

Alignment and Adjustment of IPBPMs in the IP chamber

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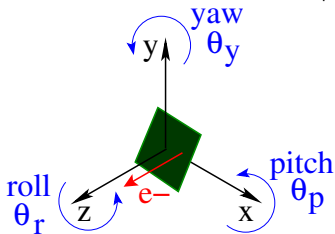
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Conclusions

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Coordinate system

Each BPM has its own coordinates with respect to a reference system centered **electrically** and aligned with the beam



Beam, BPMs

▶ Beam Position

x_A, y_A, z_A

x_B, y_B, z_B

x_C, y_C, z_C

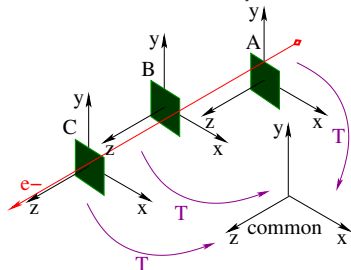
▶ BPM Angles respect to ref. system

$\theta_{Ap}, \theta_{Ar}, \theta_{Ay}$

$\theta_{Bp}, \theta_{Br}, \theta_{By}$

$\theta_{Cp}, \theta_{Cr}, \theta_{Cy}$

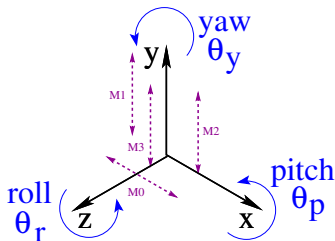
All systems relate to a common **mechanical** reference system, no rotations, just translations



One of the BPMs reference system could be chosen to coincide with the common

Movers

There is a set of movers to control BPM position



$$x = x_0 + f_x(M_0)$$

$$y = y_0 + f_y(M_1, M_2, M_3)$$

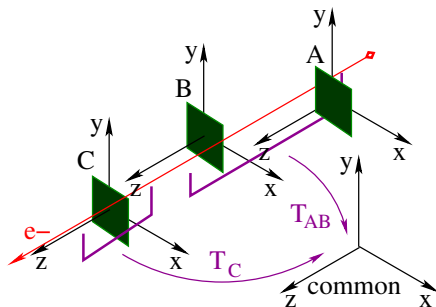
$$z = z_0$$

$$\theta_p = \theta_{p0} + f_p(M_1, M_2, M_3)$$

$$\theta_r = \theta_{r0}$$

$$\theta_y = \theta_{y0}$$

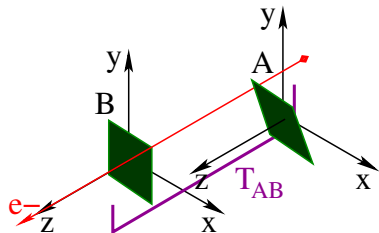
All initial values are set during the IP BPMs installation



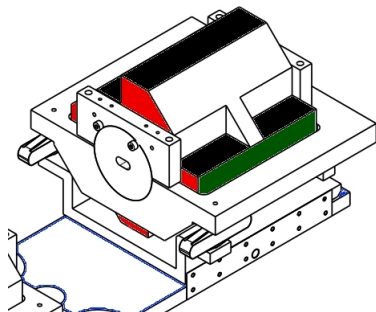
Ideally all x_0, y_0 are equal when movers at mid-range, z_0 is the BPM center and all angles are zero.

System is composed only for **two** independent blocks (AB,C)

Block AB Alignment

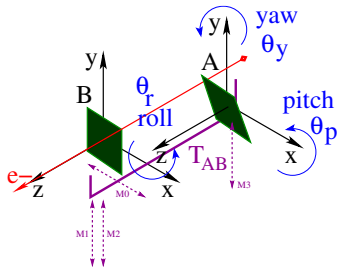


Using BPMB as reference, $1000\beta_y$ optics



| | Beam | | Mech |
|-------------------------|-------------|---------------------------------|-------------------|
| | B | A | A |
| x_0 [μm] | 0 ± 5 | 53 ± 5 | 42 ± 50 |
| y_0 [μm] | 0 ± 3 | -34 ± 3 | -83 ± 66 |
| z_0 [mm] | not meas. | not meas. | not meas. |
| θ_{p0} [mrad] | 0 ± 0.1 | 1.6 ± 0.1 | 1.6 ± 1.0 |
| θ_{r0} [mrad] | not meas. | not meas. | -0.7 ± 0.9 |
| θ_{y0} [mrad] | not meas. | not meas. | $\pm 0.9 \mp 1.1$ |

Block AB Adjustment

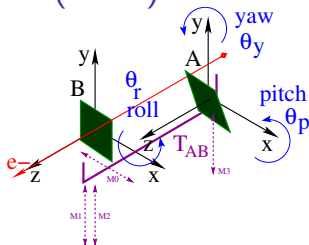


Using BPMB as reference, $1000\beta_y$ optics

| | Adjustment (if BPM B is reference and centered) | |
|-----------------------|---|--------------------------------|
| | B | A |
| x [μm] | $0 + 125M_0$ | $53 + 125M_0$ |
| y [μm] | $0 + 94.8M_{1,2} + 30.2M_3$ | $-34 + 11.2M_{1,2} + 113.8M_3$ |
| z [mm] | not meas. | not meas. |
| θ_p [mrad] | $0 + 1.03(M_3 - M_{1,2})$ | $1.6 + 1.03(M_3 - M_{1,2})$ |
| θ_r [mrad] | not meas. | -0.7 |
| θ_y [mrad] | not meas. | ± 0.9 |

$$-1 < M_{0,1,2,3} < 1, \Delta M_{0,1,2,3} \geq 1.25 \times 10^{-2}$$

Block AB Adjustment (cont.)



Using BPMB as reference, $1000\beta_y$ optics

| | Adjustment (if BPM B is reference and centered) | |
|-----------------------|---|--------------------------------|
| | B | A |
| y [μm] | $0 + 94.8M_{1,2} + 30.2M_3$ | $-34 + 11.2M_{1,2} + 113.8M_3$ |
| θ_p [mrad] | $0 + 1.03(M_3 - M_{1,2})$ | $1.6 + 1.03(M_3 - M_{1,2})$ |

POSSIBLE CORRECTIONS

- V: $y_B = 0\mu\text{m}$, $\theta_{Bp} = \mathbf{0\text{mrad}}$, $y_A = -34\mu\text{m}$, $\theta_{Bp} = 1.6\text{mrad}$
 $y_B = \mathbf{0\mu\text{m}}$, $\theta_{Bp} = 0.4\text{mrad}$, $y_A = \mathbf{0\mu\text{m}}$, $\theta_{Bp} = 2.0\text{mrad}$
 $y_B = 0\mu\text{m}$, $\theta_{Bp} = \mathbf{-0.8\text{mrad}}$, $y_A = -64.9\mu\text{m}$, $\theta_{Bp} = \mathbf{0.8\text{mrad}}$
 $y_B = 21.9\mu\text{m}$, $\theta_{Bp} = \mathbf{-1.6\text{mrad}}$, $y_A = -107.64\mu\text{m}$, $\theta_{Bp} = \mathbf{0\text{mrad}}$

Block AB Adjustment (cont.)

| | Adjustment (BPMB as reference to BPMA) | |
|-----------------------|--|---|
| | B | A |
| x [μm] | $x_{B0} + 125M_0$ | $x_{A0} - x_{B0} + 125M_0$ |
| y [μm] | $y_{B0} + 94.8M_{1,2} + 30.2M_3$ | $y_{A0} - y_{B0} + 11.2M_{1,2} + 113.8M_3$ |
| z [mm] | z_{B0} | $z_{A0} - z_{B0}$ |
| θ_p [mrad] | $\theta_{Bp0} + 1.03(M_3 - M_{1,2})$ | $\theta_{Ap0} - \theta_{Bp0} + 1.03(M_3 - M_{1,2})$ |
| θ_r [mrad] | θ_{Br0} | $\theta_{Ar0} - \theta_{Br0}$ |
| θ_y [mrad] | θ_{By0} | $\theta_{Ay0} - \theta_{By0}$ |

$$-1 < M_{0,1,2,3} < 1, \Delta M_{0,1,2,3} \geq 1.25 \times 10^{-2}$$

POSSIBLE CORRECTIONS

H: B $\pm 125\mu\text{m}$, or, A $\pm 125\mu\text{m}$

V: B $\pm 125\mu\text{m}$, or, A $\pm 125\mu\text{m}$

B $\pm 90\mu\text{m}$ and $\mp 1\text{mrad}$, or, A $\pm 110\mu\text{m}$ and $\pm 1\text{mrad}$

B $\mp 2\text{mrad}$, or, A $\pm 2\text{mrad}$

NOTE: Angle correction goes in opposite directions

Block AB Adjustment (cont.)

| | | |
|-----------------------|--------------------------------------|---|
| y [μm] | $y_{B0} + 94.8M_{1,2} + 30.2M_3$ | $y_{A0} - y_{B0} + 11.2M_{1,2} + 113.8M_3$ |
| θ_p [mrad] | $\theta_{Bp0} + 1.03(M_3 - M_{1,2})$ | $\theta_{Ap0} - \theta_{Bp0} + 1.03(M_3 - M_{1,2})$ |

Vertical signals I_y, Q_y depend on y, θ_p , it might be possible to find a minimum for $\sqrt{(I_y^2 + Q_y^2)}$ for A and B at the same time.

| | | |
|-----------------------|-------------------|-------------------------------|
| x [μm] | $x_{B0} + 125M_0$ | $x_{A0} - x_{B0} + 125M_0$ |
| θ_y [mrad] | θ_{By0} | $\theta_{Ay0} - \theta_{By0}$ |

Horizontal signals I_x, Q_x depend on x, θ_y .

| | | |
|-------------------|----------------|-------------------------------|
| θ_r [mrad] | θ_{Br0} | $\theta_{Ar0} - \theta_{Br0}$ |
|-------------------|----------------|-------------------------------|

Coupling depends on θ_r .

Conclusions

- ▶ Block AB mechanical alignment shows relative good agreement with measurements made on Dec. 2013.
- ▶ Movers adjustment is explicitly written in order to clarify movers capabilities.
- ▶ If pitch angle of 2mrad is acceptable, then BLOCK AB is OK. Otherwise movers could minimize signals I_y, Q_y on either A or B but not all at same time.

I THANK YOU ALL!

Open Questions

- ▶ Required alignment precision ($x_0, y_0, z_0, \theta_{p0}, \theta_{r0}, \theta_{y0}$) in order to check during manufacturing and assembly.
What to check? How to check?

Support slides

