between pedestal 1 pe peak (CPTA, KETEK)
- Define the error on the gain as the errors of the two fitted Gaussian mean values added in quadrature

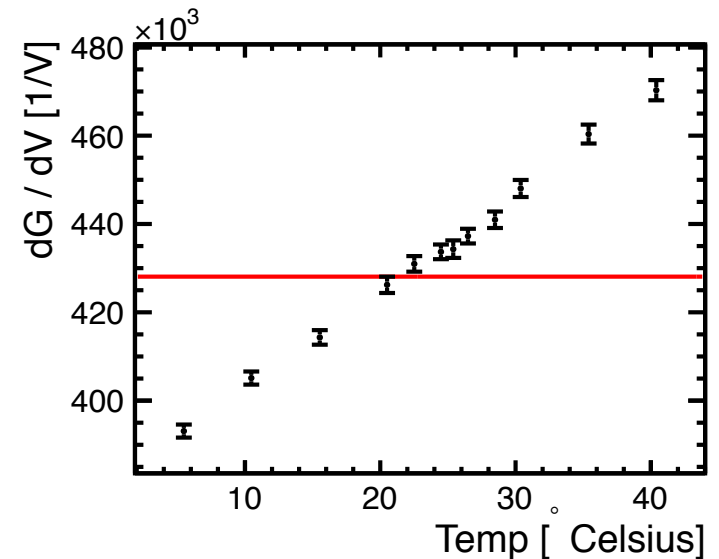
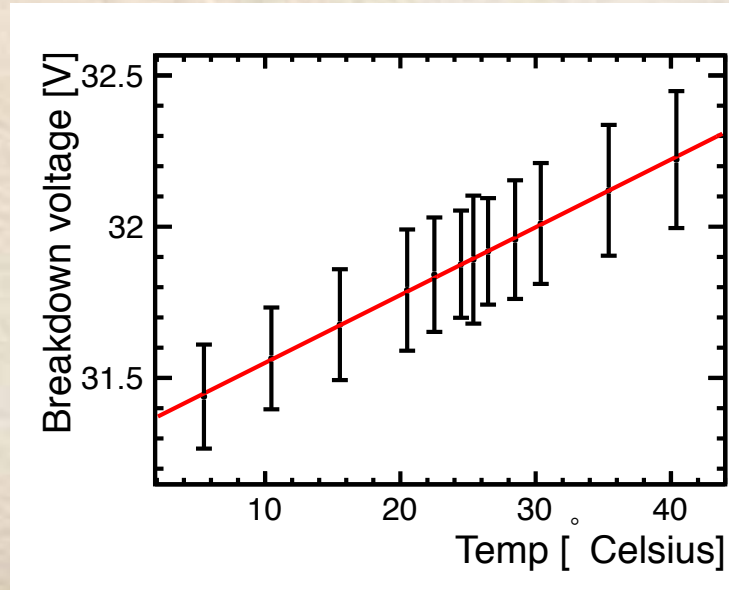
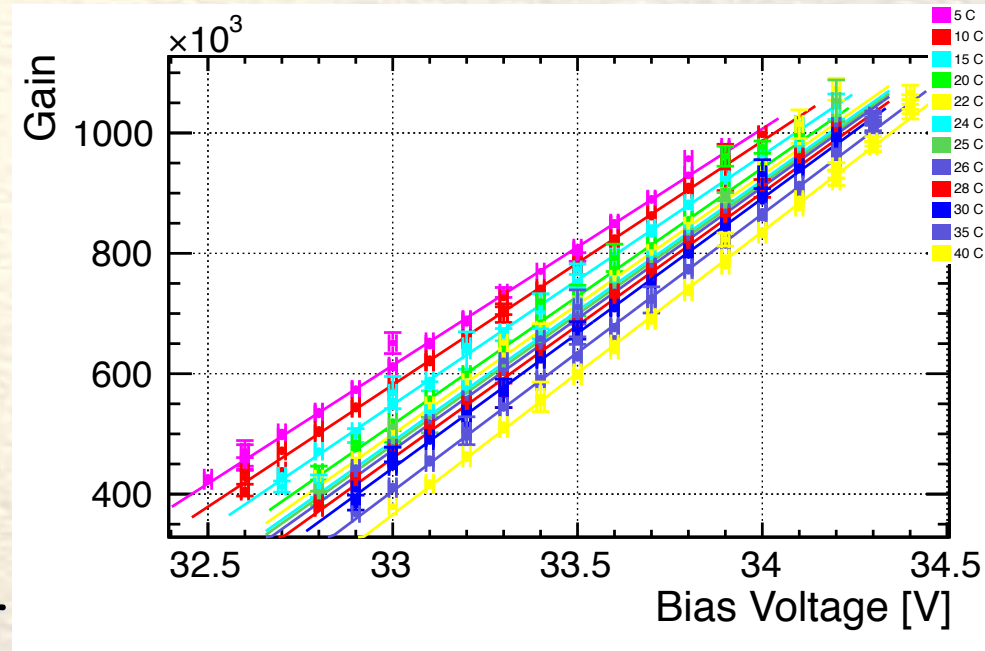


RooFit multikernel function  
Individual Gaussian fits



# Gain vs Voltage for CPTA 857

- Each point is the gain extracted from 50k waveforms of 80 ns
- Linear fit to these distributions yields break-down voltage &  $dG/dV$
- Break-down voltage drops with T
- $dG/dV \sim$  capacitance is not constant  
→ linear dependence is seen



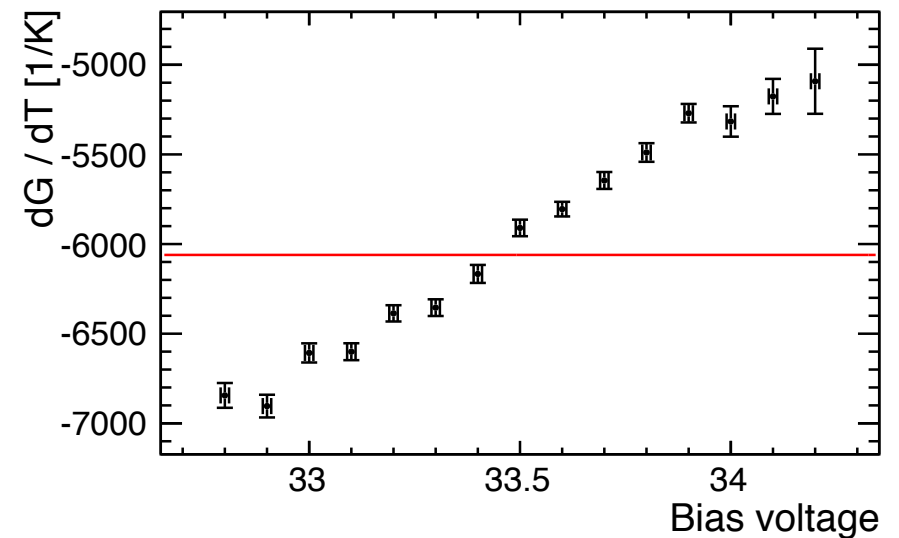
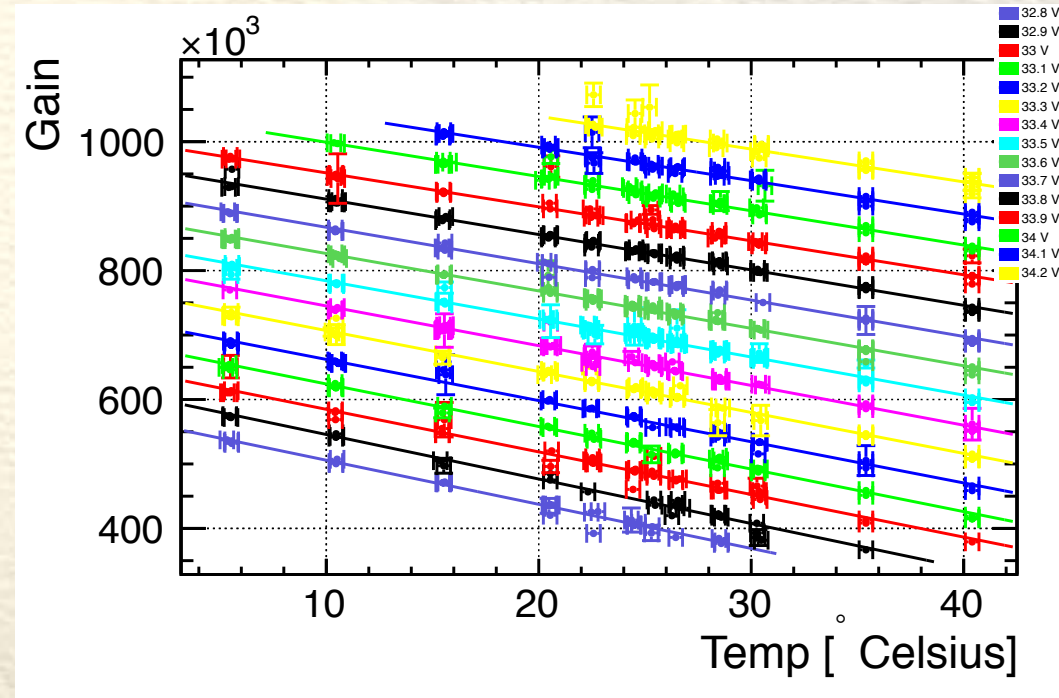


# Gain vs Temperature for CPTA 857

- Same data as last slide
- For a constant gain, need to extract  $dV/dT$
- Average fitted slopes and take spread in the slopes as uncertainty:

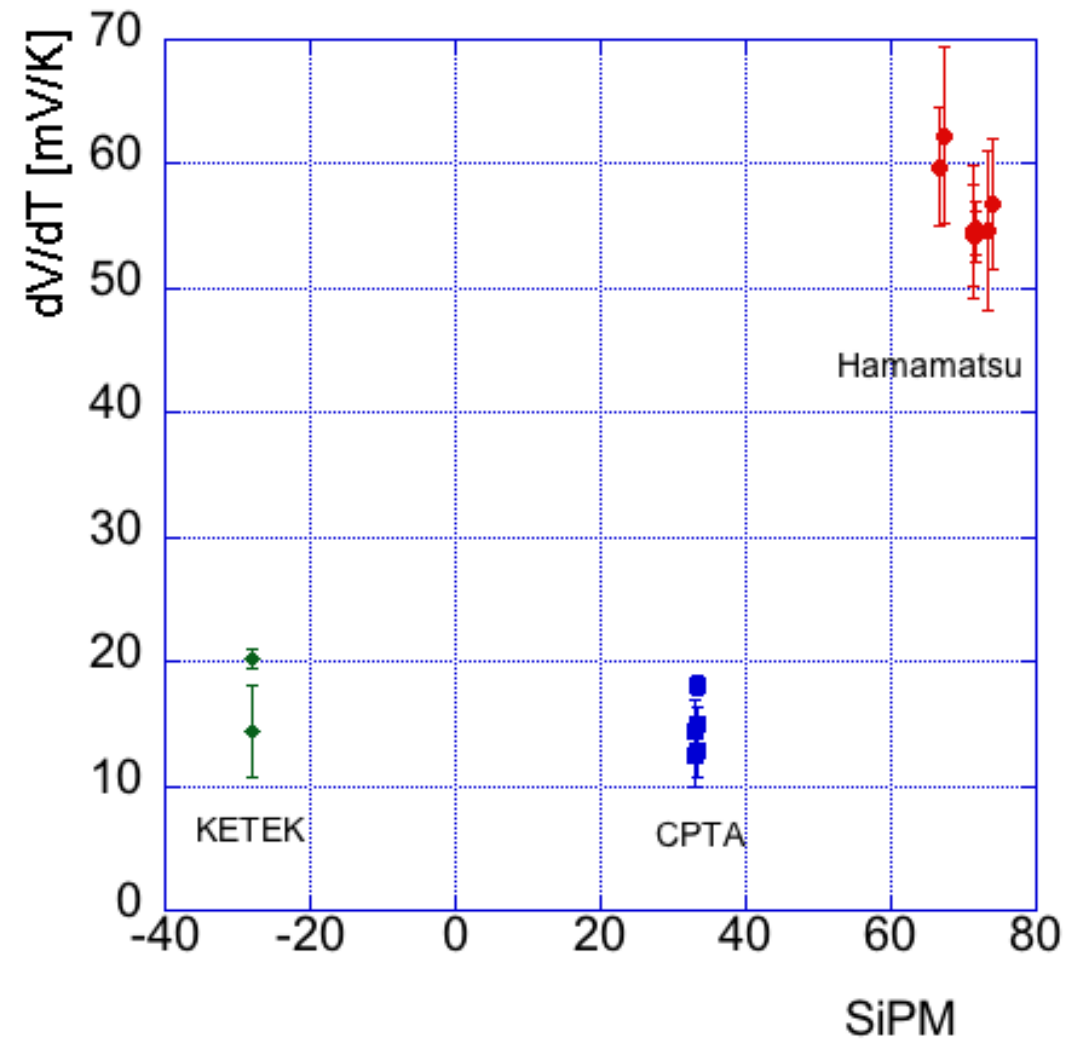
$$dV/dT = \langle dG/dT \rangle / \langle dG/dV \rangle$$

$$= 13.7 \pm 2.1 \text{ mV/K}$$



# dV/dT Measurements

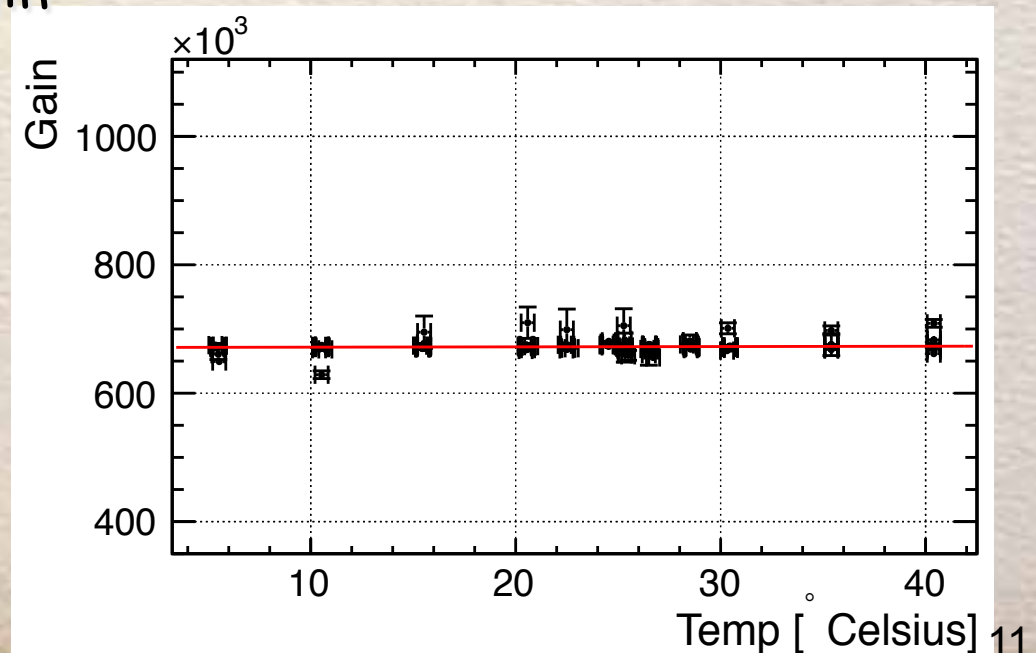
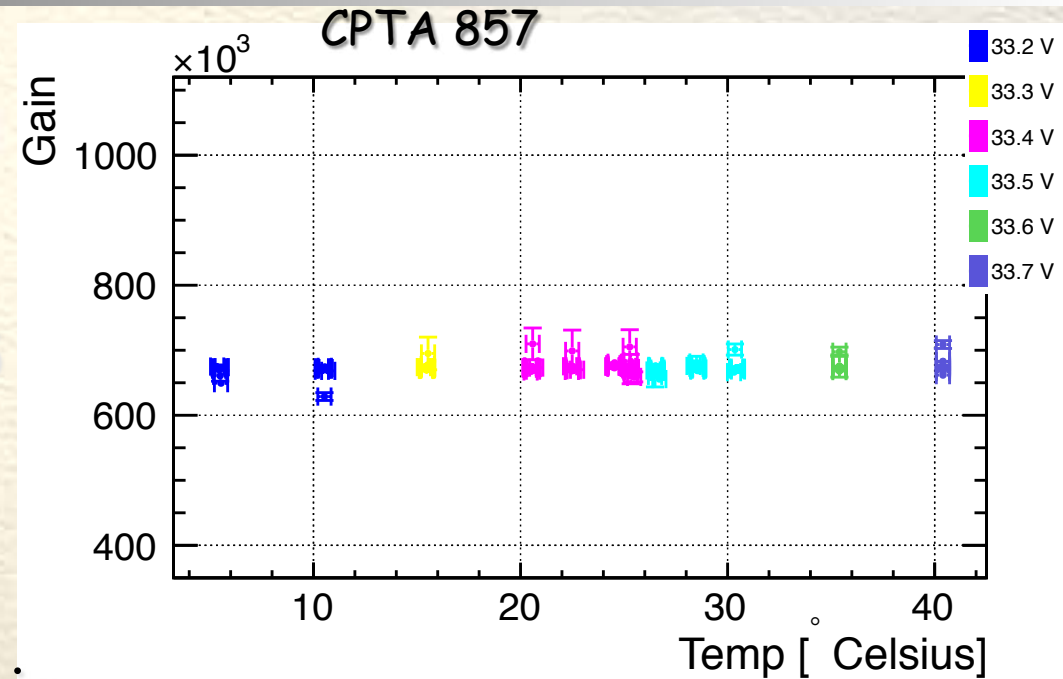
- KETEK SiPMs operate at opposite  $V_{\text{bias}}$  than CPTA and Hamamatsu SiPMs
- $V_{\text{bias}}$  for Hamamatsu is  $\sim 70\text{V}$  while  $V_{\text{bias}}$  for CPTA is  $\sim 33\text{V}$  &  $V_{\text{bias}}$  for KETEK is  $\sim 28\text{V}$
- For KETEK and CPTA, dV/dT is  $\sim 15\text{-}20\text{ mV/K}$  for Hamamatsu, dV/dT is  $\sim 55\text{ mV/K}$





# Gain after $V_{bias}$ Adjustment for CPTA 857

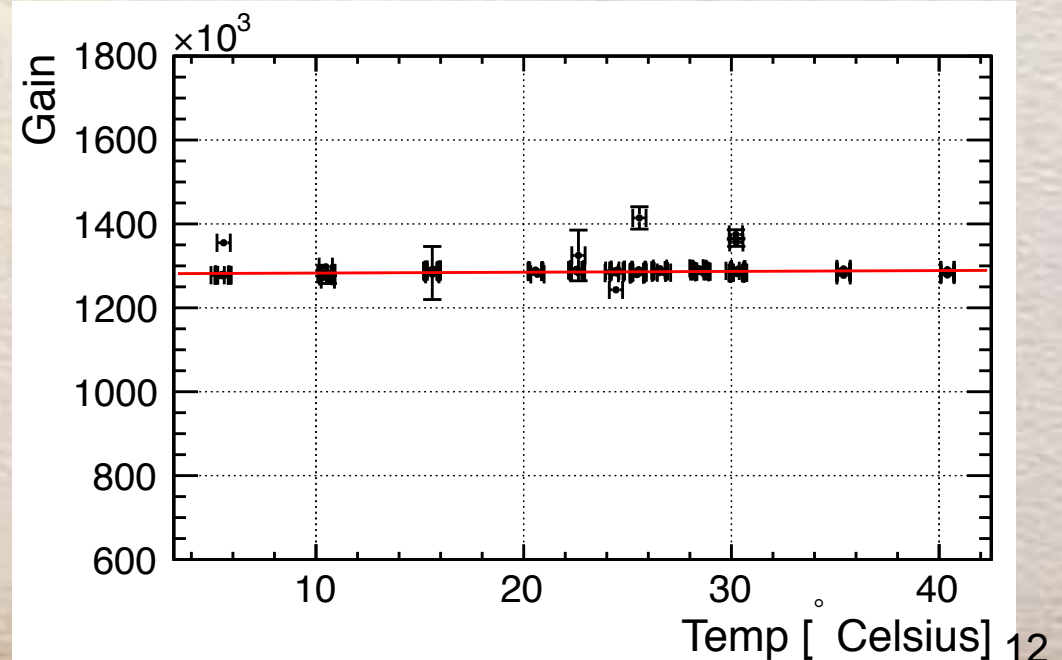
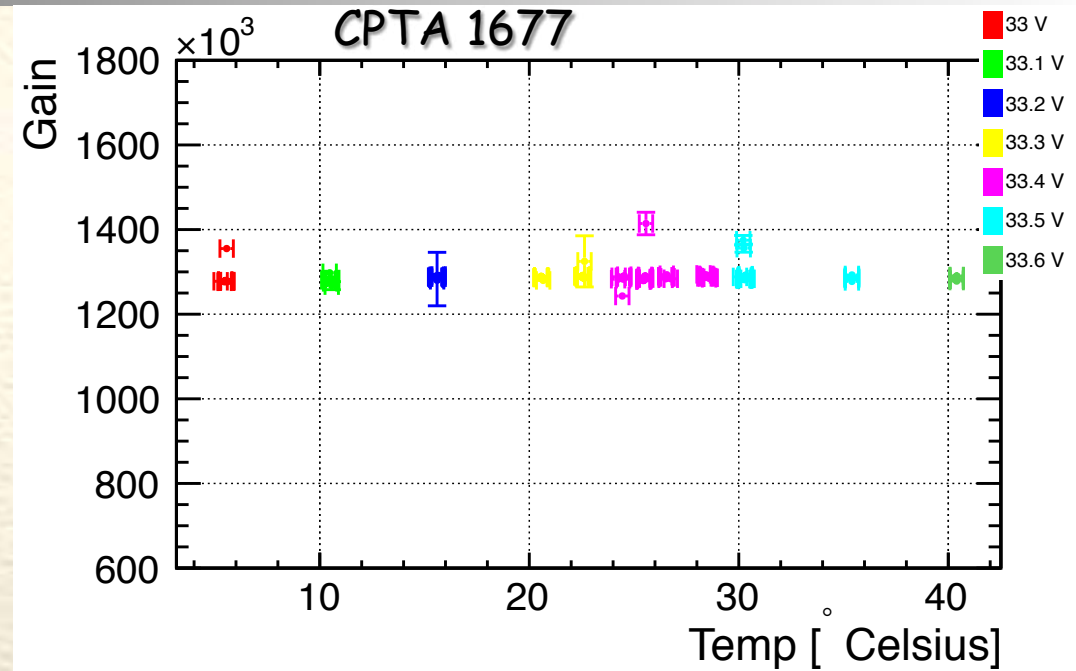
- Adjust voltage continuously using  $V_{bias}$  regulator prototype  
Note: color code gives the range of voltage applied  
e.g. magenta:  $33.35 < V_{bias} < 33.45$
- At each T, take 16 samples with 50k waveform each
- See outliers  $\rightarrow$  understand origin
- Linear fit to all data points
  - offset:  $(6.71 \pm 0.0044) \times 10^5$
  - slope:  $47.3 \pm 19.1$
- Gain is uniform in range of interest  $5^\circ - 40^\circ C \rightarrow$  measured non-linearity is  $< \pm 0.001$





# Gain after $V_{bias}$ Adjustment for CPTA 1677

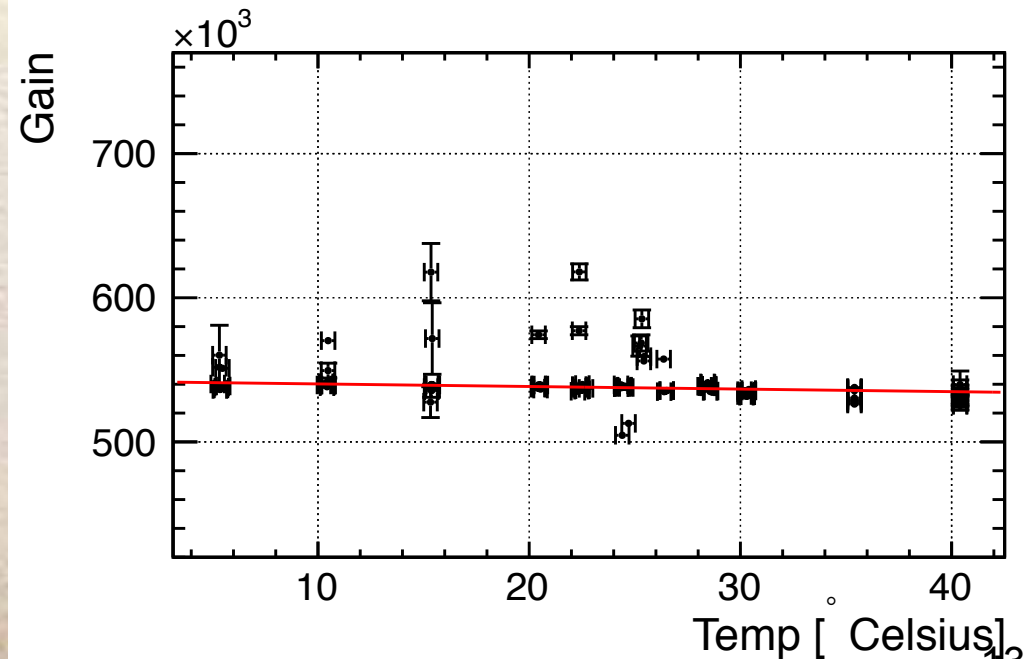
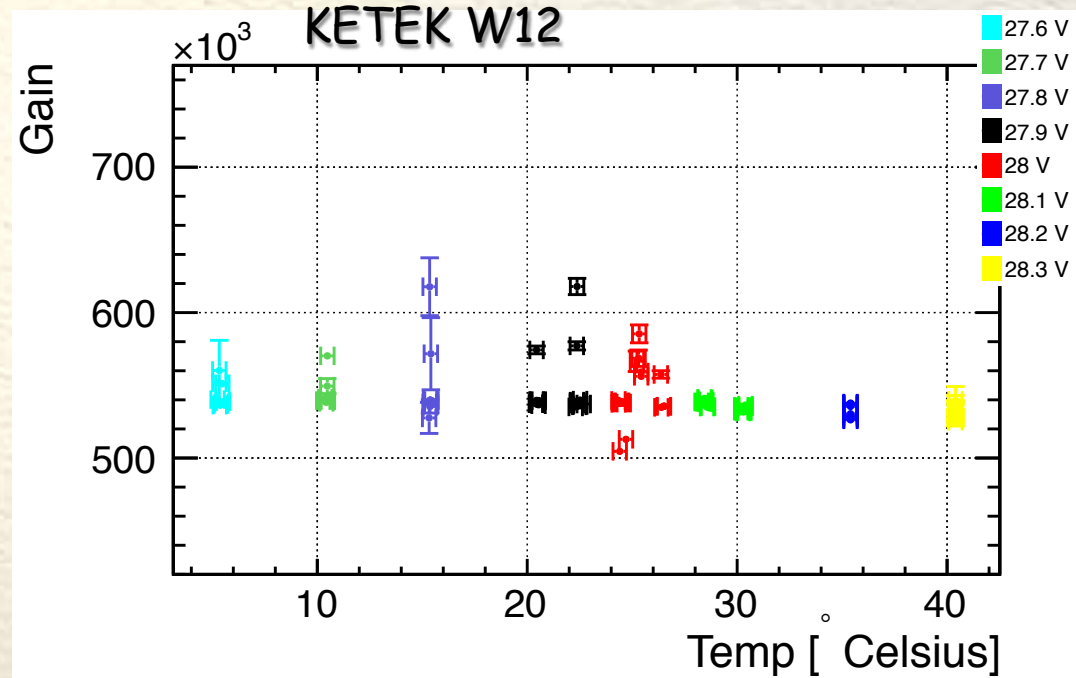
- Measured  $dV/dT$  slopes of  $18.3 \pm 0.6$  mV/K for CPTA 1677
- See few outliers
- Linear fit to all data points
  - offset:  $(1.28 \pm 0.00059) \times 10^6$
  - slope:  $198 \pm 24.7$
- Gain is basically uniform between  $5^\circ\text{C}$  &  $40^\circ\text{C}$
- $\rightarrow$  non-linearity in measured range is  $< \pm 0.002$





# Gain after $V_{bias}$ Adjustment for KETEK W12

- Measured  $dV/dT$  slopes of  $22.2 \pm 1.9$  mV/K for KETEK W12
- See more outliers  $\rightarrow$  investigate
- Linear fit to all data points
  - offset:  $(5.42 \pm 0.0032) \times 10^5$
  - slope:  $-178 \pm 14.5$
- Gain still fulfills requirement between  $5^\circ C$  &  $40^\circ C$
- $\rightarrow$  non-linearity in measured range is  $< \pm 0.0035$
- MPPC analysis is still ongoing
- Measured  $dV/dT$  slopes of  $54.3 \pm 3.3$  mV/K for MPPC 11759



# Conclusion

- Hamamatsu sensors operate at higher  $V_{\text{bias}}$  than CPTA/KETEK sensors
- $dV/dT$  is similar for CPTA & KETEK sensors (15-20 mV/K) while Hamamatsu sensors yield larger values  $\sim 55$  mV/K
- For the 3 detectors tested, the maximum voltage adjustments are less than  $\Delta V = 0.7$  V for range  $5^{\circ}\text{C} < T < 40^{\circ}\text{C}$
- The gain stabilization with the  $V_{\text{bias}}$  regulator prototype works well for all three tested SiPMs  
→ accuracy is much better than 1% for temperature range  $5^{\circ}\text{C} < T < 40^{\circ}\text{C}$



# Next Steps

- We need to understand the reason for outliers in the gain vs temperature measurements after  $V_{bias}$  adjustment
- Complete the study with the Hamamatsu sensor
- Test the  $V_{bias}$  regulator prototype on more SiPMs
- Design  $V_{bias}$  regulator PCB and test it on several SiPMs so it is ready for mass production
- Integrate the  $V_{bias}$  regulator PCB into the FE readout electronics of the AHCAL

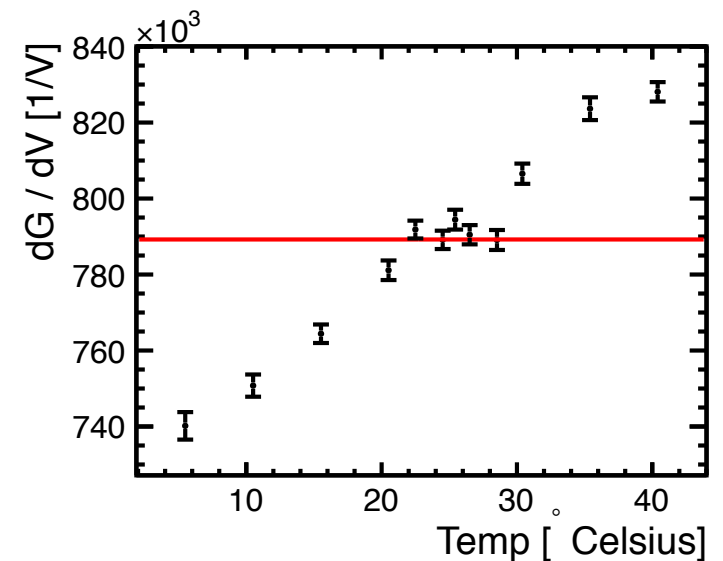
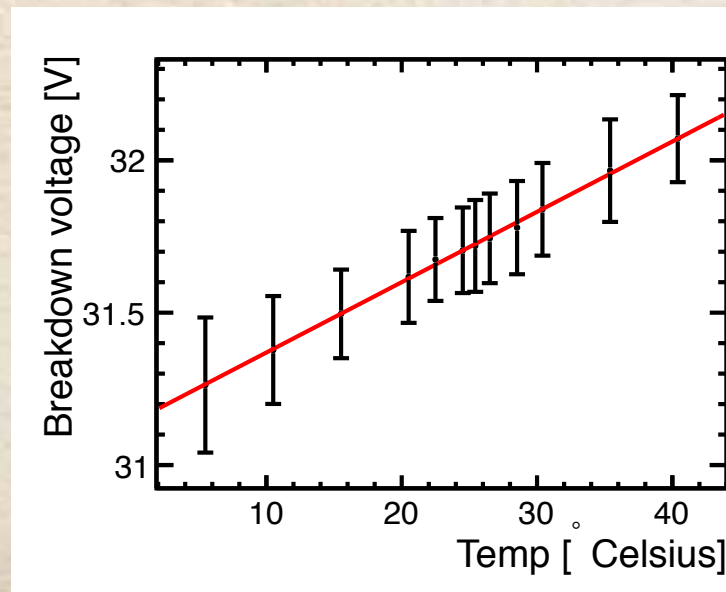
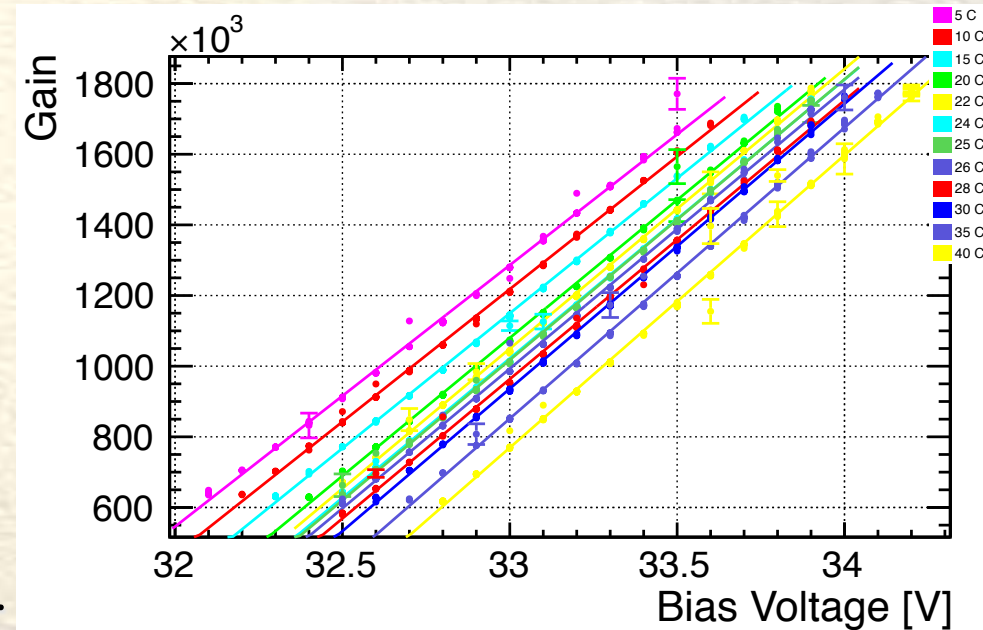


# Backup Slides



# Gain vs Voltage for CPTA 1677

- Each point is the gain extracted from 50k waveforms
- Linear fit to these distributions yields break-down voltage &  $dG/dV$
- Break-down voltage drops with  $T$
- $dG/dV \sim$  capacitance is not constant  $\rightarrow$  linear dependence is seen

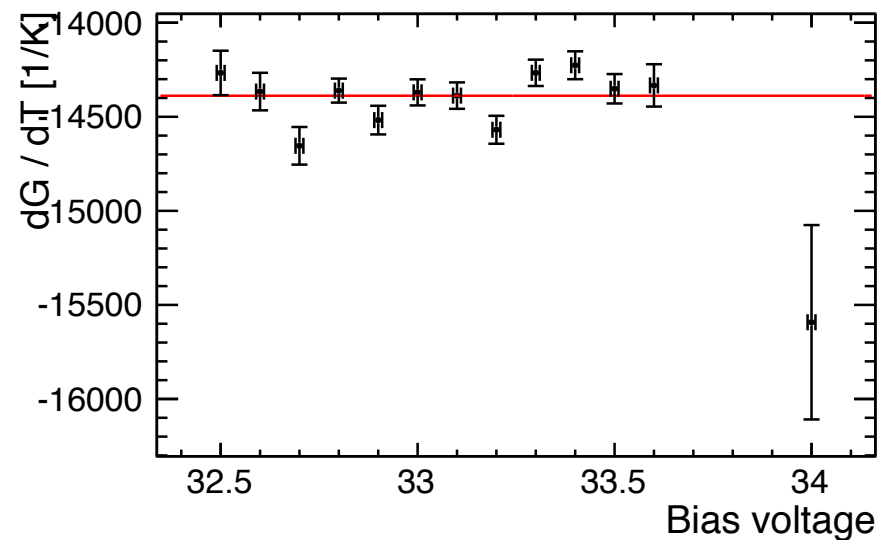
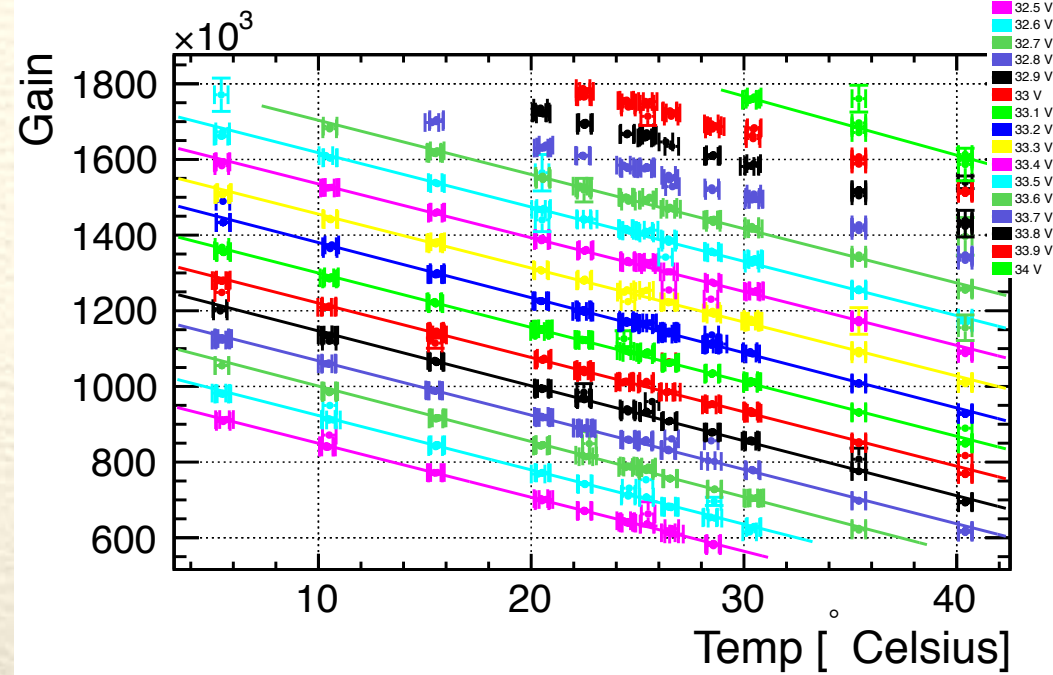


# Gain vs Temperature for CPTA 1677

- Same data as last slide
- For a constant gain, need to extract  $dV/dT$
- Average fitted slopes and take spread in the slopes as uncertainty:

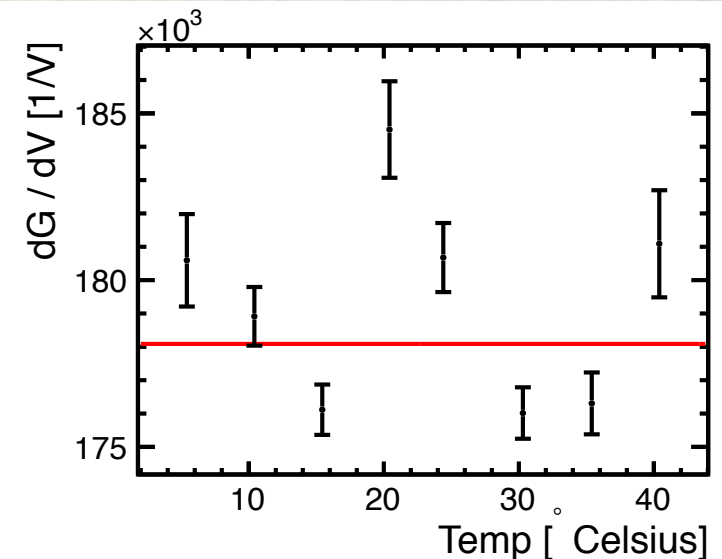
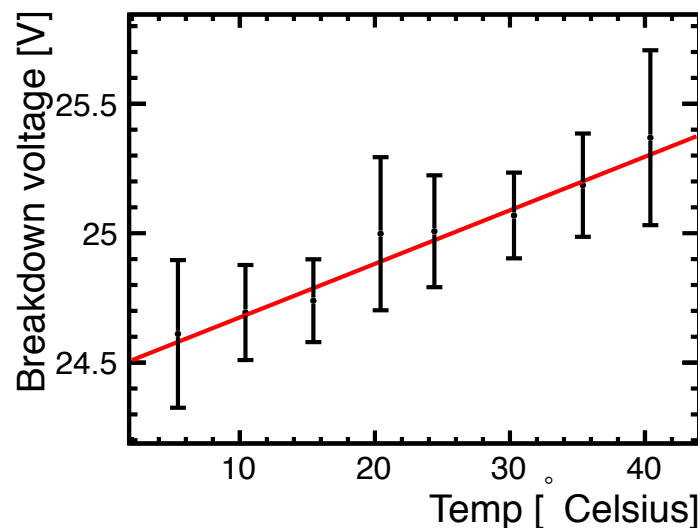
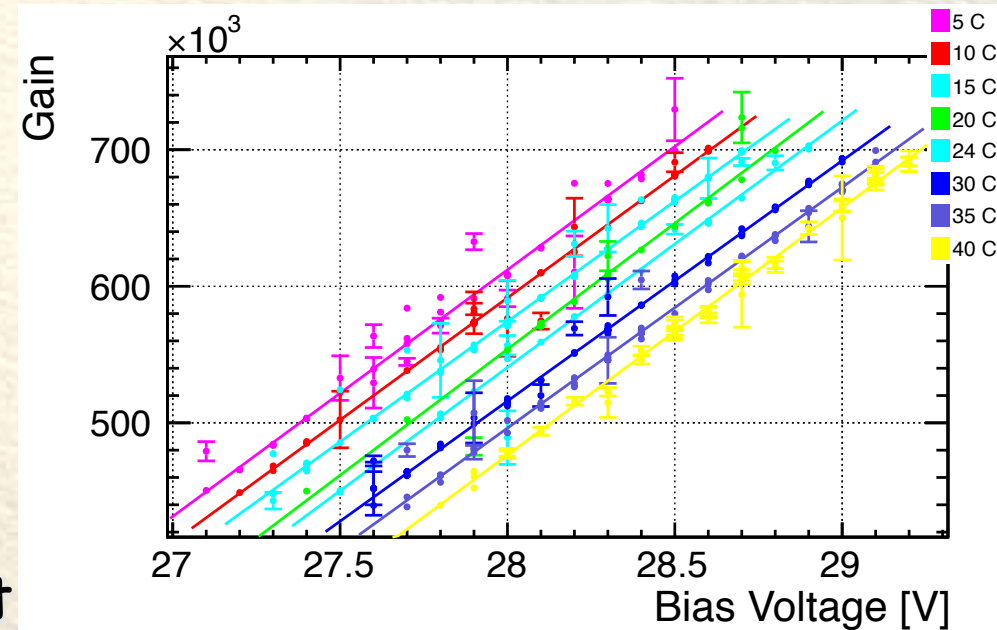
$$dV/dT = \langle dG/dT \rangle / \langle dG/dV \rangle$$

$$= 18.3 \pm 0.6 \text{ mV/K}$$



# Gain vs Voltage for KETEK W12

- Each point is the gain extracted from 50k waveforms
- Linear fit to these distributions yields break-down voltage &  $dG/dV$
- Break-down voltage drops with  $T$
- $dG/dV \sim$  capacitance is not constant  $\rightarrow$  linear dependence is seen



# Gain vs Temperature for KETEK W12

- Same data as last slide
- For a constant gain, need to extract  $dV/dT$
- Average fitted slopes and take spread in the slopes as uncertainty:

$$dV/dT = \langle dG/dT \rangle / \langle dG/dV \rangle = 22.2 \pm 1.9 \text{ mV/K}$$

