

Non-linear dynamics in damping rings Yannis PAPAPHILIPPOU Accelerator and Beam Physics group Beams Department CERN

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- Gradient error
- Chromaticity and correcting sextupoles
- Perturbation of Hills equation
- Resonance conditions and tune-spread
- Non-linear dynamics due to sextupoles and multipoles
- Chaotic motion and Dynamic apertureFrequency map analysis



Gradient error

Consider the transfer matrix for 1-turn

$$\mathcal{M}_0 = \begin{pmatrix} \cos(2\pi Q) + \alpha_0 \sin(2\pi Q) & \beta_0 \sin(2\pi Q) \\ -\gamma_0 \sin(2\pi Q) & \cos(2\pi Q) - \alpha_0 \sin(2\pi Q) \end{pmatrix}$$

Consider a gradient error in a quad. In thin element approximation the quad matrix with and without error are

$$m_{0} = \begin{pmatrix} 1 & 0 \\ -K_{0}(s)ds & 1 \end{pmatrix} \text{ and } m = \begin{pmatrix} 1 & 0 \\ -(K_{0}(s) + \delta K)ds & 1 \end{pmatrix}$$

$$\bullet \text{ The new 1-turn matrix is } \mathcal{M} = mm_{0}^{-1}\mathcal{M}_{0} = \begin{pmatrix} 1 & 0 \\ -\delta Kds & 1 \end{pmatrix} \mathcal{M}_{0}$$
which yields
$$\mathcal{M} = \begin{pmatrix} \cos(2\pi Q) + \alpha_{0}\sin(2\pi Q) & \beta_{0}\sin(2\pi Q) \\ \delta Kds(\cos(2\pi Q) - \alpha_{0}\sin(2\pi Q)) - \gamma_{0}\sin(2\pi Q) & \cos(2\pi Q) - (\delta Kds\beta_{0} + \alpha_{0})\sin(2\pi Q) \end{pmatrix}$$

$$3$$

Gradient error and tune-shift



• Consider a new matrix after 1 turn with a new tune $\chi = 2\pi(Q + \delta Q)$

$$\mathcal{M}^{\star} = \begin{pmatrix} \cos(\chi) + \alpha_0 \sin(\chi) & \beta_0 \sin(\chi) \\ -\gamma_0 \sin(\chi) & \cos(\chi) - \alpha_0 \sin(\chi) \end{pmatrix}$$

The traces of the two matrices describing the 1-turn should be equal Tra(M^{*}) = Tra(M) which gives 2 cos(2πQ) - δKdsβ₀ sin(2πQ) = 2 cos(2π(Q + δQ))
Developing the left hand side cos(2π(Q + δQ)) = cos(2πQ) cos(2πδQ) - sin(2πQ) sin(2πδQ) 1 2πδQ and finally 4πδQ = δKdsβ₀
For a quadrupole of finite length, we have

$$\delta Q = \frac{1}{4\pi} \int_{s_0}^{s_0+l} \delta K \beta_0 ds$$

Gradient error and beta distortion



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Consider the unperturbed transfer matrix for one turn

$$M_{0} = \begin{pmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{pmatrix} = B \cdot A \text{ with } \qquad \begin{array}{l} A = \begin{pmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{pmatrix} \\ B = \begin{pmatrix} b_{11} & b_{12} \\ b_{21} & b_{22} \end{pmatrix} \end{array}$$

Introduce a gradient perturbation between the two matrices

$$\mathcal{M}_0^{\star} = \begin{pmatrix} m_{11}^{\star} & m_{12}^{\star} \\ m_{21}^{\star} & m_{22}^{\star} \end{pmatrix} = B \begin{pmatrix} 1 & 0 \\ -\delta K ds & 1 \end{pmatrix} A$$

 $\mathcal{M}_{0}^{\star} = \begin{pmatrix} m_{11}^{\star} & m_{12}^{\star} \\ m_{21}^{\star} & m_{22}^{\star} \end{pmatrix} = B \begin{pmatrix} 1 & 0 \\ -\delta K ds & 1 \end{pmatrix} A$ • Recall that $m_{12} = \beta_0 \sin(2\pi Q)$ and write the perturbed term as $m_{12}^{\star} = (\beta_0 + \delta\beta) \sin(2\pi(Q + \delta Q)) = m_{12} + \delta\beta \sin(2\pi Q) + 2\pi\delta Q\beta_0 \cos(2\pi Q)$ where we used $\sin(2\pi\delta Q) \approx 2\pi\delta Q$ and $\cos(2\pi\delta Q) \approx 1$

G-Gradient error and beta distortion



• On the other hand

$$a_{12} = \sqrt{\beta_0 \beta(s_1)} \sin \psi, \ b_{12} = \sqrt{\beta_0 \beta(s_1)} \sin (2\pi Q - \psi)$$

and $m_{12}^{\star} = \underbrace{b_{11}a_{12} + b_{12}a_{22}}_{m_{12}} - a_{12}b_{12}\delta K ds = m_{12} - a_{12}b_{12}\delta K ds$

Equating the two terms

$$\delta\beta\sin(2\pi Q) + 2\pi\delta Q\beta_0\cos(2\pi Q) = -a_{12}b_{12}\delta Kds$$

Integrating through the quad

$$\frac{\delta\beta}{\beta_0} = -\frac{1}{2\sin(2\pi Q)} \int_{s_1}^{s_1+l} \beta(s)\delta K(s)\cos(2\psi - 2\pi Q)ds$$



Chromaticity

- Linear equations of motion depend on the energy (term proportional to dispersion)
- Chromaticity is defined as: $\xi_{x,y} = \frac{\delta Q_{x,y}}{\delta p/p}$
- Recall that the gradient is $k = \frac{G}{Bo} = \frac{eG}{n} \rightarrow \frac{\delta k}{k} = \mp \frac{\delta p}{n}$
- This leads to dependence of tunes and optics function on energy
- For a linear lattice the tune shift is: $\delta Q_{x,y} = \frac{1}{4\pi} \oint \beta_{x,y} \delta k(s) ds = -\frac{1}{4\pi} \frac{\delta p}{n} \oint \beta_{x,y} k(s) ds$ So the **natural** chromaticity is: $\xi_{x,y} = -\frac{1}{4\pi} \oint \beta_{x,y} k(s) ds$ Sometimes the chromaticity is quoted as $\overline{\xi_{x,y}} = \frac{\xi_{x,y}}{Q_{x,y}}$

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Chromaticity from sextupoles

- $\frac{S}{x^2}$
- The sextupole field component in the *x*-plane is: $B_y = \sum_{x \in D} B_y$
- In an area with non-zero dispersion $x = x_0 + D \frac{\delta P}{D}$
- Than the field is

$$B_y = \frac{S}{2}x_0^2 + \underbrace{SD\frac{\delta P}{P}x_0}_{\text{quadrupole}} + \underbrace{\frac{S}{2}D^2\frac{\delta P}{P}}_{\text{dipole}}^2$$

- Sextupoles introduce an equivalent focusing correction $\delta k = SD \frac{\delta P}{P}$
 - The sextupole induced chromaticity is

$$\xi_{x,y}^S = -\frac{1}{4\pi} \oint \mp \beta_{x,y}(s) S(s) D_x(s) ds$$

The total chromaticity is the sum of the natural and sextupole induced chromaticity

$$\xi_{x,y}^{\text{tot}} = -\frac{1}{4\pi} \oint \beta_{x,y}(s) \left(k(s) \mp S(s)D_x(s)\right) ds$$



Chromaticity correction

- Introduce sextupoles in high-dispersion areas
 - Tune them to achieve desired chromaticity
 - Two families are able to control horizontal and vertical chromaticity
- The off-momentum beta-beating correction needs additional families
- Sextupoles introduce non-linear fields (chaotic motion)
 - Sextupoles introduce tune-shift with amplitude

Normalized coordinates



Recall the Floquet solutions u(s) = \sqrt{\epsilon\beta(s)}\cos(\psi(s) + \psi_0)\) for betatron motion u'(s) = \sqrt{\frac{\epsilon}{\beta(s)}}\left(\sin(\psi(s) + \psi_0) + \alpha(s)\cos(\psi(s) + \psi_0)\)
 Introduce new variables

 $\mathcal{U} = \frac{u}{\sqrt{\beta}} , \quad \mathcal{U}' = \frac{d\mathcal{U}}{d\phi} = \frac{\alpha}{\sqrt{\beta}}u + \sqrt{\beta}u' , \quad \phi = \frac{\psi}{\nu} = \frac{1}{\nu} \int \frac{ds}{\beta(s)}$ In matrix form $\begin{pmatrix} \mathcal{U} \\ \mathcal{U}' \end{pmatrix} = \begin{pmatrix} \frac{1}{\sqrt{\beta}} & 0 \\ \frac{\alpha}{\sqrt{\beta}} & \sqrt{\beta} \end{pmatrix} \begin{pmatrix} u \\ u' \end{pmatrix}$ • Hill's equation becomes $\frac{1}{\nu^2 \beta^{3/2}} \left(\frac{d^2 \mathcal{U}}{d\phi^2} + \nu^2 \mathcal{U} \right) = 0$ System becomes harmonic oscillator with frequency $\begin{pmatrix} \mathcal{U} \\ \mathcal{U}' \end{pmatrix} = \sqrt{\epsilon} \begin{pmatrix} \cos(\nu\phi) \\ -\sin(\nu\phi) \end{pmatrix} \quad \text{or} \quad \mathcal{U}^2 + \mathcal{U}'^2 = \epsilon$ \mathcal{U}' **Floquet transformation** transforms phase space in circles 10

Perturbation of Hill's equations



■ Hill's equations in normalized coordinates with harmonic perturbation, using $\mathcal{U} = \mathcal{U}_x$ or \mathcal{U}_y and $\phi = \phi_x$ or ϕ_y $\frac{d^2 \mathcal{U}}{d\phi^2} + \nu^2 \mathcal{U} = \nu^2 \beta^{3/2} F(\mathcal{U}_x(\phi_x), \mathcal{U}_y(\phi_y))$

where the *F* is the Lorentz force from perturbing fields

- Linear magnet imperfections: deviation from the design dipole and quadrupole fields due to powering and alignment errors
- Time varying fields: feedback systems (damper) and wake fields due to collective effects (wall currents)
- Non-linear magnets: sextupole magnets for chromaticity correction and octupole magnets for Landau damping
- **Beam-beam interactions**: strongly non-linear field
- □ **Space charge effects**: very important for high intensity beams
- non-linear magnetic field imperfections: particularly difficult to control for super conducting magnets where the field quality is entirely determined by the coil winding accuracy

Perturbation by periodic function



In beam dynamics, perturbing fields are periodic functions The problem to solve is a generalization of the driven harmonic oscillator, $\frac{d^2u}{dt^2} + \omega_0^2 u(t) = g(t)$ with a general periodic function g(t) , with frequency $\omega_{m=+\infty}$ • The right side can be Fourier analyzed: $g(t) = \sum a_m e^{im\omega t}$ The homogeneous solution is $u_h(t) = u_0(t) \sin(\omega_0 t + \phi_0)$ • The particular solution can be found by considering that u(t)has the same form as g(t): $u_p(t) = \sum u_{pm} e^{im\omega t}$ By substituting we find the following relation for the Fourier coefficients of the particular solution $u_{pm} = \frac{a_m}{\omega_0^2 - m^2 \omega^2}$ There is a **resonance condition** for infinite number of frequencies satisfying $\omega_0^2 = m^2 \omega^2$ 12

Perturbation by single multi-pole



For a generalized multi-pole perturbation, Hill's equation is: $\frac{d^2 \mathcal{U}}{d\phi^2} + \nu_0^2 \mathcal{U} = \nu_0^2 \beta^{\frac{n}{2}+1} b_n(\phi) \mathcal{U}^{n-1} = \overline{b_n}(\phi) \mathcal{U}^{n-1}$ $As before, the multipole coefficient can be expanded in Fourier series <math display="block">\overline{b_n}(\phi) = \sum_{m=-\infty}^{\infty} \overline{b_{nm}} e^{im\phi}$

Following the perturbation steps, the zero-order solution is given by the homogeneous equation $U_0 = W_1 e^{i\nu_0\phi} + W_{-1} e^{-i\nu_0\phi}$ Then the position can be expressed as

 $\overline{W}_{q} \qquad q = -n+1, -n+3, \dots, n-1$ $\mathcal{U}_{0}^{n-1} = \sum_{k=0}^{n-1} \binom{n-1}{k} W_{1}^{n-1-k} W_{-1}^{k} e^{i(n-1-2k)\nu_{0}\phi} = \sum_{q=-n+1}^{n-1} \overline{W}_{q} e^{iq\nu_{0}\phi}$ q = -n + 1

with $\overline{W}_{n-2} = \overline{W}_{n-4} = \overline{W}_{n-6} = \cdots = \overline{W}_{-n+2} = 0$

The first order solution is written as $\frac{d^2\mathcal{U}_1}{d\phi^2} + \nu_0^2\mathcal{U}_1 = \overline{b_n}(\phi)\mathcal{U}_0^{n-1} = \sum_{i=1}^{n-1} \sum_{j=1}^{m=\infty} \overline{b_{nm}}\overline{W}_q e^{i(m+q\nu_0)\phi}$ 13 $q = -n + 1 m = -\infty$

Resonances for single multi-pole



Following the discussion on the periodic perturbation, the solution can be found by setting the leading order solution to be periodic with the same frequency as the right hand side

$$\mathcal{U}_1 = \sum_{q=-n+1}^{n-1} \sum_{m=-\infty}^{m=\infty} \mathcal{U}_{1mq} e^{i(m+q\nu_0)\phi}$$

Equating terms of equal exponential powers, the Fourier amplitudes are found to satisfy the relationship

$$\mathcal{U}_{1mq} = \frac{\overline{b}_{nm}\overline{W}_q}{\nu_0^2 - (m + q\nu_0)^2}$$

This provides the resonance condition $m \pm |q|\nu_0 = \nu_0$ or $\nu_0 = \frac{m}{1 \pm |q|}$ which means that there are resonant frequencies for and "infinite" number of rationals

Tune-shift for single multi-pole



■ Note that for even multi-poles and q = 1 or m = 0, there is a Fourier coefficient \overline{b}_{n0} , which is independent of ϕ and represents the average value of the periodic perturbation

The perturbing term in the r.h.s. is

 $\overline{b}_{n0}\overline{W}_{1}e^{i\nu_{0}\phi} = \nu_{0}^{2}\beta^{\frac{n}{2}+1}b_{n0}\binom{n-1}{\frac{n}{2}-1}W_{1}^{n-1}W_{-1}^{\frac{n}{2}-1}e^{i\nu_{0}\phi}$

which can be obtained for $k = \frac{n}{2} - 1$ (it is indeed an integer only for even multi-poles)

Following the approach of the perturbed non-linear harmonic oscillator, this term will be secular unless a perturbation in the frequency is considered, thereby resulting to a tune-shift equal to

$$\nu = -\frac{\nu_0 \beta^{\frac{n}{2}+1} b_{n0}}{2} \binom{n-1}{\frac{n}{2}-1} \widetilde{W}^{n-2} \quad \text{with} \quad \widetilde{W}^2 = W_1 W_{-1}$$

This tune-shift is amplitude dependent for n > 2

 δ



Multipole expansion II



From the complex potential we can derive the fields

$$B_{y} + iB_{x} = -\frac{\partial}{\partial x}(A_{s}(x, y) + iV(x, y)) = -\sum_{n=1}^{\infty} n(\lambda_{n} + i\mu_{n})(x + iy)^{n-1}$$
Setting $b_{n} = -n\lambda_{n}$, $a_{n} = n\mu_{n}$

$$B_{y} + iB_{x} = \sum_{n=1}^{\infty} (b_{n} - ia_{n})(x + iy)^{n-1}$$
Define normalized coefficients
 $b'_{n} = \frac{b_{n}}{10^{-4}B_{0}}r_{0}^{n-1}$, $a'_{n} = \frac{a_{n}}{10^{-4}B_{0}}r_{0}^{n-1}$
on a reference radius r_{0} , 10⁴ of the main field to get
 $B_{y} + iB_{x} = 10^{-4}B_{0}\sum_{n=1}^{\infty} (b'_{n} - ia'_{n})(\frac{x + iy}{r_{0}})^{n-1}$
Note: $n' = n - 1$ is the US convention

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General multi-pole perturbation



Equations of motion including any multi-pole error term, in both planes

$$\frac{d^2 \mathcal{U}_x}{d\phi_x^2} + \nu_{0x}^2 \mathcal{U}_x = \overline{b_{n,r}}(\phi_x) \mathcal{U}_x^{n-1} \mathcal{U}_y^{r-1}$$

Expanding perturbation coefficient in Fourier series and inserting the solution of the unperturbed system on the rhs gives the following series: $U_x^{n-1} \approx U_{0x}^{n-1} = \sum_{\substack{n=1\\ q_x = -n+1\\ r-1}}^{n-1} \overline{W}_{q_x} e^{iq_x\nu_0\phi_x}$

$$\mathbb{I}_{224}^{m=-\infty} \qquad \qquad \mathcal{U}_{y}^{r-1} \approx \mathcal{U}_{0y}^{r-1} = \sum_{q_y = -r+1} \overline{W}_{q_y} e^{iq_y \nu_{0y} \phi_x}$$

$$\mathbb{I}_{2244}^{2244}$$

$$\frac{d^2 \mathcal{U}_x}{d\phi_x^2} + \nu_{0x}^2 \mathcal{U}_x = \sum_{m,q_x,q_y} \overline{b_{nrm}} W_{q_x}^x W_{q_y}^y e^{i(m+q_x\nu_{0x}+q_y\nu_{0y})\phi_x}$$

In principle, same perturbation steps can be followed for getting an approximate solution in both planes

General resonance conditions



• The general resonance conditions is $m + q_x \nu_{0x} + q_y \nu_{0y} = \nu_{0x}$ or $m + q'_x \nu_{0x} + q_y \nu_{0y} = 0$, with order $|q_x| + |q_y| + 1$ The same condition can be obtained in the vertical plane For all the polynomial field terms of a 2*n*-pole, the main excited resonances satisfy the condition $q'_x + q_y = n$ but there are also **sub-resonances** for which $q'_x + q_y < n$ For **normal** (erect) multi-poles, the main resonances are $(q'_x, q_y) = (n, 0), (n - 2, \pm 2), \dots$ whereas for **skew** multi-poles $(q'_x, q_y) = (n - 1, \pm 1), (n - 3, \pm 3), \dots$ ■ If perturbation is large, **all** 0.8resonances can be potentially excited 0.6 ■ The resonance conditions form lines in the frequency space and fill it up as 0.4 the order grows (the rational numbers 0.2 form a dense set inside the real numbers) 19

0.2

0.4

0.6

0.8



If lattice is made out of N identical cells, and the perturbation follows the same periodicity, resulting in a reduction of the resonance conditions to the ones satisfying $q_x \nu_{0x} + q_y \nu_{0y} = jN$

These are called systematic resonances

Practically, any (linear) lattice perturbation breaks super-periodicity and any random resonance can be excited

Careful choice of the working point is necessary



Fixed points for 3rd order resonance

- In the vicinity of a third order resonance, three fixed points can be found at ψ
- For $\frac{\delta}{A_{3p}} > 0$ all three points are unstable
- Close to the elliptic one at $\psi_{20} = 0$ the motion in phase space is described by circles that they get more and more distorted to end up in the "triangular" separatrix uniting the unstable fixed points
 - The tune separation from the resonance (**stop-band width**) is $\delta = \frac{3A_{3p}}{2}J_{20}^{1/2}$





Topology of an octupole resonance



Regular motion near the center, with curves getting more deformed towards a rectangular shape

The separatrix passes through 4 unstable fixed points, but motion seems well contained

Four stable fixed points exist and they are surrounded by stable motion (islands of stability)





Path to chaos



■ When perturbation becomes higher, motion around the separatrix becomes chaotic (producing tongues or splitting of the separatrix)

Unstable fixed points are indeed the source of chaos when a perturbation is added





Chaotic motion



Poincare-Birkhoff theorem states that under perturbation of a resonance only an even number of fixed points survives (half stable and the other half unstable)

Themselves get destroyed when perturbation gets higher, etc. (self-similar fixed points)

Resonance islands grow and resonances can overlap allowing diffusion of particles

-0.002

0.002

0.004

0.006



-0.0006 -0.0004 -0.0002

(O)

0

7e-0'

(0)

 \odot

0

ZOOM

0.0002 0.0004 0.0006

2e-06

1.5e-06

1e-06

5e-07

-5e-07

-1e-06

-1.5e-06

-2e-06

-0.006

0

Beam Dynamics: Dynamic Aperture



- Dynamic aperture plots often show the maximum initial values of stable trajectories in x-y coordinate space at a particular point in the lattice, for a range of energy errors.
 - □ The beam size (injected or equilibrium) can be shown on the same plot.
 - Generally, the goal is to allow some significant margin in the design the measured dynamic aperture is often significantly smaller than the predicted dynamic aperture.
- This is often useful for comparison, but is not a complete characterization of the dynamic aperture: a more thorough analysis is needed for full optimization.



C• Example: The ILC DR DA





- Dynamic aperture for lattice with specified misalignments, multipole errors, and wiggler nonlinearities
- Specification for the phase space distribution of the injected positron bunch is an amplitude of Ax + Ay = 0.07m rad (normalized) and an energy spread of E/E = 0.75%
- DA is larger then the specified beam acceptance

Dynamic aperture including damping







Including radiation damping and excitation shows that 0.7% of the particles are lost during the damping Certain particles seem to damp away from the beam core, on resonance islands

Frequency map analysis



- Frequency Map Analysis (FMA) is a numerical method which springs from the studies of J. Laskar (Paris Observatory) putting in evidence the chaotic motion in the Solar Systems
- FMA was successively applied to several dynamical systems
 - Stability of Earth Obliquity and climate stabilization (Laskar, Robutel, 1993)
 - □ 4D maps (Laskar 1993)
 - Galactic Dynamics (Y.P and Laskar, 1996 and 1998)
 - Accelerator beam dynamics: lepton and hadron rings (Dumas, Laskar, 1993, Laskar, Robin, 1996, Y.P, 1999, Nadolski and Laskar 2001)

Motion on torus



Consider an integrable Hamiltonian system of the usual form $H(\boldsymbol{J}, \boldsymbol{\varphi}, \theta) = H_0(\boldsymbol{J})$ $i \quad \partial H_0(\boldsymbol{J}) \quad \text{if } (\boldsymbol{J}) \rightarrow f \quad \text{if } (\boldsymbol{J}) \rightarrow f$

Hamilton's equations give

$$\dot{\phi}_{j} = \frac{\partial H_{0}(\mathbf{J})}{\partial J_{j}} = \omega_{j}(\mathbf{J}) \Rightarrow \phi_{j} = \omega_{j}(\mathbf{J})t + \phi_{j0}$$
$$\dot{J}_{j} = -\frac{\partial H_{0}(\mathbf{J})}{\partial \phi_{j}} = 0 \Rightarrow J_{j} = \text{const.}$$

The actions define the surface of an invariant torus In complex coordinates the motion is described by $\zeta_i(t) = J_i(0)e^{i\omega_j t} = z_{j0}e^{i\omega_j t}$ For a **non-degenerate** system $\det \left| \frac{\partial \omega(J)}{\partial J} \right| = \det \left| \frac{\partial^2 H_0(J)}{\partial J^2} \right| \neq 0$ there is a one-to-one correspondence between the actions and the frequency, a frequency map can be defined parameterizing the tori in the frequency space $F: (\mathbf{I}) \longrightarrow (\omega)$

Building the frequency map



When a quasi-periodic function f(t) = q(t) + ip(t) in the complex domain is given numerically, it is possible to recover a quasi-periodic approximation

$$f'(t) = \sum_{k=1}^{N} a'_k e^{i\omega'_k t}$$

 ΛI

in a very precise way over a finite time span [-T, T] several orders of magnitude more precisely than simple Fourier techniques

- This approximation is provided by the Numerical Analysis of Fundamental Frequencies **NAFF** algorithm
- The frequencies ω'_k and complex amplitudes a'_k are computed through an iterative scheme.

Aspects of the frequency map



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- In the vicinity of a resonance the system behaves like a pendulum
- Passing through the elliptic point for a fixed angle, a fixed frequency (or rotation number) is observed
- Passing through the hyperbolic point, a frequency jump is oberved



Building the frequency map



- Choose coordinates (x_i, y_i) with p_x and $p_y=0$
- Numerically integrate the phase trajectories through the lattice for sufficient number of turns
- Compute through NAFF Q_x and Q_y after sufficient number of turns
 Plot them in the tune diagram







Frequency maps for the target error table (left) and an increased random skew octupole error in the super-conducting dipoles (right)

Calculate frequencies for two equal and successive time spans and compute frequency diffusion vector:

$$D|_{t=\tau} = \nu|_{t\in(0,\tau/2]} - \nu|_{t\in(\tau/2,\tau]}$$

Plot the initial condition space color-coded with the norm of the diffusion vector

Compute a diffusion quality factor by averaging all diffusion coefficients normalized with the initial conditions radius

$$D_{QF} = \left\langle \begin{array}{c} |D| \\ (I_{x0}^2 + I_{y0}^2)^{1/2} \end{array} \right\rangle_R$$







Diffusion maps for the target error table (left) and an increased random skew octupole error in the super-conducting dipoles (right)

Resonance free lattice for CLIC PDR



Non linear

optimization based on phase advance scan for minimization of resonance driving terms and tune-shift with amplitude



$$\sum_{p=0}^{N_{c}-1} e^{ip(n_{x}\mu_{x,c}+n_{y}\mu_{y,c})} = \sqrt{\frac{1-\cos\left[N_{c}(n_{x}\mu_{x,c}+n_{y}\mu_{y,c})\right]}{1-\cos(n_{x}\mu_{x,c}+n_{y}\mu_{y,c})}} = 0$$

$$\sum_{n_{c}(n_{x}\mu_{x,c}+n_{y}\mu_{y,c}) = 2k\pi$$

$$n_{x}\mu_{x,c}+n_{y}\mu_{y,c} \neq 2k'\pi$$



C • Dynamic aperture for CLIC DR





- Dynamic aperture and diffusion map
- Very comfortable DA especially in the vertical plane
 - Vertical beam size very small, to be reviewed especially for removing electron PDR
- Need to include non-linear fields of magnets and wigglers

•• Frequency maps for the ILC DR





Frequency maps enabled the comparison and steering of different lattice designs with respect to non-linear dynamics

Working point optimisation, on and off-momentum dynamics, effect of multi-pole errors in wigglers

Working point choice for SUPERB



- Figure of merit for choosing best working point is sum of diffusion rates with a constant added for every lost particle
- Each point is produced after tracking 100 particles
- Nominal working point had to be moved towards "blue" area

$$e^{D} = \sqrt{\frac{(\nu_{x,1} - \nu_{x,2})^2 + (\nu_{y,1} - \nu_{y,2})^2}{N/2}}$$

S. Liuzzo et al., IPAC 2012



 $WPS = 0.1N_{lost} + \sum e^D$

Experimental frequency maps



D. Robin, C. Steier, J. Laskar, and L. Nadolski, PRL 2000

 Frequency analysis of turnby-turn data of beam oscillations produced by a fast kicker magnet and recorded on a Beam Position Monitors

Reproduction of the nonlinear model of the Advanced Light Source storage ring and working point optimization for increasing beam lifetime







Damping rings non-linear dynamics is dominated by very strong sextupoles used to correct chromaticity

 Important effect of wiggler magnets
 Dynamic aperture computation is essential for assuring good injection efficiency in the damping rings

Frequency map analysis is a very well adapted method for revealing global picture of resonance structure in tune space and enable detailed non-linear optimisation